

**TUGAS AKHIR
(KL 1702)**

**PENGGUNAAN PIRANTI LUNAK UNTUK PERENCANAAN
PENGERUKAN KOLAM LABUH PELABUHAN
UMUM BENOA SAMPAI TAHUN 2018**



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**JURUSAN TEKNIK KELAUTAN
FAKULTAS TEKNOLOGI KELAUTAN
INSTITUT TEKNOLOGI SEPULUH NOPEMBER
SURABAYA**

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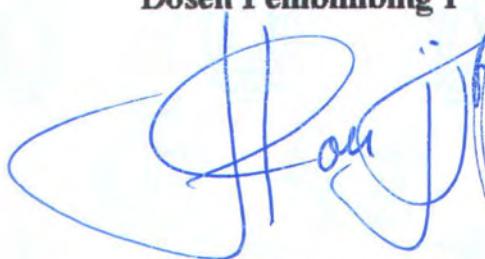
PENGGUNAAN PIRANTI LUNAK UNTUK PERENCANAAN PENGERUKAN KOLAM LABUH PELABUHAN UMUM BENOA SAMPAI TAHUN 2018

TUGAS AKHIR (KL 1701)

**Diajukan Guna Memenuhi Salah Satu Syarat
Untuk Menyelesaikan Studi Program Sarjana
Pada
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ABSTRAK

Pelabuhan lazimnya dilengkapi dengan fasilitas di darat seperti: jalan, gudang, lapangan penumpukan peti kemas, dan lain-lain, serta fasilitas perairan seperti alur pelayaran, kolam labuh, dan lain-lain.

Kolam labuh merupakan daerah perairan dimana kapal berlabuh sementara sebelum atau sesudah melakukan bongkar muat, melakukan gerakan memutar (*turning basin*) dan sebagainya. Untuk memperlebar dan memperdalam kolam labuh maka perlu diadakan pengerukan.

Pengerukan adalah penggalian atau pengambilan tanah dan batuan dasar bawah air. Pekerjaan pengerukan umumnya dilakukan untuk memperdalam atau memperlebar alur pelayaran atau kolam labuh, sungai, dan lain-lain.

Perencanaan pengerukan selama ini dilakukan melalui analisa yang panjang dan tidak jarang waktu yang diperlukan cukup lama. Untuk mengatasi hal tersebut maka penggunaan piranti lunak merupakan alternatif yang baik. Hasil yang didapatkan cepat dan cukup akurat.

Piranti lunak Pengerukan 1.0 adalah hasil pengembangan awal yang dibuat dengan bantuan Borlan Delphi 5.0. Pengerukan 1.0 utamanya digunakan untuk perhitungan kedalaman rencana kolam labuh, sedimentasi kolam labuh (metode Bijker), dan analisa teknokonomi pemilihan kapal keruk. Sebagai contoh atau studi kasus untuk rencana pengerukan adalah kolam labuh Pelabuhan umum Banoa-Bali.

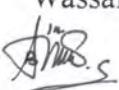
KATA PENGANTAR

Alhamdulillahirobbil‘alamin,

Segala puji syukur kepada Allah SWT atas semua rahmat, ampunan, hidayah dan kesabaran yang dilimpahkan kepada penulis sehingga laporan Tugas Akhir ini terselesaikan.

Sebagai manusia biasa penulis sadar akan segala kekurangan dan keterbatasan diri dan karena itu penulis ingin menyampaikan terimakasih yang sebesar-besarnya kepada siapa saaj yang ikut berperan dalam penulisan laporan Tugas Akhir ini, terutama:

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BAB I

PENDAHULUAN

BAB I

PENDAHULUAN

1.1. Latar Belakang

Pelabuhan Benoa sebagai salah satu pelabuhan terbesar di Bali mempunyai posisi yang strategis baik ditinjau secara geografis maupun terhadap kegiatan-kegiatan yang bertaraf nasional maupun internasional. Untuk proyeksi pengembangan Pelabuhan Benoa dalam rangka mengantisipasi permintaan jasa yang terus meningkat setiap tahun diperlukan penyiapan fasilitas dan peralatan yang memadai, dengan strategi utama pengembangan: pelebaran dan pendalaman alur pelayaran dan kolam labuh, meningkatkan kelancaran bongkar muat melalui pembangunan fasilitas tambat serta lapangan penumpukan peti kemas dan penanganan pencemaran lingkungan .

Zona pelabuhan umum saat ini melayani kapal penumpang, kapal wisata dan sekaligus kapal peti kemas. Hal ini dapat menimbulkan masalah keselamatan pelayaran dan operasional. Kemampuan kolam labuh dan fasilitas tambat yang terbatas dan kurang sebanding dengan kunjungan kapal, terutama kapal dengan ukuran panjang lebih dari 180 m atau draft lebih dari 8 m.

Berdasarkan masterplan Pelabuhan Benoa maka kolam labuh pelabuhan umum yang semula kedalamannya 9,0 m akan diperdalam menjadi 11,00 m dan luas menjadi 25,5 Ha (850 x 300 m).



1.2. Perumusan Masalah

Dari uraian di atas dapat dirumuskan permasalahan:

- a. Berapakah besarnya volume pengerukan ?
- b. Berapakah sedimentasi yang terjadi ?
- c. Bagaimana pemilihan kapal keruk yang memenuhi syarat teknis dan ekonomis?

1.3. Batasan Masalah

Untuk memperjelas permasalahan dan mempermudah dalam penyelesaian Tugas Akhir ini, maka diperlukan adanya asumsi dan batasan masalah tanpa mengurangi bobot dari penulisan ini :

- a. Data yang dipakai adalah data sekunder.
- b. Letak dermaga dan kolam labuh yang direncanakan sudah ditentukan sesuai masterplan.
- c. Syarat teknis pemilihan kapal keruk dibatasi pada hal-hal: jenis/sifat material tanah dasar kerukan, posisi tempat pembuangan hasil kerukan, kondisi perairan di daerah itu, produktivitas, serta volume kerukan. Syarat teknis tersebut didasarkan pada tabel evaluasi peralatan keruk (*British standart code*).
- d. Pertimbangan ekonomi yang dibahas : depresiasi (penyusutan), asuransi, biaya tenaga kerja, kebutuhan bahan bakar dan oli, dan biaya perawatan dan perbaikan.
- e. Studi pengaruh pengerukan terhadap dampak lingkungan tidak dibahas.

- f. Perhitungan sedimentasi memakai salah satu rumus saja, yaitu formula Bijker jadi tidak bertujuan membandingkan beberapa rumus.

1.4. Tujuan

- a. Menentukan volume pengeringan kolam labuh yang direncanakan.
- b. Menghitung besarnya sedimentasi serta pengaruhnya terhadap pengeringan.
- c. Memilih kapal keruk yang memenuhi syarat teknis dan ekonomis.

1.5. Manfaat

Manfaat yang diharapkan adalah dapat memberikan informasi dan pertimbangan untuk perencanaan kolam labuh zona pelabuhan umum sampai dengan tahun 2018.

1.6. SISTEMATIKA PENULISAN

Abstrak

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BAB I PENDAHULUAN

I.1. Latar belakang

I.2. Perumusan Masalah

I.3. Tujuan dan Manfaat

I.4. Batasan Masalah

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BAB V PEMBAHASAN

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BAB VI PENUTUP

VI.1 Kesimpulan

VI.2 Saran

Daftar Pustaka

Lampiran-lampiran

BAB II

TINJAUAN PUSTAKA DAN LANDASAN TEORI

BAB II

TINJAUAN PUSTAKA DAN LANDASAN TEORI

2. 1. Tinjauan Pustaka

Pelabuhan adalah salah satu simpul dari mata rantai bagi kelancaran angkutan muatan laut dan darat. Jadi secara umum pelabuhan adalah suatu daerah perairan yang terlindung terhadap badai, ombak, arus, sehingga kapal dapat berputar (*turning basin*), bersandar/membuang sauh, sedemikian rupa hingga bongkar muat atas barang dan perpindahan penumpang dapat dilaksanakan (Soedjono, 1987).

Dari sudut teknis, maka dikenal beberapa jenis pelabuhan, yaitu :

- a. Pelabuhan alam (*natural harbour*), dimana daerah tersebut terlindung oleh pulau, jazirah, atau terletak disuatu teluk.
Contoh: Pelabuhan Benoa, yang terlindung oleh Pulau Serangan dan Pulau Penyu.
- b. Pelabuhan buatan (*artificial harbour*), daerah perairan dibuat manusia sedemikian hingga terlindung terhadap ombak, badai, arus, sehingga memungkinkan kapal merapat.
- c. Pelabuhan semi alam (*seminatural harbour*), sebagai contoh: Pelabuhan Palembang.

Pelabuhan lazimnya dilengkapi dengan fasilitas di darat seperti: jalan, gudang, lapangan penumpukan peti kemas, dan lain-lain, serta fasilitas perairan seperti alur pelayaran, kolam labuh, dan lain-lain.

Kolam labuh merupakan daerah perairan dimana kapal berlabuh sementara sebelum atau sesudah melakukan bongkar muat, melakukan gerakan memutar (*turning basin*) dan sebagainya. Kolam labuh harus terlindung dari gangguan gelombang dan mempunyai kedalaman yang cukup (Triatmodjo, 1996). Untuk memperlebar dan memperdalam kolam labuh maka perlu diadakan penggerukan.

Pengerukan adalah penggalian atau pengambilan tanah dan batuan dasar bawah air. Pekerjaan penggerukan umumnya dilakukan untuk memperdalam atau memperlebar alur pelayaran atau kolam labuh, sungai, dan lain-lain. (Triatmodjo, 1996). Ada 2 macam penggerukan yaitu penggerukan awal (*capital dredging*) dan penggerukan pemeliharaan (*maintenance dredging*).

Ada 2 macam tujuan utama penggerukan yaitu (Yuwono, 1992) :

1. mendapatkan suatu kedalaman tertentu untuk keperluan navigasi, pengendalian banjir, ataupun penampungan air.
2. menambang atau mendapatkan material dari bawah air untuk keperluan reklamasi, industri, dan lain-lain.

Syarat batas gelombang maksimum untuk peralatan penggerukan (Yuwono, 1992) :

Tabel 2.1 Syarat batas (Yuwono, 1992)

| Jenis peralatan: | Tinggi gelombang maksimum: |
|------------------------|----------------------------|
| 1. Dipper | 0.8 m |
| 2. Backhoe | 0.8 m |
| 3. Bucket | 1.0 m |
| 4. Self propelled grab | 3.5 m |
| 5. Cutter suction | 4.0 m |
| 6. trailer suction | 4.0 m |

Sedangkan syarat batas kedalaman perairan oleh Land (1997) :

Tabel 2.2 Syarat batas kedalaman perairan (Land, 1997)

| Tipe: | Jenis: | Ukuran: | Min. Depth | Max. depth |
|--------|--------|------------------------------|------------|------------|
| TSHD | Small | Hopper < 1500 m ³ | 5 m | 15 m |
| | Medium | 1500-4000 m ³ | 7 m | 20 m |
| | Large | > 4000 m ³ | 9 m | 35 m |
| CSD | Small | Diam. discharge < 400 mm | 1 m | 9 m |
| | Medium | 400-800 mm | 1.5 m | 17 m |
| | Large | > 800 mm | 2 m | 30 m |
| BUCKET | Small | Bucket < 300 LITER | 5 m | 12 m |
| | Medium | 300-600 LITER | 7.5 m | 19 m |
| | Large | > 600 LITER | 10 m | 30 m |
| GRAB | Small | Bucket < 3 m ³ | 1 m | |
| | Medium | 3-6 m ³ | 1.5 m | Nolimit |
| | Large | > 6 m ³ | 2 m | |

Pemilihan peralatan keruk dipengaruhi oleh jenis material, keadaan perairan (terlindung, tertutup, atau terbuka), jarak/lokasi pembuangan, besarnya volume kerukan, dan kondisi lalu lintas di perairan (pelabuhan) tersebut (Land, 1997). British Standard Code of Practice for Maritim Structures (part 5) Recommendations for Dredging and Land Reclamation dalam Land (1997) memberikan pedoman evaluasi peralatan pengeringan sebagai berikut :

Tabel 2.3 Evaluasi Jenis Peralatan Keruk (BS 6349: Part 5:1991)

A. Maintenance Dredging

| Site con. | Stan | Light | Cutter | Bucket | Wheel | Grab | Grab | Back | Bucket | Dipper | Barge |
|----------------------|------|-------|--------|--------|--------|---------|------|------|--------|--------|-------|
| | | | | | hopper | pontoon | | | | | |
| Bed material | | | | | | | | | | | |
| Loose silt | 1 | 1 | 1 | 1 | 2 | 2 | 2 | 2 | N | 1 | |
| Cohesive silt | 1 | 2 | 1 | 1 | 1 | 1 | 2 | 1 | N | 1 | |
| Fine sand | 1 | 1 | 1 | 1 | 2 | 2 | 2 | 2 | N | 1 | |
| Medium sand | 1 | 1 | 1 | 1 | 2 | 2 | 1 | 2 | N | 1 | |
| coarse sand | 1 | 2 | 1 | 1 | 2 | 2 | 1 | 2 | N | 1 | |
| Sea condition | | | | | | | | | | | |
| Impounded water | 3 | 2 | 1 | 1 | 1 | 2 | 2 | 2 | N | 1 | |
| Sheltered water | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | N | 2 | |
| Exposed water | 1 | 2 | 3 | 3 | 3 | N | 3 | 3 | N | N | |

| Disposal to: | | | | | | | | | | | |
|---------------------|---|---|---|---|---|---|---|---|---|---|--|
| Shore | 2 | 2 | 1 | 1 | N | 2 | 2 | 2 | N | 1 | |
| Tide | 1 | 1 | 1 | N | N | N | N | N | N | N | |
| Sea | 1 | 1 | N | N | 1 | 1 | 1 | 1 | N | N | |
| Quantities | | | | | | | | | | | |
| < 100,000 m | 2 | 1 | 1 | 1 | 1 | 1 | 2 | 1 | N | 1 | |
| < 250,000 m | 1 | 2 | 1 | 1 | 1 | 2 | 1 | 2 | N | 1 | |
| < 500,000 m | 1 | 2 | 1 | 1 | 3 | 2 | 1 | 2 | N | 1 | |
| > 500,000 m | 1 | 2 | 1 | 1 | 3 | 3 | 1 | 3 | N | 1 | |
| Heavy traffic | 1 | 1 | 3 | 3 | 2 | 2 | 3 | 1 | N | 2 | |
| Light traffic | 1 | 2 | 1 | 1 | 2 | 2 | 2 | 1 | N | 2 | |

B. Capital Dredging :

| Site con | Stan | Light | Cutter | Bucket | Grab wheel | Grab hopper | Grab pontoon | Back | Bucket | Dipper | Barge |
|---------------|------|-------|--------|--------|---------------|----------------|-----------------|------|--------|--------|-------|
| Bed material | | | | | | | | | | | |
| Loose silt | 1 | 1 | 1 | 1 | 2 | 2 | 2 | 2 | 3 | 1 | |
| Cohesive silt | 1 | 1 | 1 | 1 | 1 | 1 | 2 | 1 | 3 | 1 | |
| Fine sand | 1 | 1 | 1 | 1 | 2 | 2 | 2 | 2 | 3 | 1 | |
| Medium sand | 1 | 1 | 1 | 1 | 2 | 2 | 1 | 2 | 2 | 1 | |
| Coarse sand | 1 | 1 | 1 | 1 | 1 | 1 | 2 | 2 | 1 | 1 | |
| Gravel | 1 | 2 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | |
| Soft Clay | 1 | 2 | 3 | 1 | 1 | 2 | 2 | 1 | 2 | 1 | |

| | | | | | | | | | | |
|----------------------|---|---|---|---|---|---|---|---|---|---|
| Medium clay | 2 | 3 | 3 | 2 | 2 | 2 | 1 | 1 | 2 | 2 |
| Boulders | N | N | 3 | 3 | 3 | 2 | 1 | 2 | 1 | N |
| Weak rock | N | N | 1 | 3 | N | N | 1 | 3 | 1 | N |
| Sea condition | | | | | | | | | | |
| Impounded water | N | 3 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Sheltered water | 1 | 1 | 1 | 2 | 2 | 1 | 1 | 2 | 2 | 3 |
| Exposed water | 1 | 2 | 3 | 3 | 3 | 3 | 2 | 3 | 3 | N |
| Disposal to: | 1 | | | | | | | | | |
| Shore | 1 | 2 | 1 | 1 | N | N | N | N | N | 1 |
| Tide | 1 | 1 | 2 | 1 | N | N | N | N | N | N |
| Sea | 1 | 1 | 3 | 3 | 1 | 1 | 1 | 1 | 1 | N |
| Quantities | | | | | | | | | | |
| < 100,000 m | 2 | 1 | 1 | 1 | 1 | 1 | 1 | 2 | 1 | 1 |
| < 250,000 m | 1 | 2 | 1 | 1 | 2 | 2 | 1 | 1 | 2 | 1 |
| < 500,000 m | 1 | 3 | 1 | 1 | 3 | 2 | 2 | 1 | 3 | 1 |
| > 500,000 m | 1 | 3 | 1 | 1 | 3 | 3 | 3 | 1 | 3 | 1 |
| Heavy traffic | 1 | 1 | 1 | 2 | 2 | 3 | 2 | 3 | 2 | 2 |
| Light traffic | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 2 | 2 |

(Sumber : Land (1997)

Keterangan tabel:

Site con. = site condition = kondisi lapangan, Stan = standart trailer, Light= light trailer,

Cutter = cutter suction dredger, Back = backhoe, 1 = Suitable (cocok), 2 = Acceptable

(dapat diterima), 3 = Marginal (terbatas) N = not suitable (tidak cocok/digunakan)

Kapasitas kapal keruk bermacam-macam tergantung daya pompa dan peralatan pendukungnya. Kapal dengan diameter *discharge pipe* 30" (762 mm) dengan daya pompa 5000-8000 hp (3782-5964 kW) dan daya *cutter* 2000 hp(1491 kW) akan memompa 2000-4500 yd^3/jam (1529-3440 m^3/jam) material lunak dan 200-2000 yd^3/jam (153-1529 m^3/jam) untuk material lunak sampai keras melalui pipa dengan panjang sampai 15000 ft atau 4572 m (Heirbich, 1992).

Sedimen transport berperan penting dalam berbagai masalah teknik pantai. Erosi yang tidak diinginkan pada bangunan pantai, abrasi garis pantai atau pengndapan sedimen pada muara, alur pelayaran, atau kolam labuh merupakan contoh permasalahan yang berkaitan dengan sedimen transport ini. Ada dua jenis sedimen transport, yaitu *Cohesive* dan *Non Cohesive*. Transport sedimen kohesif sering diistilahkan menjadi *Suspended Load Transport* karena kebanyakan sifatnya yang melayang di air, Sementara transport sedimen non kohesif disebut *Bed Load Transport* (Pratikto dkk, 1997).

Transportasi sedimen pantai merupakan gerakan sedimen di daerah pantai yang disebabkan oleh arus dan gelombang. Daerah transportasi pantai terbentang dari garis pantai sampai tepat di luar daerah gelombang pecah (*sufra zone*) (SPM, 1984).

Karakteristik sedimen yang meliputi ukuran partikel dan distribusinya serta bentuk dan *specific gravity* (ρ) juga sangat penting untuk diketahui, karena sangat berpengaruh pada proses pengendapan/ kecepatan jatuh partikel sedimen setelah terapung.

Biaya untuk melakukan pekerjaan pengerukan adalah biaya “hidup”, dalam artian besarnya tergantung pada waktu dan lingkungan. Pada kebanyakan pekerjaan pengerukan, biaya total pengerukan terdiri atas 2 elemen penting: biaya mobilisasi dan demobilisasi, buruh dan perlengkapan, serta biaya pelaksanaan pekerjaan yang sebenarnya. Umumnya biaya mobilisasi dan demobilisasi tidak begitu jauh berbeda (Land, 1997).

2. 2. Landasan Teori

2. 2. 1. Pasang Surut

Pasang surut adalah fluktuasi muka air laut karena adanya gaya tarik benda-benda langit, terutama matahari dan bulan terhadap massa air laut bumi.

Tinggi pasang surut adalah jarak vertikal antara air tertinggi (puncak air pasang) dan air terendah (lembah air surut) yang berurutan. Periode pasang surut adalah waktu yang diperlukan dari posisi muka air pada muka air rerata ke posisi yang sama berikutnya. Variasi muka air laut dapat menimbulkan arus pasang surut yang mengangkut massa air dalam jumlah sangat besar.

Bentuk pasang surut diberbagai daerah tidak sama. Secara umum pasang surut di berbagai daerah dapat dibedakan dalam empat tipe, yaitu:

- a. Pasang surut harian ganda (*semi diurnal tide*).

Dalam satu hari terjadi dua kali air pasang dan dua kali air surut dengan tinggi yang hampir sama dan pasang surut terjadi secara berurutan secara teratur. Periode pasang surut rata-rata adalah 12 jam 24 menit.

- b. Pasang surut harian tunggal (*diumal tide*).

Dalam satu hari terjadi satu kali air pasang dan satu kali air surut. Periode pasang surut rata-rata adalah 24 jam 50 menit

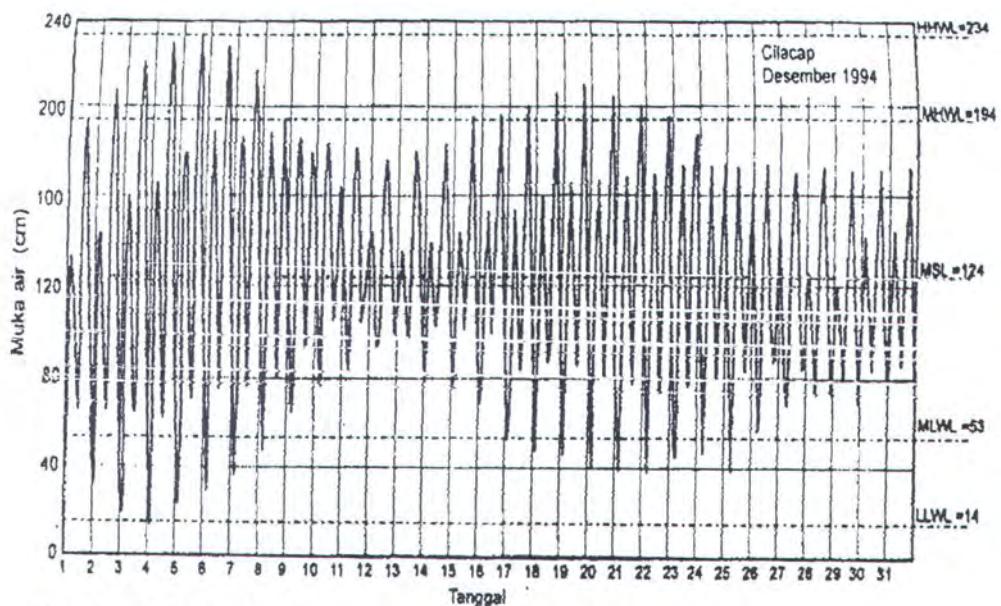
- c. Pasang surut campuran condong ke harian ganda (*mixed tide prevailing semidiumal*).

Dalam satu hari terjadi dua kali air pasang dan dua kali air surut, tetapi tinggi dan periodenya berbeda

- d. Pasang surut campuran condong ke harian tunggal (*mixed tide prevailing diurnal*).

Dalam satu hari terjadi satu kali air pasang dan satu kali air surut, tetapi kadang-kadang untuk sementara waktu terjadi dua kali pasang dan dua kali surut.

Contoh kurva pasang surut dapat dilihat pada gambar 2.1 berikut ini:



Gambar 2.1 Contoh kurva pasang surut (sumber: Triatmodjo, 1996)

Beberapa istilah dalam pasang surut :

MHWS : *mean high water spring* = rata-rata kenaikan air sepanjang periode tertentu, biasanya 19 tahun. biasa disingkat HWS.

MLWS : *mean low water spring* rata-rata muka air rendah sepanjang periode tertentu, biasanya 19 tahun, biasa disingkat LWS.

MSL : *mean sea level* = muka air laut rerata, adalah muka air rerata antara muka air tinggi rerata muka air rendah rerata. Elevasi ini biasa digunakan referensi untuk elevasi di darat.

HHWS : *higher high water spring* = kenaikan tertinggi diantara 2 pasang naik sepanjang sehari pasang diurnal (pada saat pasang surut purnama atau bulan mati).

LLWS : *lower low water spring* = surut terendah diantara 2 pasang surut sepanjang sehari pasang diurnal. (pada saat pasang surut purnama atau bulan mati).



MHHWS : rata-rata tertinggi dari pasang tertinggi sepanjang periode tertentu, biasanya 19 tahun.

MLLWS : rata-rata terendah dari surut terendah sepanjang periode tertentu, biasanya 19 tahun.

Untuk melakukan pekerjaan pengeringan perlu menggunakan elevasi referensi yang biasa disebut datum. Ada 2 macam datum yang biasa digunakan, yaitu:

1. *Land datum* (LD)

Pada beberapa negara yang biasa diambil atau didefinisikan sebagai muka air laut rata-rata (MSL)

2. *Chart datum* (CD)

Chart datum pada umumnya diambil sebagai muka air laut rata-rata pada saat *Low Water Spring*.

Pengetahuan pasang surut ini diperlukan agar kapal keruk tidak mengalami hambatan saat beroperasi.

2. 2. 2. Analisa Tanah

- Analisa Ukuran Butir Tanah

Untuk menentukan kapal keruk yang akan digunakan dalam pekerjaan pengeringan maka harus diketahui terlebih dahulu ukuran butiran tanah sehingga dapat dipilih peralatan keruk yang tepat.

Disamping analisa ukuran butiran tanah, maka diperlukan pengujian SPT untuk mengetahui kondisi tanah- keras atau lunak.

Analisa sifat-sifat tanah juga diperlukan untuk menentukan apakah tanah tersebut layak digunakan sebagai bahan timbunan reklamasi.

- Analisa Stabilitas Lereng

Suatu analisa stabilitas terdiri dari perkiraan model keruntuhan dan kuat gesernya. Model keruntuhan akan memerlukan peramalan tentang berat yang harus ditahan dan pengaruh air. Beberapa metode yang dapat dipakai untuk analisa stabilitas lereng : metode busur lingkaran, metode lingkaran, metode sayatan dan metode irisan. Cousins (1978) dalam Bowles (1984) menyelesaikan lereng yang sederhana termasuk pengaruh-pengaruh tekanan pori tetapi tidak mencakup setiap kekuatan di dalam zona. Hasil-hasilnya diringkas dalam suatu grafik dalam besaran: sudut kemiringan lereng α , rasio tekanan pori $r_u (=u/(\gamma H))$ yang menghasilkan tegangan efektif sebesar $\sigma'_y = (1-r_u)\gamma H$, dan faktor $\lambda c\phi$ serta faktor N_F . Untuk memudahkan analisa stabilitas lereng ini maka pelaksanaannya dibantu dengan software STABLE.

Penjelasan program stable adalah sebagai berikut:

Profil

Untuk mendefinisikan lapisan tanah sebagai suatu frame garis dengan batas koordinat. Penguraian data profil harus berurutan dari koordinat x, y, batas kiri dan batas kanan, dan pengindikasian tipe tanah, misalnya frame nomor satu terletak pada koordinat (x,y) pada jenis tanah pertama.

Soil

Setiap tipe tanah diuraikan parameter-parameternya, berat unit total (γ), berat unit tanah jenuh (γ_{sat}), gaya kohesi (C), sudut geser (ϕ), parameter dan konstanta tekanan pori didapat dari data lapangan (data tugas), jika

tidak ada maka ditulis nol untuk input program. Berat unit total dan berat unit tanah jenuh adalah dua parameter yang sangat penting, dan keduanya dikhkususkan untuk menentukan dapat atau tidaknya program tersebut berjalan. Untuk kasus dimana zona tanah ada diatas permukaan air, berat unit jenuh tidak akan digunakan saat program melakukan perhitungan namun harus tetap dituliskan sebagai input program.. begitu juga untuk kasus dimana zona tanah dibawah permukaan air, berat unit total tidak akan digunakan saat program melakukan perhitungan, namun tetap harus dituliskan juga sebagai input program.

Water

Option ini digunakan untuk mendefinisikan berat jenis air yang ditinjau dan juga permukaan air dengan koordinat x dan y.

Circle

Digunakan untuk menentukan jumlah titik awal bidang gelincir serta jumlah generation yang diinginkan. Titik awal bidang gelincir dituliskan dengan koordinat x awal sampai x akhir. Begitu juga titik akhir bidang gelincir (koordinat terminal) dituliskan dengan koordinat x awal sampai x akhir.

Sudut geser material (*angle of response*) mempunyai nilai yang sama baik di dalam maupun di atas air. Untuk penentuan slope/lereng, maka Riddle dari Strathclyde University dalam Yuwono (1992) memberikan pedoman kasar sebagai berikut:

| | |
|-------------|----------------|
| Stiff clay | 1:1.5 |
| Firm clay | 1:1.5 - 1:4.5 |
| Sandy clay | 1:4.0 - 1:7.0 |
| Coarse sand | 1:3.0 - 1:6.0 |
| Fine sand | 1:5.0 - 1:10.0 |
| Mud | 1:8.0 - 1:50.0 |

2. 2. 3. Transport Sedimen

Transport sedimen yang terjadi pada suatu perairan dalam hal ini kolam labuh mempengaruhi besarnya volume pengerukan yang direncanakan. Untuk itulah disamping pengerukan awal (*capital dredging*) juga diperlukan penegrukan rutin (*maintenance dredging*).

Untuk mencari besarnya angkutan sedimen sepanjang pantai di zone gelombang pecah dapat dihitung dengan menggunakan berbagai metode, dalam hal ini yang dipakai adalah metode Bijker, dimana dalam metode ini yang berperan penting adalah faktor arus, butiran partikel. Metode Bijker adalah rumus yang paling sederhana dari kelompok rumus yang berdasarkan aliran. Perumusan Bijker lebih kompleks daripada metode CERC. Pemakaian perumusan Bijker mempunyai beberapa kelebihan antara lain:

1. Metode Bijker tidak mengindahkan apakah aliran yang terjadi disebabkan oleh gelombang atau pasang surut. Jadi metode Bijker tetap berlaku untuk semua kondisi aliran.
2. Metode Bijker dapat memberi informasi tentang distribusi pengangkutan pada *surf zone*. Transport sedimen dapat

digambarkan sebagai produk konsentrasi dan kecepatan. Untuk menghitung *longshore sediment transport* maka formula yang digunakan adalah Bijker.

Bijker (1971) dalam Velden (1989) menurunkan formula untuk menghitung sedimen transport tanpa mempedulikan daerah yang ditinjau (di dalam atau di luar breaker zone). Rumus bedload dari Bijker dinyatakan sebagai berikut:

$$S_b = b D_{50} \frac{v}{C} \sqrt{g} \exp \left(-\frac{0.27 \Delta D_{50} C^2}{\mu v^2 \left[1 + \frac{1}{2} \left(\xi \frac{u_b}{v} \right)^2 \right]} \right) \quad (2.1)$$

dimana:

S_b = Transport bedload

b = Konstanta

v = Kecepatan arus

D₅₀ = Diameter butir rata-rata

C = Koefisien Chezy = 18 log (12 h/r)

h = Kedalaman air

r = Kekasaran dasar

g = Percapatan gravitasi

Δ = Berat massa = (ρ_s - ρ_w)/ρ_w

ρ_s = Berat massa pasir

ρ_w = Berat massa air

μ = (C/C₉₀)^{1.5} dengan C₉₀ = log (12 h/D₉₀)

ξ = C (f_w/2g)^{0.5}, dengan f_w = exp (-6.0 + 5.2 (a₀/r)^{0.19})

a_0 = Amplitudo dari lintasan partikel di dasar

u_b = Amplitudo dari lintasan partikel di dasar

(Bijker, 1971) dalam Velden (1989) merumuskan transport sedimen sebagai:

$$S_s = 1.83 \left[I_1 \ln \left(\frac{33h}{r} \right) + I_2 \right] = 1.83 Q S_b \quad (2. 2)$$

dimana:

S_s = Transport dari suspended load

S_b = Tranport dari bed load

I_1, I_2 = Integral dari Einstein

Q = Fungsi relatif kekasaran dasar r/h

Jika harga dari $1.83 Q$ diketahui maka sedimen transport total menurut

Bijker (1971) dalam Velden (1989) adalah:

$$S = S_b + S_s = (1 + 1.83 Q) S_b \quad (2. 3)$$

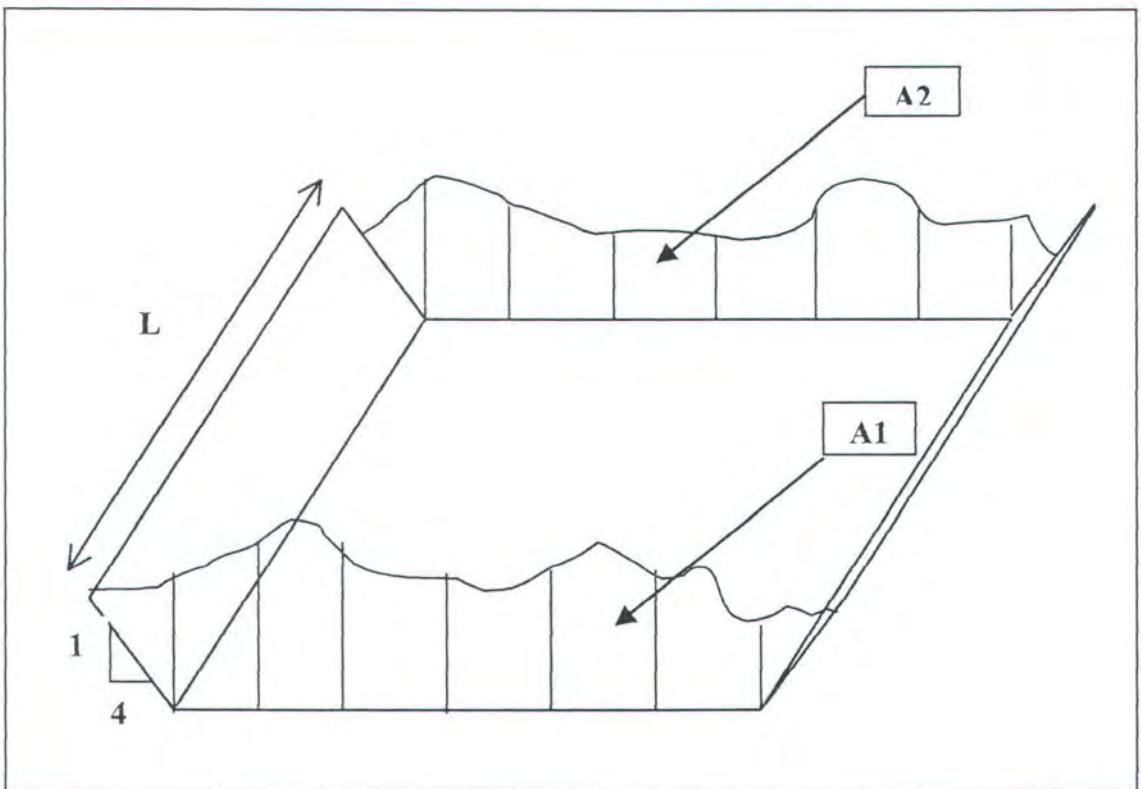
2. 2. 4. Perhitungan Pengerukan

Perhitungan dilakukan dengan menggunakan metode *Average End Area Formula* (Soedjono, 1987). Menurut metode ini volume pengerukan diantara 2 pias yang berurutan diberikan oleh luas rata-rata pias dan jarak antara keduanya (lihat gambar 2.2) :

$$V = \frac{Lx(A_1 + A_2)}{2} \quad (2. 4)$$

Untuk jumlah pias yang cukup banyak $A_1, A_2, A_3, \dots, A_n$, dengan jarak L yang sama maka dapat ditulis :

$$V = \frac{Lx[(A_1 + A_n) + 2x(A_2 + A_3 + A_4 + \dots)]}{2} \quad (2. 5)$$



Gambar 2.2 Sket perhitungan volume pengerukan

2. 2. 5. Jenis Kapal Keruk

Dilihat dari segi teknis pengerukan maka dikenal 2 jenis peralatan, yaitu (Soedjono, 1987) :

- a. Kapal keruk mekanis (*mechanical dredgers*). Kapal keruk jenis ini dapat dikatakan sederhana, yaitu mempunyai kemiripan dengan peralatan gali darat. Dari jenis ini dikenal beberapa tipe dasar, yaitu :
 - Kapal keruk cakram (*grapple/clamshell dredger*), terdiri dari satu tongkang dengan dilengkapi peralatan cakram. Jenis ini biasa digunakan untuk pengerukan tanah lembek atau pada bagian-bagian dalam kolam labuh dan muka dermaga.

- Kapal keruk penggali (*dipper dredger*), jenis ini mempunyai tenaga pengungkit dan desak yang besar, sehingga baik untuk digunakan bagi pengeringan lapisan tanah keras dan tanah padat atau tanah berpasir.
 - Kapal keruk timba (*bucket dredger*), merupakan jenis kapal keruk dengan rantai ban yang tidak berujung pangkal dimana pada rantai ban tersebut dilekatil timba-timba pengering. Gerakan rantai ban dan timbanya merupakan gerak berputar mengelilingi suatu *ladder*. *Ladder* ini dapat bergerak naik turun disesuaikan kedalaman keruk yang diinginkan.
- b. Kapal keruk hidrolis (*hydrollic or suction dredger*). Tanah yang bercampur dengan air laut dikeruk kemudian campuran tersebut dihisap oleh pompa melalui pipa penghisap untuk selanjutnya melalui pipa pembuang dialirkan ke daerah penimbunan. Salah satu contoh tipe kapal keruk hidrolis yaitu kapal keruk CSD (*cutter suction dredger*). Kapal keruk ini dilengkapi dengan konus pisau pemotong tanah keras/karang yang ditempatkan di bagian ujung bawah *ladder*.

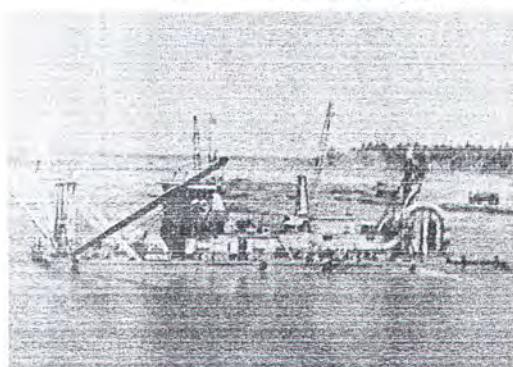
Beberapa jenis kapal keruk dapat dilihat pada gambar 2.2.



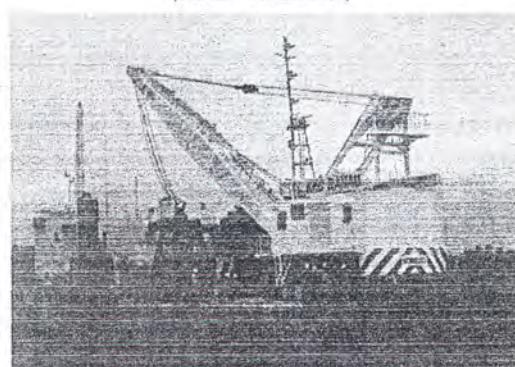
KAPAL KERUK PENGHISAP LUMPUR
(TRAILING SUCTION HOPPER DREDGERS)



KAPAL KERUK TIMBA
(BUCKET DREDGERS)



KAPAL KERUK BOR PENGHISAP LUMPUR
(CUTTER SUCTION DREDGERS)



KAPAL KERUK CANGKRAM
(GRAB/CLAMSHELL DREDGERS)

Gambar 2.3. Beberapa jenis kapal keruk

2. 2. 6. Pertimbangan ekonomi

- Depresiasi (penyusutan)

Penyusutan adalah menurunnya nilai suatu barang seiring dengan umur kerja barang tersebut. Umumnya depresiasi dalam pengerukan adalah model garis lurus.(Land, 1997). Penentuan depresiasi dengan metode garis lurus adalah penentuan besarnya biaya depresiasi setiap tahun dengan jumlah yang sama selama umur ekonomis aktiva yang bersangkutan.

Rumus penyusutan model garis lurus :

$$V_t = P - (P-S)/n \times t = P \times (1 - (t \times P_t)) \quad (2.6)$$

Dengan :

V_t : nilai pada saat t

P : nilai awal

n : umur ekonomis, untuk kapal keruk ditetapkan 30 tahun sesuai standar perusahaan kapal internasional.

S : nilai akhir barang

t : waktu yang ditinjau

- Kebutuhan bahan bakar dan oli

Kebutuhan bahan bakar (minyak diesel) ditentukan berdasarkan Heirbich (1992) yaitu mencapai rata-rata 15% dari Total Tenaga Terpasang (HP) dalam liter/jam. Kebutuhan oli mencapai total 0,07% dari Total Tenaga (HP) per jam dan dihitung mengikuti kurs yang berlaku. Sedangkan menurut Land (1997) kebutuhan pelumas sekitar 10 % dari biaya bahan bakar.

- Biaya perawatan dan perbaikan (*maintenance and repair*)

Dinyatakan sebagai persentase tertentu atas harga kapal. Besarnya tergantung pada tipe kapal keruk. Land (1997) memberikan faktor (persentase) tersebut sebagai berikut:

| Tipe kapal: | Faktor (persentase): |
|-----------------------|----------------------|
| TSHD | 0.000135 |
| CSD | 0.000140 |
| Backhoe | 0.000140 |
| Grab dredger | 0.000130 |
| Self propelled hopper | 0.000130 |
| Dumb hopper | 0.000025 |
| Workboat | 0.000145 |

- Biaya tenaga kerja

Besarnya biaya tenaga kerja tergantung pada jumlah kru yang umumnya terdiri atas master dredger, operator mesin, dan pembantu. Umumnya kru yang diperlukan berkisar antara 3 sampai 10 orang yang bergantung pada daerah dan besarnya kapal. Sebagai contoh di Eropa Utara umumnya mempekerjakan 3 orang untuk kapal keruk TS HD (trailing suction hopper dredger) ukuran kecil (Land, 1997).

- Asuransi

Asuransi mungkin bervariasi antara pemilik. Premi asuransi umumnya berdasarkan pada persentase modal, atau nilai kapal yang diasuransikan. Premi tahunan berdasarkan nilai/harga mungkin bervariasi antara 1 % hingga 5 % atau lebih untuk kontraktor dengan catatan klaim yang tinggi. Sedangkan untuk kontrak pekerjaan umum diasumsikan premi tahunan sebesar 2,5 % (Land, 1997).

2. 2. 7. Kedalaman Kolam Kolam labuh

Menurut Dirjen Pelabuhan dan Pengerukan (1984) maka kedalaman kolam labuh adalah :

$$\text{Kedalaman} = \text{draft kapal} + \text{clearance} (0,8\text{--}1,0 \text{ m}) \quad (2.8)$$

Sedangkan menurut Triatmodjo (1996), maka :

$$\text{Kedalamam} = 1,1 \times \text{draft kapal dibawah elevasi muka air rencana.} \quad (2.9)$$

BAB III

METODOLOGI TUGAS AKHIR

BAB III

METODOLOGI TUGAS AKHIR

III. 1. METODOLOGI TUGAS AKHIR

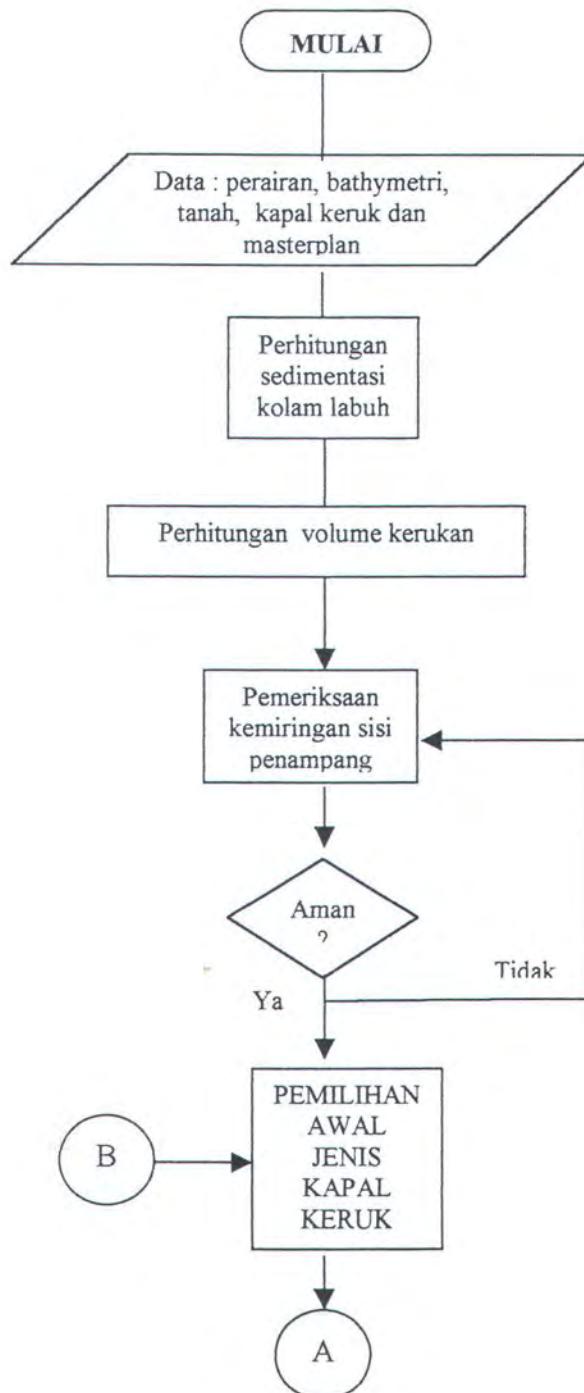
Dalam menyelesaikan penulisan Tugas Akhir ini metodologi yang akan ditempuh dalam beberapa tahapan, yaitu:

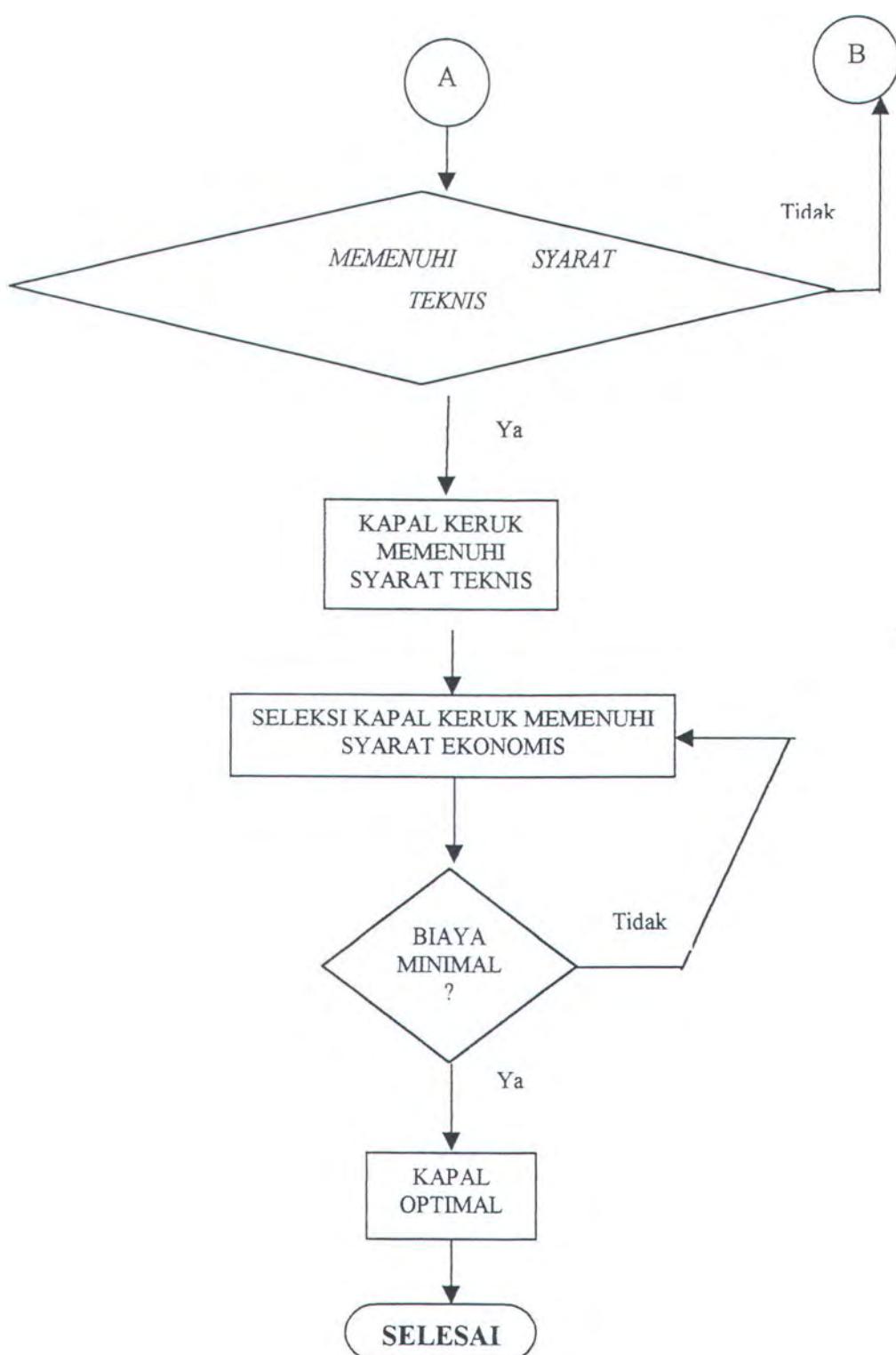
1. Studi literatur yang berkaitan dengan perencanaan pelabuhan, khususnya pengeringan kolam labuh. Studi literatur ini diperlukan untuk memperluas dan memperjelas dasar pemikiran serta landasan teori yang digunakan untuk pengolahan data dalam penulisan Tugas Akhir ini.
2. Pengumpulan data-data perairan, bathymetri, tanah, dan data-data kapal keruk serta master plan Pelabuhan Benoa yang berupa data-data sekunder yang diperoleh dari berbagai sumber antara lain dari PELINDO III dan PT. RUKINDO.
 - Data perairan diperlukan untuk perhitungan sedimentasi serta sebagai pertimbangan dalam pemilihan tipe alat keruk yang sesuai.
 - Data-data bathymetri dan tanah diperlukan untuk menghitung volume pengeringan yang direncanakan serta untuk mengetahui jenis material dasar laut yang akan dikeruk. Data tanah juga diperlukan untuk analisa stabilitas lereng kolam labuh.

- Data-data kapal keruk diperlukan untuk penentuan kapal keruk yang sesuai untuk pengeringan tersebut.
3. Perhitungan sedimentasi kolam labuh untuk mengetahui pengaruhnya terhadap rencana pengeringan.
 4. Perhitungan kebutuhan pengeringan kolam labuh yang meliputi: perhitungan luas pias dan volume kerukan dengan. Kemiringan sisi-sisi penampang 1:4 sesuai dengan kemiringan kolam sebelum dikeruk. Pemeriksaan keamanan kemiringan diperlukan untuk mengetahui apakah kemiringan sisi kolam yang direncanakan telah aman dari longsor.
 5. Pemilihan kapal yang memenuhi syarat teknis dan ekonomis .

III. 2. DIAGRAM ALIR TUGAS AKHIR

Metodologi penyelesaian TA tersebut di atas digambarkan sebagai diagram alir di bawah ini:





Gambar 3.1. Diagram Alir Tugas Akhir

BAB IV

PENGOPERASIAN PIRANTI LUNAK

BAB IV

PENGOPERASIAN PIRANTI LUNAK

IV. 1. Pemodelan

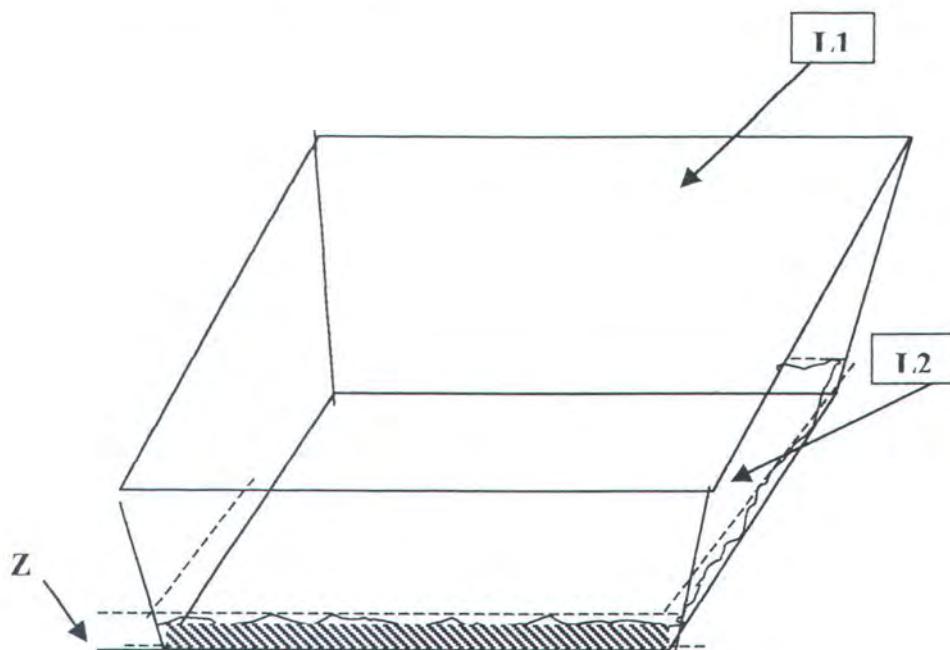
- Sedimentasi

Untuk menghitung besarnya sedimentasi pertahunnya, maka dihitung terlebih dahulu sedimentasi perdetiknya. Model perhitungannya adalah sebagai berikut:

$$\text{Sedimentasi/tahun} = \text{sedimentasi (m}^3/\text{detik)} \times 3600 \times 24 \times 365 \\ (\text{m}^3/\text{tahun}) \dots \dots \dots \quad (\text{IV.1})$$

Sedangkan tebal sedimentasi/tahun dihitung dengan metode perhitungan volume kerukan *average end area* (rumus 2.8), dengan luas pias I diganti luas kolam labuh (L1) dan luas pias II diganti dengan luas dasar kolam labuh (L2) dan panjang kolam labuh diganti dengan tebal sedimentasi yang dicari (Z) (lihat gambar 4.1) Sehingga:

$$\text{Tebal/tahun} = \text{sedimen/tahun (m}^3/\text{tahun)} / \text{luas rerata dari kolam labuh dan} \\ \text{dasar kolam} \dots \dots \dots \quad (\text{IV.2})$$



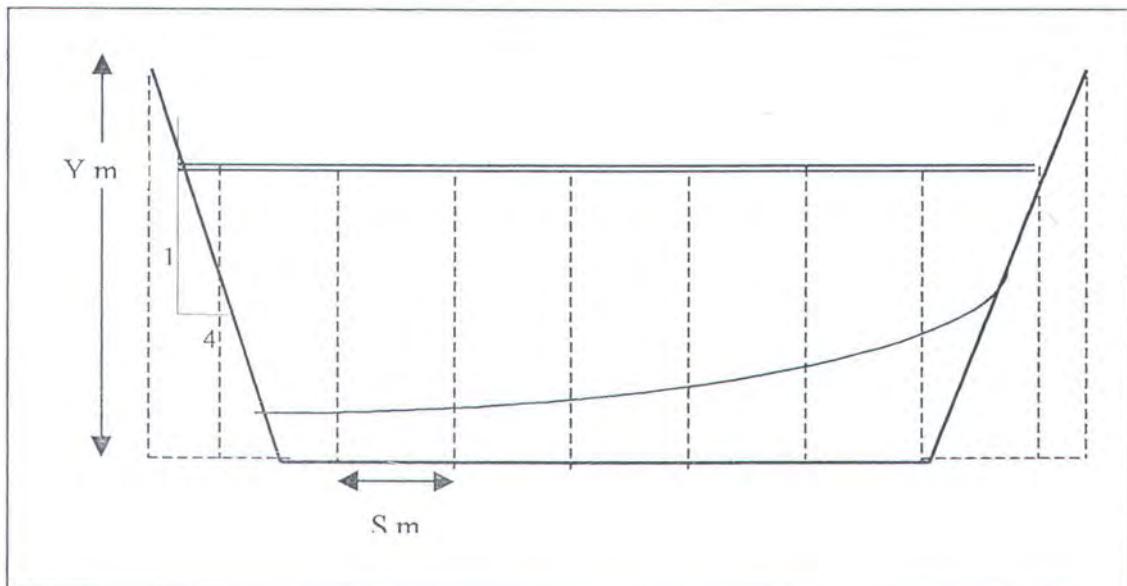
Gambar 4.1 Sket perhitungan ketebalan sedimentasi

- Perhitungan Volume Pengerukan

Perhitungan dilakukan dengan menggunakan metode *Average End Area Formula*. Menurut metode ini volume pengerukan diantara 2 pias yang berurutan diberikan oleh luas rata-rata pias dan jarak antara keduanya (rumus 2.4 dan 2.5).

Dalam perhitungan volume kerukan ini maka peta bathymetri terlebih dahulu dibagi menjadi beberapa pias agar memudahkan dalam perhitungannya, dalam hal ini dibagi menjadi 9 pias. Masing-masing pias terdiri atas beberapa titik-titik sounding (16 titik) dengan jarak antara titik-titik sounding (S) tersebut adalah 20 meter (yaitu lebar kolam 300 m dibagi 15 bagian). Lebar tiap pias adalah 100 meter kecuali pada pias terakhir lebarnya 50 m.

Untuk menghitung luas pias maka dipakai model simpson II, dengan tebal/tinggi kerukan masing-masing titik yang berdekatan (Y). Sedangkan lebarnya adalah jarak antara 2 titik yang berdekatan yaitu 20 m (lihat gambar 4.2).



Gambar 4.2 Sket Perhitungan Luas Pias

Sehingga luas pias = luas total - (luas batas lereng kiri-kanan)

$$= 3/8 \times \text{lebar} \times (\Sigma \text{produk}) - 2 \times \{(Y + 0)/2 \times (Y: (1/4))\}$$

- STABILITAS LERENG KOLAM LABUH

Slope (kemiringan) kolam labuh yang direncanakan tergantung jenis material (tanah) kolam labuh. Sebagai pedoman kasar maka dipakai acuan dari Riddle dalam Yuwono (1992). Hasil ini perlu dibandingkan dengan menggunakan program stable.

- ANALISA TEKNIS PEMILIHAN KAPAL KERUK

Berdasarkan table 2.2 maka dibuat penilaian peralatan keruk sebagai berikut:

| Kondisi: | nilai: |
|--------------------------------------|--------|
| Suitable (sesuai) | 3 |
| Acceptable (dapat diterima) | 2 |
| Marginal (terbatas) | 1 |
| Not applicable (tidak dapat dipakai) | 0 |

Kemudian dari input data lapangan maka dapat diketahui jumlah nilai/skor untuk masing-masing peralatan keruk. Dari total nilai yang diperoleh maka peralatan keruk yang mempunyai nilai/skor terbesar yang diambil.

- ANALISA EKONOMI PEMILIHAN KAPAL KERUK

Menurut Heirbich (1992) maka kebutuhan bahan bakar (minyak diesel) mencapai 15% dari total tenaga terpasang (hp) dalam l/jam. Sedangkan kebutuhan oli mencapai $0.07\% \times \text{hp}$ dalam l/jam. Sedangkan asuransi/tahun mencapai 2.5% dari harga alat.

Model analisa ekonomi disusun dengan cara mengkonversikan semua biaya menjadi biaya (Rp/jam) sebagai berikut:

Biaya bahan bakar = harga satuan BBM \times kebutuhan BBM (liter/jam)

Biaya pelumas = harga satuan pelumas rerata \times kebutuhan pelumas (liter/jam)

Pelumas meliputi oli transmisi, final drive, hidrolis, grease/gemuk, filter, dan komponen lain. Jenis oli dan besarnya kebutuhan dianggap sama yaitu 0.07% dari tenaga mesin. Atau secara total = $6 \times 0.07\% \times \text{tenaga mesin}$.

Biaya perawatan dan perbaikan rutin = faktor alat x harga alat (Rp/hari)
= faktor alat x harga alat/jam kerja
(Rp/jam).

Untuk faktor alat di atas dapat dilihat pada Bab II.

Biaya pekerja = upah perorang perbulan/(30 hari x jam kerja) (Rp/jam)

Asuransi = Harga x 2.5%/(48 minggu x 6hari kerja per tahun) (Rp/hari)
= Harga x 2.5%/(48 minggu x 6hari kerja per tahun x jam kerja
perhari) (Rp/jam).

Penyusutan modal/tahun = (harga awal – nilai sisa (5% dari harga))/(umur
alat yang ditetapkan 30 tahun)

Nilai penyusutan/jam = (penyusutan modal/tahun)/(48 minggu x 6 hari
kerja x jam kerja perhari)

Biaya pengerukan (Rp/m³) = total biaya (Rp/jam)/kapasitas produksi
(m³/jam).

Biaya total = biaya/m³ x volume pengerukan.

IV. 2. Pengoperasian dan Keterbatasan

Untuk memulai menjalankan piranti lunak **PENGERUKAN 1.0**
maka klik ganda **FILE PENGERUKAN 1.0.EXE**. Untuk permulaan
program akan menampilkan jendela (*window*) seperti pada gambar 4.3.
Untuk memulai aplikasi baru maka klik File dilanjutkan Baru atau klik *icon*
yang terdapat pada toolbar. Selanjutnya akan tampak tampilan seperti pada
gambar 4.4.

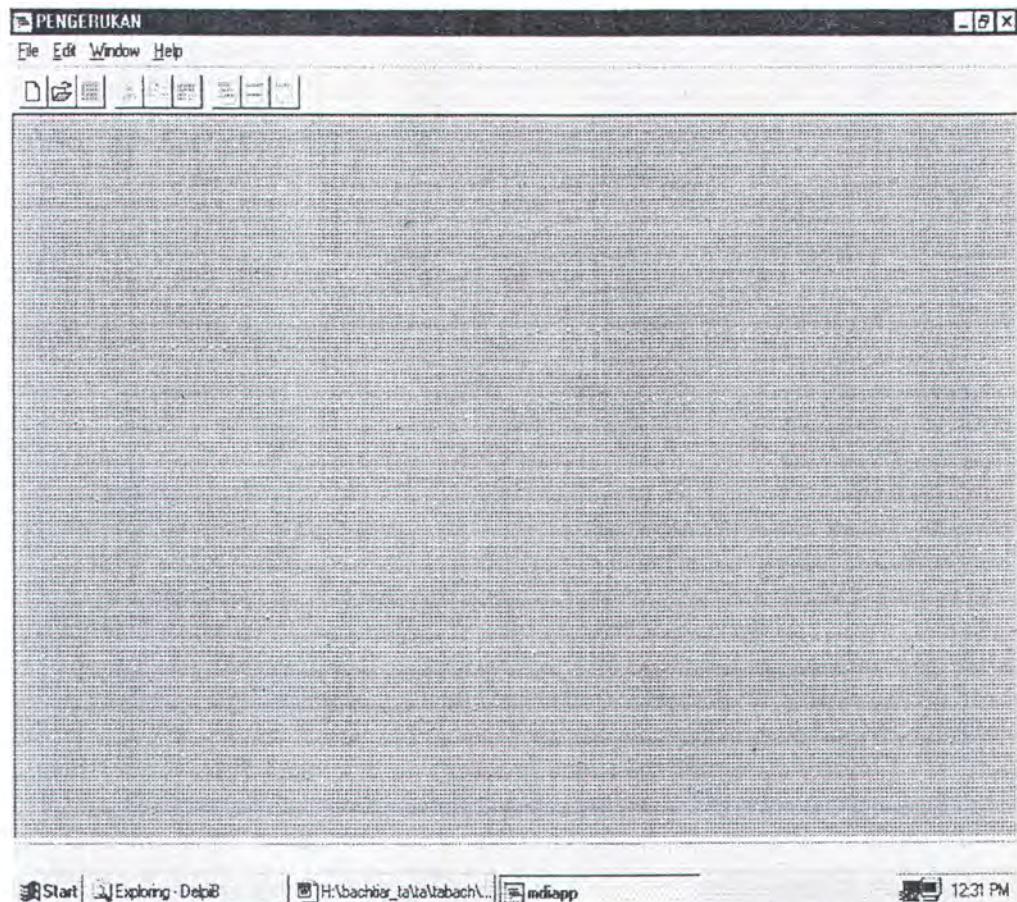
Pada jendela tersebut terdapat 5 *tabsheet* yang masing-masing adalah: data kapal dan kolam labuh, sedimentasi, analisa teknis, analisa ekonomi, dan database. Masing-masing *tabsheet* tersebut akan dijelaskan sebagai berikut.

a. Tabsheet data kapal dan kolam labuh

Tabsheet ini untuk menghitung kedalaman kolam yang direncanakan berdasarkan ukuran kapal (saraf) terbesar . Untuk itu maka input yang diperlukan adalah ukuran draft/sarat kapal maksimum, serta kedalaman eksisting kolam labuh. Kemudian klik tombol **OK**. Maka kedalaman kolam yang direncanakan serta besarnya penggerakan yang diperlukan akan ditampilkan. Untuk membatalkan atau mengganti input maka klik tombol **BATAL** dan ganti dengan input nilai yang dikehendaki. Sedangkan untuk menentukan slope kolam labuh maka klik combobox slope dan pilih material yang sesuai. Hasilnya akan ditampilkan pada edit slope. Sedangkan untuk menghitung volume kerukan maka input yang dimasukkan adalah luas pias. Klik tombol **OK** untuk menghitung total volumenya. (lihat gambar 4.4).

b. Tabsheet sedimentasi

Untuk menghitung sedimentasi maka input yang diperlukan adalah kecepatan arus, arah, d50, d90, dan kekasaran (r). Klik pada cell pertama dan masukkan nilai arus. Untuk pindah ke cell berikutnya maka gunakan tab, demikian seterusnya. Untuk membatalkan input klik tombol **BATAL** dan ganti dengan input nilai yang dikehendaki. Untuk menambah data klik tombol tambah data. (lihat gambar 4.5).

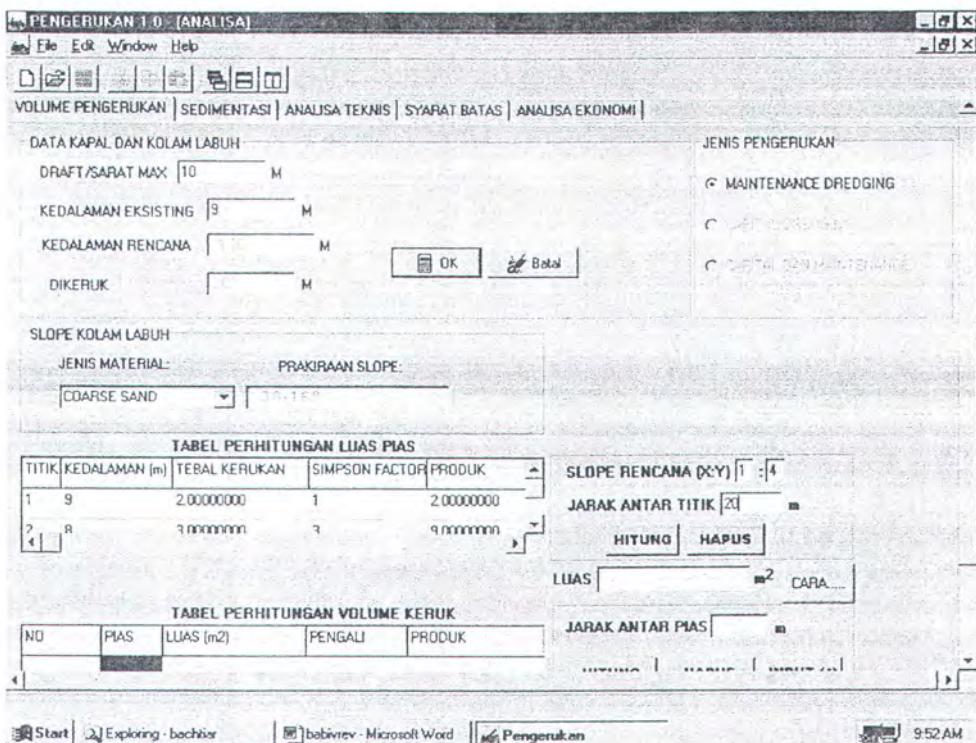


Gambar 4.3 Tampilan utama

c. Tabsheet analisa teknis

Analisa teknis dibuat dengan mengacu pada *BRITISH STANDART CODE (BSI)* yang memberikan nilai/skor untuk kondisi/parameter tertentu. BSI membedakan penilaian atau evaluasi peralatan keruk untuk capital dredging dan maintenance dredging.

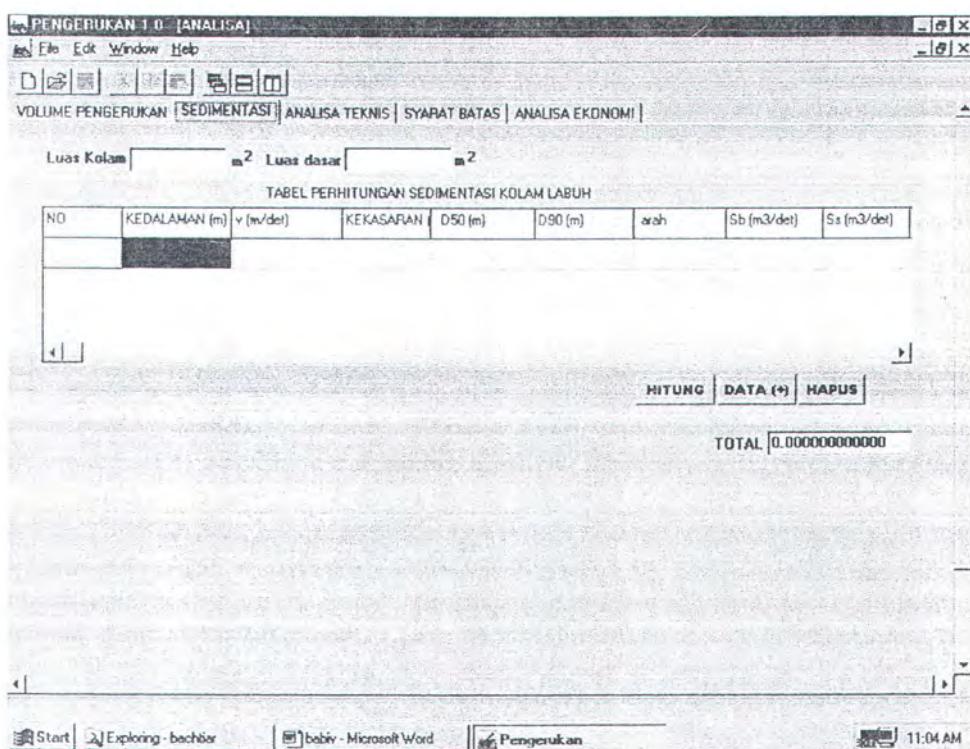
PENGOPERASIAN PIRANTI LUNAK



Gambar 4.4 Tampilan awal (Tabsheet Data Kapal dan Kolam Labuh)

Untuk input jenis material maka klik *combobox* jenis material dan pilih material yang sesuai atau mendekati kondisi kolam labuh tersebut. Demikian pula input untuk lokasi pembuangan, kondisi perairan, volume kerukan dan kondisi lalu lintas dilakuakan dengan cara yang sama. Setelah semua input dimasukkan maka klik tombol **OK**. Untuk membatalkan input klik tombol **BATAL** dan ganti dengan input nilai yang dikehendaki. (lihat gambar 4.6).

PENGOPERASIAN PIRANTI LUNAK



Gambar 4.5 Tampilan tabsheet sedimentasi kolam labuh

c. Tabsheet syarat batas

Untuk menguji apakah peralatan keruk yang dipilih memenuhi syarat batas gelombang maksimum maka masukkan tinggi gelombang , kemudian klik combobox tipe peralatan yang dimaksud. Jika peralatan tersebut memenuhi syarat batas maka pesan akan ditampilkan pada memo. (lihat gambar 4.7).

d. Tabsheet analisa ekonomi

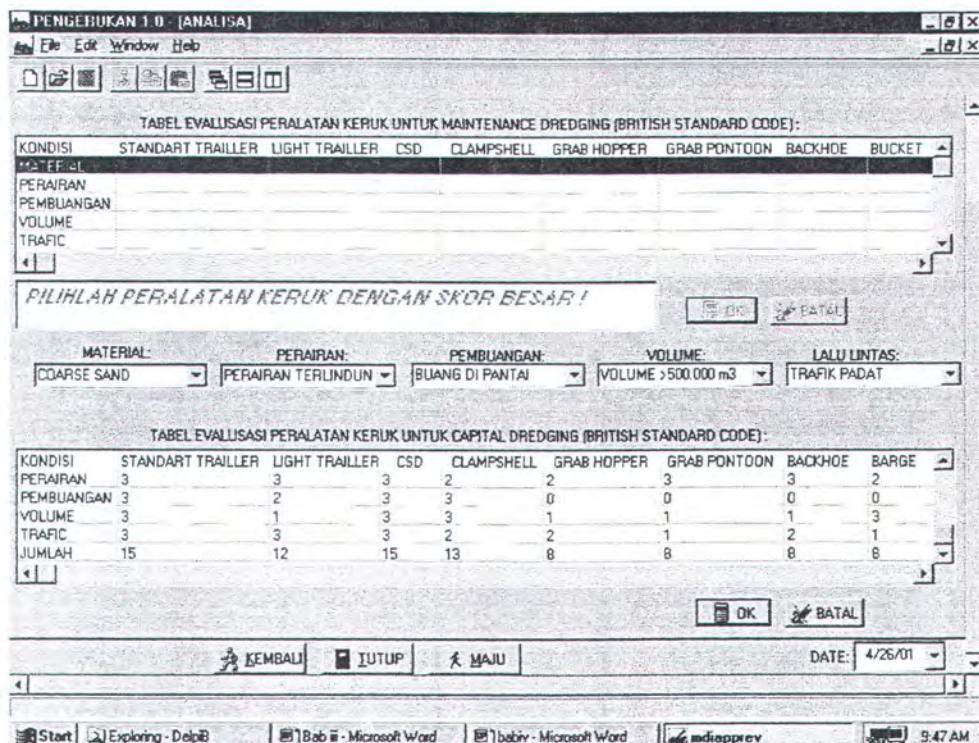
Untuk menghitung besarnya biaya pengeringan/ m^3 maka input yang diperlukan adalah: tipe dan nama kapal, ukuran kapal (LOA, B, T),



PENGOPERASIAN PIRANTI LUNAK

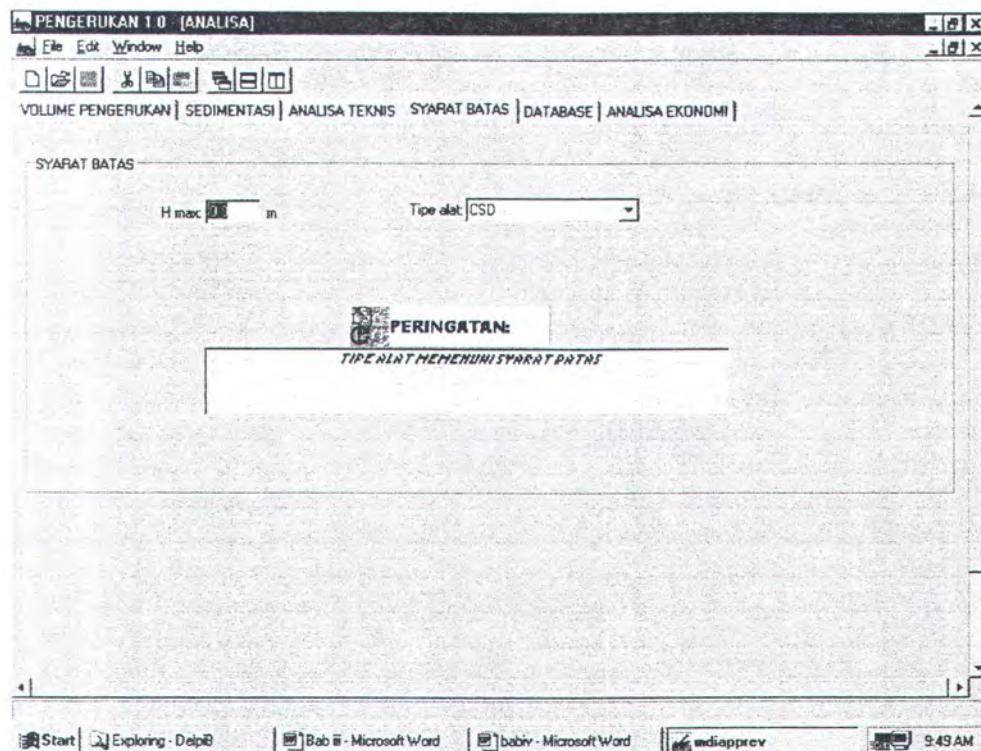
kedalaman keruk, diameter pipa, daya pompa, kapasitas produksi, harga beli, biaya tenaga kerja.

Setelah semua input dimasukkan maka klik tombol **OK**. Untuk membatalkan maka klik tombol **BATAL** dan ganti dengan input nilai yang dikehendaki. (lihat gambar 4.8).

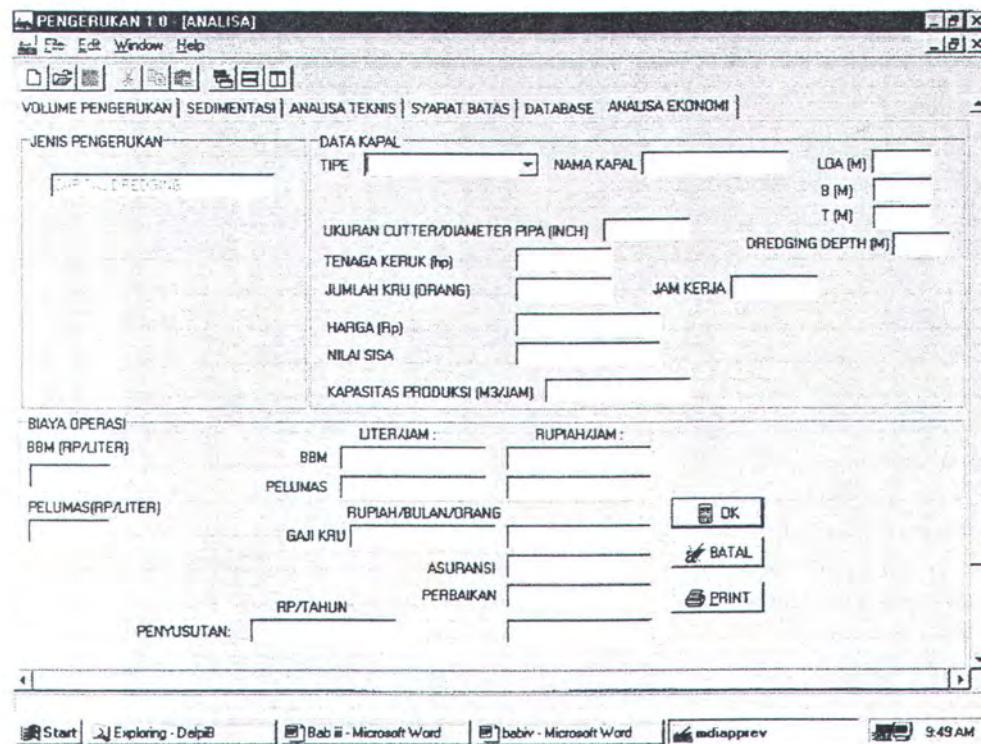


Gambar 4.6 Tampilan tabsheet analisa teknis

PENGOPERASIAN PIRANTI LUNAK



Gambar 4.7 Tampilan Tabsheet Syarat Batas



Gambar 4.8 Tampilan Tabsheet Analisa ekonomi

BAB V

PEMBAHASAN

BAB V

PEMBAHASAN

V. 1. Analisa Data

V. 1. 1. Umum

Pelabuhan Benoa sebagai salah satu pelabuhan terbesar di Bali mempunyai posisi yang strategis baik ditinjau secara geografis maupun terhadap kegiatan-kegiatan yang bertaraf nasional maupun internasional. Ditinjau secara geografis Pelabuhan Benoa berada di Teluk Benoa di bagian Selatan Pulau Bali pada posisi $08^{\circ}44'22''$ LS dan $115^{\circ}12'20''$ BT sehingga kurang terpengaruh oleh perubahan musim. Jarak dari pusat kota Denpasar kurang lebih 10 km atau 15 menit dari Bandara Internasional Ngurah Rai.

V. 1. 2. Gelombang, Arus dan Pasang Surut

Kondisi Pelabuhan Benoa yang relatif terlindung oleh pulau-pulau disekitarnya (Pulau Penyu dan Pulau Serangan) tentunya menjadikan perairan di kolam labuh cukup tenang. Gelombang tertinggi (tahunan) yang terjadi di kolam labuh adalah 0.8 meter yang biasa terjadi pada bulan Januari-Februari, sedangkan tinggi gelombang rerata besarnya 0.5 meter (Pelindo III, 2000).

Variasi muka air laut dapat menimbulkan arus pasang surut yang mengangkut massa air dalam jumlah sangat besar. Tinggi pasang surut

adalah jarak vertikal antara air tertinggi (puncak air pasang) dan air terendah (lembah air surut) yang berurutan. Berikut ini adalah data pasang surut (data tahunan):

| |
|------------------------------|
| HWS = 2,70 m |
| MHWS = 2,5 m |
| MSL = 1,25 m |
| Air terendah (LLWS) = 0,4 m |
| Chart datum (LWS) = 0,00 LWS |

Gambar 5.1 Data pasang surut Pelabuhan Benoa (Pelindo III, 2000)

V. 1. 3. Data Tanah

Peta bathymetri menunjukkan kontur dasar laut di daerah itu. Untuk peta *bathy metri* kolam labuh dermaga umum dapat dilihat pada lampiran peta bathymetri.

Posisi titik-titik pengeboran (*borehole*, disingkat BH) BH.1 sampai dengan BH.21 dapat dilihat pada lampiran. Hasil uji tanah tersebut dapat dilihat dalam tabel 5.1.

Dari hasil uji tanah di lokasi perairan Pelabuhan Benoa, tampak bahwa sebagian besar kondisi kepadatan dan jenis tanah yang ada didominasi oleh *loose sand* dengan sedikit kandungan *silt* dan *clay* di dalamnya. Satu-satunya jenis tanah yang tergolong medium dan padat adalah di zona BH.21(utara-barat dermaga benoa lama). Selanjutnya areal

keruk Pelabuhan Benoa dapat dikelompokkan dalam 4 zona berdasarkan kedalaman perairan yang ada dan posisi lokasi keruk.

Zona A: berada di sisi Timur Pelabuhan Benoa pada posisi antara lahan sisi Timur pelabuhan sampai sisi barat Pulau Serangan atau BTID dengan kondisi perairan terlindung. Kedalaman berkisar antara -2.0 m LWS sampai dengan 0.0 m LWS, bahkan di beberapa tempat terdapat terdapat daerah dengan elevasi kontur +1.0 m LWS. Titik penyelidikan yang diambil di sekitar Zona A adalah BH.1 hingga BH.9. Jenis tanah sangat bervariasi antara silt, sand dan gravel.

Zona B: berada di sisi Timur Pelabuhan Benoa, merupakan areal kolam pelabuhan lama. Kedalaman berkisar -9.0 m LWS, seluruhnya merupakan perairan kolam labuh. Titik penyelidikan tanah yang diambil disekitar zona B adalah BH.13 dan BH.18.

Zona C: berada di sebelah barat areal Pelabuhan Benoa, merupakan areal perairan kosong dengan pantai berbakau dan agak ke arah selatan terdapat ujung runway Bandara Ngurah Rai. Kedalaman perairan berkisar antara -5,0 m LWS sampai dengan +1.0 m LWS, sebagian perairan digunakan untuk alur pelabuhan menuju dermaga perikanan di sebelah barat. Titik penyelidikan tanah yang di ambil pada zona C meliputi BH.11, 12, 14, 15, 16, dan BH.21.

Zona D: merupakan areal alur pelayaran Pelabuhan Benoa yang diperdalam berulang kali dan mengalami pengeringan rutin 2 sampai 4 tahun sekali. Kedalaman berkisar antara -12 m LWS sampai dengan -5.0 m LWS, areal ini mencakup perairan di bagian selatan yang merupakan

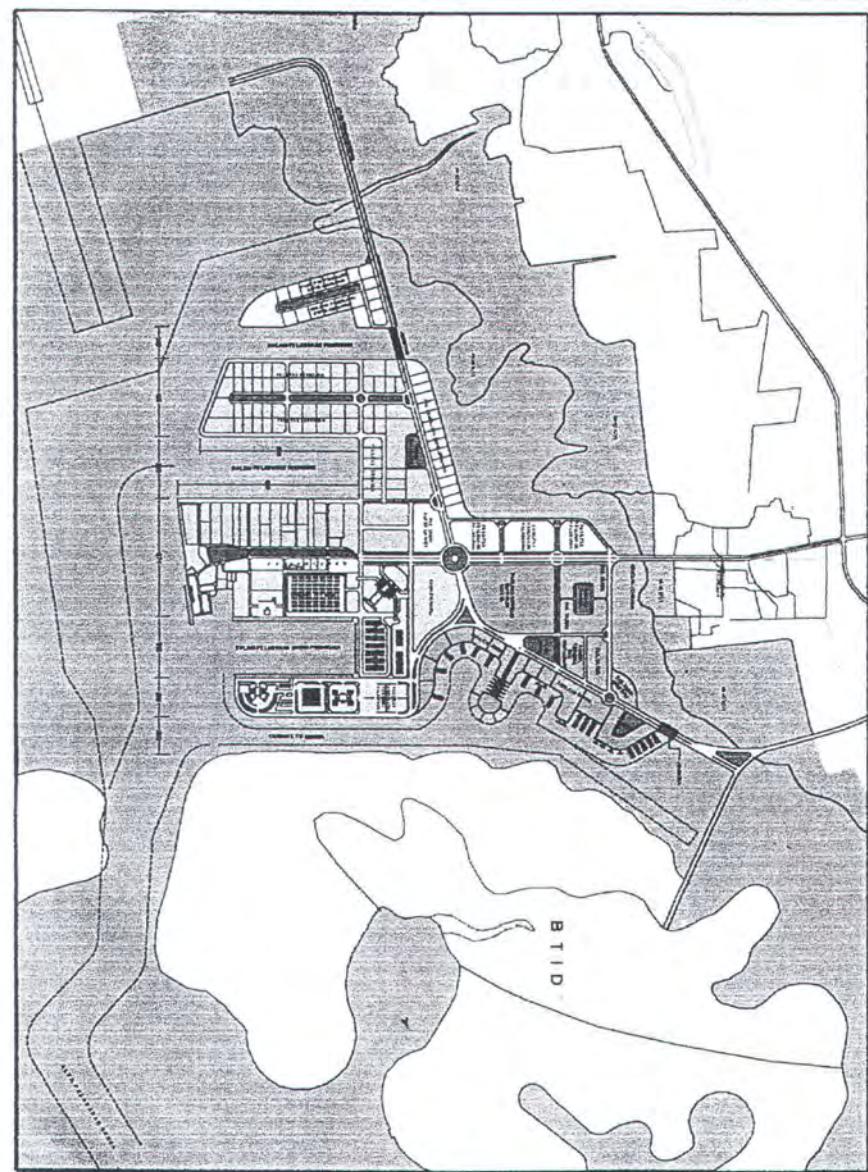
perairan terbuka. Titik penyelidikan meliputi BH.10, 17, 19, dan BH.20. Untuk jelasnya lihat lampiran (gambar perkiraan profil tanah serta tabel prosentase distribusi ukuran tanah).

V. 1. 4. Kolam Labuh

Berdasarkan masterplan Pelabuhan Benoa 2018 maka direncanakan kolam labuh pelabuhan umum dapat melayani kapal dengan ukuran panjang 300 m atau draft 10 m. Untuk merealisasikannya diperlukan perluasan kolam labuh yang semula panjang 450 m, lebar 150 m dengan kedalaman 9,0 m menjadi panjang 850 m, lebar 300 m, atau luas 25,5 Ha dengan kedalaman 11,0 m.

Perlu diadakan pemeriksaan apakah dimensi tersebut sudah sesuai. Dari hasil perhitungan dengan memakai piranti lunak **PENGERUKAN 1.0** diadapatkan kedalaman rencana 11m untuk sarat kapal maksimum 10 m. Besar pengerukan didapat 2 m. Jadi kedalaman kolam yang direncanakan sesuai dengan masterplan.

Berkaitan dengan rencana jangka panjang pengembangan Pelabuhan Benoa yang memerlukan reklamasi pantai dan dermaga (untuk perlusan dermaga), khususnya dermaga pelabuhan umum maka tanah dasar di Pelabuhan Benoa dapat dipakai sebagai material timbunan reklamasi. Dengan demikian maka lokasi buangan ditetapkan pada daerah dermaga pelabuhan umum (lihat gambar 5.1 master plan Pelabuhan Benoa).



Gambar 5.2 Master Plan Pelabuhan Benoa Bali (sumber: Pelindo, III)

V. 2. Perhitungan Sedimentasi Kolam Labuh

Data-data yang diperlukan meliputi: data tanah, angin/gelombang dan arus. Untuk data tanah dirangkumkan pada table 5.1.

Tabel 5.1. Rangkuman data tanah untuk lokasi yang ditinjau (Zona B)

| No | Kedalaman - (m LWS) | BH-13 | BH-18 | BH-13 | BH-18 | BH-13 | BH-18 |
|----|------------------------|----------------------|-------|----------------------|-------|-------|-------|
| | | D ₅₀ (mm) | | D ₉₀ (mm) | | Gs | |
| 1 | 2-3 | 1.2 | 0.7 | 15 | 4 | 2.68 | 2.72 |
| 2 | 4-5 | 1.5 | 0.9 | 10 | 10 | 2.7 | 2.71 |
| 3 | 6-7 | 0.7 | 0.65 | 9 | 11 | 2.72 | 2.69 |
| 4 | 9-10 | - | 0.18 | - | 1.2 | - | 2.64 |
| 5 | 11-12 | - | 0.18 | - | 0.6 | - | 2.77 |

Untuk data arus dapat dilihat pada table 5.2 :

Tabel 5.2 Kondisi arus pada masing-masing titik (Pelindo III, 2000)

| Titik | | Kondisi pasang | | Kondisi surut | | Kecepatan rata-rata (m/det) |
|-------|-------|----------------|----------|---------------|----------|--------------------------------|
| | | Kec.(m/det) | Arah (0) | Kec.(m/det) | Arah (0) | |
| AR1 | Maks. | 1.2 | 130 | 1.2 | 130 | 1.200 |
| | Min. | 0.4 | 40 | 0.2 | 40 | 0.300 |
| AR2 | Maks. | 0.8 | 120 | 0.2 | 130 | 0.500 |
| | Min. | 0.1 | 40 | 0.1 | 45 | 0.100 |
| AR3 | Maks. | 0.2 | 35 | 0.3 | 40 | 0.250 |
| | Min. | 0.1 | 40 | 0.1 | 60 | 0.100 |
| AR4 | Maks. | 0.4 | 40 | 0.4 | 40 | 0.400 |
| | Min. | 0.05 | 30 | 0.05 | 30 | 0.050 |
| AR5 | Maks. | 0.5 | 90 | 0.5 | 100 | 0.500 |
| | Min. | 0.1 | 70 | 0.1 | 70 | 0.100 |
| AR6 | Maks. | 0.5 | 80 | 0.6 | 90 | 0.550 |
| | Min. | 0.1 | 60 | 0.1 | 75 | 0.100 |

Dengan menggunakan piranti lunak **PENGERUKAN 1.0** maka diperoleh besarnya sedimentasi pertahun adalah 0.0624 m (untuk titik AR3) atau 6.24 cm/tahun (lihat lampiran).

Apabila toleransi sedimentasi adalah sebesar kedalaman rencana dikurangi sarat kapal terbesar (atau $11-10 = 1$ m), maka dari perhitungan tersebut diperlukan pengeringan rutin (*maintenance dredging*) dengan jangka waktu paling lambat $1:0.0624 = 16.03$ tahun atau hampir 16 tahun.

V. 3. Perhitungan Volume Pengeringan

Dari hasil perhitungan dengan menggunakan piranti lunak **PENGERUKAN 1.0** maka diperoleh luas pias (ditabelkan) adalah sebagai berikut:

Tabel 5.3 Input Luas Pias Untuk Perhitungan Volume Keruk

| Pias | Luas (m ²) |
|------|---------------------------|
| 1 | 2597.40 |
| 2 | 2600.00 |
| 3 | 2754.80 |
| 4 | 2207.40 |
| 5 | 2160.40 |
| 6 | 2011.80 |
| 7 | 1148.20 |
| 8 | 705.20 |
| 9 | 443.00 |

Dari hasil perhitungan dengan memakai piranti lunak **PENGERUKAN 1.0** dengan memakai rumus (2.5) maka diperoleh hasil perhitungan volume kerukan sebagai berikut:

Tabel 5.4 Hasil Perhitungan Volume Keruk

Jarak antar pias: 100 m

| No | Luas Pias (m ²) | Pengali (m ²) | Produk |
|---------------|--------------------------------|------------------------------|----------------|
| 1 | 2596.60 | 1 | 2596.6 |
| 2 | 2598.10 | 2 | 5196.2 |
| 3 | 2755.83 | 2 | 5511.65 |
| 4 | 2208.70 | 2 | 4417.4 |
| 5 | 2161.75 | 2 | 4323.5 |
| 6 | 1989.55 | 2 | 3979.1 |
| 7 | 1342.15 | 2 | 2684.3 |
| 8 | 654.55 | 2 | 1309.1 |
| 9 | 364.75 | 0.5 | 182.375 |
| VOLUME | | | 1510011 |

Jadi besarnya volume pengerukan = 1.510.011 m³. Sedangkan berdasarkan masterplan Pelabuhan Benoa, maka besarnya volume pengerukan diperkirakan adalah 1.633.386 m³ (berarti terdapat selisih 7.55%). Selisih ini dikarenakan untuk menghitung luas pias memakai pendekatan model Simpson II (Bab IV) sedangkan pihak Pelindo III menghitungnya secara manual dan mendetail titik-pertitik.

V. 4. ANALISA STABILITAS LERENG KOLAM LABUH

Dengan memakai piranti lunak **PENGERUKAN 1.0** maka diperoleh slope kolam labuh yang direncanakan adalah 1:4 untuk jenis material dominan sand (dengan variasi fine, medium, dan coarse sand). Hasil ini dibandingkan dengan program stable (lihat lampiran).

V. 5. ANALISA TEKNIS PEMILIHAN KAPAL KERUK

Input data kondisi untuk kolam labuh Pelabuhan Umum Benoa adalah sebagai berikut:

Tabel 5.5 Input data analisa teknis

| Parameter | Input |
|--|--|
| <i>Bed material</i> (jenis tanah): | dominan <i>coarse sand</i> ($\pm 55\%$) |
| <i>Sea condition</i> (kondisi perairan): | <i>sheltered water</i> (perairan terlindung) |
| <i>Disposal to</i> (lokasi pembuangan): | <i>shore</i> (pantai, untuk reklamasi). |
| <i>Quantities</i> (volume): | $> 500,000 \text{ m}^3$ |
| <i>Traffic</i> (kondisi lalu lintas): | <i>heavy traffic</i> (padat) |

Dengan menggunakan program **PENGERUKAN 1.0** maka nilai untuk masing-masing jenis peralatan keruk adalah sebagai berikut:

Tabel 5.6 Penilaian Peralatan Keruk (capital dredging)

| Parameter | Stan | Light | Cutter | Bucket Wheel | Grab hopper | grab pontoon | Back | Bucket | Dipper | Barge unloader |
|-------------------------|------|-------|--------|--------------|-------------|--------------|------|--------|--------|----------------|
| <i>Bed material:</i> | | | | | | | | | | |
| Coarse sand | 3 | 3 | 3 | 3 | 3 | 3 | 2 | 2 | 3 | 3 |
| <i>Sea condition</i> | | | | | | | | | | |
| Sheltered water | 3 | 3 | 3 | 2 | 2 | 3 | 3 | 2 | 2 | 1 |
| <i>Disposal to:</i> | | | | | | | | | | |
| Shore | 3 | 2 | 3 | 3 | 0 | 0 | 0 | 0 | 0 | 3 |
| <i>Quantities</i> | | | | | | | | | | |
| $> 500,000 \text{ m}^3$ | 3 | 1 | 3 | 3 | 1 | 1 | 1 | 3 | 1 | 3 |
| <i>Traffic:</i> | | | | | | | | | | |
| Heavy traffic | 3 | 3 | 3 | 2 | 2 | 1 | 2 | 1 | 2 | 2 |
| Total | 15 | 12 | 15 | 13 | 8 | 8 | 8 | 8 | 8 | 12 |

Keterangan tabel: Stan: standart trailer, Light: light trailer, Cutter: cutter suction dredger, Back: backhoe



Dari table 5.5 tersebut diambil peralatan dengan nilai yang besar, Sehingga peralatan yang memenuhi parameter tersebut di atas: *Standart trailler* dan CSD (*cutter suction dredger*). Dengan demikian peralatan keruk yang akan dipakai adalah *Standart trailler* dan CSD (*cutter suction dredger*). Pilihan ini juga memenuhi syarat batas oleh Yuwono (1992) (lihat bab 2) untuk kondisi perairan dan kolam labuh di Pelabuhan Benoa:

- Gelombang tertinggi: 0.8 m
- Gelombang rerata: 0.5 m

Sedangkan untuk syarat batas kedalaman perairan oleh Land (1997), maka untuk data Pelabuhan Umum Benoa:

- Kedalaman eksisting: 9 m
- Air terendah (LLWS): 0.4 m LWS

Peralatan keruk tipe *Standart trailler* yang dapat dipakai adalah TSHD (*trailing suction hopper dredger*) kecil hingga besar, namun demikian untuk mempercepat proyek ini dapat dipilih ukuran medium hingga besar dan CSD (*cutter suction dredger*) dengan ukuran medium hingga besar dengan diameter discharge pipe > 400 mm atau 15.75" (lihat Bab 2).

V. 6. ANALISA EKONOMI PEMILIHAN KAPAL KERUK

Data kapal keruk yang digunakan bersumber pada Rukindo (2000). Namun karena alasan rahasia perusahaan maka data tersebut hanya bersifat umum, sedangkan harga beli atau analisa ekonomi lainnya tidak diberikan. Data kapal keruk adalah sebagai berikut:

PEMBAHASAN

Tipe: CSD (*cutter suction dredger*), ukuran diameter pipa: 30 inchi, tenaga keruk/daya mesin (HP) : 3600, jumlah kru : 10 orang.

Harga alat: Rp 25.000.000.000,00 (asumsi).

Nilai sisa (5%): $5\% \times 25.000.000.000,00 = \text{Rp } 1.250.000.000,00$.

Harga BBM/liter: Rp 1000.00

Harga Oli/liter: Rp. 15,000.00

Sedangkan untuk kapal keruk tipe TSHD (*trailing suction hopper dredger*), maka data-datanya adalah sebagai berikut:

Ukuran diameter pipa: 30 inchi, tenaga keruk/daya mesin (HP) : 2×898 (1796), jumlah kru : 10 orang.

Harga alat: Rp 50.000.000.000,00 (asumsi).

Nilai sisa (5%): $5\% \times 50.000.000.000,00 = \text{Rp } 2.500.000.000,00$

Harga BBM/liter: Rp 1000.00

Harga Oli/liter: Rp. 15,000.00

Dengan menggunakan piranti lunak **PENGERUKAN 1.0** maka diperoleh besarnya biaya pengeringan sebagai berikut:

Tabel 5.7. Perhitungan ekonomi kapal keruk

a. Tipe CSD (*cutter suction dredger*)

| 1. Biaya operasi | | liter/jam | rupiah/jam |
|---|---|-----------|----------------|
| a. Bahan bakar dan pelumas | | | |
| Bahan bakar | (15% x Tenaga Keruk)l/jam | 540 | 540.000,00 |
| Pelumas | (6 x 15% x Tenaga Keruk)l/jam | 17.64 | 264.600,00 |
| b. Biaya perawatan dan perbaikan rutin | Faktor (0.000140) x harga beli (Rp/hari) | | 175,000.00 |
| c. Upah pekerja | Rata-rata Rp 6000.000,00/bulan | | 125,000.00 |
| d. asuransi | Harga x 2.5% /hari kerja per tahun (Rp/hari) | | 108,506.94 |
| 2. Biaya kepemilikan | | | |
| Penyusutan modal/tahun | | | 791,666,666.67 |
| Nilai penyusutan/jam | | | 137.442,13 |
| Kapasitas produksi | 200 m ³ /Jam | | |
| Jadi biaya pengerukan (Rp/m ³) | Total/200 | | 6752,75 |
| Biaya total | Biaya/m ³ x volume pengerukan | | 10.196.728.468 |

b. Tipe TSHD (*trailler suction hopper dredger*)

| 1. Biaya operasi | | liter/jam | rupiah/jam |
|--|---|-----------|-----------------|
| a. Bahan bakar dan pelumas | | | |
| Bahan bakar | (15% x Tenaga Keruk)l/jam | 269.4 | 269.400,00 |
| Pelumas | (6 x 0.07%* Tenaga Keruk)l/jam | 8.8 | 132.006,00 |
| b. Biaya perawatan dan perbaikan rutin | Factor (0.000135) x harga beli (Rp/hari) | | 337.500,00 |
| c. Upah pekerja | Rata-rata Rp 6000.000,00/bulan | | 125.000,00 |
| d. asuransi | Harga x 2.5% /hari kerja per tahun (Rp/hari) | | 207.013,88 |
| 2. Biaya kepemilikan | | | |
| Penyusutan modal/tahun | | | 1.583.333.333,3 |
| Nilai penyusutan/jam | | | 274.884,26 |
| Kapasitas produksi | 200 m ³ /Jam | | |
| Jadi biaya pengeringan (Rp/M ³) | Total/200 | | 5,402,75 |
| Biaya total | Biaya/m ³ x volume pengeringan | | 8.158.213.281 |

Dari perhitungan tersebut tampak bahwa biaya pengeringan antara CSD (*cutter suction dredger*) dengan TSHD (*trailler suction hopper dredger*) tidak begitu jauh berbeda. Hal ini berarti bahwa peralatan keruk yang dapat digunakan bisa keduanya. Namun demikian perlu diingat bahwa hasil perhitungan tersebut didasarkan asumsi yang diambil sebagaimana diuraikan di atas.

BAB VI

KESIMPULAN DAN SARAN

BAB VI

KESIMPULAN

VI. 1. Kesimpulan

Dari pembahasan dan analisa di muka maka dapat ditarik kesimpulan sebagai berikut:

- a. Besarnya volume pengerukan yang direncanakan adalah sebesar 1.510.011 m³. Hasil perhitungan ini berbeda dengan hasil perhitungan Pelindo III yaitu sebesar 1.633.386 m³. Selisih hitungan dengan masterplan mencapai 7.55%. Perbedaan ini timbul karena pihak Pelindo III menghitungnya secara mendetail untuk tiap titik. Kedalaman kolam yang direncanakan sudah memenuhi syarat yaitu 11m untuk sarat kapal maksimum 10 m. Kedalaman ini diperoleh dengan mengambil nilai toleransi 10% terhadap sarat kapal maksimum. Kemiringan sisi-sisi penampang direncanakan 1:4 untuk material yang didominasi oleh coarse sand (54%) dan setelah diperiksa dengan stable hasilnya memang sesuai. Kemiringan slope ini juga sesuai yang ditetapkan oleh Pelindo III.
- b. Sedimentasi kolam labuh besarnya adalah 6.624 cm/tahun yang merupakan sedimentasi di titik AR 3.
- c. Sementara kapal keruk yang memenuhi syarat teknik adalah Standart trailler dan CSD (cutter suction dredger). Dengan demikian peralatan keruk yang akan dipakai adalah TSHD dan CSD. Berdasarkan hasil perhitungan dimuka maka dapat diperoleh besarnya biaya pengerukan besarnya Rp 6752,75/m³ untuk CSD (cutter suction dredger) atau total sebesar Rp 10.196.728.468 dan untuk

KESIMPULAN

TSHD (trailing suction hopper dredger) sebesar Rp 5,402.75/m³ atau total sebesar Rp 8.158.213.281.

Dengan demikian maka kedua peralatan keruk (CSD dan TSHD) tersebut dapat digunakan semua (memenuhi persyaratan teknis dan ekonomi).

VI. 2. Saran

Piranti lunak Pengerukan 1.0 masih memiliki beberapa keterbatasan dan kelemahan, diantaranya adalah perlunya program analisa stabilitas lereng terpisah (STABLE). Untuk itu perlu adanya perbaikan atau pengembangan lebih lanjut.

Hasil perhitungan juga mungkin berbeda dengan kenyataan di lapangan mengingat beberapa asumsi atau batasan masalah yang di ambil . Disamping itu keterbatasan data yang ada (dimiliki) dapat membuat perhitungan yang dilakukan dapat kurang teliti, seperti pada perhitungan sedimentasi kolam labuh, dimana data yang dipakai sangat minim terutama data arus. Untuk hal ini perhitungan dapat diulangi dengan ketelitian lebih baik jika data yang ada mencukupi. Agar hasil perhitungan valid dan teliti maka hendaknya data yang dipakai harus lengkap dan cukup.

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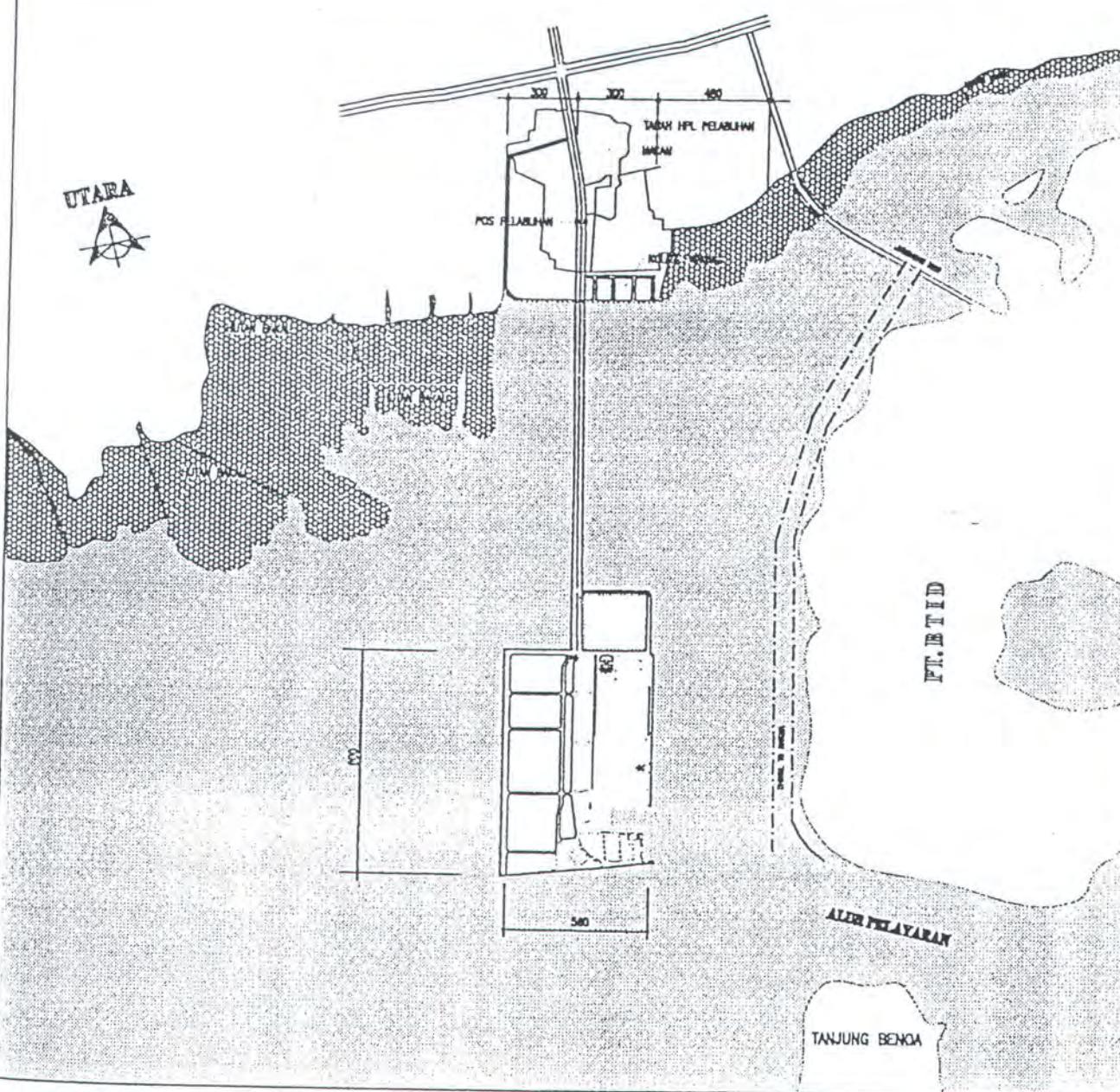
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LAMPIRAN

Multi Lasa

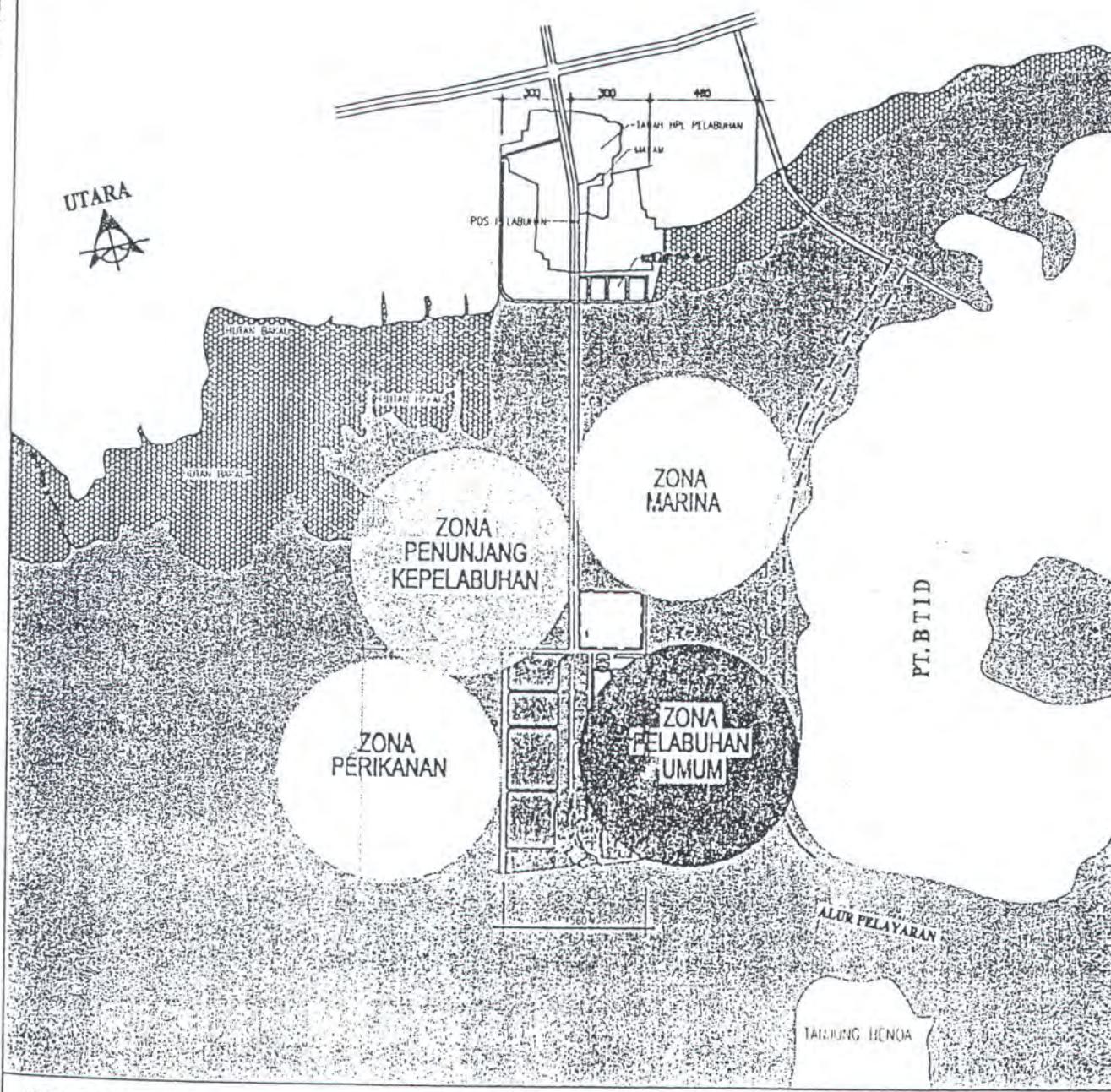
EXISTING PELABUHAN BENOA SAMPAI DENGAN TAHUN 1999



KETERANGAN

EXISTING s/d TAHUN 1999

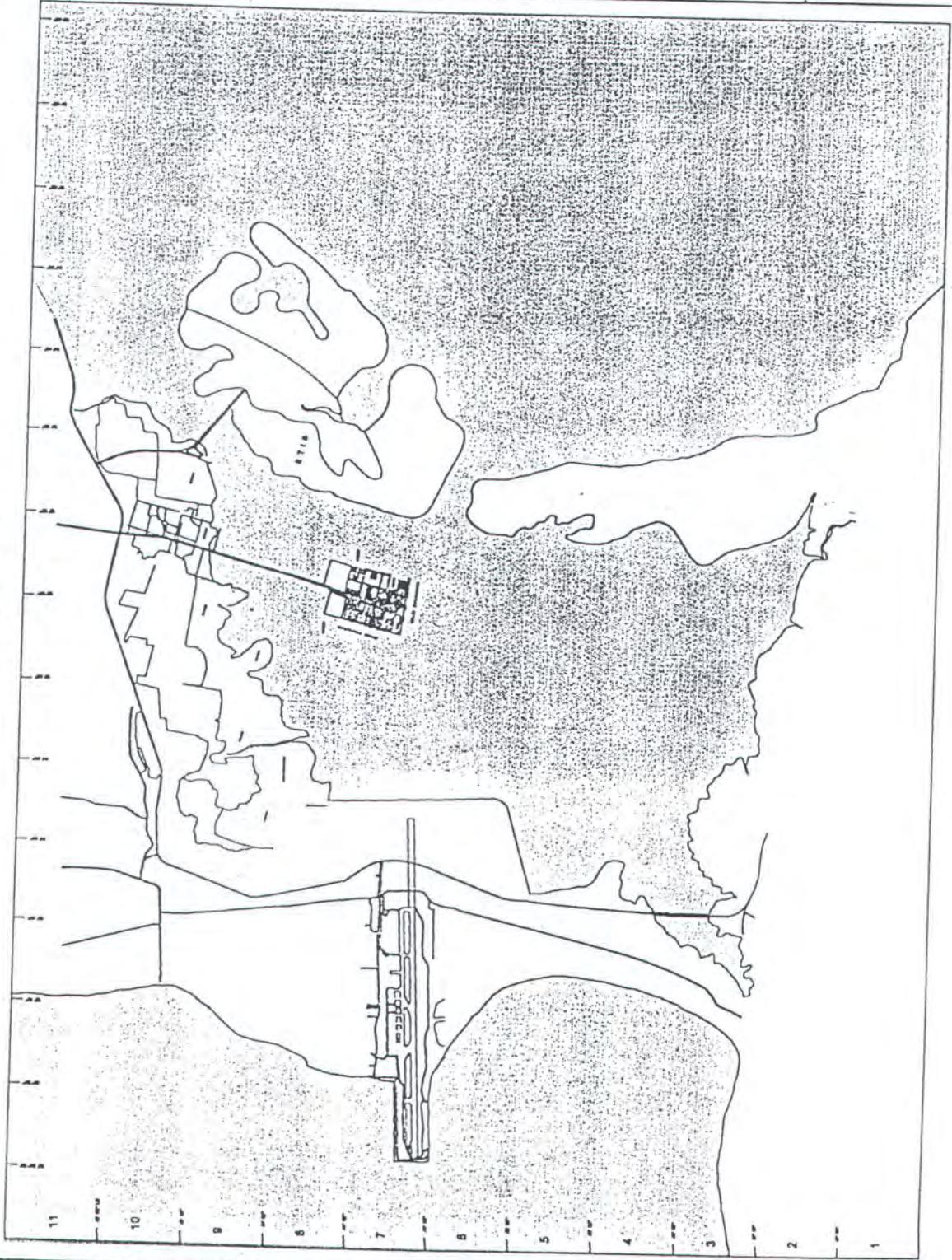
RENCANA PEMBAGIAN ZONA PELABUHAN BENOA



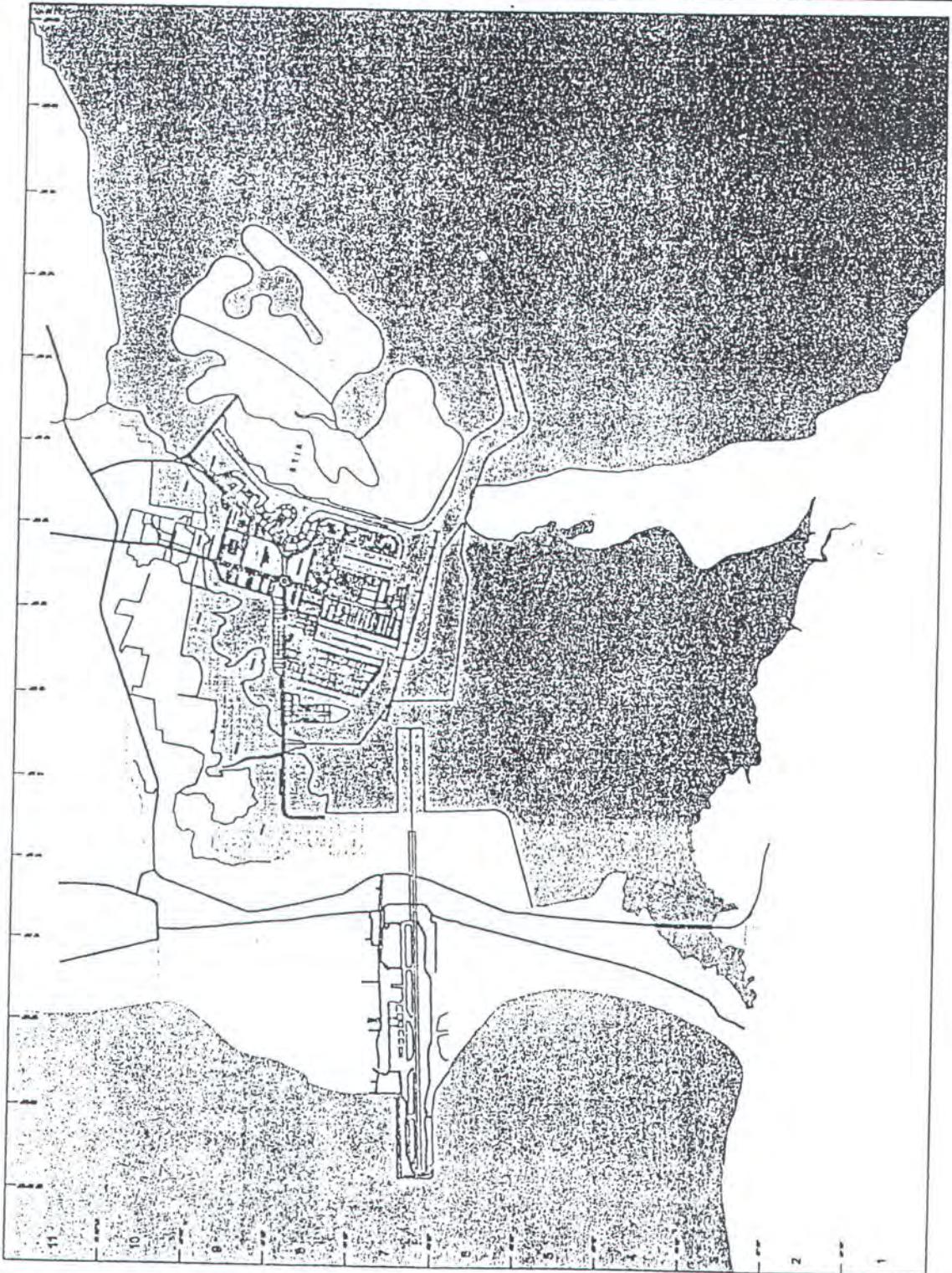
KETERANGAN

EXISTING s/d TAHUN 1999

SITUASI
TELUK BENOA - BALI
SAMPAI TAHUN 2000



SITUASI
TELUK BENOA - BALI
SAMPAI TAHUN 2018

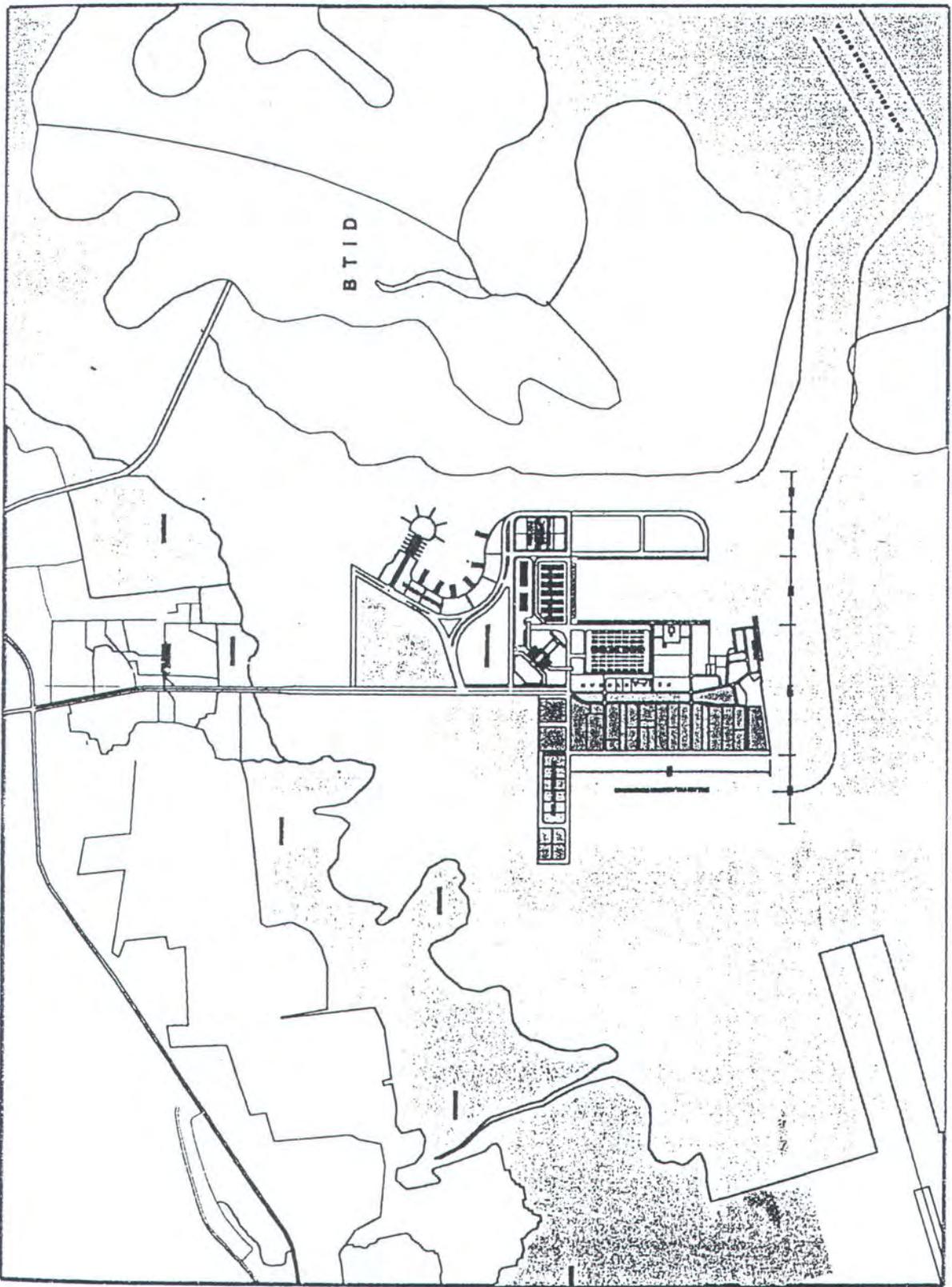


KOTA SURABAYA
ZONA PEMERINTAHAN
ZONA INDUSTRIAL
JALAN PADA
KAWASAN CILAN
KAWASAN CILUP

BUMN
BUMD
BUMR

LAPORAN
BANTUAN DILAKUKAN PADA

SAMPAI TAHUN 2003

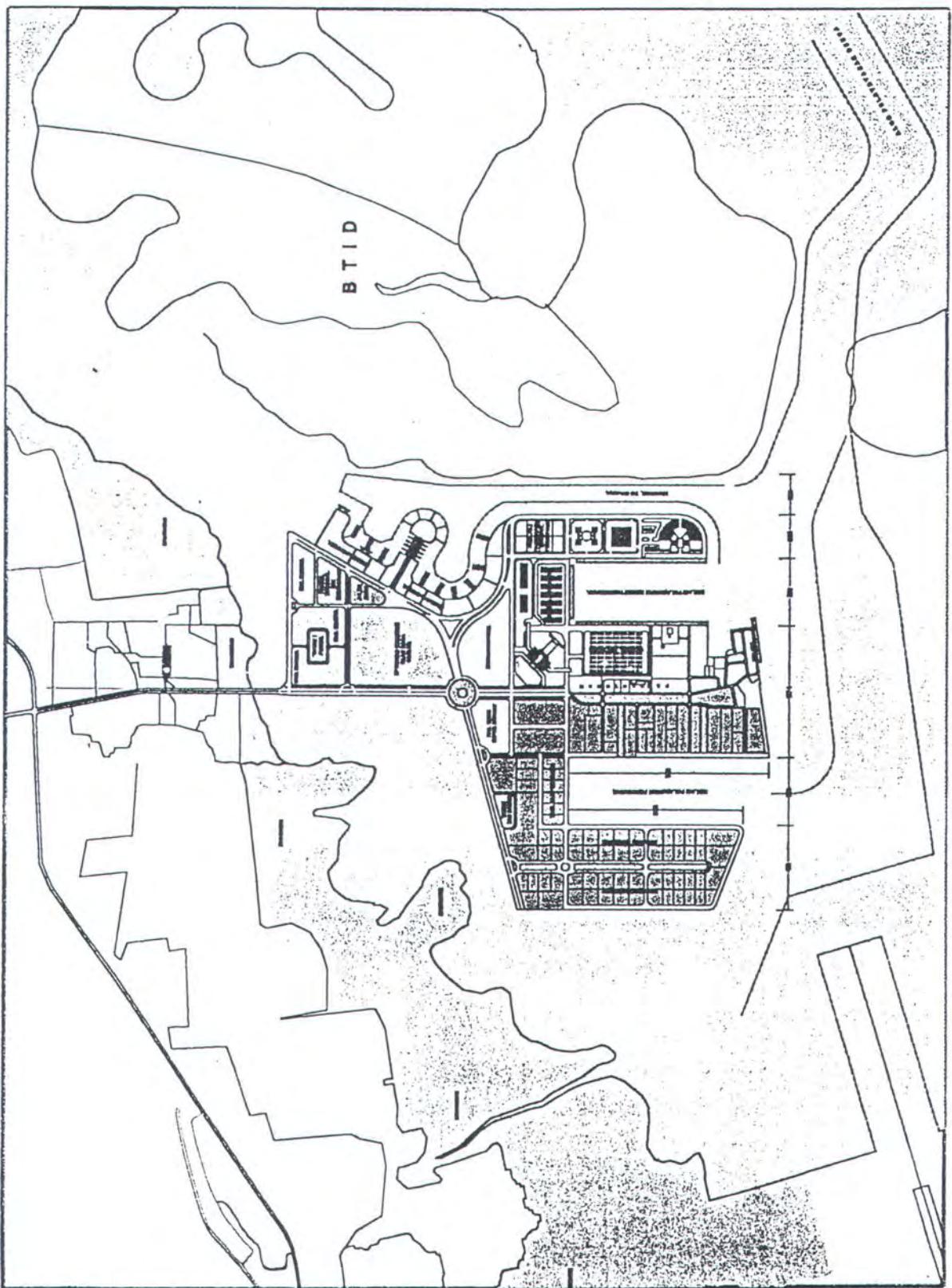




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I DONA MADE BHINNATHA

SAMPAI TAHUN 2008



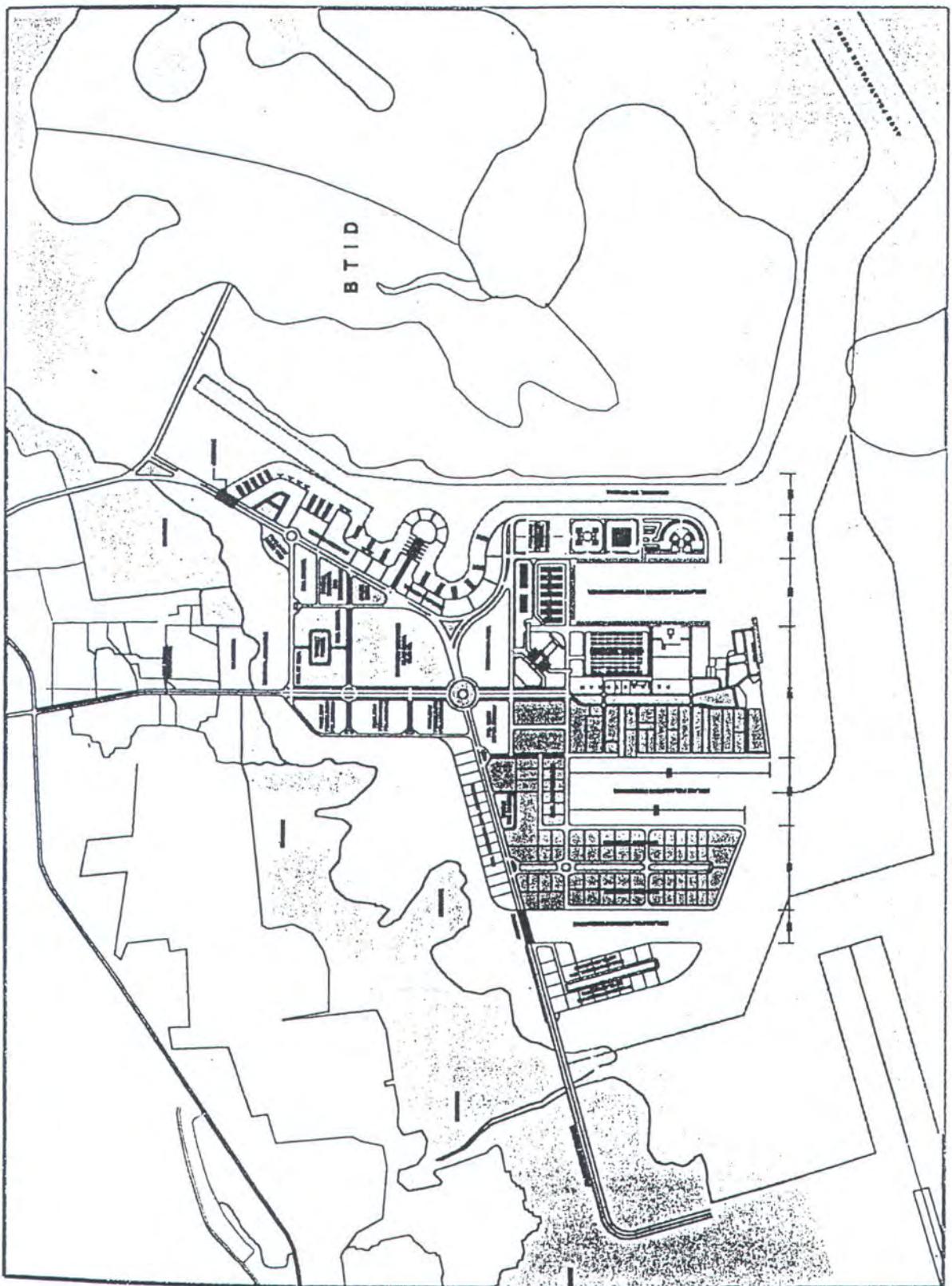
DAFTAR LAMPU DAN PAPARAN
DILAKUKAN PADA TAHUN
2010

JUMLAH
SIMPATI DLM
SIMPATI DLP

DAFTAR
JUMLAH
PAPARAN DALI

LAMPU DAN
PAPARAN DALI

SAMPAI TAHUN 2018



TABEL 4.5
Prosentase Distribusi Ukuran Butiran Tanah

| TIPIK BORING | KEDALAMAN M LWS | SILT % | SAND % | GRAVEL % | TIPIK BORING | KEDALAMAN M LWS | SILT % | SAND % | GRAVEL % |
|--------------|-------------------|--------|--------|----------|---|--------------------|--------|--------|----------|
| BH.1 | - 1.00 S/D -2.00 | 18,57 | 48,82 | 32,61 | BH.15 | - 0.50 S/D -1.50 | 8,71 | 54,65 | 36,64 |
| | - 3.00 S/D -4.00 | 15,37 | 42,64 | 41,99 | | - 2.50 S/D -3.50 | 22,4 | 47,94 | 29,66 |
| | - 5.00 S/D -6.00 | 20,38 | 49,21 | 30,41 | | - 4.50 S/D -5.50 | 12,98 | 47,41 | 39,61 |
| BH.2 | + 0.00 S/D -1.00 | 28,7 | 45,75 | 25,55 | | - 7.00 S/D -8.00 | 36,19 | 26,82 | 36,99 |
| | - 2.00 S/D -3.00 | 24,1 | 38,95 | 36,95 | | - 9,20 S/D -10.00 | 45,91 | 46,88 | 7,21 |
| | - 4.00 S/D -5.00 | 19,9 | 35,1 | 45 | | - 10,50 S/D -11,50 | 20,35 | 35,8 | 43,85 |
| BH.3 | - 1.00 S/D -2.00 | 19,45 | 53,44 | 27,11 | BH.16 | - 2.00 S/D -3.00 | 16,77 | 67,54 | 15,69 |
| | - 3.00 S/D -4.00 | 16,38 | 32,58 | 51,04 | | - 3,75 S/D -4,75 | 35,65 | 31,25 | 33,1 |
| | - 5.00 S/D -6.00 | 14,3 | 26,43 | 59,27 | | - 6,00 S/D -7,00 | 19,88 | 32,11 | 48,01 |
| BH.4 | + 0.00 S/D -1.00 | 4,24 | 93,92 | 1,84 | | - 8,00 S/D -9,00 | 18,72 | 41,14 | 40,14 |
| | - 3.00 S/D -4.00 | 17,01 | 82,38 | 0,61 | | - 10,00 S/D -11,00 | 39,46 | 52,12 | 8,42 |
| | - 5.00 S/D -5.50 | 2,33 | 95,42 | 2,25 | | - 12,00 S/D -12,75 | 38,76 | 54,07 | 7,17 |
| BH.5 | + 0.00 S/D -1.00 | 13,01 | 48,84 | 38,15 | BH.17 | - 1.00 S/D -2.00 | 2,28 | 92,13 | 5,59 |
| | - 2.00 S/D -3.00 | 7,72 | 46,5 | 45,78 | | - 3,00 S/D -4,00 | 4,41 | 86,95 | 8,64 |
| | - 5.00 S/D -6.00 | 12,61 | 52,19 | 35,2 | | - 4,20 S/D -5,00 | 19,33 | 78,54 | 2,13 |
| BH.6 | - 1,50 S/D -2,50 | 12,86 | 86,91 | 0,23 | | - 6,00 S/D -7,00 | 25,71 | 72,88 | 1,41 |
| | - 3,50 S/D -4,50 | 5,6 | 91,96 | 2,44 | | - 8,00 S/D -9,00 | 25,99 | 64,55 | 9,46 |
| | - 5,50 S/D -6,50 | 3,08 | 93,99 | 2,93 | | - 10,50 S/D -11,00 | 35,22 | 62,27 | 2,51 |
| BH.7 | - 1.00 S/D -2.00 | 2,61 | 97,19 | 0,2 | BH.18 | - 2,00 S/D -3,00 | 72,46 | 72,33 | 15,21 |
| | - 3.00 S/D -4.00 | 4,21 | 95,73 | 0,06 | | - 4,00 S/D -5,00 | 8,41 | 61,29 | 30,3 |
| | - 5.00 S/D -6.00 | 2,98 | 96,86 | 0,16 | | - 6,00 S/D -7,00 | 17,86 | 47,08 | 35,06 |
| BH.8 | + 0.00 S/D -0,50 | 15,74 | 41,41 | 42,85 | | - 9,00 S/D -10,00 | 23,55 | 70,99 | 5,46 |
| | - 1.00 S/D -2.00 | 14,83 | 35,67 | 49,5 | | - 11,00 S/D -12,00 | 27,58 | 69,71 | 2,71 |
| | - 4.00 S/D -5.00 | 1,37 | 42,01 | 44,32 | | - 2,00 S/D -3,00 | 0,13 | 94,97 | 4,2 |
| BH.9 | + 0.00 S/D -1.00 | 18,29 | 41,73 | 39,98 | BH.19 | - 4,00 S/D -5,00 | 8,29 | 88,43 | 3,28 |
| | - 3.00 S/D -4.00 | 19,43 | 36,78 | 43,79 | | - 6,00 S/D -7,00 | 29,38 | 69,5 | 1,12 |
| | - 5.00 S/D -6.00 | 25,87 | 29,3 | 44,83 | | - 8,00 S/D -9,00 | 19,12 | 68,57 | 12,31 |
| BH.10 | - 2.00 S/D -3.00 | 19,79 | 34,81 | 45,4 | | - 10,00 S/D -10,50 | 21,86 | 67,44 | 10,7 |
| | - 3.00 S/D -4.00 | 22,77 | 39,49 | 37,74 | | - 11,00 S/D -12,00 | 15,12 | 76,59 | 8,29 |
| | - 5.00 S/D -6.00 | 20,58 | 27,6 | 51,82 | BH.20 | + 0,00 S/D -1,00 | 9,25 | 72,12 | 18,63 |
| BH.11 | - 2,00 S/D -3,00 | 12,69 | 38,14 | 49,17 | | - 2,00 S/D -3,00 | 15,95 | 75,71 | 8,34 |
| | - 4,00 S/D -5,00 | 25,31 | 32,17 | 42,52 | | - 5,00 S/D -5,70 | 5,87 | 67,41 | 26,72 |
| | - 6,00 S/D -7,00 | 32,68 | 32,98 | 34,34 | | - 6,00 S/D -7,00 | 14,6 | 38,31 | 47,09 |
| BH.12 | + 1,00 S/D ± 0,00 | 12,07 | 40,28 | 47,65 | | - 8,00 S/D -9,00 | 14,15 | 35,87 | 49,98 |
| | - 2,00 S/D -3,00 | 14,95 | 36,2 | 48,85 | | - 10,00 S/D -11,00 | 13,13 | 38,31 | 48,56 |
| | - 4,00 S/D -5,00 | 24,85 | 41,32 | 33,83 | BH.21 | - 0,00 S/D -1,00 | 14,54 | 23,52 | 61,94 |
| | - 6,00 S/D -7,00 | 18,23 | 47,77 | 34 | | - 2,00 S/D -3,00 | 12,27 | 44,25 | 43,48 |
| | - 8,00 S/D -9,00 | 17,11 | 53,14 | 29,75 | | - 4,00 S/D -5,00 | 12,83 | 39,07 | 48,1 |
| BH.13 | - 2,00 S/D -3,00 | 25,01 | 35,53 | 39,46 | | - 6,00 S/D -7,00 | 14,55 | 52,57 | 32,88 |
| | - 4,00 S/D -5,00 | 18,61 | 39,9 | 41,49 | | - 8,00 S/D -9,00 | 16,33 | 64,40 | 19,27 |
| | - 6,00 S/D -7,00 | 25,33 | 40,51 | 34,16 | Sumber: Analisis Konsultasi | | | | |
| BH.14 | - 0,00 S/D -1,00 | 13,52 | 39,94 | 46,54 | KESIMPULAN : SILT (%) SAND (%) GRAVEL (%) | | | | |
| | - 2,00 S/D -3,00 | 19,15 | 33,84 | 47,01 | ZONA A : | 13,82 | 58,58 | 27,59 | |
| | - 4,00 S/D -5,00 | 33,26 | 36,32 | 30,42 | ZONA B : | 19,85 | 54,67 | 25,48 | |
| | - 6,00 S/D -7,00 | 47,87 | 21,52 | 30,61 | ZONA C : | 23,73 | 40,77 | 35,50 | |
| | - 8,20 S/D -9,00 | 46,38 | 31,57 | 22,05 | ZONA D : | 16,33 | 64,40 | 19,27 | |

BORING LOG

BOREHOLE #: BH - 1

PROJECT : Pengembangan Pelabuhan Benoa Bali

COORDINATE

: 304,792.531 ; 9,035,000.068

LOCATION : Pelabuhan Benoa, Bali

ELEVATION OF SEA BED

: ± 0.00 m

| Elevation LWS, m | SOIL DESCRIPTION | STANDARD PENETRATION TEST | | | | | SOIL COMPOSITION (%) | | | | ATTERBERG LIMITS | | | | | Gs | USCS |
|---------------------|---|------------------------------|----|----|----|----|----------------------|------|------|------|---------------------|----|----|----|----|----|------|
| | | 0 | 10 | 20 | 30 | 40 | Coral/U Shells | Sand | Silt | Clay | 0 | 20 | 40 | 60 | 80 | | |
| +1 | | | | | | | | | | | | | | | | | |
| ±0 | | | | | | | | | | | | | | | | | |
| -1 | | | | | | | | | | | | | | | | | |
| -2 | □ | | | | | | | | | | | | | | | | |
| -3 | Sand, grey, some lo and coral/shells, little silt, trace clay, very loose to loose. | | | | | | | | | | | | | | | | |
| -4 | □ | | | | | | | | | | | | | | | | |
| -5 | | | | | | | | | | | | | | | | | |
| -6 | □ | | | | | | | | | | | | | | | | |
| -6.5 | End of boring. | | | | | | | | | | | | | | | | |
| -7 | | | | | | | | | | | | | | | | | |
| -8 | | | | | | | | | | | | | | | | | |
| -9 | | | | | | | | | | | | | | | | | |
| -10 | | | | | | | | | | | | | | | | | |
| -11 | | | | | | | | | | | | | | | | | |
| -12 | | | | | | | | | | | | | | | | | |
| -13 | | | | | | | | | | | | | | | | | |

NOTE : 0 to 10 % = Trace

10 to 20 % = Little

20 to 35 % = Some

35 to 50 % = And

□ = SPT

SPT = Standard penetration test (blows / 1)

● = Wp = Plastic limit, %

△ = WL = Liquid limit, %

Gs = Specific Gravity

USCS = Unified Soil Classification System

BORING LOG

BOREHOLE #: BH - 2

PROJECT : Pengembangan Pelabuhan Benoa Bali

LOCATION : Pelabuhan Benoa, Bali

COORDINATE : 304,365.322 ; 9,034,650.043.

ELEVATION OF SEA BED : ± 0.00 m

| Elevation LWS, m | SOIL DESCRIPTION | STANDARD PENETRATION TEST | | | | | SOIL COMPOSITION (%) | | | | ATTERBERG LIMITS | | | | | Gs | USCS |
|---------------------|--|------------------------------|----|----|----|----|----------------------|-------|-------|-------|---------------------|----|----|----|----|------|-------|
| | | 0 | 10 | 20 | 30 | 40 | Coral Shells | Sand | Silt | Clay | 0 | 20 | 40 | 60 | 80 | | |
| +1 | | | | | | | ≥50 | | | | | | | | | | |
| ±0 | | | | | | | | | | | | | | | | | |
| -1 | Sand, brown, some clay, little coral/shells, trace silt. | | | | | | | 18.11 | 53.19 | 5.94 | 22.76 | 23 | 30 | 0 | 1 | 2.70 | SC-SM |
| -2 | Sand, brownish grey, some coral/shells, little silt, trace clay, very loose. | 3 | | | | | | 27.86 | 48.04 | 16.05 | 8.05 | 26 | 34 | 0 | 1 | 2.75 | SM |
| -3 | Sand, brown, some coral/shells, trace silt. | 4 | | | | | | 36.06 | 44.04 | 11.30 | 8.60 | 26 | 34 | 0 | 1 | 2.75 | SM |
| -4 | Sand and coral/shells, grey, little silt, trace clay, loose. | 5 | | | | | | | | | | | | | | | |
| -5 | | | | | | | | | | | | | | | | | |
| -6 | | | | | | | | | | | | | | | | | |
| -7 | | | | | | | | | | | | | | | | | |
| -8 | End of boring. | | | | | | | | | | | | | | | | |
| -9 | | | | | | | | | | | | | | | | | |
| -10 | | | | | | | | | | | | | | | | | |
| -11 | | | | | | | | | | | | | | | | | |
| -12 | | | | | | | | | | | | | | | | | |
| -13 | | | | | | | | | | | | | | | | | |

NOTE : 0 to 10 % = Trace

10 to 20 % = Little

20 to 35 % = Some

35 to 50 % = And

 = SPT

SPT = Standard penetration test (blows / ft)

◆ = Wp = Plastic limit, %

△ = WL = Liquid limit, %

Gs = Specific Gravity

USCS = Unified Soil Classification System

BORING LOG

BOREHOLE #: BH - 3

PROJECT : Pengembangan Pelabuhan Benoa Bali

LOCATION: Pelabuhan Benoa, Bali

· COORDINATE : 304,270.239 ; 9,034,315.115.

ELEVATION OF SEA BED

: 304,270.239 ; 9,034,315.115.

: ± 0.00 m

NOTE : 0 to 10 % = Trace
 10 to 20 % = Little
 20 to 35 % = Some
 35 to 50 % = A lot

 = SPT

SPT = Standard penetration test (blows / ft)

* = Wp = Plastic limit, %

Δ = WI = Liquid limit, %

Gs = Specific Gravity

USCS = Unified Soil Classification System

BORING LOG

BOREHOLE #: BH - 4

PROJECT : Pengembangan Pelabuhan Benoa Bali

LOCATION : Pelabuhan Benoa, Bali

COORDINATE

: 304.000.088 ; 9.034.315.435.

ELEVATION OF SEA BED

: -0.550 m LWS

| Elevation LWS, m | SOIL DESCRIPTION | STANDARD PENETRATION TEST | | | | | SOIL COMPOSITION (%) | | | | ATTERBERG LIMITS | | | | | Gs | USCS | |
|---------------------|--|------------------------------|----|----|----|----|----------------------|------|------|------|---------------------|----|-----|-----|-----|-----|------|----|
| | | 0 | 10 | 20 | 30 | 40 | Coral Shells | Sand | Silt | Clay | 0 | 10 | 40 | 60 | 30 | | | |
| | | +1 | ±0 | -1 | -2 | -3 | -4 | -5 | -6 | -7 | -8 | -9 | -10 | -11 | -12 | -13 | | |
| | | | | | | | | | | | | | | | | | | |
| +1 | | | | | | | | | | | | | | | | | | |
| ±0 | | | | | | | | | | | | | | | | | | |
| -1 | Sand, greyish brown, trace silt, contains shells. | | | | | | | | | | | | | | | | 2.69 | SP |
| -2 | | | | | | | | | | | | | | | | | | |
| -3 | Sand, greyish brown, little silt, trace clay, contains shells, very loose. | 1/45 | | | | | | | | | | | | | | | 2.67 | SM |
| -4 | | 1/45 | | | | | | | | | | | | | | | | |
| -5 | Sand, grey, trace silt, trace shells, very loose. | 1/45 | | | | | | | | | | | | | | | 2.75 | SP |
| -6 | | 1/45 | | | | | | | | | | | | | | | | |
| -7 | End of boring. | | | | | | | | | | | | | | | | | |
| -8 | | | | | | | | | | | | | | | | | | |
| -9 | | | | | | | | | | | | | | | | | | |
| -10 | | | | | | | | | | | | | | | | | | |
| -11 | | | | | | | | | | | | | | | | | | |
| -12 | | | | | | | | | | | | | | | | | | |
| -13 | | | | | | | | | | | | | | | | | | |

NOTE :
 0 to 10 % = Trace
 10 to 20 % = Little
 20 to 35 % = Some
 35 to 50 % = And

= SPT
 SPT = Standard penetration test (blows / it)

● = Wp = Plastic limit, %
 △ = WL = Liquid limit, %
 Gs = Specific Gravity
 USCS = Unified Soil Classification System

BORING LOG

BOREHOLE #: BH - 5

PROJECT : Pengembangan Pelabuhan Benoa Bali

LOCATION : Pelabuhan Benoa, Bali

COORDINATE : 304,110.151 ; 9,034,087.543.

ELEVATION OF SEA BED : ± 0.00 m

| Elevation LW.S, m | SOIL DESCRIPTION | STANDARD PENETRATION TEST | | | | | SOIL COMPOSITION (%) | | | | ATTERBERG LIMITS | | | | | Gs | USCS |
|----------------------|--|------------------------------|----|----|----|----|----------------------|------|----|------|---------------------|-------|-------|------|----|------|-------|
| | | 0 | 10 | 20 | 30 | 40 | Coral Shells | Sand | SM | Clay | 0 | 20 | 40 | 60 | 30 | | |
| +1 | | | | | | | | | | | | | | | | | |
| ±0 | | | | | | | | | | | | | | | | | |
| -1 | | | | | | | | | | | | | | | | | |
| -2 | Sand, grey, some lo and coral/shells, trace to little silt, trace clay, loose. | | 5 | | | | | | | | 27.99 | 59.00 | 4.15 | 8.86 | | 2.65 | SC |
| -3 | | | 6 | | | | | | | | 38.83 | 53.45 | 4.04 | 3.63 | | 2.70 | SP-SM |
| -4 | | | 8 | | | | | | | | 28.32 | 59.07 | 10.34 | 2.27 | | 2.68 | SM |
| -5 | End of boring. | | | | | | | | | | | | | | | | |
| -6 | | | | | | | | | | | | | | | | | |
| -7 | | | | | | | | | | | | | | | | | |
| -8 | | | | | | | | | | | | | | | | | |
| -9 | | | | | | | | | | | | | | | | | |
| -10 | | | | | | | | | | | | | | | | | |
| -11 | | | | | | | | | | | | | | | | | |
| -12 | | | | | | | | | | | | | | | | | |
| -13 | | | | | | | | | | | | | | | | | |

NOTE : 0 to 10 % = Trace
10 to 20 % = Little
20 to 35 % = Some
35 to 50 % = A.l.d

= SPT

SPT = Standard penetration test (blows / ft)

● = Wp = Plastic limit, %

△ = WL = Liquid limit, %

Gs = Specific Gravity

USCS = Unified Soil Classification System

BORING LOG

BOREHOLE #: BH - 6

PROJECT : Pengembangan Pelabuhan Benoa Bali

LOCATION : Pelabuhan Benoa, Bali

COORDINATE : 303,702.531 ; 9,034,045.266

ELEVATION OF SEA BED : -0.65 m LWS

| Elevation LWS, m | SOIL DESCRIPTION | STANDARD PENETRATION TEST | | | | | SOIL COMPOSITION (%) | | | | ATTERBERG LIMITS | | | | | Gs | USCS | |
|---------------------|--|------------------------------|------|----|----|----|----------------------|------|-------|-------|---------------------|----|----|----|----|----|------|----|
| | | 0 | 10 | 20 | 30 | 40 | Coral Shells | Sand | SM | Clay | 0 | 20 | 40 | 60 | 80 | | | |
| | | | | | | | | | | | | | | | | | | |
| +1 | | | | | | | | | | | | | | | | | | |
| ±0 | | | | | | | | | | | | | | | | | | |
| -1 | | | | | | | | | | | | | | | | | | |
| -2 | <input checked="" type="checkbox"/> Sand, greyish brown, little silt, trace clay, contains shells, very loose. | | 1/45 | | | | | 0 | 87.14 | 10.91 | 1.95 | | | | | | 2.63 | SM |
| -3 | | | | | | | | 0.35 | 94.05 | 5.60 | - | | | | | | 2.66 | SP |
| -4 | | | 5 | | | | | 1.01 | 95.91 | 3.08 | - | | | | | | 2.60 | SP |
| -5 | | | 7 | | | | | | | | | | | | | | | |
| -6 | | | | | | | | | | | | | | | | | | |
| -7 | End of boring. | | | | | | | | | | | | | | | | | |
| -8 | | | | | | | | | | | | | | | | | | |
| -9 | | | | | | | | | | | | | | | | | | |
| -10 | | | | | | | | | | | | | | | | | | |
| -11 | | | | | | | | | | | | | | | | | | |
| -12 | | | | | | | | | | | | | | | | | | |
| -13 | | | | | | | | | | | | | | | | | | |

NOTE : 0 to 10 % = Trace
10 to 20 % = Little
20 to 35 % = Some
35 to 50 % = And

= SPT

SPT = Standard penetration test (blows / ft)

♦ = Wp = Plastic limit, %

Δ = WL = Liquid limit, %

Gs = Specific Gravity

USCS = Unified Soil Classification System

BORING LOG

BOREHOLE #: BH - 7

PROJECT : Pengembangan Pelabuhan Benoa Bali
LOCATION : Pelabuhan Benoa, Bali

COORDINATE : 303,950.063 ; 9,033,859.972
ELEVATION OF SEA BED : +0.20 m

| Elevation L.W.S, m | SOIL DESCRIPTION | STANDARD PENETRATION TEST | | | | | SOIL COMPOSITION (%) | | | | ATTERBERG LIMITS | | | | | Gs | USCS |
|-----------------------|--|------------------------------|----|----|----|----|----------------------|------|------|------|---------------------|----|----|----|----|-----|---------|
| | | 0 | 10 | 20 | 30 | 40 | Coral Shells | Sand | Silt | Clay | 0 | 20 | 40 | 60 | 30 | 100 | |
| +1 | | | | | | | | | | | | | | | | | |
| ±0 | | | | | | | | | | | | | | | | | |
| -1 | | | | | | | | | | | | | | | | | |
| -2 | <input checked="" type="checkbox"/> | | | | | | | | | | | | | | | | 2.62 SP |
| -3 | Sand, grey, trace silt, contains shells, very loose. | | | | | | | | | | | | | | | | |
| -4 | <input checked="" type="checkbox"/> | | | | | | | | | | | | | | | | 2.75 SP |
| -5 | | | | | | | | | | | | | | | | | |
| -6 | <input checked="" type="checkbox"/> | | | | | | | | | | | | | | | | 2.66 SP |
| -6.0 | End of boring. | | | | | | | | | | | | | | | | |
| -7 | | | | | | | | | | | | | | | | | |
| -8 | | | | | | | | | | | | | | | | | |
| -9 | | | | | | | | | | | | | | | | | |
| -10 | | | | | | | | | | | | | | | | | |
| -11 | | | | | | | | | | | | | | | | | |
| -12 | | | | | | | | | | | | | | | | | |
| -13 | | | | | | | | | | | | | | | | | |

NOTE : 0 to 10 % = Trace
10 to 20 % = Little
20 to 35 % = Some
+ > 35 % = A lot

= SPT
SPT = Standard penetration test (blows / ft)

● = Wp = Plastic limit, %
△ = WL = Liquid limit, %
Gs = Specific Gravity
USCS = Unified Soil Classification System

BORING LOG

BOREHOLE #: BH - 8

PROJECT : Pengembangan Pelabuhan Benoa Bali

COORDINATE : 303,912.516 ; 9,033,859.972

LOCATION : Pelabuhan Benoa, Bali

ELEVATION OF SEA BED : + 0.25 m

| Elevation LWS, m | SOIL DESCRIPTION | STANDARD PENETRATION TEST | | | | | SOIL COMPOSITION (%) | | | | ATTERBERG LIMITS | | | | | Gs | USCS |
|---------------------|--|------------------------------|----|----|----|----|----------------------|------|------|------|---------------------|-------|-------|------|----|------|------|
| | | | | | | | Coral/ Shells | Sand | Silt | Clay | 0 | 20 | 40 | 60 | 80 | | |
| | | 0 | 10 | 20 | 30 | 40 | | | | | | | | | | | |
| +1 | | | | | | | | | | | | | | | | | |
| ±0 | Sand, brown, some coral/shells, little silt, trace clay. | | | | | | | | | | 34.28 | 49.98 | 12.72 | 3.02 | | 2.76 | SM |
| -1 | | | | | | | | | | | 38.03 | 47.14 | 12.34 | 2.49 | | 2.74 | SM |
| -2 | Sand, grey, some lo and coral/shells, trace to little silt, trace clay, loose. | | | | | | | | | | 32.71 | 51.62 | 8.51 | 5.16 | | 2.69 | SM |
| -3 | | | | | | | | | | | | | | | | | |
| -4 | | | | | | | | | | | | | | | | | |
| -5 | Coral, very fine. | | | | | | | | | | | | | | | | |
| -6 | Sand, grey, some coral/shells, trace silt, trace clay, medium. | | | | | | | | | | | | | | | | |
| -7 | End of boring. | | | | | | | | | | | | | | | | |
| -8 | | | | | | | | | | | | | | | | | |
| -9 | | | | | | | | | | | | | | | | | |
| -10 | | | | | | | | | | | | | | | | | |
| -11 | | | | | | | | | | | | | | | | | |
| -12 | | | | | | | | | | | | | | | | | |
| -13 | | | | | | | | | | | | | | | | | |

NOTE :
 0 to 10 % = Trace
 10 to 20 % = Little
 20 to 35 % = Some
 35 to 50 % = And

= SPT

SPT = Standard penetration test (blows / ft)

♦ = W_P = Plastic limit, %

△ = W_L = Liquid limit, %

Gs = Specific Gravity

USCS = Unified Soil Classification System

BORING LOG

BOREHOLE #: BH - 9

PROJECT : Pengembangan Pelabuhan Benoa Bali

COORDINATE : 303,815.009 ; 9,033,067.452

LOCATION : Pelabuhan Benoa, Bali

ELEVATION OF SEA BED : + 0.20 m

| Elevation LWS, m | SOIL DESCRIPTION | STANDARD PENETRATION TEST | | | | | SOIL COMPOSITION (%) | | | | ATTERBERG LIMITS | | | | | Gs | USCS |
|---------------------|---|------------------------------|----|----|----|----|----------------------|------|------|------|---------------------|----|----|----|----|-----|------|
| | | 0 | 10 | 20 | 30 | 40 | Corall/ Shells | Sand | Silt | Clay | 0 | 20 | 40 | 60 | 80 | 100 | |
| +1 | | | | | | | | | | | | | | | | | |
| ±0 | Sand, brown, some coral/shells, little silt, trace clay. | | | | | | | | | | | | | | | | |
| -1 | | | | | | | | | | | | | | | | | |
| -2 | | | | | | | | | | | | | | | | | |
| -3 | | | | | | | | | | | | | | | | | |
| -4 | Sand, grey, some coral/shells, little silt, trace clay, loose to medium | | | | | | | | | | | | | | | | |
| -5 | | | | | | | | | | | | | | | | | |
| -6 | End of boring | | | | | | | | | | | | | | | | |
| -7 | | | | | | | | | | | | | | | | | |
| -8 | | | | | | | | | | | | | | | | | |
| -9 | | | | | | | | | | | | | | | | | |
| -10 | | | | | | | | | | | | | | | | | |
| -11 | | | | | | | | | | | | | | | | | |
| -12 | | | | | | | | | | | | | | | | | |
| -13 | | | | | | | | | | | | | | | | | |

NOTE :
 0 to 10 % = Trace
 10 to 20 % = Little
 20 to 35 % = Some
 35 to 50 % = And

= SPT
 SPT = Standard penetration test (blows / ft)

* = W_p = Plastic limit, %
 Δ = W_L = Liquid limit, %
 Gs = Specific Gravity
 USCS = Unified Soil Classification System

250
 31.46 50.25 13.04 5.25
 27 33

32.67 47.90 14.27 5.16
 25 31

24.67 49.46 18.95 6.92
 27 31

2.72 SM

2.75 SM

2.70 SM

BORING LOG

BOREHOLE #: BH - 10

PROJECT : Pengembangan Pelabuhan Benoa Bali

COORDINATE : 303,751.780 ; 9,032,731.038

LOCATION : Pelabuhan Benoa, Bali

ELEVATION OF SEA BED : -0.90 m LWS

| Elevation LWS, m | SOIL DESCRIPTION | STANDARD PENETRATION TEST | | | | | SOIL COMPOSITION (%) | | | | ATTERBERG LIMITS | | | | | Gs | USCS |
|---------------------|--|------------------------------|----|----|----|----|----------------------|------|------|------|---------------------|----|-----|-----|-----|-----|------|
| | | 0 | 10 | 20 | 30 | 40 | Coral & Shells | Sand | Silt | Clay | 0 | 20 | 40 | 60 | 80 | | |
| | | +1 | ±0 | -1 | -2 | -3 | -4 | -5 | -6 | -7 | -8 | -9 | -10 | -11 | -12 | -13 | |
| | | | | | | | | | | | | | | | | | |
| +1 | | | | | | | | | | | | | | | | | |
| ±0 | | | | | | | | | | | | | | | | | |
| -1 | Sand, brown, some coral/shells, trace silt, trace clay. | | | | | | | | | | | | | | | | |
| -2 | | | | | | | | | | | | | | | | | |
| -3 | Sand, grey, some coral/shells, little silt, trace clay, loose. | | | | | | | | | | | | | | | | |
| -4 | | | | | | | | | | | | | | | | | |
| -5 | | | | | | | | | | | | | | | | | |
| -6 | O.C Coral and sand, grey, little silt, trace clay, medium. | | | | | | | | | | | | | | | | |
| -7 | END | | | | | | | | | | | | | | | | |
| -8 | | | | | | | | | | | | | | | | | |
| -9 | | | | | | | | | | | | | | | | | |
| -10 | | | | | | | | | | | | | | | | | |
| -11 | | | | | | | | | | | | | | | | | |
| -12 | | | | | | | | | | | | | | | | | |
| -13 | | | | | | | | | | | | | | | | | |

NOTE :
 0 to 10 % = Trace
 10 to 20 % = Little
 20 to 35 % = Some
 35 to 50 % = And

□ = SPT
 SPT = Standard penetration test (blows / ft)

♦ = Wp = Plastic limit, %
 △ = Wl = Liquid limit, %
 Gs = Specific Gravity
 USCS = Unified Soil Classification System

BORING LOG

BOREHOLE #: BH - 11

PROJECT : Pengembangan Pelabuhan Benoa Bali

LOCATION : Pelabuhan Benoa, Bali

COORDINATE

: 301,950.216 ; 9,033,597.532

ELEVATION OF SEA BED

: -0.90 m LWS

| Elevation LWS, m | SOIL DESCRIPTION | STANDARD PENETRATION TEST | | | | | SOIL COMPOSITION (%) | | | | ATTERBERG LIMITS | | | | | Gs | USCS | |
|---------------------|---|------------------------------|----|----|----|----|----------------------|------|------|------|---------------------|----|----|----|----|-----|------|----|
| | | 0 | 10 | 20 | 30 | 40 | Coral Shells | Sand | Silt | Clay | 0 | 20 | 40 | 60 | 80 | 100 | | |
| +1 | | | | | | | | | | | | | | | | | | |
| ±0 | | | | | | | | | | | | | | | | | | |
| -1 | | | | | | | | | | | | | | | | | | |
| -2 | Sand and coral/shells, brown, trace silt, trace clay, loose. | | | | | | | | | | | | | | | | 2.72 | SM |
| -3 | | 6 | | | | | | | | | | | | | | | | |
| -4 | | 7 | | | | | | | | | | | | | | | 2.69 | SC |
| -5 | Sand, grey, some coral/shells, trace to little silt, little clay, loose | | | | | | | | | | | | | | | | | |
| -6 | | 8 | | | | | | | | | | | | | | | 2.68 | SM |
| -7 | | | | | | | | | | | | | | | | | | |
| -8 | End of boring | | | | | | | | | | | | | | | | | |
| -9 | | | | | | | | | | | | | | | | | | |
| -10 | | | | | | | | | | | | | | | | | | |
| -11 | | | | | | | | | | | | | | | | | | |
| -12 | | | | | | | | | | | | | | | | | | |
| -13 | | | | | | | | | | | | | | | | | | |

NOTE :
 0 to 10 % = Trace
 10 to 20 % = Little
 20 to 35 % = Some
 35 to 50 % = And

= SPT

SPT = Standard penetration test (blows / ft)

● = Wp = Plastic limit, %

Δ = WL = Liquid limit, %

Gs = Specific Gravity

USCS = Unified Soil Classification System

BORING LOG

BOREHOLE #: BH - 12

PROJECT : Pengembangan Pelabuhan Benoa Bali

LOCATION : Pelabuhan Benoa, Bali

COORDINATE : 302,545.335 ; 9,033,195.178

ELEVATION OF SEA BED : + 1.30 m LWS

| Elevation LWS, m | SOIL DESCRIPTION | STANDARD PENETRATION TEST | | | | | SOIL COMPOSITION (%) | | | | ATTERBERG LIMITS | | | | | Gs | USCS | |
|---------------------|--|------------------------------|----|----|----|----|----------------------|-------|-------|-------|---------------------|-------|----|----|----|-----|------|-------|
| | | | | | | | Coral/ Shells | Sand | Silt | Clay | 0 | 20 | 40 | 60 | 80 | 100 | | |
| | | 0 | 10 | 20 | 30 | 40 | | | | | | | | | | | | |
| +1 | Sand and coral/shells, brown, trace silt, trace clay, loose. | | | | | | 230 | 28.57 | 49.36 | 7.31 | 4.76 | | | | | | 2.73 | SM |
| ±0 | | ● | 4 | | | | | | | | | | | | | | | |
| -1 | | ● | 4 | | | | | | | | | | | | | | | |
| -2 | | ● | 4 | | | | | | | | | | | | | | | |
| -3 | Sand, grey, some to and coral/shells, trace lo little silt, trace clay, loose. | | | | | | | 40.43 | 44.57 | 9.44 | 5.51 | | | | | | 2.68 | SM |
| -4 | | ● | 6 | | | | | | | | | | | | | | | |
| -5 | | ● | 6 | | | | | | | | | | | | | | 2.69 | SC-SM |
| -6 | | ● | 7 | | | | | | | | | | | | | | | |
| -7 | Sand, greyish brown, little coral/shells, little silt, trace clay, loose | | | | | | | 25.02 | 50.13 | 18.41 | 6.44 | 21.25 | | | | | 2.77 | SM |
| -8 | | ● | 8 | | | | | | | | | | | | | | | |
| -9 | End of boring | | | | | | | 19.15 | 62.62 | 10.38 | 7.85 | 21.24 | | | | | 2.68 | SM |
| -10 | | | | | | | | | | | | | | | | | | |
| -11 | | | | | | | | | | | | | | | | | | |
| -12 | | | | | | | | | | | | | | | | | | |
| -13 | | | | | | | | | | | | | | | | | | |

NOTE :
 0 to 10 % = Trace
 10 to 20 % = Little
 20 to 35 % = Some
 35 to 50 % = And

= SPT

SPT = Standard penetration test (blows / ft)

● = Wp = Plastic limit, %

Δ = WL = Liquid limit, %

Gs = Specific Gravity

USCS = Unified Soil Classification System

BORING LOG

BOREHOLE #: BH - 13

PROJECT : Pengembangan Pelabuhan Benoa Bali
LOCATION : Pelabuhan Benoa, Bali

COORDINATE : 303,465.088 ; 9,033,210.158
ELEVATION OF SEA BED : -1.100 m

| Elevation LWS, m | SOIL DESCRIPTION | STANDARD PENETRATION TEST | | | | | SOIL COMPOSITION (%) | | | | ATTERBERG LIMITS | | | | | Gs | USCS |
|---------------------|--|------------------------------|----|----|----|----|----------------------|------|------|------|---------------------|----|----|----|----|----|------|
| | | 0 | 10 | 20 | 30 | 40 | Coral/ Shells | Sand | Silt | Clay | 0 | 20 | 40 | 60 | 80 | | |
| +1 | | | | | | | | | | | | | | | | | |
| ±0 | | | | | | | | | | | | | | | | | |
| -1 | | | | | | | | | | | | | | | | | |
| -2 | | | | | | | | | | | | | | | | | |
| -3 | | | | | | | | | | | | | | | | | |
| -3.5 | Sand, grey, some coral/shells, little silt, trace clay, loose. | | | | | | | | | | | | | | | | |
| -4 | | | | | | | | | | | | | | | | | |
| -5 | | | | | | | | | | | | | | | | | |
| -6 | | | | | | | | | | | | | | | | | |
| -7 | | | | | | | | | | | | | | | | | |
| -8 | End of boring | | | | | | | | | | | | | | | | |
| -9 | | | | | | | | | | | | | | | | | |
| -10 | | | | | | | | | | | | | | | | | |
| -11 | | | | | | | | | | | | | | | | | |
| -12 | | | | | | | | | | | | | | | | | |
| -13 | | | | | | | | | | | | | | | | | |

NOTE : 0 to 10 % = Trace
10 to 20 % = Little
20 to 35 % = Some
≥50 to ≥60 % = And

◆ = SPT
SPT = Standard penetration test (blows / ft)

* = Wp = Plastic limit, %
Δ = WL = Liquid limit, %
Gs = Specific Gravity
USCS = Unified Soil Classification System

BORING LOG

BOREHOLE #: BH - 15

PROJECT : Pengembangan Pelabuhan Benoa Ball

LOCATION: Pelabuhan Benoa, Ball

COORDINATE

: 301,579.160 ; 9,032,969.136

ELEVATION OF SEA BED

: -0.25 m LWS

| Elevation LWS, m | SOIL DESCRIPTION | STANDARD PENETRATION TEST | | | | | SOIL COMPOSITION (%) | | | | ATTERBERG LIMITS | | | | | Gs | USCS |
|---------------------|--|------------------------------|----|----|----|----|----------------------|-------|-------|-------|---------------------|----|----|----|----|-----|------------|
| | | 0 | 10 | 20 | 30 | 40 | Coral/ Shells | Sand | Silt | Clay | 0 | 20 | 40 | 60 | 80 | 100 | |
| +1 | | | | | | | ≥50 | | | | | | | | | | |
| ±0 | | | | | | | | | | | | | | | | | |
| -1 | Sand, brown, some coral/shells, trace silt, trace clay, loose. | 6 | | | | | | 23.27 | 68.02 | 6.79 | 1.92 | 21 | 25 | | | | 2.68 SP-SM |
| -2 | | 6 | | | | | | 20.58 | 57.02 | 13.56 | 8.84 | 21 | 25 | | | | 2.73 SC-SM |
| -3 | Sand, greyish brown, some coral/shells, little silt, trace clay. | 6 | | | | | | 22.73 | 64.29 | 6.05 | 6.93 | 21 | 28 | | | | 2.72 SM |
| -4 | | 7 | | | | | | 27.97 | 35.84 | 16.13 | 20.06 | 20 | 24 | | | | 2.71 SC-SM |
| -5 | | 10 | | | | | | 3.84 | 50.25 | 31.29 | 14.62 | 26 | 27 | | | | 2.69 SC-SM |
| -6 | Sand, grey, some silt, little clay, trace shells, loose. | 13 | | | | | | 33.01 | 46.64 | 14.02 | 6.33 | 21 | 28 | | | | 2.65 SM |
| -7 | | | | | | | | | | | | | | | | | |
| -8 | | | | | | | | | | | | | | | | | |
| -9 | | | | | | | | | | | | | | | | | |
| -10 | | | | | | | | | | | | | | | | | |
| -11 | | | | | | | | | | | | | | | | | |
| -12 | | | | | | | | | | | | | | | | | |
| -13 | End of boring | | | | | | | | | | | | | | | | |

NOTE : 0 to 10 % = Trace

10 to 20 % = Little

20 to 35 % = Some

35 to 50 % = And

◆ = Wp

= Plastic limit, %

△ = WL

= Liquid limit, %

Gs = Specific Gravity

USCS = Unified Soil Classification System

□ = SPT

SPT = Standard penetration test (blows / ft)

BORING LOG

BOREHOLE #: BH - 16

PROJECT : Pengembangan Pelabuhan Benoa Ball

COORDINATE : 302,073.863 ; 9,032,941.691

LOCATION : Pelabuhan Benoa, Ball

ELEVATION OF SEA BED : -0.75 m LWS

| Elevation LWS, m | SOIL DESCRIPTION | STANDARD PENETRATION TEST | | | | | SOIL COMPOSITION (%) | | | | ATTERBERG LIMITS | | | | | Gs | USCS | |
|---------------------|--|------------------------------|----|----|----|----|----------------------|------|------|------|---------------------|----|----|----|----|----|------|----|
| | | 0 | 10 | 20 | 30 | 40 | Coral/ Shells | Sand | Silt | Clay | 0 | 20 | 40 | 60 | 80 | | | |
| +1 | | | | | | | | | | | | | | | | | | |
| ±0 | | | | | | | | | | | | | | | | | | |
| -1 | | | | | | | | | | | | | | | | | | |
| -2 | Sand, brown, trace coral/shells, trace silt, trace clay, very loose. | 3 | | | | | | | | | | | | | | | 2.70 | SM |
| -3 | | 3 | | | | | | | | | | | | | | | 2.75 | SC |
| -4 | Sand, grey, some coral/shells, some silt, little clay, very loose | 3 | | | | | | | | | | | | | | | | |
| -5 | | 5 | | | | | | | | | | | | | | | 2.67 | SM |
| -6 | | 9 | | | | | | | | | | | | | | | | |
| -7 | Sand, grey, some coral/shells, little silt, trace clay, loose | 24 | | | | | | | | | | | | | | | 2.71 | SM |
| -8 | | 17 | | | | | | | | | | | | | | | | |
| -9 | | | | | | | | | | | | | | | | | | |
| -10 | | | | | | | | | | | | | | | | | | |
| -11 | Sand, grey, some silt, trace to little clay, trace coral/shells, medium. | 25 | | | | | | | | | | | | | | | 2.61 | SM |
| -12 | | 27 | | | | | | | | | | | | | | | | |
| -13 | End of boring | 27 | | | | | | | | | | | | | | | | |

NOTE :
0 to 10 % = Trace
10 to 20 % = Little
20 to 35 % = Some
35 to 50 % = And

□ = SPT

SPT = Standard penetration test (blows / ft)

♦ = Wp = Plastic limit, %

△ = WL = Liquid limit, %

Gs = Specific Gravity

USCS = Unified Soil Classification System

| BORING LOG | | | | | | | BOREHOLE #: BH - 17 | | | | | | | | | | | | | |
|---|--|------------------------------|----|----------------------|----|----------------------|-------------------------------|------|---------------------|------|---|----|----|----|----|-----|----|------|------|----|
| PROJECT : Pengembangan Pelabuhan Benoa Ball | | | | COORDINATE | | | : 302,755.169 ; 9,032,209.897 | | | | | | | | | | | | | |
| LOCATION : Pelabuhan Benoa, Bali | | | | ELEVATION OF SEA BED | | | : -0.80 m LWS | | | | | | | | | | | | | |
| Elevation LWS, m | SOIL DESCRIPTION | STANDARD PENETRATION TEST | | | | SOIL COMPOSITION (%) | | | ATTERBERG LIMITS | | | | | | | | | | | |
| | | 0 | 10 | 20 | 30 | 40 | Coral/ Shells | Sand | SM | Clay | 0 | 20 | 40 | 60 | 30 | 100 | Gs | USCS | | |
| +1 | | | | | | | | | | | | | | | | | | | | |
| ±0 | | | | | | | | | | | | | | | | | | | | |
| -1 | | | | | | | | | | | | | | | | | | | | |
| -2 | Sand, brown, trace shells, trace silt, loose | 4 | | | | | | | | | | | | | | | | | 2.78 | SP |
| -3 | | 4 | | | | | | | | | | | | | | | | | 2.71 | SP |
| -4 | | 4 | | | | | | | | | | | | | | | | | 2.70 | SM |
| -5 | Sand, brownish grey, little silt, trace clay, trace shells, loose to medium. | 5 | | | | | | | | | | | | | | | | | 2.76 | SM |
| -6 | | 12 | | | | | | | | | | | | | | | | | 2.68 | SM |
| -7 | | 9 | | | | | | | | | | | | | | | | | 2.75 | SM |
| -8 | | | | | | | | | | | | | | | | | | | | |
| -9 | | | | | | | | | | | | | | | | | | | | |
| -10 | | | | | | | | | | | | | | | | | | | | |
| -11 | Sand, grey, little silt, little clay, trace shells, loose. | | | | | | | | | | | | | | | | | | | |
| -12 | End of boring | | | | | | | | | | | | | | | | | | | |
| -13 | | | | | | | | | | | | | | | | | | | | |

NOTE :
 0 to 10 % = Trace
 10 to 20 % = Little
 20 to 35 % = Some
 35 to 50 % = And

= SPT

SPT = Standard penetration test (blows / ft)

♦ = Wp = Plastic limit, %

Δ = WL = Liquid limit, %

Gs = Specific Gravity

USCS = Unified Soil Classification System

BORING LOG

BOREHOLE #: BH - 18

PROJECT : Pengembangan Pelabuhan Benoa Bali
LOCATION: Pelabuhan Benoa, Bali

COORDINATE : 303.485.088 ; 9.032.975.158
ELEVATION OF SEA BED : -1.80 m LWS

| Elevation LWS, m | SOIL DESCRIPTION | STANDARD PENETRATION TEST | | | | | SOIL COMPOSITION (%) | | | | ATTERBERG LIMITS | | | | | Gs | USCS | |
|---------------------|---|------------------------------|----|----|----|----|----------------------|------|------|------|---------------------|-------|-------|------|-------|----|------|-------|
| | | 0 | 10 | 20 | 30 | 40 | Coral Shells | Sand | Silt | Clay | 0 | 20 | 40 | 60 | 80 | | | |
| +1 | | | | | | | | | | | | | | | | | | |
| ±0 | | | | | | | | | | | | | | | | | | |
| -1 | | | | | | | | | | | | | | | | | | |
| -2 | | | | | | | | | | | | | | | | | | |
| -3 | Sand, brownish grey, trace to little coral/shells, trace silt, trace clay, loose. | | | | | | | | | | 9.53 | 78.01 | 9.50 | 2.96 | | | 2.72 | SM |
| -4 | | 4 | | | | | | | | | 20.27 | 72.05 | 7.68 | - | | | 2.71 | SP-SM |
| -5 | | 4 | | | | | | | | | 25.14 | 57.20 | 9.59 | 8.07 | | | 2.69 | SM |
| -6 | Sand, grey, some coral/shells, trace silt, trace clay, loose. | | | | | | | | | | | | | | | | | |
| -7 | | 6 | | | | | | | | | | | | | | | | |
| -8 | | | | | | | | | | | | | | | | | | |
| -9 | | | | | | | | | | | | | | | | | | |
| -10 | Sand, grey, little silt, trace coral/shells, trace clay, loose | | | | | | | | | | 3.40 | 73.05 | 16.21 | 7.34 | 20 23 | | 2.64 | SM |
| -11 | | 7 | | | | | | | | | 1.27 | 71.15 | 20.82 | 6.76 | 20 21 | | 2.77 | SM |
| -12 | End of boring. | | | | | | | | | | | | | | | | | |
| -13 | | 8 | | | | | | | | | | | | | | | | |

NOTE : 0 to 10 % = Trace
10 to 20 % = Little
20 to 35 % = Some
35 to 50 % = And

= SPT

SPT = Standard penetration test (blows / ft)

● = Wp = Plastic limit, %

△ = WL = Liquid limit, %

Gs = Specific Gravity

USCS = Unified Soil Classification System

BORING LOG

BOREHOLE #: BH - 19

PROJECT : Pengembangan Pelabuhan Benoa Bali
LOCATION : Pelabuhan Benoa, Bali

COORDINATE : 303,525.492; 9,032,181.628
ELEVATION OF SEA BED : -1.03 m

| Elevation LWS, m | SOIL DESCRIPTION | STANDARD PENETRATION TEST | | | | | SOIL COMPOSITION (%) | | | | ATTERBERG LIMITS | | | | | Gs | USCS | |
|---------------------|--|------------------------------|----|----|----|----|----------------------|------|-------|-------|---------------------|-------|----|----|----|-----|------|-------|
| | | 0 | 10 | 20 | 30 | 40 | Coral Shells | Sand | Silt | Clay | 0 | 20 | 40 | 60 | 80 | 100 | | |
| +1 | | | | | | | | | | | | | | | | | | |
| ±0 | | | | | | | | | | | | | | | | | | |
| -1 | | | | | | | | | | | | | | | | | | |
| -2 | | | | | | | | | | | | | | | | | | |
| -3 | Sand, brown, trace shells, trace silt, very loose | 2 | | | | | | 1.50 | 98.27 | 0.13 | | | | | | | 2.72 | SP |
| -4 | | 3 | | | | | | 1.00 | 90.71 | 5.38 | 2.91 | | | | | | 2.66 | SF-SM |
| -5 | | 5 | | | | | | 0.59 | 70.03 | 19.58 | 9.80 | 21 23 | | | | | 2.76 | SM |
| -6 | | 12 | | | | | | 8.31 | 72.57 | 11.89 | 7.23 | 20 22 | | | | | 2.64 | SM |
| -7 | Sand, brownish grey, trace to little silt, trace shells, trace clay, very loose to medium. | 8 | | | | | | 5.82 | 72.32 | 13.24 | 8.62 | 20 23 | | | | | 2.73 | SM |
| -8 | | | | | | | | 4.60 | 80.28 | 11.28 | 3.74 | | | | | | | |
| -9 | | | | | | | | | | | | | | | | | | |
| -10 | | | | | | | | | | | | | | | | | | |
| -11 | Sand, grey, little silt, trace clay, trace shells, loose. | | | | | | | | | | | | | | | | 2.70 | SM |
| -12 | End of boring. | | | | | | | | | | | | | | | | | |
| -13 | | | | | | | | | | | | | | | | | | |

NOTE : 0 to 10 % = Trace
10 to 20 % = Little
20 to 35 % = Some
35 to 50 % = And

= SPT

SPT = Standard penetration test (blows / 1')

● = Wp = Plastic limit, %

△ = WL = Liquid limit, %

Gs = Specific Gravity

USCS = Unified Soil Classification System

| | | BORING LOG | | | | | | BOREHOLE # : BH - 20 | | | | | | | | | | |
|---|---|------------------------------|----|----|----|----------------------|--|-------------------------------|----|------|---|----|----|----|---|-----|----|------|
| PROJECT : Pengembangan Pelabuhan Benoa Bali | | COORDINATE | | | | | | : 304,157.777 ; 9,032,390.417 | | | | | | | | | | |
| LOCATION : Pelabuhan Benoa, Bali | | ELEVATION OF SEA BED | | | | | | : + 0.20 m LWS | | | | | | | | | | |
| Elevation LWS, m | SOIL DESCRIPTION | STANDARD PENETRATION TEST | | | | SOIL COMPOSITION (%) | | ATTERBERG LIMITS | | | | | | | | | | |
| | | 0 | 10 | 20 | 30 | 40 | Coral/ Shells | Sand | SM | Clay | 0 | 20 | 40 | 60 | 80 | 100 | Gs | USCS |
| | | | | | | ≥50 | | | | | | | | | | | | |
| +1 | | | | | | | | | | | | | | | | | | |
| ±0 | Sand, greyish brown, little shells, trace silt, trace clay. | | | | | | | | | | | | | | | | | |
| -1 | | | | | | | | | | | | | | | | | | |
| -2 | Sand, grey, little silt, trace clay, trace shells, loose to medium. | | | | | | | | | | | | | | | | | |
| -3 | | | | | | | | | | | | | | | | | | |
| -4 | Sand, brown, little coral/shells, trace silt, medium. | | | | | | | | | | | | | | | | | |
| -5 | | | | | | | | | | | | | | | | | | |
| -6 | | | | | | | | | | | | | | | | | | |
| -7 | | | | | | | | | | | | | | | | | | |
| -8 | Sand, and coral/shells, grey, trace silt, trace clay, medium | | | | | | | | | | | | | | | | | |
| -9 | | | | | | | | | | | | | | | | | | |
| -10 | | | | | | | | | | | | | | | | | | |
| -11 | | | | | | | | | | | | | | | | | | |
| -12 | | | | | | | | | | | | | | | | | | |
| -13 | End of boring. | | | | | | | | | | | | | | | | | |
| NOTE : | | 0 to 10 % = Trace | | | | | | | | | | | | | ● = Wp = Plastic limit, % | | | |
| | | 10 to 20 % = Little | | | | | <input checked="" type="checkbox"/> = SPT | | | | | | | | Δ = WL = Liquid limit, % | | | |
| | | 20 to 35 % = Some | | | | | SPT = Standard penetration test (blows / ft) | | | | | | | | Gs = Specific Gravity | | | |
| | | 35 to 50 % = And | | | | | | | | | | | | | USCS = Unified Soil Classification System | | | |

BORING LOG

BOREHOLE # : BH - 21

PROJECT : Pengembangan Pelabuhan Benoa Ball
LOCATION : Pelabuhan Benoa, Ball

COORDINATE : 302,531.788 ; 9,033,420.178
ELEVATION OF SEA BED : + 1.20 m LWS

| Elevation LWS, m | SOIL DESCRIPTION | STANDARD PENETRATION TEST | | | | | SOIL COMPOSITION (%) | | | | ATTERBERG LIMITS | | | | | Gs | USC |
|---------------------|---|------------------------------|----|----|----|----|----------------------|------|------|------|---------------------|----|----|----|----|----|-----|
| | | 0 | 10 | 20 | 30 | 40 | Coral/ Shells | Sand | Silt | Clay | 0 | 20 | 40 | 60 | 80 | | |
| +1 | Sand, brown, trace silt, trace clay, trace shells. | | | | | | | | | | | | | | | | |
| ±0 | Coral/shells and sand, grey, little silt, trace clay, medium. | | | | | | | | | | | | | | | | |
| -1 | | | | | | | | | | | | | | | | | |
| -2 | | | | | | | | | | | | | | | | | |
| -3 | Sand, grey, some to and coral/shells, trace to little silt, trace clay, medium to dense | | | | | | | | | | | | | | | | |
| -4 | | | | | | | | | | | | | | | | | |
| -5 | | | | | | | | | | | | | | | | | |
| -6 | | | | | | | | | | | | | | | | | |
| -7 | End of boring | | | | | | | | | | | | | | | | |
| -8 | | | | | | | | | | | | | | | | | |
| -9 | | | | | | | | | | | | | | | | | |
| -10 | | | | | | | | | | | | | | | | | |
| -11 | | | | | | | | | | | | | | | | | |
| -12 | | | | | | | | | | | | | | | | | |
| -13 | | | | | | | | | | | | | | | | | |

NOTE :
0 to 10 % = Trace
10 to 20 % = Little
20 to 35 % = Some
35 to 50 % = And

= SPT

SPT = Standard penetration test (b/lws / ▲)

◆ = Wp = Plastic limit, %

▲ = WL = Liquid limit, %

Gs = Specific Gravity

USCS = Unified Soil Classification System

GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali

Location : Pelabuhan Benoa Bali

Sieve Analysis

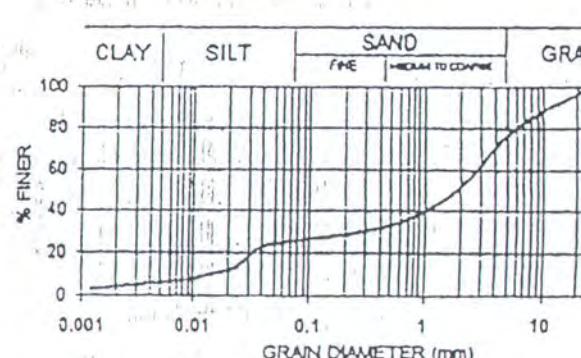
| Sieve opening No. | mean (mm) | % weight gr | % retained | Cumulative % retained | % finer |
|----------------------|--------------|-------------------|---------------|--------------------------|---------|
| 1.5* | 39.100 | 0.00 | 0.00 | 0.00 | 100.00 |
| 1.0* | 25.400 | 0.00 | 0.00 | 0.00 | 100.00 |
| 3/4 | 13.000 | 33.10 | 4.87 | 4.87 | 95.13 |
| 3/8 | 9.500 | 54.15 | 7.98 | 12.83 | 97.17 |
| 4 | 4.750 | 80.50 | 11.84 | 24.67 | 75.23 |
| 8 | 2.360 | 137.10 | 20.16 | 44.83 | 45.17 |
| 16 | 1.180 | 88.34 | 12.70 | 57.53 | 42.47 |
| 30 | 0.800 | 54.75 | 8.05 | 65.58 | 34.42 |
| 50 | 0.300 | 28.80 | 3.98 | 69.54 | 30.48 |
| 100 | 0.150 | 17.34 | 2.55 | 72.09 | 27.91 |
| 200 | 0.075 | 13.90 | 2.04 | 74.13 | 25.87 |
| TOTAL | | 504.98 | 74.13 | - | - |
| TOTAL SAMPLE gr | | 580 | | | |

Hydrometer

| Time (min) | Actual Hyd. (Ra) | Corr. Hyd. (Rc) | Effective depth L (cm) | Hyd. Corr. only for meniscus (R) | % finer | U | K | D. mm |
|---------------|---------------------|--------------------|------------------------------|--|---------|--------|-------|--------|
| 0.25 | 52 | 49.05 | 7.6 | 53 | 25.13 | 30.400 | 0.012 | 0.083* |
| 0.5 | 50 | 47.05 | 7.9 | 51 | 24.10 | 15.600 | 0.012 | 0.043 |
| 1 | 45 | 42.05 | 8.8 | 48 | 21.54 | 8.800 | 0.012 | 0.033 |
| 2 | 35 | 32.05 | 10.4 | 38 | 18.42 | 5.200 | 0.012 | 0.027 |
| 3 | 29 | 28.05 | 11.4 | 30 | 13.34 | 3.000 | 0.012 | 0.023 |
| 4 | 28 | 23.05 | 11.9 | 27 | 11.81 | 2.975 | 0.012 | 0.021 |
| 8 | 23 | 20.05 | 12.4 | 24 | 10.27 | 1.550 | 0.012 | 0.015 |
| 15 | 19 | 16.05 | 13 | 20 | 9.22 | 0.813 | 0.012 | 0.011 |
| 30 | 17 | 14.05 | 13.3 | 18 | 7.20 | 0.443 | 0.012 | 0.003 |
| 50 | 15 | 12.05 | 13.7 | 18 | 6.7 | 0.228 | 0.012 | 0.003 |
| 100 | 14 | 11.05 | 12.3 | 15 | 5.88 | 0.115 | 0.012 | 0.004 |
| 200 | | | | | | | | |
| 24 hrs | 3 | 8.05 | 14.7 | 10 | 3.0 | 0.010 | 0.012 | 0.001 |

Bore/depth : BH-9 / -5.00 s/d -8.00 m LWS

Soil description : Sand, grey, some coral/shells, little silt, trace clay



Visual description : Sand, grey, some coral/shells, little silt, trace clay

Soil classification (USCS) : SM

GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali

Location : Pelabuhan Benoa Bali

Sieve Analysis

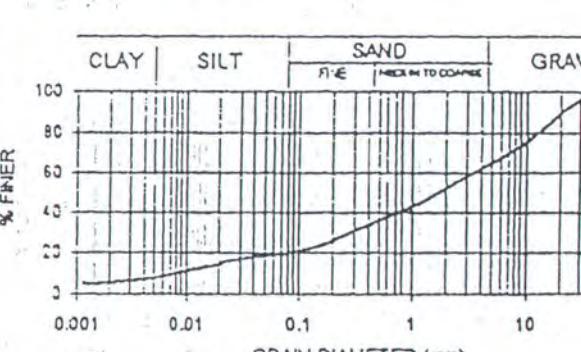
| Sieve opening No. | mean (mm) | % weight gr | % retained | Cumulative % retained | % finer |
|----------------------|--------------|-------------------|---------------|--------------------------|---------|
| 1.5* | 33.100 | 0.00 | 0.00 | 0.00 | 100.00 |
| 1.0* | 25.400 | 42.88 | 6.81 | 6.81 | 93.19 |
| 3/4 | 13.000 | 30.74 | 4.98 | 11.99 | 80.31 |
| 3/8 | 9.500 | 97.57 | 13.90 | 25.59 | 74.41 |
| 4 | 4.750 | 84.43 | 10.23 | 25.81 | 64.19 |
| 8 | 2.360 | 80.38 | 9.58 | 45.40 | 54.60 |
| 16 | 1.180 | 82.16 | 9.97 | 55.27 | 44.73 |
| 30 | 0.800 | 44.88 | 7.12 | 52.39 | 37.01 |
| 50 | 0.300 | 41.23 | 6.54 | 63.93 | 31.07 |
| 100 | 0.150 | 46.88 | 7.44 | 73.37 | 13.83 |
| 200 | 0.075 | 24.17 | 3.94 | 50.21 | 18.79 |
| TOTAL | | 505.23 | 80.21 | - | - |
| TOTAL SAMPLE gr | | 630 | | | |

Hydrometer

| Time (min) | Actual Hyd. (Ra) | Corr. Hyd. (Rc) | Effective depth L (cm) | Hyd. Corr. only for meniscus (R) | % finer | U | K | D. mm |
|---------------|---------------------|--------------------|------------------------------|--|---------|--------|---------|--------|
| 0.25 | 52 | 49.05 | 7.6 | 53 | 18.25 | 30.400 | 0.01204 | 0.083* |
| 0.5 | 50 | 47.05 | 7.9 | 51 | 18.47 | 15.600 | 0.01204 | 0.043 |
| 1 | 48 | 45.05 | 8.8 | 48 | 17.88 | 8.300 | 0.01204 | 0.035 |
| 2 | 45 | 42.05 | 9.8 | 48 | 16.51 | 4.400 | 0.01204 | 0.025 |
| 3 | 41 | 38.05 | 9.4 | 42 | 14.94 | 3.133 | 0.01204 | 0.021 |
| 4 | 39 | 35.05 | 9.9 | 39 | 13.78 | 2.475 | 0.01204 | 0.019 |
| 8 | 35 | 32.05 | 10.4 | 36 | 12.58 | 1.300 | 0.01204 | 0.014 |
| 15 | 31 | 28.05 | 11.1 | 32 | 11.01 | 0.694 | 0.01204 | 0.010 |
| 30 | 27 | 24.05 | 11.7 | 28 | 9.44 | 0.330 | 0.01204 | 0.003 |
| 50 | 23 | 20.05 | 12.4 | 24 | 7.97 | 0.207 | 0.01204 | 0.005 |
| 100 | 20 | 17.05 | 12.9 | 21 | 6.39 | 0.108 | 0.01204 | 0.004 |
| 200 | | | | | | | | |
| 24 hrs | 15 | 12.05 | 13.7 | 16 | 4.73 | 0.010 | 0.01204 | 0.001 |

Bore/depth : BH-10 / -2.00 s/d -3.00 m LWS

Soil description : Sand and coral/shells, little silt, trace clay



Visual description : Sand and coral/shells, little silt, trace clay

Soil classification (USCS) : SM

GRAIN SIZE DISTRIBUTION

petan

Project : Pengembangan Pelabuhan Benoa Bali

Location : Pelabuhan Benoa Bali

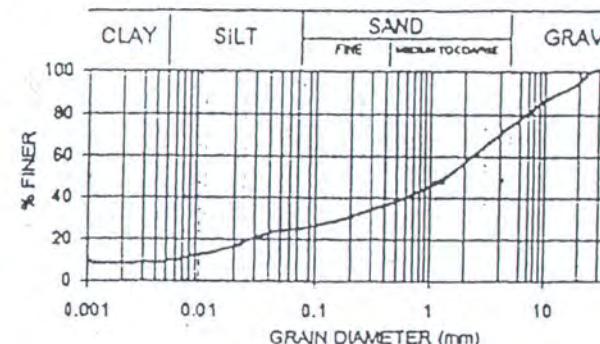
Sieve Analysis

| Sieve opening No. | mean (mm) | weight gr | mean | Cumulative | % |
|----------------------|--------------|--------------|----------|------------|--------|
| | | | retained | % retained | finer |
| 1.5* | 33.100 | 0.03 | 0.03 | 0.00 | 100.00 |
| 1.0* | 25.400 | 0.03 | 0.03 | 0.00 | 100.00 |
| 3/4 | 19.000 | 34.51 | 8.01 | 8.01 | 92.99 |
| 3/8 | 9.500 | 117.33 | 8.33 | 14.40 | 86.80 |
| 4 | 4.750 | 163.47 | 11.63 | 29.24 | 72.98 |
| 8 | 2.360 | 188.58 | 13.42 | 39.46 | 66.54 |
| 16 | 1.180 | 179.98 | 12.80 | 52.76 | 47.74 |
| 32 | 0.600 | 105.38 | 7.52 | 59.78 | 40.22 |
| 50 | 0.300 | 79.57 | 5.63 | 65.45 | 34.55 |
| 100 | 0.150 | 77.01 | 5.43 | 70.53 | 26.07 |
| 200 | 0.075 | 57.14 | 4.07 | 74.39 | 25.01 |
| TOTAL | | 1089.67 | 74.93 | | |
| TOTAL SAMPLE gr | | 1405 | | | |

Hydrometer

| Time (min) | Actual Hyd. (P1) | Corr. Hyd. (Pc) | Effective depth L (cm) | Hyc. Corr. only for meniscus (R) | % finer | Lt | K | D, mm |
|---------------|---------------------|--------------------|------------------------------|--|---------|--------|--------------|-------|
| | | | | | reading | depth | meniscus (R) | |
| 0.25 | 53 | 50.05 | 7.4 | 54 | 24.88 | 26.800 | 0.01208 | 0.068 |
| 0.5 | 52 | 49.05 | 7.8 | 53 | 24.38 | 15.200 | 0.01208 | 0.047 |
| 1 | 48 | 45.05 | 8.3 | 49 | 22.30 | 8.300 | 0.01208 | 0.035 |
| 2 | 42 | 39.05 | 9.2 | 43 | 18.4 | 4.800 | 0.01208 | 0.028 |
| 3 | 39 | 35.05 | 9.9 | 38 | 17.42 | 3.300 | 0.01208 | 0.022 |
| 4 | 36 | 33.05 | 10.2 | 37 | 18.43 | 2.550 | 0.01208 | 0.019 |
| 8 | 32 | 29.05 | 10.9 | 33 | 14.44 | 1.363 | 0.01208 | 0.014 |
| 16 | 29 | 28.05 | 11.4 | 30 | 12.85 | 0.712 | 0.01208 | 0.010 |
| 30 | 28 | 23.05 | 11.9 | 27 | 11.48 | 0.397 | 0.01208 | 0.008 |
| 30 | 23 | 20.05 | 12.4 | 24 | 9.97 | 0.207 | 0.01208 | 0.005 |
| 120 | 21 | 19.05 | 12.7 | 22 | 8.87 | 0.10E | 0.01208 | 0.004 |
| 24 hrs | 19 | 17.05 | 12.9 | 21 | 8.48 | 0.00E | 0.01208 | 0.001 |

Bore/depth : BH-13 / 2.00 s/d -3.00 m LWS



Visual description: Sand, grey, some corals/shells, little silt, trace clay
Soil classification (USCS) : SC

Project : Pengembangan Pelabuhan Benoa Bali

Location : Pelabuhan Benoa Bali

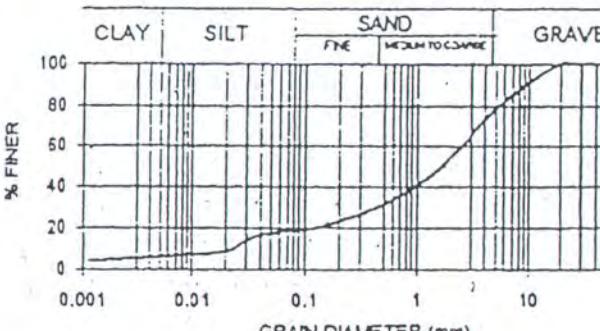
Sieve Analysis

| Sieve opening No. | mean (mm) | weight gr | mean | Cumulative | % |
|----------------------|--------------|--------------|----------|------------|--------|
| | | | retained | % retained | finer |
| 1.5* | 33.100 | 0.03 | 0.03 | 0.00 | 100.00 |
| 1.0* | 25.400 | 0.03 | 0.03 | 0.00 | 100.00 |
| 3/4 | 19.000 | 0.03 | 0.03 | 0.00 | 100.00 |
| 3/8 | 9.500 | 56.00 | 9.63 | 9.63 | 90.37 |
| 4 | 4.750 | 79.14 | 13.41 | 23.04 | 76.86 |
| 8 | 2.360 | 108.38 | 18.45 | 41.49 | 56.51 |
| 16 | 1.180 | 39.50 | 15.17 | 58.36 | 43.34 |
| 32 | 0.600 | 59.40 | 10.07 | 89.73 | 33.27 |
| 50 | 0.300 | 39.00 | 8.73 | 73.49 | 26.51 |
| 100 | 0.150 | 31.90 | 5.41 | 78.30 | 21.10 |
| 200 | 0.075 | 14.70 | 2.43 | 91.39 | 16.81 |
| TOTAL | | 480.20 | 31.39 | | |
| TOTAL SAMPLE gr | | 590 | | | |

Hydrometer

| Time (min) | Actual Hyd. (P1) | Corr. Hyd. (Pc) | Effective depth L (cm) | Hyc. Corr. only for meniscus (R) | % finer | Lt | K | D, mm |
|---------------|---------------------|--------------------|------------------------------|--|---------|--------|--------------|-------|
| | | | | | reading | depth | meniscus (R) | |
| 0.25 | 53 | 50.05 | 7.4 | 54 | 18.44 | 26.800 | 0.01208 | 0.068 |
| 0.5 | 52 | 49.05 | 7.8 | 53 | 17.34 | 15.800 | 0.01208 | 0.048 |
| 1 | 48 | 45.05 | 8.3 | 47 | 15.88 | 8.800 | 0.01208 | 0.036 |
| 2 | 37 | 34.05 | 10.1 | 38 | 12.55 | 5.050 | 0.01208 | 0.027 |
| 3 | 30 | 27.05 | 11.2 | 31 | 9.97 | 3.733 | 0.01208 | 0.023 |
| 4 | 27 | 24.05 | 11.7 | 28 | 8.88 | 2.925 | 0.01208 | 0.021 |
| 8 | 25 | 22.05 | 12 | 25 | 9.13 | 1.500 | 0.01208 | 0.015 |
| 16 | 23 | 20.05 | 12.4 | 24 | 7.39 | 0.775 | 0.01208 | 0.011 |
| 30 | 21 | 18.05 | 12.7 | 22 | 8.85 | 0.425 | 0.01208 | 0.008 |
| 50 | 20 | 17.05 | 12.9 | 21 | 9.28 | 0.215 | 0.01208 | 0.006 |
| 120 | 19 | 18.05 | 13 | 20 | 5.91 | 0.10E | 0.01208 | 0.004 |
| 24 hrs | 15 | 12.05 | 13.7 | 16 | 4.44 | 0.01E | 0.01208 | 0.001 |

Bore/depth : BH-13 / -4.00 s/d -5.00 m LWS



Visual description: Sand, grey, some corals/shells, little silt, trace clay
Soil classification (USCS) : SM

GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali

Location : Pelabuhan Benoa Bali

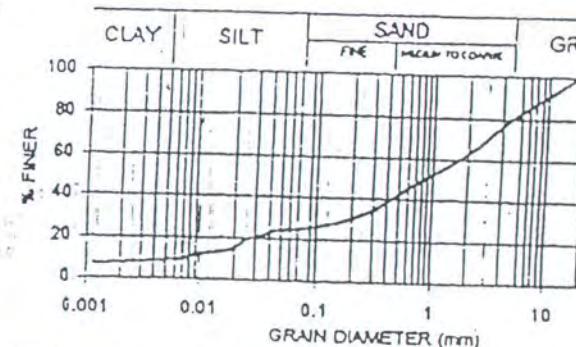
Sieve Analysis

| Sieve opening No. | mean (mtr) | mean | % | Cumulative | % |
|----------------------|---------------|--------------|----------|------------|--------|
| | | weight gr | retained | % retained | finer |
| 1.5* | 33.100 | 0.00 | 0.00 | 0.00 | 100.00 |
| 1.0* | 25.400 | 0.00 | 0.00 | 0.00 | 100.00 |
| 3/4 | 13.000 | 0.00 | 0.00 | 0.00 | 100.00 |
| 3/8 | 9.500 | 148.25 | 10.34 | 10.34 | 89.86 |
| 4 | 4.750 | 144.38 | 10.24 | 20.57 | 79.43 |
| 8 | 2.360 | 182.30 | 13.59 | 34.16 | 66.94 |
| 16 | 1.180 | 167.80 | 11.14 | 45.30 | 54.70 |
| 30 | 0.600 | 128.54 | 9.03 | 54.39 | 45.61 |
| 50 | 0.300 | 154.30 | 10.95 | 65.23 | 34.87 |
| 100 | 0.150 | 31.05 | 8.43 | 71.77 | 26.23 |
| 200 | 0.075 | 41.13 | 2.91 | 74.57 | 21.33 |
| TOTAL | | 1356.86 | 74.67 | - | - |
| TOTAL SAMPLE gr | | 1415 | | | |

Hydrometer

| Time (min) | Actual Hyd. | | Corr. Hyd. | Effective depth (cm) | Hyc. Corr only for meriscus (F) | % finer | LA | K | D. mm |
|---------------|-------------|-------------------|-------------------|----------------------------|---------------------------------------|---------|---------|-------|-------|
| | reading | (P ₁) | (P _c) | | | | | | |
| 0.25 | 53 | 50.05 | 7.4 | 54 | 25.00 | 26.800 | 0.01182 | 0.065 | |
| 0.5 | 51 | 48.05 | 7.8 | 52 | 24.00 | 15.800 | 0.01182 | 0.047 | |
| 1 | 48 | 43.05 | 8.6 | 47 | 21.50 | 9.800 | 0.01182 | 0.035 | |
| 2 | 42 | 39.05 | 9.2 | 43 | 19.50 | 4.800 | 0.01182 | 0.028 | |
| 3 | 37 | 34.05 | 10.1 | 38 | 17.00 | 3.387 | 0.01182 | 0.022 | |
| 4 | 33 | 30.05 | 10.7 | 34 | 15.01 | 2.875 | 0.01182 | 0.019 | |
| 8 | 30 | 27.05 | 11.2 | 31 | 13.51 | 1.400 | 0.01182 | 0.014 | |
| 16 | 27 | 24.05 | 11.7 | 28 | 12.01 | 0.731 | 0.01182 | 0.010 | |
| 30 | 24 | 21.05 | 12.2 | 25 | 10.51 | 0.407 | 0.01182 | 0.008 | |
| 50 | 21 | 19.05 | 12.7 | 22 | 9.01 | 0.212 | 0.01182 | 0.005 | |
| 100 | 19 | 15.05 | 13 | 20 | 8.02 | 0.108 | 0.01182 | 0.004 | |
| 200 | 15 | 13.05 | 13.5 | 17 | 8.52 | 0.005 | 0.01182 | 0.001 | |
| 24 hrs | | | | | | | | | |

Bore/depth : BH-13 / 8.00 s/d 7.00 m LWS



Visual description : Sand, grey, some coral/shells, little silt, trace clay
Soil classification (USCS) : SM

GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali

Location : Pelabuhan Benoa Bali

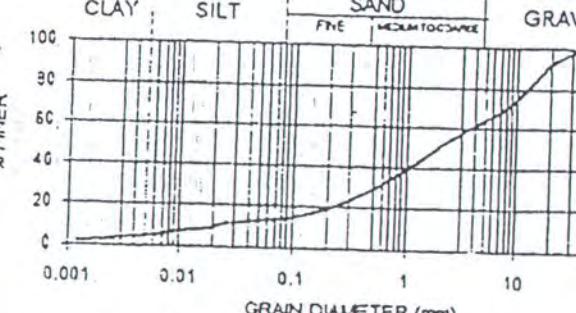
Sieve Analysis

| Sieve opening No. | mean (mtr) | mean | % | Cumulative | % |
|----------------------|---------------|--------------|----------|------------|--------|
| | | weight gr | retained | % retained | finer |
| 1.5* | 33.100 | 0.00 | 0.00 | 0.00 | 100.00 |
| 1.0* | 25.400 | 33.15 | 4.03 | 4.03 | 95.91 |
| 3/4 | 13.000 | 71.58 | 4.57 | 8.65 | 91.34 |
| 3/8 | 9.500 | 191.72 | 10.10 | 26.35 | 73.34 |
| 4 | 4.750 | 180.77 | 10.27 | 36.33 | 83.07 |
| 8 | 2.360 | 150.30 | 9.63 | 46.54 | 53.48 |
| 16 | 1.180 | 191.50 | 12.24 | 56.77 | 41.23 |
| 30 | 0.600 | 153.30 | 9.53 | 68.30 | 31.40 |
| 50 | 0.300 | 121.40 | 7.73 | 79.36 | 23.84 |
| 100 | 0.150 | 103.30 | 8.63 | 92.96 | 17.04 |
| 200 | 0.075 | 55.10 | 3.52 | 96.49 | 12.52 |
| TOTAL | | 1353.42 | 36.48 | - | - |
| TOTAL SAMPLE gr | | 1585 | | | |

Hydrometer

| Time (min) | Actual Hyd. | | Corr. Hyd. | Effective depth (cm) | Hyc. Corr only for meriscus (F) | % finer | LA | K | D. mm |
|---------------|-------------|-------------------|-------------------|----------------------------|---------------------------------------|---------|---------|-------|-------|
| | reading | (P ₁) | (P _c) | | | | | | |
| 0.25 | 53 | 50.05 | 7.4 | 54 | 13.37 | 26.800 | 0.01182 | 0.065 | |
| 0.5 | 50 | 47.05 | 7.9 | 51 | 12.52 | 15.800 | 0.01182 | 0.046 | |
| 1 | 47 | 44.05 | 8.4 | 48 | 11.77 | 8.400 | 0.01182 | 0.035 | |
| 2 | 45 | 42.05 | 9.8 | 46 | 11.23 | 4.400 | 0.01182 | 0.025 | |
| 3 | 41 | 38.05 | 9.4 | 42 | 10.18 | 3.133 | 0.01182 | 0.021 | |
| 4 | 37 | 34.05 | 10.1 | 38 | 9.10 | 2.525 | 0.01182 | 0.019 | |
| 8 | 33 | 30.05 | 10.7 | 34 | 8.03 | 1.33E | 0.01182 | 0.014 | |
| 16 | 30 | 27.05 | 11.2 | 31 | 7.23 | 0.700 | 0.01182 | 0.010 | |
| 30 | 27 | 24.05 | 11.7 | 28 | 6.42 | 0.390 | 0.01182 | 0.007 | |
| 50 | 24 | 21.05 | 12.7 | 25 | 4.92 | 0.212 | 0.01182 | 0.008 | |
| 100 | 21 | 18.05 | 13.2 | 22 | 4.02 | 0.110 | 0.01182 | 0.004 | |
| 200 | 19 | 15.05 | 13.2 | 16 | 4.02 | 0.010 | 0.01182 | 0.001 | |
| 24 hrs | | | | | | | | | |

Bore/depth : BH-14 / -0.00 s/d -1.00 m LWS



Visual description : Sand and coral/shells, brown, trace silt, trace clay
Soil classification (USCS) : SM

GRAIN SIZE DISTRIBUTION

-Project : Pengembangan Pelabuhan Benoa Bali
Location : Pelabuhan Benoa Bali

Sieve Analysis

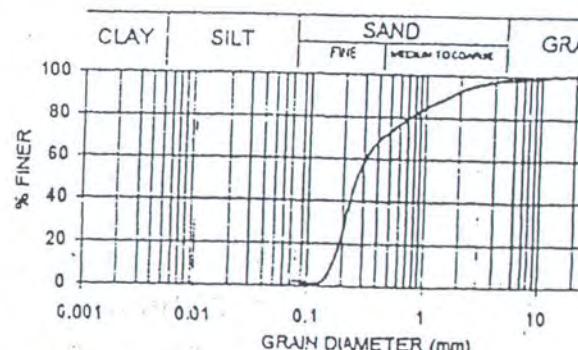
| Sieve opening No | mean (mm) | mean weight gr | % retained | Cumulative % retained | % finer |
|---------------------|--------------|----------------------|---------------|--------------------------|------------|
| 1.5* | 39.100 | 0.00 | 0.00 | 0.00 | 100.00 |
| 1.0* | 25.400 | 0.00 | 0.00 | 0.00 | 100.00 |
| 3/4 | 13.000 | 0.00 | 0.00 | 0.00 | 100.00 |
| 3/8 | 9.500 | 13.74 | 1.13 | 1.19 | 98.81 |
| 4 | 4.750 | 12.13 | 1.05 | 2.24 | 97.76 |
| 9 | 2.360 | 38.74 | 3.35 | 5.59 | 94.41 |
| 16 | 1.160 | 92.80 | 8.01 | 13.50 | 86.40 |
| 30 | 0.600 | 117.37 | 10.21 | 23.30 | 76.20 |
| 50 | 0.300 | 108.70 | 17.08 | 41.39 | 56.31 |
| 100 | 0.150 | 515.50 | 53.23 | 94.31 | 5.08 |
| 200 | 0.075 | 32.70 | 2.93 | 97.74 | 2.28 |
| TOTAL | | 1129.88 | 37.74 | - | - |
| TOTAL SAMPLE gr | | 1156 | | | |

Hydrometer

| Time (min) | Actual Hyd (F1) | Corr Hyd (Fc) | Effective depth L (cm) | Hyd Corr only for meniscus (F) | % finer | Lt | K | D, mm |
|---------------|--------------------|------------------|------------------------------|--------------------------------------|---------|----|---|-------|
| 0.25 | | | | | | | | |
| 0.5 | | | | | | | | |
| 1 | | | | | | | | |
| 2 | | | | | | | | |
| 3 | | | | | | | | |
| 4 | | | | | | | | |
| 8 | | | | | | | | |
| 10 | | | | | | | | |
| 20 | | | | | | | | |
| 30 | | | | | | | | |
| 50 | | | | | | | | |
| 100 | | | | | | | | |
| 200 | | | | | | | | |
| 24 hrs | | | | | | | | |

No Test

Bore/depth : BH-17 / -1.00 s/d -2.00 m LWS



Visual description : Sand, brown, trace shells, trace silt.
Soil classification (USCS) : SP

GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali
Location : Pelabuhan Benoa Bali

Sieve Analysis

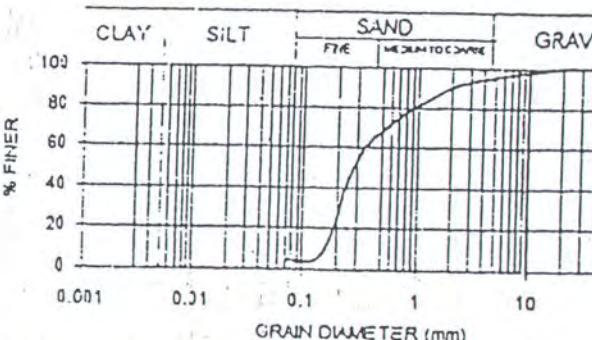
| Sieve opening No | mean (mm) | mean weight gr | % retained | Cumulative % retained | % finer |
|---------------------|--------------|----------------------|---------------|--------------------------|------------|
| 1.5* | 39.100 | 0.00 | 0.00 | 0.00 | 100.00 |
| 1.0* | 25.400 | 0.00 | 0.00 | 0.00 | 100.00 |
| 3/4 | 13.000 | 0.00 | 0.00 | 0.00 | 100.00 |
| 3/8 | 9.500 | 25.89 | 2.14 | 2.14 | 97.86 |
| 4 | 4.750 | 32.36 | 2.70 | 4.24 | 95.16 |
| 9 | 2.360 | 15.67 | 3.91 | 8.14 | 91.36 |
| 16 | 1.160 | 39.53 | 8.23 | 18.34 | 83.06 |
| 30 | 0.600 | 136.29 | 11.42 | 29.35 | 71.65 |
| 50 | 0.300 | 223.58 | 18.03 | 46.29 | 53.02 |
| 100 | 0.150 | 549.59 | 45.10 | 92.78 | 7.22 |
| 200 | 0.075 | 33.08 | 2.81 | 95.59 | 4.41 |
| TOTAL | | 1147.08 | 35.9 | - | - |
| TOTAL SAMPLE gr | | 1200 | | | |

Hydrometer

| Time (min) | Actual Hyd (F1) | Corr Hyd (Fc) | Effective depth L (cm) | Hyd Corr only for meniscus (F) | % finer | Lt | K | D, mm |
|---------------|--------------------|------------------|------------------------------|--------------------------------------|---------|----|---|-------|
| 0.25 | | | | | | | | |
| 0.5 | | | | | | | | |
| 1 | | | | | | | | |
| 2 | | | | | | | | |
| 3 | | | | | | | | |
| 8 | | | | | | | | |
| 10 | | | | | | | | |
| 20 | | | | | | | | |
| 30 | | | | | | | | |
| 50 | | | | | | | | |
| 100 | | | | | | | | |
| 200 | | | | | | | | |
| 24 hrs | | | | | | | | |

No Test

Bore/depth : BH-17 / -3.00 s/d -4.00 m LWS



Visual description : Sand brown, trace shells, trace silt.
Soil classification (USCS) : SP



GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali

Location : Pelabuhan Benoa Bali

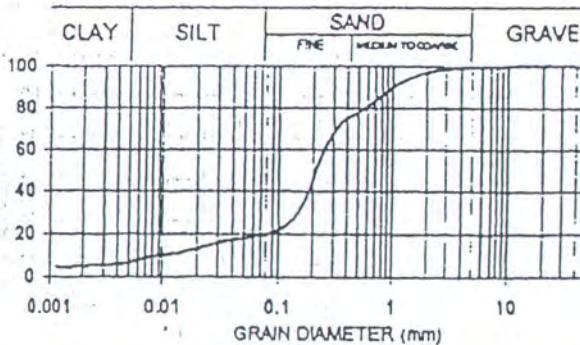
Sieve Analysis

| Sieve opening No. | (mm) | mean weight gr | % retained | Cumulative % | % finer |
|----------------------|--------|----------------------|---------------|-----------------|------------|
| | | gr | % retained | finer | |
| 1.5* | 38.100 | 0.00 | 0.00 | 0.00 | 100.00 |
| 1.0* | 25.400 | 0.03 | 0.00 | 0.00 | 100.00 |
| 3/4 | 19.000 | 0.03 | 0.03 | 0.00 | 100.00 |
| 3/8 | 9.500 | 0.03 | 0.00 | 0.00 | 100.00 |
| 4 | 4.750 | 3.14 | 0.35 | 0.35 | 99.85 |
| 8 | 2.380 | 18.20 | 1.79 | 2.13 | 97.87 |
| 16 | 1.180 | 52.00 | 5.79 | 7.91 | 92.09 |
| 30 | 0.600 | 108.60 | 11.71 | 19.62 | 80.38 |
| 50 | 0.300 | 112.30 | 12.34 | 31.36 | 86.04 |
| 100 | 0.150 | 348.40 | 38.07 | 70.03 | 29.97 |
| 200 | 0.075 | 36.85 | 10.64 | 90.37 | 16.33 |
| TOTAL | | 734.39 | 20.67 | - | - |
| TOTAL SAMPLE, gr | | 910 | | | |

Hydrometer

| Time (min) | Actual Hyd. (R _a) | Corr. Hyd. (R _c) | Effective depth L (cm) | Hyd. Corr. only for meniscus (R) | % finer | LA | K | D, mm |
|---------------|----------------------------------|---------------------------------|------------------------------|--|---------|--------|-------|-------|
| | | | | | | L | LA | K |
| 0.25 | 53 | 50.05 | 7.4 | 54 | 19.18 | 29.800 | 0.012 | 0.065 |
| 0.5 | 50 | 47.05 | 7.3 | 51 | 18.01 | 16.800 | 0.012 | 0.048 |
| 1 | 47 | 44.05 | 8.4 | 48 | 18.08 | 8.400 | 0.012 | 0.035 |
| 2 | 42 | 39.05 | 9.2 | 43 | 14.85 | 4.800 | 0.012 | 0.028 |
| 3 | 39 | 35.05 | 9.7 | 40 | 13.80 | 3.233 | 0.012 | 0.022 |
| 4 | 38 | 32.05 | 10.2 | 37 | 12.85 | 2.550 | 0.012 | 0.019 |
| 8 | 33 | 30.05 | 10.7 | 34 | 11.50 | 1.338 | 0.012 | 0.014 |
| 16 | 30 | 27.05 | 11.2 | 31 | 10.35 | 0.700 | 0.012 | 0.010 |
| 30 | 27 | 24.05 | 11.7 | 28 | 9.21 | 0.390 | 0.012 | 0.007 |
| 50 | 22 | 16.05 | 12.5 | 23 | 7.29 | 0.208 | 0.012 | 0.005 |
| 100 | 19 | 15.05 | 13.2 | 19 | 5.76 | 0.110 | 0.012 | 0.004 |
| 200 | 18 | 15.05 | 13.0 | 18 | 9.07 | 0.108 | 0.012 | 0.004 |
| 24 hrs | 14 | 11.05 | 13.8 | 15 | 4.23 | 0.010 | 0.012 | 0.001 |

Bore/depth : BH-17 / -4.20 s/d -5.00 m LWS



Visual description : Sand, brownish grey, trace shells, little silt, trace clay
Soil classification (USCS) : SM

GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali

Location : Pelabuhan Benoa Bali

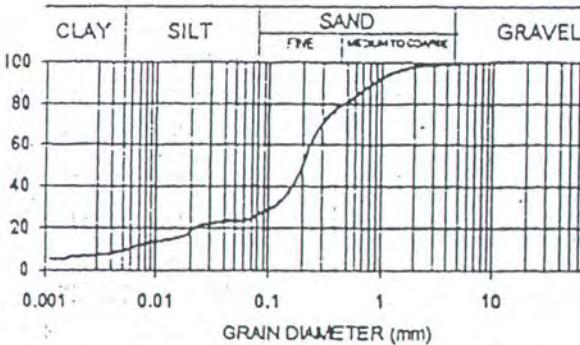
Sieve Analysis

| Sieve opening No. | (mm) | mean weight gr | % retained | Cumulative % | % finer |
|----------------------|--------|----------------------|---------------|-----------------|------------|
| | | gr | % retained | finer | |
| 1.5* | 33.100 | 0.00 | 0.03 | 0.00 | 100.00 |
| 1.0* | 25.400 | 0.03 | 0.03 | 0.10 | 100.00 |
| 3/4 | 19.000 | 0.03 | 0.03 | 0.00 | 100.00 |
| 3/8 | 9.500 | 2.43 | 0.23 | 0.20 | 99.80 |
| 4 | 4.750 | 2.63 | 0.22 | 0.42 | 99.58 |
| 8 | 2.380 | 11.96 | 1.03 | 1.41 | 98.59 |
| 16 | 1.180 | 54.12 | 4.51 | 5.92 | 94.08 |
| 30 | 0.600 | 125.30 | 10.47 | 16.39 | 83.81 |
| 50 | 0.300 | 182.30 | 13.58 | 29.37 | 70.04 |
| 100 | 0.150 | 401.11 | 33.43 | 53.39 | 38.81 |
| 200 | 0.075 | 130.75 | 10.90 | 74.29 | 25.71 |
| TOTAL | | 891.44 | 74.19 | - | - |
| TOTAL SAMPLE, gr | | 1200 | | | |

Hydrometer

| Time (min) | Actual Hyd. (R _a) | Corr. Hyd. (R _c) | Effective depth L (cm) | Hyd. Corr. only for meniscus (R) | % finer | LA | K | D, mm |
|---------------|----------------------------------|---------------------------------|------------------------------|--|---------|--------|---------|-------|
| | | | | | | L | LA | K |
| 0.25 | 51 | 48.05 | 7.8 | 52 | 24.17 | 31.200 | 0.01178 | 0.068 |
| 0.5 | 50 | 47.05 | 7.3 | 51 | 23.68 | 16.800 | 0.01178 | 0.047 |
| 1 | 48 | 44.05 | 8.3 | 49 | 22.68 | 8.300 | 0.01178 | 0.034 |
| 2 | 45 | 42.05 | 8.9 | 46 | 21.15 | 4.400 | 0.01178 | 0.025 |
| 3 | 41 | 38.05 | 9.4 | 42 | 19.14 | 3.133 | 0.01178 | 0.021 |
| 4 | 37 | 34.05 | 10.1 | 38 | 17.13 | 2.525 | 0.01178 | 0.019 |
| 8 | 33 | 30.05 | 10.7 | 34 | 15.11 | 1.338 | 0.01178 | 0.014 |
| 16 | 30 | 27.05 | 11.2 | 31 | 13.60 | 0.700 | 0.01178 | 0.010 |
| 30 | 27 | 24.05 | 11.7 | 28 | 12.10 | 0.390 | 0.01178 | 0.007 |
| 50 | 22 | 16.05 | 12.5 | 23 | 9.58 | 0.208 | 0.01178 | 0.005 |
| 100 | 18 | 15.05 | 13.0 | 19 | 9.07 | 0.108 | 0.01178 | 0.004 |
| 200 | 14 | 11.05 | 13.8 | 15 | 5.56 | 0.010 | 0.01178 | 0.001 |

Bore/depth : BH-17 / -6.00 s/d -7.00 m LWS



Visual description : Sand, brownish grey, little silt, trace clay, trace shells
Soil classification (USCS) : SM

GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali

Location : Pelabuhan Benoa Bali

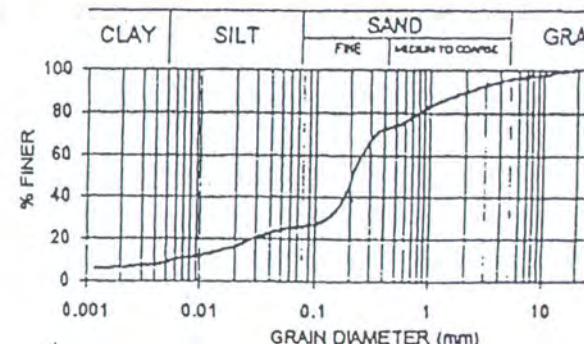
Sieve Analysis

| Sieve opening No (mm) | mean gr | mean | % | Cumulative | % |
|--------------------------|------------|---------------|--------------|------------|--------|
| | | retained | % retained | finer | |
| 1.5* | 38.100 | 0.00 | 0.00 | 0.00 | 100.00 |
| 1.0* | 25.400 | 0.00 | 0.00 | 0.00 | 100.00 |
| 3/4 | 13.000 | 0.00 | 0.00 | 0.00 | 100.00 |
| 3/8 | 9.500 | 19.30 | 2.57 | 2.57 | 97.43 |
| 4 | 4.750 | 17.12 | 2.28 | 4.86 | 95.14 |
| 8 | 2.360 | 34.58 | 4.81 | 9.48 | 80.54 |
| 16 | 1.180 | 43.00 | 5.73 | 15.20 | 84.80 |
| 30 | 0.600 | 57.80 | 9.01 | 24.21 | 75.79 |
| 50 | 0.300 | 37.72 | 9.03 | 33.24 | 86.76 |
| 100 | 0.150 | 250.40 | 33.09 | 68.63 | 33.37 |
| 200 | 0.075 | 58.14 | 7.43 | 74.11 | 24.98 |
| TOTAL | | 556.34 | 74.11 | | |
| TOTAL SAMPLE gr | | 750 | | | |

Hydrometer

| Time (min) | Actual Hyd. (R _a) | Corr. Hyd. (P _c) | Effective depth L (cm) | Hyd. Cor. only for meniscus (R) | % finer | U _f | K | D, mm |
|---------------|----------------------------------|---------------------------------|------------------------------|---------------------------------------|---------|----------------|---------|-------|
| | | | | | | L _f | | |
| 0.25 | 53 | 50.05 | 7.4 | 54 | 25.78 | 29.800 | 0.01208 | 0.066 |
| 0.5 | 50 | 47.05 | 7.9 | 51 | 24.21 | 15.800 | 0.01208 | 0.048 |
| 1 | 48 | 43.05 | 8.6 | 47 | 22.16 | 8.800 | 0.01208 | 0.035 |
| 2 | 41 | 38.05 | 9.4 | 42 | 19.58 | 4.700 | 0.01208 | 0.026 |
| 3 | 37 | 34.05 | 10.1 | 38 | 17.52 | 3.387 | 0.01208 | 0.022 |
| 4 | 34 | 31.05 | 10.5 | 35 | 15.98 | 2.826 | 0.01208 | 0.020 |
| 8 | 31 | 28.05 | 11.1 | 32 | 14.44 | 1.388 | 0.01208 | 0.014 |
| 16 | 27 | 24.05 | 11.7 | 28 | 12.38 | 0.731 | 0.01208 | 0.010 |
| 30 | 25 | 22.05 | 12 | 28 | 11.35 | 0.400 | 0.01208 | 0.009 |
| 50 | 22 | 19.05 | 12.5 | 23 | 9.80 | 0.208 | 0.01208 | 0.008 |
| 100 | 18 | 15.05 | 13.2 | 19 | 7.75 | 0.110 | 0.01208 | 0.004 |
| 200 | 15 | 12.05 | 13.8 | 15 | 5.99 | 0.010 | 0.01208 | 0.001 |
| 24 hrs | 14 | 11.05 | 12.8 | 14 | 5.09 | 0.010 | 0.01208 | 0.001 |

Bore/depth : BH-17 / -8.00 s/d -9.00 m LWS



Visual description : Sand, brownish gray, little silt, trace clay, trace s.

Soil classification (USCS) : SM

GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali

Location : Pelabuhan Benoa Bali

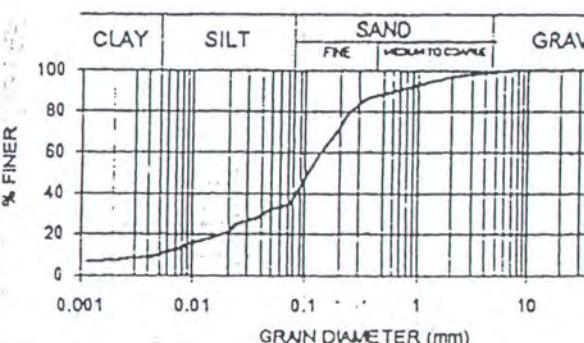
Sieve Analysis

| Sieve opening No (mm) | mean gr | mean | % | Cumulative | % |
|--------------------------|------------|---------------|--------------|------------|--------|
| | | retained | % retained | finer | |
| 1.5* | 33.100 | 0.00 | 0.00 | 0.00 | 100.00 |
| 1.0* | 25.400 | 0.00 | 0.00 | 0.00 | 100.00 |
| 3/4 | 13.000 | 0.00 | 0.00 | 0.00 | 100.00 |
| 3/8 | 9.500 | 0.00 | 0.00 | 0.00 | 100.00 |
| 4 | 4.750 | 3.83 | 0.45 | 0.45 | 98.55 |
| 8 | 2.360 | 18.47 | 2.08 | 2.51 | 97.40 |
| 16 | 1.180 | 30.85 | 3.83 | 6.37 | 93.64 |
| 30 | 0.600 | 35.41 | 4.43 | 10.79 | 86.21 |
| 50 | 0.300 | 45.83 | 5.73 | 18.52 | 82.48 |
| 100 | 0.150 | 164.70 | 20.59 | 37.11 | 82.89 |
| 200 | 0.075 | 214.40 | 27.68 | 84.78 | 91.22 |
| TOTAL | | 518.26 | 34.78 | | |
| TOTAL SAMPLE gr | | 900 | | | |

Hydrometer

| Time (min) | Actual Hyd. (R _a) | Corr. Hyd. (P _c) | Effective depth L (cm) | Hyd. Cor. only for meniscus (R) | % finer | U _f | K | D, mm |
|---------------|----------------------------------|---------------------------------|------------------------------|---------------------------------------|---------|----------------|--------|-------|
| | | | | | | L _f | | |
| 0.25 | 52 | 49.05 | 7.8 | 53 | 33.88 | 30.400 | 0.0118 | 0.065 |
| 0.5 | 49 | 46.05 | 9.1 | 50 | 31.70 | 15.200 | 0.0118 | 0.047 |
| 1 | 45 | 40.05 | 9.1 | 44 | 27.85 | 9.100 | 0.0118 | 0.038 |
| 2 | 40 | 37.05 | 9.8 | 41 | 25.57 | 4.800 | 0.0118 | 0.028 |
| 3 | 36 | 33.05 | 10.2 | 37 | 22.87 | 3.400 | 0.0118 | 0.022 |
| 4 | 33 | 30.05 | 10.7 | 34 | 20.74 | 2.875 | 0.0118 | 0.019 |
| 8 | 29 | 28.05 | 11.4 | 30 | 17.80 | 1.425 | 0.0118 | 0.014 |
| 16 | 25 | 23.05 | 11.9 | 27 | 15.97 | 0.744 | 0.0118 | 0.010 |
| 30 | 22 | 19.05 | 12.5 | 23 | 13.15 | 0.417 | 0.0118 | 0.008 |
| 50 | 20 | 18.05 | 13 | 20 | 11.08 | 0.217 | 0.0118 | 0.005 |
| 100 | 18 | 13.05 | 13.5 | 17 | 9.01 | 0.112 | 0.0118 | 0.004 |
| 200 | 15 | 10.05 | 14 | 14 | 8.04 | 0.010 | 0.0118 | 0.001 |
| 24 hrs | 13 | 10.05 | 14 | 14 | 8.04 | 0.010 | 0.0118 | 0.001 |

Bore/depth : BH-17 / -10.50 s/d -11.00 m LWS



Visual description : Sand, grey, little silt, trace clay, trace shells.

Soil classification (USCS) : SM

GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali

Location : Pelabuhan Benoa Bali

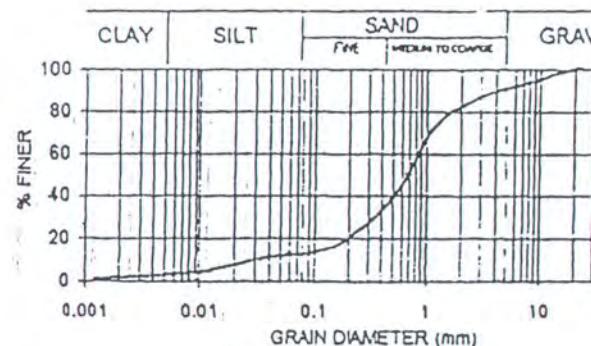
Sieve Analysis

| Sieve opening No. | mean (mm) | weight gr | % retained | Cumulative % retained | % finer |
|----------------------|--------------|--------------|------------|-----------------------|---------|
| 1.5* | 38.100 | 0.00 | 0.00 | 0.00 | 100.00 |
| 1.0* | 25.400 | 0.00 | 0.00 | 0.00 | 100.00 |
| 3/4 | 19.000 | 0.00 | 0.00 | 0.00 | 100.00 |
| 3/8 | 9.500 | 68.10 | 5.20 | 5.20 | 94.80 |
| 4 | 4.750 | 54.90 | 4.32 | 9.53 | 90.47 |
| 8 | 2.380 | 72.20 | 5.89 | 15.21 | 84.79 |
| 16 | 1.180 | 145.40 | 11.45 | 26.56 | 72.34 |
| 30 | 0.600 | 284.30 | 28.09 | 55.35 | 44.85 |
| 50 | 0.300 | 222.35 | 17.51 | 72.35 | 27.15 |
| 100 | 0.150 | 135.30 | 10.65 | 83.51 | 16.49 |
| 200 | 0.075 | 51.24 | 4.03 | 87.54 | 11.46 |
| TOTAL | | 1111.79 | 37.54 | - | - |
| TOTAL SAMPLE, gr: | | 1270 | | | |

Hydrometer

| Time (min) | Actual Hyd (P _a) | Corr. Hyd (P _c) | Effective depth L (cm) | Hyd. Corr only for meniscus (R) | % finer | U _f | K | D, mm |
|---------------|---------------------------------|--------------------------------|------------------------------|---------------------------------------|---------|----------------|---------|-------|
| 0.25 | 53 | 50.05 | 7.4 | 54 | 12.30 | 29.800 | 0.01192 | 0.065 |
| 0.5 | 51 | 48.05 | 7.8 | 52 | 11.80 | 14.600 | 0.01182 | 0.047 |
| 1 | 46 | 43.05 | 8.8 | 47 | 10.58 | 8.800 | 0.01192 | 0.035 |
| 2 | 41 | 38.05 | 9.4 | 42 | 9.35 | 4.700 | 0.01192 | 0.028 |
| 3 | 38 | 31.05 | 10.2 | 37 | 8.12 | 3.400 | 0.01192 | 0.022 |
| 4 | 33 | 20.05 | 10.7 | 34 | 7.38 | 2.875 | 0.01192 | 0.019 |
| 8 | 28 | 25.05 | 11.5 | 29 | 6.15 | 1.438 | 0.01192 | 0.014 |
| 16 | 22 | 19.05 | 12.5 | 23 | 4.88 | 0.781 | 0.01192 | 0.011 |
| 30 | 18 | 16.05 | 13 | 20 | 3.04 | 0.433 | 0.01192 | 0.008 |
| 60 | 16 | 13.05 | 13.5 | 17 | 3.21 | 0.225 | 0.01192 | 0.006 |
| 120 | 14 | 11.05 | 13.8 | 15 | 2.71 | 0.115 | 0.01192 | 0.004 |
| 24 hrs | 7 | 4.05 | 15 | 9 | 0.89 | 0.010 | 0.01192 | 0.001 |

Bore/depth : BH-18 / -2.00 s/d -3.00 m LWS



Visual description : Sand, brownish grey, little silt, trace clay, trace coral shells
Soil classification (USCS) : SM

GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali

Location : Pelabuhan Benoa Bali

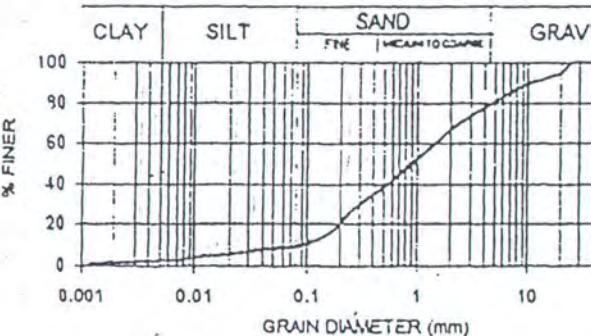
Sieve Analysis

| Sieve opening No. | mean (mm) | weight gr | % retained | Cumulative % retained | % finer |
|----------------------|--------------|--------------|------------|-----------------------|---------|
| 1.5* | 38.100 | 0.00 | 0.00 | 0.00 | 100.00 |
| 1.0* | 25.400 | 0.00 | 0.00 | 0.00 | 100.00 |
| 3/4 | 19.000 | 53.50 | 5.62 | 5.62 | 94.38 |
| 3/8 | 9.500 | 34.03 | 5.87 | 11.29 | 88.71 |
| 4 | 4.750 | 101.50 | 8.93 | 20.27 | 79.73 |
| 8 | 2.380 | 113.40 | 10.04 | 30.30 | 69.70 |
| 16 | 1.180 | 153.70 | 13.50 | 43.31 | 56.09 |
| 30 | 0.600 | 162.50 | 14.59 | 58.29 | 41.71 |
| 50 | 0.300 | 138.40 | 12.07 | 70.36 | 26.94 |
| 100 | 0.150 | 172.50 | 15.27 | 85.32 | 14.38 |
| 200 | 0.075 | 97.40 | 5.95 | 91.39 | 8.41 |
| TOTAL | | 134.93 | 31.59 | - | - |
| TOTAL SAMPLE, gr: | | 1130 | | | |

Hydrometer

| Time (min) | Actual Hyd (P _a) | Corr. Hyd (P _c) | Effective depth L (cm) | Hyd. Corr only for meniscus (R) | % finer | U _f | K | D, mm |
|---------------|---------------------------------|--------------------------------|------------------------------|---------------------------------------|---------|----------------|---------|-------|
| 0.25 | 53 | 50.05 | 7.4 | 54 | 8.32 | 28.800 | 0.01196 | 0.065 |
| 0.5 | 51 | 48.05 | 7.9 | 52 | 7.99 | 15.800 | 0.01186 | 0.047 |
| 1 | 48 | 45.05 | 9.3 | 48 | 7.49 | 8.300 | 0.01196 | 0.034 |
| 2 | 41 | 38.05 | 9.4 | 42 | 8.03 | 4.700 | 0.01196 | 0.026 |
| 3 | 38 | 31.05 | 9.9 | 38 | 5.83 | 3.300 | 0.01196 | 0.022 |
| 4 | 34 | 21.05 | 10.5 | 35 | 5.16 | 2.825 | 0.01196 | 0.019 |
| 8 | 31 | 28.05 | 11.1 | 32 | 4.86 | 1.286 | 0.01196 | 0.014 |
| 16 | 27 | 24.05 | 11.7 | 29 | 4.00 | 0.731 | 0.01196 | 0.010 |
| 30 | 23 | 20.05 | 12.4 | 24 | 3.33 | 0.413 | 0.01196 | 0.009 |
| 60 | 20 | 17.05 | 12.9 | 21 | 2.83 | 0.215 | 0.01196 | 0.008 |
| 120 | 17 | 14.05 | 13.3 | 18 | 2.34 | 0.111 | 0.01128 | 0.004 |
| 24 hrs | 10 | 7.05 | 14.5 | 11 | 1.17 | 0.010 | 0.01196 | 0.001 |

Bore/depth : BH-18 / -4.00 s/d -5.00 m LWS



Visual description : Sand, brownish grey, little coral shells, trace silt, trace clay
Soil classification (USCS) : SP-SM

Project : Pengembangan Pelabuhan Benoa Bali
 Location : Pelabuhan Benoa Bali

Sieve Analysis

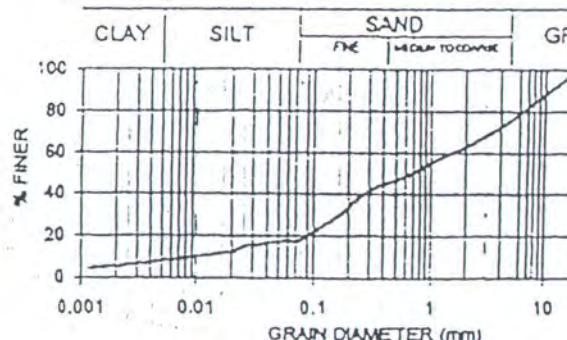
| Sieve opening No. (mm) | mean gr | mean | % | Cumulative % | % |
|---------------------------|------------|----------|------------|-----------------|--------|
| | | retained | % retained | finer | |
| 1.5* | 33.100 | 0.03 | 0.03 | 0.00 | 100.00 |
| 1.0* | 25.400 | 0.03 | 0.03 | 0.00 | 100.00 |
| 3/4 | 13.000 | 15.80 | 1.21 | 1.21 | 98.09 |
| 3/8 | 9.500 | 140.20 | 11.59 | 12.39 | 97.11 |
| 4 | 4.750 | 148.20 | 12.25 | 25.14 | 74.86 |
| 8 | 2.360 | 120.21 | 9.92 | 25.36 | 84.94 |
| 16 | 1.180 | 94.84 | 7.84 | 12.30 | 57.10 |
| 32 | 0.600 | 102.20 | 8.45 | 51.24 | 48.66 |
| 50 | 0.300 | 33.50 | 8.93 | 59.24 | 41.76 |
| 100 | 0.150 | 159.20 | 13.16 | 71.40 | 26.80 |
| 200 | 0.075 | 132.40 | 10.94 | 82.34 | 17.86 |
| TOTAL | 996.35 | 32.04 | - | - | - |
| TOTAL SAMPLE gr | 1210 | | | | |

Hydrometer

| Time (min) | Actual Hyd. | | Corr. Hyd. depth (cm) | Effective Hyd. Corr. only for mercuric (R) | % finer | LA | K | D, mm |
|---------------|----------------|-----------------|-----------------------------|---|---------|--------|---------|-------|
| | reading (R) | reading (Pc) | | | | | | |
| | L (cm) | mercuric (R) | | | | | | |
| 0.25 | 53 | 50.05 | 7.4 | 54 | 17.53 | 26.800 | 0.01204 | 0.066 |
| 0.5 | 51 | 48.05 | 7.9 | 52 | 18.83 | 15.800 | 0.01204 | 0.048 |
| 1 | 48 | 45.05 | 8.3 | 49 | 15.78 | 8.300 | 0.01204 | 0.035 |
| 2 | 45 | 42.05 | 9.2 | 46 | 14.73 | 4.400 | 0.01204 | 0.025 |
| 3 | 40 | 37.05 | 9.8 | 41 | 12.98 | 3.200 | 0.01204 | 0.022 |
| 4 | 37 | 34.05 | 10.1 | 38 | 11.93 | 2.525 | 0.01204 | 0.019 |
| 9 | 35 | 32.05 | 10.4 | 36 | 11.23 | 1.300 | 0.01204 | 0.014 |
| 16 | 32 | 29.05 | 10.9 | 33 | 10.18 | 0.881 | 0.01204 | 0.010 |
| 30 | 29 | 26.05 | 11.4 | 30 | 9.13 | 0.380 | 0.01204 | 0.007 |
| 50 | 26 | 23.05 | 11.9 | 27 | 8.07 | 0.186 | 0.01204 | 0.005 |
| 120 | 24 | 21.05 | 12.2 | 25 | 7.37 | 0.102 | 0.01204 | 0.004 |
| 24 hrs | 14 | 11.05 | 13.8 | 15 | 3.87 | 0.010 | 0.01204 | 0.001 |

GRAIN SIZE DISTRIBUTION

Bore/depth : BH-18 / -8.00 s/b -7.00 m LWS



Project : Pengembangan Pelabuhan Benoa Bali
 Location : Pelabuhan Benoa Bali

Sieve Analysis

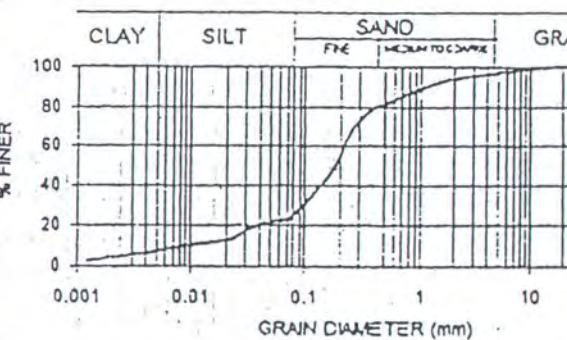
| Sieve opening No. (mm) | mean gr | mean | % | Cumulative % | % |
|---------------------------|------------|----------|------------|-----------------|--------|
| | | retained | % retained | finer | |
| 1.5* | 33.100 | 0.03 | 0.03 | 0.00 | 100.00 |
| 1.0* | 25.400 | 0.03 | 0.03 | 0.00 | 100.00 |
| 3/4 | 13.000 | 0.03 | 0.03 | 0.00 | 100.00 |
| 3/8 | 9.500 | 15.32 | 1.17 | 1.17 | 98.83 |
| 4 | 4.750 | 28.99 | 2.22 | 3.40 | 98.80 |
| 8 | 2.360 | 27.00 | 2.07 | 5.46 | 94.54 |
| 16 | 1.180 | 52.34 | 4.01 | 9.46 | 90.52 |
| 32 | 0.600 | 39.35 | 6.65 | 16.32 | 83.88 |
| 50 | 0.300 | 139.39 | 10.72 | 27.24 | 72.96 |
| 100 | 0.150 | 199.58 | 30.62 | 57.35 | 42.34 |
| 200 | 0.075 | 245.23 | 19.79 | 76.45 | 23.55 |
| TOTAL | 997.38 | 76.43 | - | - | - |
| TOTAL SAMPLE gr | 1305 | | | | |

Hydrometer

| Time (min) | Actual Hyd. | | Corr. Hyd. depth (cm) | Effective Hyd. Corr. only for mercuric (R) | % finer | LA | K | D, mm |
|---------------|----------------|-----------------|-----------------------------|---|---------|--------|---------|-------|
| | reading (R) | reading (Pc) | | | | | | |
| | L (cm) | mercuric (R) | | | | | | |
| 0.25 | 53 | 50.05 | 7.4 | 54 | 17.53 | 26.800 | 0.01224 | 0.066 |
| 0.5 | 51 | 48.05 | 7.9 | 52 | 18.83 | 15.800 | 0.01224 | 0.048 |
| 1 | 48 | 45.05 | 8.3 | 49 | 15.78 | 8.300 | 0.01224 | 0.035 |
| 2 | 45 | 42.05 | 9.2 | 46 | 14.73 | 4.400 | 0.01224 | 0.025 |
| 3 | 40 | 37.05 | 9.8 | 41 | 12.98 | 3.200 | 0.01224 | 0.022 |
| 4 | 37 | 34.05 | 10.1 | 38 | 11.93 | 2.525 | 0.01224 | 0.019 |
| 9 | 35 | 32.05 | 10.4 | 36 | 11.23 | 1.300 | 0.01224 | 0.014 |
| 16 | 32 | 29.05 | 10.9 | 33 | 10.18 | 0.881 | 0.01224 | 0.010 |
| 30 | 29 | 26.05 | 11.4 | 30 | 9.13 | 0.380 | 0.01224 | 0.007 |
| 50 | 26 | 23.05 | 11.9 | 27 | 8.07 | 0.186 | 0.01224 | 0.005 |
| 120 | 24 | 21.05 | 12.2 | 25 | 7.37 | 0.102 | 0.01224 | 0.004 |
| 24 hrs | 14 | 11.05 | 13.8 | 15 | 3.87 | 0.010 | 0.01224 | 0.001 |

GRAIN SIZE DISTRIBUTION

Bore/depth : BH-18 / -9.00 s/d -10.00 m LWS



GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali

Location : Pelabuhan Benoa Bali

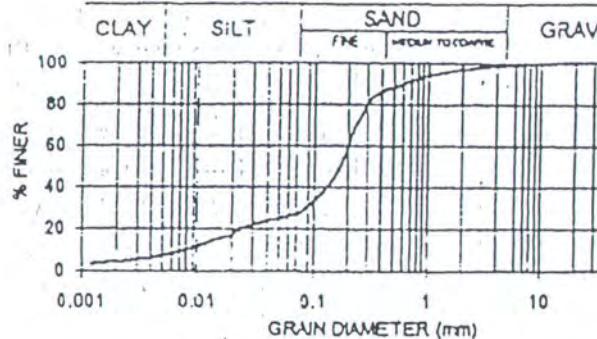
Sieve Analysis

| Sieve opening No | mean (mm) | weight gr | % retained | Cumulative % retained | % finer |
|---------------------|--------------|--------------|---------------|--------------------------|------------|
| 1.5* | 33.100 | 0.03 | 0.03 | 0.00 | 100.00 |
| 1.0* | 25.400 | 0.03 | 0.03 | 0.00 | 100.00 |
| 3/4 | 19.000 | 0.03 | 0.03 | 0.00 | 100.00 |
| 3/8 | 9.500 | 5.02 | 0.40 | 0.40 | 98.60 |
| 2 | 4.750 | 10.74 | 0.87 | 1.27 | 98.73 |
| 3 | 2.360 | 17.90 | 1.44 | 2.71 | 97.28 |
| 5 | 1.180 | 29.74 | 2.40 | 5.11 | 94.88 |
| 10 | 0.500 | 32.20 | 5.02 | 10.13 | 89.87 |
| 20 | 0.300 | 118.30 | 9.33 | 19.51 | 80.49 |
| 50 | 0.150 | 448.15 | 35.98 | 56.49 | 44.51 |
| 100 | 0.075 | 209.35 | 16.93 | 72.42 | 27.58 |
| TOTAL | | 898.30 | 72.42 | - | - |
| TOTAL SAMPLE gr | | 1240 | | | |

Hydrometer

| Time (min) | Actual Hyd. (P) | Corr Hyd. (Pc) | Effective depth L (cm) | Hyc Corr meritius (P) | % Finer | U1 | U2 | D. mm |
|---------------|--------------------|-------------------|------------------------------|--------------------------|---------|--------|---------|-------|
| 0.25 | 50 | 50.05 | 7.4 | 54 | 28.85 | 25.800 | 0.01173 | 0.064 |
| 0.5 | 49 | 48.05 | 9.1 | 50 | 24.70 | 16.200 | 0.01176 | 0.047 |
| 1 | 48 | 47.05 | 8.8 | 47 | 23.18 | 8.800 | 0.01178 | 0.034 |
| 2 | 41 | 38.05 | 9.4 | 42 | 20.49 | 4.700 | 0.01175 | 0.025 |
| 3 | 38 | 35.05 | 9.9 | 38 | 18.87 | 3.300 | 0.01178 | 0.021 |
| 4 | 34 | 31.05 | 10.5 | 35 | 18.72 | 2.825 | 0.01178 | 0.019 |
| 8 | 31 | 29.05 | 11.1 | 32 | 15.10 | 1.388 | 0.01175 | 0.014 |
| 16 | 25 | 22.05 | 12 | 26 | 11.87 | 0.750 | 0.01175 | 0.010 |
| 20 | 21 | 19.05 | 12.7 | 22 | 9.72 | 0.423 | 0.01178 | 0.008 |
| 20 | 17 | 14.05 | 13.3 | 19 | 7.56 | 0.222 | 0.01178 | 0.006 |
| 120 | 14 | 11.05 | 13.9 | 15 | 5.95 | 0.115 | 0.01178 | 0.004 |
| 24 hrs | 2 | 5.05 | 14.7 | 16 | 1.26 | 0.010 | 0.01178 | 0.001 |

Bore/depth : BH-18 / -11.00 s/d -12.00 m LWS



GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali

Location : Pelabuhan Benoa Bali

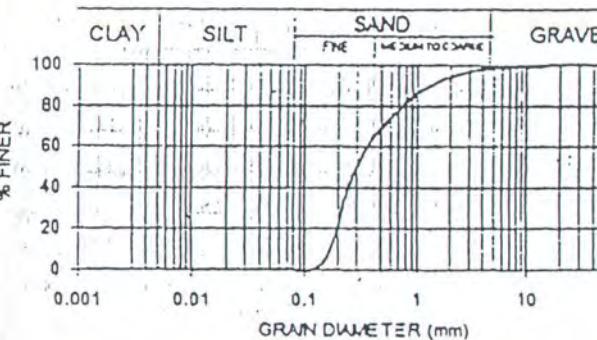
Sieve Analysis

| Sieve opening No | mean (mm) | weight gr | % retained | Cumulative % retained | % finer |
|---------------------|--------------|--------------|---------------|--------------------------|------------|
| 1.5* | 33.100 | 0.03 | 0.03 | 0.00 | 100.00 |
| 1.0* | 25.400 | 0.03 | 0.03 | 0.00 | 100.00 |
| 3/4 | 19.000 | 0.03 | 0.03 | 0.00 | 100.00 |
| 3/8 | 9.500 | 6.83 | 0.81 | 0.81 | 98.18 |
| 2 | 4.750 | 6.85 | 0.73 | 1.56 | 98.40 |
| 3 | 2.360 | 27.00 | 3.33 | 4.90 | 95.10 |
| 5 | 1.180 | 55.75 | 6.62 | 11.52 | 88.48 |
| 10 | 0.600 | 121.34 | 14.41 | 25.33 | 74.07 |
| 20 | 0.300 | 204.40 | 24.28 | 50.21 | 48.79 |
| 50 | 0.150 | 384.34 | 45.72 | 25.33 | 4.07 |
| 100 | 0.075 | 33.14 | 3.94 | 99.37 | 0.13 |
| TOTAL | | 940.32 | 99.87 | - | - |
| TOTAL SAMPLE gr | | 941.32 | | | |

Hydrometer

| Time (min) | Actual Hyd. (P) | Corr Hyd. (Pc) | Effective depth L (cm) | Hyc Corr meritius (P) | % Finer | U1 | U2 | D. mm |
|---------------|--------------------|-------------------|------------------------------|--------------------------|---------|--------|---------|-------|
| 0.25 | 50 | 50.05 | 7.4 | 54 | 28.85 | 25.800 | 0.01173 | 0.064 |
| 0.5 | 49 | 48.05 | 9.1 | 50 | 24.70 | 16.200 | 0.01176 | 0.047 |
| 1 | 48 | 47.05 | 8.8 | 47 | 23.18 | 8.800 | 0.01178 | 0.034 |
| 2 | 41 | 38.05 | 9.4 | 42 | 20.49 | 4.700 | 0.01175 | 0.025 |
| 3 | 38 | 35.05 | 9.9 | 38 | 18.87 | 3.300 | 0.01178 | 0.021 |
| 4 | 34 | 31.05 | 10.5 | 35 | 18.72 | 2.825 | 0.01178 | 0.019 |
| 8 | 31 | 29.05 | 11.1 | 32 | 15.10 | 1.388 | 0.01175 | 0.014 |
| 16 | 25 | 22.05 | 12 | 26 | 11.87 | 0.750 | 0.01175 | 0.010 |
| 20 | 21 | 19.05 | 12.7 | 22 | 9.72 | 0.423 | 0.01178 | 0.008 |
| 20 | 17 | 14.05 | 13.3 | 19 | 7.56 | 0.222 | 0.01178 | 0.006 |
| 120 | 14 | 11.05 | 13.9 | 15 | 5.95 | 0.115 | 0.01178 | 0.004 |
| 24 hrs | 2 | 5.05 | 14.7 | 16 | 1.26 | 0.010 | 0.01178 | 0.001 |

Bore/depth : BH-19 / -2.00 s/d -3.00 m LWS



GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali

Location : Pelabuhan Benoa Bali

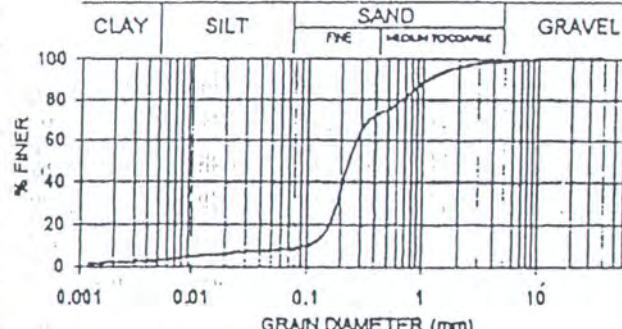
Sieve Analysis

| Sieve opening No. | mean (mm) | mean | % | Cumulative | % |
|----------------------|--------------|--------|----------|------------|--------|
| | | weight | retained | % retained | finer |
| | | gr | % | | |
| 1 | 4.100 | 0.00 | 0.00 | 0.00 | 100.00 |
| 10 | 25.400 | 0.00 | 0.00 | 0.00 | 100.00 |
| 24 | 19.700 | 0.00 | 0.00 | 0.00 | 100.00 |
| 30 | 9.500 | 1.54 | 0.18 | 0.18 | 98.82 |
| 4 | 4.750 | 7.20 | 0.83 | 1.00 | 99.00 |
| 8 | 2.360 | 19.80 | 2.28 | 3.28 | 98.72 |
| 16 | 1.180 | 48.84 | 5.81 | 8.23 | 91.11 |
| 30 | 0.600 | 115.73 | 13.20 | 22.20 | 77.80 |
| 50 | 0.300 | 119.00 | 13.60 | 25.29 | 84.21 |
| 100 | 0.150 | 407.04 | 46.79 | 82.58 | 17.42 |
| 200 | 0.075 | 79.44 | 9.13 | 91.71 | 8.28 |
| TOTAL | | 797.32 | 31.71 | - | - |
| TOTAL SAMPLE, gr | | 870 | - | - | - |

Bore/depth : BH-19 / -4.00 s/d -5.00 m LWS

Hydrometer

| Time (min) | Actual Hyd (Pc) | Corr. Hyd (Pc) | Effective | Hyo. Corr only for mercuric (P) | % finer | L | K | D, mm |
|---------------|--------------------|-------------------|-----------|---------------------------------------|---------|--------------|---------|-------|
| | | | depth | | | L (cm) | | |
| | | | reading | | | mercuric (P) | | |
| 0.25 | 53 | 50.05 | 7.4 | 54 | 8.28 | 26.800 | 0.01216 | 0.066 |
| 0.5 | 51 | 48.05 | 7.9 | 52 | 7.35 | 15.800 | 0.01216 | 0.048 |
| 1 | 48 | 45.05 | 9.3 | 49 | 7.45 | 8.300 | 0.01216 | 0.036 |
| 2 | 45 | 42.05 | 9.8 | 46 | 8.85 | 4.400 | 0.01216 | 0.028 |
| 3 | 40 | 37.05 | 9.6 | 41 | 5.13 | 3.200 | 0.01216 | 0.022 |
| 4 | 37 | 34.05 | 10.1 | 38 | 5.83 | 2.525 | 0.01216 | 0.019 |
| 8 | 33 | 30.05 | 10.7 | 34 | 4.87 | 1.338 | 0.01216 | 0.014 |
| 16 | 30 | 27.05 | 11.2 | 31 | 4.48 | 0.700 | 0.01216 | 0.010 |
| 30 | 27 | 24.05 | 11.7 | 28 | 1.98 | 0.390 | 0.01216 | 0.008 |
| 60 | 22 | 19.05 | 12.5 | 23 | 0.15 | 0.208 | 0.01216 | 0.008 |
| 120 | 18 | 15.05 | 13 | 20 | 0.06 | 0.108 | 0.01216 | 0.004 |
| 24 hrs | 11 | 5.05 | 14.2 | 12 | 0.03 | 0.010 | 0.01216 | 0.001 |



Visual description : Sand, brownish gray, trace silt, trace clay
Soil classification (USCS) : SP-SM

GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali

Location : Pelabuhan Benoa Bali

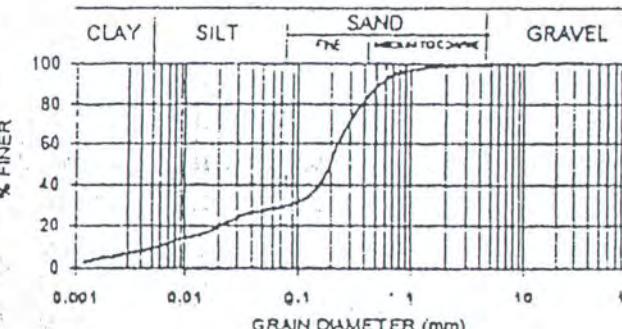
Sieve Analysis

| Sieve opening No. | mean (mm) | mean | % | Cumulative | % |
|----------------------|--------------|--------|----------|------------|--------|
| | | weight | retained | % retained | finer |
| | | gr | % | | |
| 1.5 | 33.100 | 0.00 | 0.00 | 0.00 | 100.00 |
| 10 | 25.400 | 0.00 | 0.00 | 0.00 | 100.00 |
| 24 | 19.700 | 0.00 | 0.00 | 0.00 | 100.00 |
| 30 | 9.500 | 3.73 | 0.23 | 0.28 | 98.72 |
| 4 | 4.750 | 4.10 | 0.21 | 0.59 | 95.41 |
| 8 | 2.360 | 6.94 | 0.53 | 1.12 | 98.93 |
| 16 | 1.180 | 21.80 | 1.54 | 2.78 | 97.24 |
| 30 | 0.600 | 37.80 | 3.14 | 7.19 | 97.11 |
| 50 | 0.300 | 270.31 | 20.46 | 29.35 | 71.85 |
| 100 | 0.150 | 437.70 | 33.16 | 81.51 | 38.49 |
| 200 | 0.075 | 120.30 | 9.11 | 20.32 | 29.38 |
| TOTAL | | 932.18 | 70.82 | - | - |
| TOTAL SAMPLE, gr | | 1320 | - | - | - |

Bore/depth : BH-19 / -6.00 s/d -7.00 m LWS

Hydrometer

| Time (min) | Actual Hyd (Pc) | Corr. Hyd (Pc) | Effective | Hyo. Corr only for mercuric (P) | % finer | L | K | D, mm |
|---------------|--------------------|-------------------|-----------|---------------------------------------|---------|--------------|---------|-------|
| | | | depth | | | L (cm) | | |
| | | | reading | | | mercuric (P) | | |
| 0.15 | 53 | 50.05 | 7.4 | 54 | 29.78 | 26.800 | 0.01178 | 0.064 |
| 0.5 | 50 | 47.05 | 7.9 | 51 | 27.04 | 15.800 | 0.01178 | 0.047 |
| 1 | 47 | 44.05 | 9.4 | 48 | 25.21 | 8.400 | 0.01178 | 0.034 |
| 2 | 42 | 39.05 | 9.2 | 43 | 22.44 | 4.800 | 0.01178 | 0.025 |
| 3 | 38 | 35.05 | 9.7 | 40 | 20.72 | 3.200 | 0.01178 | 0.021 |
| 4 | 35 | 32.05 | 10.4 | 38 | 16.42 | 2.000 | 0.01178 | 0.019 |
| 8 | 31 | 29.05 | 11.1 | 32 | 16.12 | 1.080 | 0.01178 | 0.014 |
| 16 | 28 | 25.05 | 11.5 | 29 | 14.40 | 0.710 | 0.01178 | 0.010 |
| 30 | 24 | 21.05 | 12.2 | 25 | 12.10 | 0.400 | 0.01178 | 0.003 |
| 60 | 20 | 17.05 | 12.8 | 21 | 9.30 | 0.210 | 0.01178 | 0.005 |
| 120 | 17 | 14.05 | 13.3 | 18 | 3.07 | 0.111 | 0.01178 | 0.004 |
| 24 hrs | 8 | 5.05 | 14.8 | 9 | 2.90 | 0.010 | 0.01178 | 0.001 |



Visual description : Sand, brownish gray, little silt, trace clay, trace shells.
Soil classification (USCS) : SM

GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali
 Location : Pelabuhan Benoa Bali

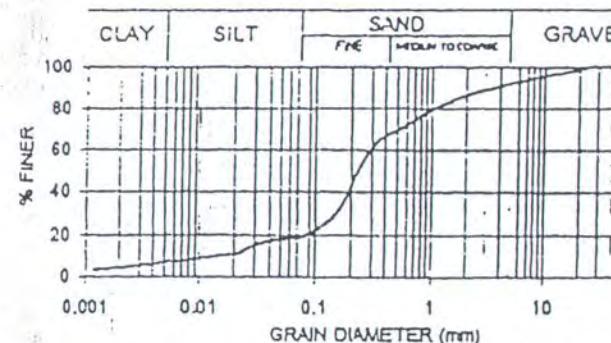
Sieve Analysis

| Sieve opening No. (mm) | mean weight gr | mean | % | Cumulative % retained | % finer |
|---------------------------|----------------------|--------|-------|--------------------------|---------|
| | | % | % | | |
| 1.5* | 33.100 | 0.00 | 0.00 | 0.00 | 100.00 |
| 1.0* | 25.400 | 0.00 | 0.00 | 0.00 | 100.00 |
| 3/4 | 13.000 | 12.00 | 1.31 | 1.24 | 98.88 |
| 3/8 | 9.500 | 30.70 | 3.00 | 4.65 | 95.35 |
| 4 | 4.750 | 34.10 | 3.67 | 8.31 | 91.89 |
| 8 | 2.380 | 37.16 | 4.00 | 12.31 | 87.99 |
| 16 | 1.180 | 57.30 | 6.18 | 18.47 | 81.53 |
| 30 | 0.600 | 32.02 | 9.82 | 29.28 | 71.84 |
| 50 | 0.300 | 100.30 | 10.84 | 29.20 | 80.80 |
| 100 | 0.150 | 282.35 | 20.42 | 68.53 | 30.37 |
| 200 | 0.075 | 104.34 | 11.25 | 20.58 | 16.12 |
| TOTAL | | 752.17 | 30.98 | - | - |
| TOTAL SAMPLE gr | | 930 | | | |

Hydrometer

| Time (min) | Actual Hyd | | Corr Hyd | Effective depth (cm) | Hyd. Con. only for meniscus (F) | % finer | L1 | k | D, mm |
|---------------|------------|-------|----------|----------------------------|---------------------------------------|---------|---------|-------|-------|
| | F1 | Pc | | | | | | | |
| 0.25 | 50 | 50.05 | 7.4 | 54 | 18.99 | 25.800 | 0.01204 | 0.066 | |
| 0.5 | 51 | 48.05 | 7.9 | 52 | 18.23 | 15.800 | 0.01204 | 0.048 | |
| 1 | 41 | 44.05 | 8.4 | 48 | 19.71 | 8.400 | 0.01204 | 0.035 | |
| 2 | 39 | 38.05 | 9.7 | 40 | 19.68 | 4.850 | 0.01204 | 0.027 | |
| 3 | 34 | 31.05 | 10.5 | 25 | 11.78 | 3.500 | 0.01204 | 0.023 | |
| 4 | 32 | 29.05 | 10.9 | 33 | 11.02 | 2.725 | 0.01204 | 0.020 | |
| 6 | 30 | 27.05 | 11.2 | 31 | 10.28 | 1.400 | 0.01204 | 0.014 | |
| 10 | 25 | 23.05 | 12 | 26 | 9.50 | 0.719 | 0.01204 | 0.010 | |
| 20 | 22 | 19.05 | 12.5 | 23 | 7.23 | 0.20E | 0.01204 | 0.005 | |
| 30 | 13 | 18.05 | 13 | 20 | 8.09 | 0.10E | 0.01204 | 0.004 | |
| 120 | 11 | 2.05 | 14.0 | 12 | 7.05 | 0.01C | 0.01204 | 0.001 | |
| 24 hrs | | | | | | | | | |

Bore/depth : BH-19 / -8.00 s/d -9.00 m LWS



Visual description : Sand, brownish grey, little silt, trace clay, trace shell
 Soil classification (USCS) : SM

GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali
 Location : Pelabuhan Benoa Bali

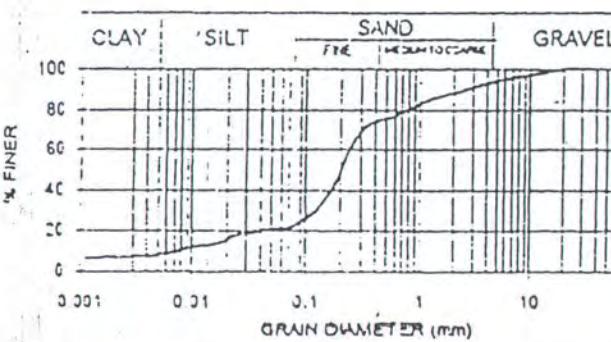
Sieve Analysis

| Sieve opening No. (mm) | mean weight gr | mean | % | Cumulative % retained | % finer |
|---------------------------|----------------------|--------|-------|--------------------------|---------|
| | | % | % | | |
| 1.5* | 33.100 | 0.03 | 0.00 | 0.00 | 100.00 |
| 1.0* | 25.400 | 0.03 | 0.00 | 0.00 | 100.00 |
| 3/4 | 13.000 | 0.03 | 0.00 | 0.00 | 100.00 |
| 3/8 | 9.500 | 21.90 | 3.04 | 3.04 | 98.56 |
| 4 | 4.750 | 20.03 | 2.73 | 5.82 | 94.10 |
| 8 | 2.380 | 35.10 | 4.83 | 10.70 | 99.50 |
| 16 | 1.180 | 34.85 | 4.54 | 15.54 | 84.46 |
| 30 | 0.600 | 57.30 | 7.53 | 23.50 | 76.50 |
| 50 | 0.300 | 54.20 | 7.53 | 31.53 | 86.97 |
| 100 | 0.150 | 244.33 | 33.98 | 65.20 | 95.00 |
| 200 | 0.075 | 34.00 | 13.14 | 78.14 | 21.86 |
| TOTAL | | 562.52 | 78.14 | - | - |
| TOTAL SAMPLE gr | | 720 | | | |

Hydrometer

| Time (min) | Actual Hyd | | Corr Hyd | Effective depth (cm) | Hyd. Con. only for meniscus (F) | % finer | L1 | k | D, mm |
|---------------|------------|-------|----------|----------------------------|---------------------------------------|---------|---------|-------|-------|
| | F1 | Pc | | | | | | | |
| 0.25 | 50 | 50.05 | 7.4 | 54 | 21.53 | 26.800 | 0.01188 | 0.065 | |
| 0.5 | 51 | 48.05 | 7.8 | 51 | 20.67 | 15.800 | 0.01188 | 0.047 | |
| 1 | 40 | 45.05 | 8.3 | 45 | 19.38 | 8.300 | 0.01188 | 0.034 | |
| 2 | 45 | 42.05 | 8.8 | 46 | 18.09 | 4.400 | 0.01188 | 0.025 | |
| 3 | 41 | 32.05 | 9.4 | 45 | 16.37 | 3.120 | 0.01188 | 0.021 | |
| 4 | 37 | 34.05 | 10.1 | 38 | 14.55 | 2.520 | 0.01188 | 0.019 | |
| 6 | 33 | 29.05 | 10.7 | 34 | 12.53 | 1.33E | 0.01188 | 0.014 | |
| 10 | 31 | 23.05 | 11.1 | 32 | 12.07 | 0.894 | 0.01188 | 0.010 | |
| 20 | 27 | 24.05 | 11.7 | 28 | 10.35 | 0.380 | 0.01188 | 0.007 | |
| 30 | 23 | 20.05 | 12.4 | 24 | 8.62 | 0.207 | 0.01188 | 0.005 | |
| 120 | 20 | 17.05 | 12.9 | 21 | 7.33 | 0.10E | 0.01188 | 0.004 | |
| 24 hrs | 18 | 15.05 | 13.2 | 19 | 8.47 | 0.009 | 0.01188 | 0.001 | |

Bore/depth : BH-19 / -10.00 s/d -10.50 m LWS



Visual description : Sand, brownish grey, little silt, trace clay, trace shell
 Soil classification (USCS) : SM

GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali

Location : Pelabuhan Benoa Bali

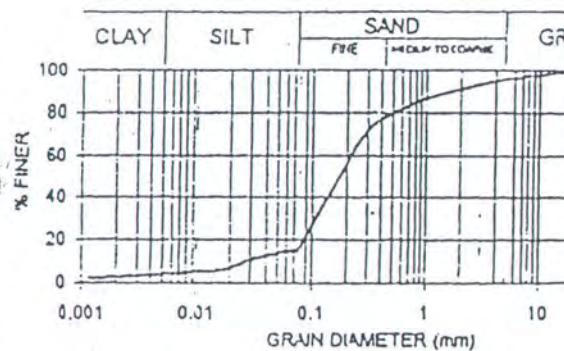
Sieve Analysis

| Sieve opening No. | (mm) | mean | % | Cumulative | % |
|------------------------|--------|---------------|--------------|------------|--------|
| | | weight gr | retained | % retained | finer |
| 1.5* | 38.100 | 0.00 | 0.03 | 0.10 | 100.00 |
| 1.0* | 25.400 | 0.03 | 0.03 | 0.00 | 100.00 |
| 3/4 | 13.000 | 9.13 | 1.22 | 1.22 | 86.78 |
| 3/8 | 9.500 | 9.10 | 1.21 | 2.43 | 87.57 |
| 4 | 4.750 | 18.30 | 2.17 | 4.50 | 85.40 |
| 8 | 2.360 | 27.64 | 3.63 | 8.29 | 91.71 |
| 16 | 1.180 | 30.01 | 4.00 | 12.29 | 87.71 |
| 32 | 0.800 | 48.33 | 5.44 | 19.73 | 81.27 |
| 50 | 0.300 | 73.44 | 9.73 | 29.53 | 71.47 |
| 100 | 0.150 | 108.39 | 27.59 | 56.12 | 43.28 |
| 200 | 0.075 | 215.70 | 29.76 | 94.58 | 15.12 |
| TOTAL | | 636.58 | 34.28 | - | - |
| TOTAL SAMPLE gr | | 750 | | | |

Hydrometer

| Time (min) | Actual Hyd. | | Effective depth (cm) | Hyd. Con. mm/100g | % finer | L4 | K | D, mm |
|---------------|-----------------|--------------------|----------------------------|----------------------|---------|--------|---------|-------|
| | reading (F1) | Corr. Hyd. (Fc) | | | | | | |
| 0.25 | 53 | 50.05 | 7.4 | 54 | 14.90 | 26.800 | 0.01108 | 0.065 |
| 0.5 | 48 | 45.05 | 9.3 | 49 | 13.41 | 18.800 | 0.01108 | 0.048 |
| 1 | 43 | 40.05 | 9.1 | 44 | 11.92 | 9.100 | 0.01108 | 0.036 |
| 2 | 35 | 32.05 | 10.4 | 36 | 9.54 | 5.200 | 0.01108 | 0.027 |
| 3 | 30 | 27.05 | 11.2 | 31 | 9.05 | 3.735 | 0.01108 | 0.023 |
| 4 | 28 | 25.05 | 11.5 | 29 | 7.46 | 2.975 | 0.01108 | 0.020 |
| 8 | 22 | 19.05 | 12.5 | 23 | 5.67 | 1.563 | 0.01108 | 0.015 |
| 16 | 20 | 17.05 | 12.9 | 21 | 5.07 | 0.808 | 0.01108 | 0.011 |
| 30 | 19 | 15.05 | 13.2 | 19 | 4.48 | 0.440 | 0.01108 | 0.008 |
| 50 | 18 | 13.05 | 13.5 | 17 | 3.88 | 0.225 | 0.01108 | 0.008 |
| 100 | 15 | 12.05 | 13.7 | 16 | 3.59 | 0.114 | 0.01108 | 0.004 |
| 200 | 10 | 9.05 | 14.5 | 11 | 2.10 | 0.010 | 0.01108 | 0.001 |

Bore/depth : BH-19 / -11.00 s/d -12.00 m LWS



Visual description : Sand, grey, trace shells, little silt, trace clay.
Soil classification (USCS) : SM

GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali

Location : Pelabuhan Benoa Bali

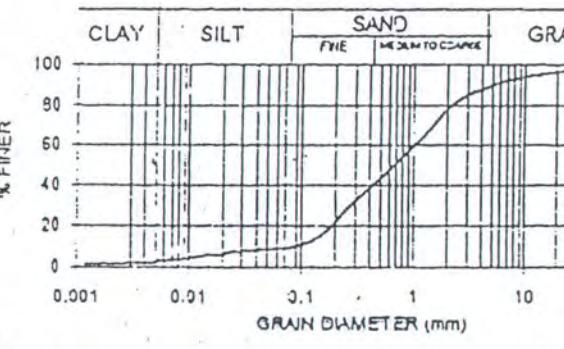
Sieve Analysis

| Sieve opening No. | (mm) | mean | % | Cumulative | % |
|------------------------|--------|---------------|--------------|------------|--------|
| | | weight gr | retained | % retained | finer |
| 1.5* | 38.100 | 0.00 | 0.03 | 0.10 | 100.00 |
| 1.0* | 25.400 | 22.04 | 3.61 | 3.61 | 96.99 |
| 3/4 | 13.000 | 8.63 | 0.81 | 3.82 | 96.10 |
| 3/8 | 9.500 | 28.63 | 2.93 | 6.51 | 93.48 |
| 4 | 4.750 | 42.11 | 3.95 | 10.46 | 86.54 |
| 8 | 2.360 | 37.02 | 3.17 | 13.53 | 81.37 |
| 16 | 1.180 | 190.30 | 17.92 | 36.33 | 83.45 |
| 32 | 0.800 | 189.37 | 15.45 | 52.50 | 47.50 |
| 50 | 0.300 | 160.21 | 15.02 | 57.52 | 32.48 |
| 100 | 0.150 | 179.54 | 16.97 | 34.39 | 15.81 |
| 200 | 0.075 | 37.70 | 5.23 | 10.75 | 8.25 |
| TOTAL | | 608.45 | 30.75 | - | - |
| TOTAL SAMPLE gr | | 1055 | | | |

Hydrometer

| Time (min) | Actual Hyd. | | Effective depth (cm) | Hyd. Con. mm/100g | % finer | L4 | K | D, mm |
|---------------|-----------------|--------------------|----------------------------|----------------------|---------|--------|---------|-------|
| | reading (F1) | Corr. Hyd. (Fc) | | | | | | |
| 0.25 | 53 | 50.05 | 7.4 | 54 | 14.90 | 26.800 | 0.01104 | 0.065 |
| 0.5 | 50 | 47.05 | 7.9 | 51 | 13.84 | 18.800 | 0.01104 | 0.048 |
| 1 | 46 | 43.05 | 9.6 | 47 | 11.90 | 8.800 | 0.01104 | 0.035 |
| 2 | 43 | 40.05 | 10.1 | 44 | 9.35 | 4.550 | 0.01104 | 0.026 |
| 3 | 40 | 37.05 | 9.8 | 41 | 8.80 | 3.200 | 0.01104 | 0.022 |
| 4 | 38 | 35.05 | 10.2 | 39 | 9.07 | 2.550 | 0.01104 | 0.019 |
| 8 | 34 | 31.05 | 10.5 | 35 | 6.70 | 1.310 | 0.01104 | 0.014 |
| 16 | 29 | 26.05 | 11.4 | 30 | 4.78 | 0.713 | 0.01104 | 0.010 |
| 30 | 22 | 19.05 | 12.1 | 23 | 3.50 | 0.417 | 0.01104 | 0.008 |
| 50 | 19 | 15.05 | 12.3 | 20 | 2.05 | 0.217 | 0.01104 | 0.006 |
| 100 | 15 | 12.05 | 13.7 | 16 | 2.21 | 0.114 | 0.01104 | 0.004 |
| 200 | 12 | 9.05 | 14.2 | 13 | 9.8 | 0.010 | 0.01104 | 0.001 |

Bore/depth : BH-20 / ±0.00 s/d -1.00 m LWS



Visual description : Sand, greyish brown, trace shells, trace silt, trace clay.
Soil classification (USCS) : SP-SM

GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali

Location : Pelabuhan Benoa Bali

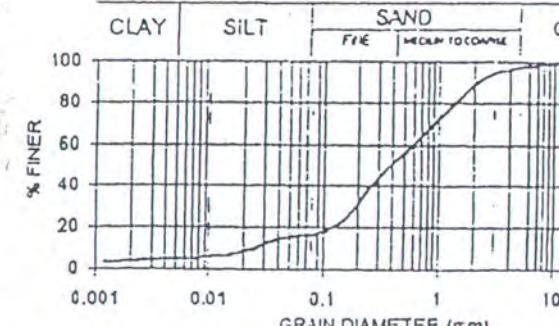
Sieve Analysis

| Sieve opening No. | mean (mm) | mean weight gr | % retained | Cumulative % retained | % finer |
|----------------------|--------------|----------------------|---------------|--------------------------|------------|
| 1.5* | 33.100 | 0.00 | 0.00 | 0.00 | 100.00 |
| 1.0* | 25.400 | 0.03 | 0.03 | 0.10 | 100.00 |
| .74 | 19.000 | 0.03 | 0.03 | 0.00 | 100.00 |
| .50 | 9.500 | 7.05 | 0.06 | 0.06 | 96.14 |
| .4 | 4.750 | 16.75 | 2.04 | 2.90 | 97.10 |
| .8 | 2.350 | 44.55 | 5.43 | 8.34 | 91.88 |
| 1.5 | 1.180 | 124.34 | 15.16 | 23.50 | 76.50 |
| 3.0 | 0.600 | 133.70 | 16.30 | 39.20 | 86.20 |
| 5.0 | 0.300 | 131.35 | 16.02 | 55.32 | 44.18 |
| 10.0 | 0.150 | 171.70 | 20.94 | 78.76 | 25.24 |
| 20.0 | 0.075 | 59.73 | 7.23 | 34.25 | 15.95 |
| TOTAL | | 589.17 | 34.05 | - | - |
| TOTAL SAMPLE gr | | 820 | | | |

Bore/depth : BH-20 / -2.00 s/d -3.00 m LWS

Hydrometer

| Time (min) | Actual Hyd. reading (F1) | Corr. Hyd. reading (Fc) | Effective depth L (cm) | Hys. Corr. only for meniscus (F) | % finer | L1 | K | D. mm |
|---------------|--------------------------------|-------------------------------|------------------------------|--|---------|--------|---------|-------|
| 0.25 | 53 | 50.05 | 7.4 | 54 | 15.78 | 26.800 | 0.01196 | 0.065 |
| 0.5 | 51 | 48.05 | 7.8 | 52 | 15.15 | 16.800 | 0.01198 | 0.047 |
| 1 | 45 | 42.05 | 9.8 | 46 | 13.29 | 8.800 | 0.01196 | 0.035 |
| 2 | 37 | 34.05 | 10.1 | 38 | 10.78 | 5.050 | 0.01196 | 0.027 |
| 3 | 32 | 29.05 | 10.9 | 33 | 9.18 | 3.632 | 0.01126 | 0.023 |
| 4 | 30 | 27.05 | 11.2 | 31 | 8.53 | 2.800 | 0.01196 | 0.020 |
| 9 | 25 | 22.05 | 12 | 26 | 8.05 | 1.500 | 0.01196 | 0.015 |
| 16 | 22 | 19.05 | 12.5 | 23 | 8.01 | 0.781 | 0.01196 | 0.011 |
| 30 | 20 | 17.05 | 12.9 | 21 | 5.38 | 0.430 | 0.01196 | 0.009 |
| 20 | 19 | 15.05 | 13.2 | 19 | 4.74 | 0.220 | 0.01196 | 0.008 |
| 120 | 17 | 14.05 | 13.3 | 18 | 4.43 | 0.111 | 0.01196 | 0.004 |
| 24 hrs | 12 | 9.05 | 14.2 | 13 | 2.85 | 0.010 | 0.01196 | 0.001 |



Visual description : Sand, grey, little silt, trace clay, trace shells.
Soil classification (USCS) : SM

GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali

Location : Pelabuhan Benoa Bali

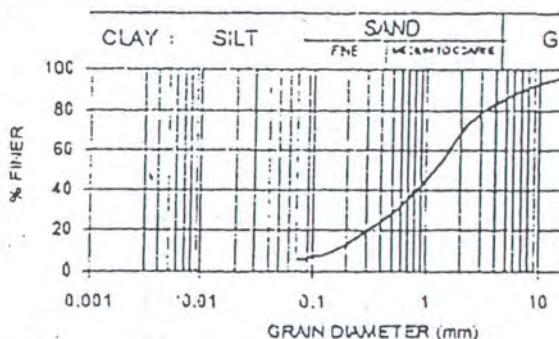
Sieve Analysis

| Sieve opening No. | mean (mm) | mean weight gr | % retained | Cumulative % retained | % finer |
|----------------------|--------------|----------------------|---------------|--------------------------|------------|
| 1.5* | 33.100 | 0.03 | 0.03 | 0.03 | 100.00 |
| 1.0* | 25.400 | 17.54 | 1.65 | 1.65 | 86.35 |
| .74 | 19.000 | 14.00 | 1.37 | 3.02 | 96.96 |
| .50 | 9.500 | 54.53 | 5.12 | 8.14 | 81.56 |
| .4 | 4.750 | 59.76 | 8.55 | 14.39 | 85.31 |
| .8 | 2.350 | 128.16 | 12.03 | 29.72 | 75.28 |
| 1.5 | 1.180 | 253.10 | 23.77 | 56.49 | 45.51 |
| 3.0 | 0.600 | 187.24 | 17.08 | 66.37 | 31.32 |
| 5.0 | 0.300 | 131.90 | 12.08 | 80.45 | 16.55 |
| 10.0 | 0.150 | 103.52 | 9.72 | 90.17 | 9.83 |
| 20.0 | 0.075 | 44.22 | 4.15 | 34.33 | 5.67 |
| TOTAL | | 1204.57 | 34.03 | - | - |
| TOTAL SAMPLE gr | | 1055 | | | |

Bore/depth : BH-20 / -5.00 s/d -5.70 m LWS

Hydrometer

| Time (min) | Actual Hyd. reading (F1) | Corr. Hyd. reading (Fc) | Effective depth L (cm) | Hys. Corr. only for meniscus (F) | % finer | L1 | K | D. mm |
|---------------|--------------------------------|-------------------------------|------------------------------|--|---------|----|---|-------|
| 0.25 | | | | | | | | |
| 0.5 | | | | | | | | |
| 1 | | | | | | | | |
| 2 | | | | | | | | |
| 3 | | | | | | | | |
| 4 | | | | | | | | |
| 9 | | | | | | | | |
| 16 | | | | | | | | |
| 30 | | | | | | | | |
| 20 | | | | | | | | |
| 120 | | | | | | | | |
| 24 hrs | | | | | | | | |



Visual description : Sand, brown, trace silt, little shells.
Soil classification (USCS) : SP

GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali
 Location : Pelabuhan Benoa Bali

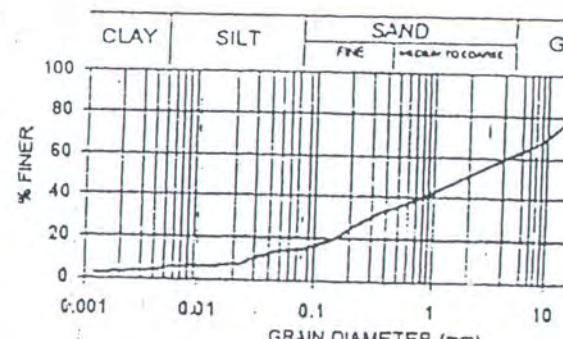
Sieve Analysis

| Sieve opening No. | mean (mm) | weight gr | mean | % | Cumulative % | % finer |
|------------------------|--------------|----------------|--------------|----------|-----------------|---------|
| | | | retained | retained | finer | |
| 1.5* | 33.100 | 122.06 | 8.52 | 8.52 | 91.48 | |
| 1.0* | 25.400 | 31.59 | 5.91 | 14.43 | 85.57 | |
| 3/4 | 13.000 | 49.45 | 3.13 | 17.32 | 81.38 | |
| 3/8 | 9.500 | 211.77 | 13.06 | 31.29 | 66.72 | |
| 4 | 4.750 | 125.32 | 8.12 | 39.40 | 60.00 | |
| 8 | 2.360 | 119.15 | 7.83 | 47.09 | 52.91 | |
| 16 | 1.180 | 124.97 | 8.03 | 55.14 | 44.86 | |
| 30 | 0.800 | 118.38 | 7.51 | 82.95 | 37.05 | |
| 50 | 0.300 | 105.78 | 5.83 | 69.49 | 30.52 | |
| 100 | 0.150 | 160.48 | 10.35 | 79.33 | 20.17 | |
| 200 | 0.075 | 36.34 | 5.57 | 25.40 | 14.80 | |
| TOTAL | | 1320.88 | 35.40 | - | - | |
| TOTAL SAMPLE gr | | 1550 | | | | |

Hydrometer

| Time (min) | Actual Hyd (F1) | Corr Hyd (Fc) | Effective depth (cm) | Hyo Corr anhydor mercuric (R) | Finer | L1 | K | D, mm |
|---------------|--------------------|------------------|----------------------------|-------------------------------------|---------|--------|---------|-------|
| | | | | | % finer | L1 | K | D, mm |
| 0.25 | 53 | 50.05 | 7.4 | 54 | 14.58 | 28.800 | 0.01212 | 0.066 |
| 0.5 | 50 | 47.05 | 7.9 | 51 | 13.68 | 15.800 | 0.01212 | 0.048 |
| 1 | 44 | 41.05 | 9.3 | 45 | 11.94 | 9.900 | 0.01212 | 0.028 |
| 2 | 37 | 34.05 | 10.1 | 38 | 9.30 | 5.050 | 0.01212 | 0.027 |
| 3 | 30 | 27.05 | 11.2 | 31 | 7.87 | 3.730 | 0.01212 | 0.023 |
| 4 | 29 | 25.05 | 11.5 | 29 | 7.29 | 2.275 | 0.01212 | 0.021 |
| 9 | 25 | 23.05 | 11.9 | 27 | 5.70 | 1.480 | 0.01212 | 0.015 |
| 16 | 25 | 22.05 | 12 | 26 | 3.41 | 0.750 | 0.01212 | 0.010 |
| 30 | 24 | 21.05 | 12.2 | 25 | 3.12 | 0.407 | 0.01212 | 0.006 |
| 60 | 23 | 20.05 | 12.4 | 24 | 5.83 | 0.207 | 0.01212 | 0.006 |
| 120 | 17 | 14.05 | 13.3 | 18 | 4.09 | 0.111 | 0.01212 | 0.004 |
| 24 hrs | 12 | 9.05 | 14.2 | 13 | 2.83 | 0.010 | 0.01212 | 0.001 |

Bore/depth : BH-20 / -8.00 s/d -7.00 m LWS



GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali
 Location : Pelabuhan Benoa Bali

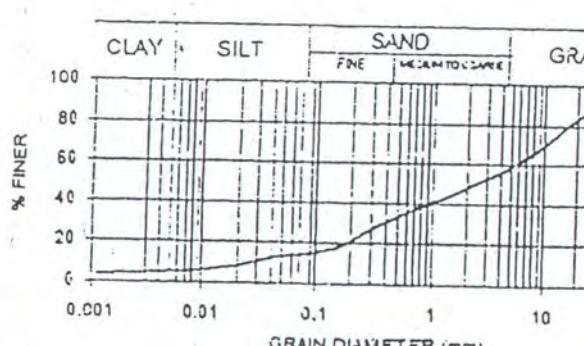
Sieve Analysis

| Sieve opening No. | mean (mm) | weight gr | mean | % | Cumulative % | % finer |
|------------------------|--------------|----------------|--------------|----------|-----------------|---------|
| | | | retained | retained | finer | |
| 1.5* | 33.100 | 131.38 | 8.51 | 8.51 | 91.48 | |
| 1.0* | 25.400 | 73.02 | 4.71 | 13.22 | 86.78 | |
| 3/4 | 13.000 | 37.05 | 4.33 | 17.15 | 82.45 | |
| 3/8 | 9.500 | 217.46 | 14.03 | 31.57 | 68.43 | |
| 4 | 4.750 | 185.38 | 10.65 | 42.23 | 57.77 | |
| 8 | 2.360 | 120.26 | 7.73 | 49.39 | 50.02 | |
| 16 | 1.180 | 122.33 | 7.92 | 57.31 | 42.09 | |
| 30 | 0.800 | 108.73 | 7.01 | 34.32 | 35.98 | |
| 50 | 0.300 | 120.25 | 7.73 | 72.38 | 27.32 | |
| 100 | 0.150 | 162.32 | 9.83 | 32.51 | 11.49 | |
| 200 | 0.075 | 51.82 | 3.34 | 66.35 | 14.15 | |
| TOTAL | | 1320.98 | 35.05 | - | - | |
| TOTAL SAMPLE gr | | 1550 | | | | |

Hydrometer

| Time (min) | Actual Hyd (F1) | Corr Hyd (Fc) | Effective depth (cm) | Hyo Corr anhydor mercuric (R) | Finer | L1 | K | D, mm |
|---------------|--------------------|------------------|----------------------------|-------------------------------------|---------|--------|---------|-------|
| | | | | | % finer | L1 | K | D, mm |
| 0.25 | 53 | 50.05 | 7.4 | 54 | 14.58 | 28.800 | 0.01178 | 0.064 |
| 0.5 | 51 | 48.05 | 7.9 | 52 | 13.27 | 15.500 | 0.01178 | 0.048 |
| 1 | 46 | 42.05 | 9.3 | 46 | 11.51 | 8.600 | 0.01178 | 0.036 |
| 2 | 39 | 36.05 | 10.1 | 40 | 9.96 | 4.850 | 0.01178 | 0.026 |
| 3 | 35 | 32.05 | 10.4 | 36 | 8.05 | 3.460 | 0.01178 | 0.022 |
| 4 | 32 | 29.05 | 10.9 | 33 | 6.02 | 2.725 | 0.01178 | 0.019 |
| 9 | 29 | 25.05 | 11.4 | 30 | 4.19 | 1.425 | 0.01178 | 0.014 |
| 16 | 29 | 23.05 | 11.6 | 27 | 3.37 | 0.744 | 0.01178 | 0.010 |
| 30 | 24 | 21.05 | 12.0 | 25 | 2.51 | 0.401 | 0.01178 | 0.007 |
| 60 | 21 | 21.05 | 12.3 | 23 | 1.68 | 0.266 | 0.01178 | 0.005 |
| 120 | 17 | 17.05 | 12.9 | 21 | 4.71 | 0.136 | 0.01178 | 0.004 |
| 24 hrs | 12 | 14.05 | 13.1 | 18 | 3.80 | 0.035 | 0.01178 | 0.001 |

Bore/depth : BH-20 / -8.00 s/d -9.00 m LWS



GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelabuhan Benoa Bali

Location : Pelabuhan Benoa Bali

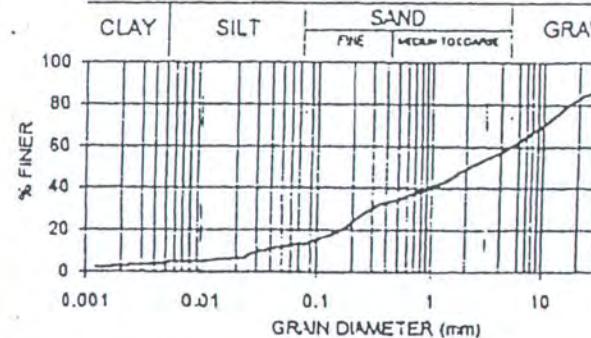
Sieve Analysis

| Sieve opening No. | mean (mm) | mean weight gr | % retained | Cumulative % retained | % finer |
|------------------------|--------------|----------------------|---------------|--------------------------|------------|
| 1.5* | 39.100 | 135.30 | 8.55 | 8.16 | 91.42 |
| 1.0* | 25.400 | 103.56 | 8.55 | 12.14 | 84.86 |
| 0.4 | 13.000 | 45.45 | 2.83 | 15.01 | 81.99 |
| 0.8 | 9.500 | 200.29 | 12.88 | 30.19 | 69.31 |
| 4 | 4.750 | 158.88 | 10.11 | 40.20 | 59.20 |
| 8 | 2.360 | 122.56 | 7.76 | 48.56 | 51.44 |
| 15 | 1.180 | 145.85 | 9.22 | 57.79 | 42.22 |
| 30 | 0.600 | 39.89 | 6.32 | 64.10 | 35.90 |
| 50 | 0.300 | 37.59 | 5.54 | 69.54 | 30.36 |
| 100 | 0.150 | 175.39 | 11.13 | 80.79 | 19.22 |
| 200 | 0.075 | 36.25 | 6.03 | 86.37 | 13.13 |
| TOTAL | | 1372.51 | 36.87 | - | - |
| TOTAL SAMPLE gr | | 1580 | - | - | - |

Hydrometer

| Time (min) | Actual Hyd. (F1) | Corr. Hyd. (Fc) | Effective depth L (cm) | Hyo. Corr only for meniscus (R) | % finer | L1 | K | D, mm |
|---------------|---------------------|--------------------|------------------------------|---------------------------------------|---------|--------|---------|-------|
| 0.25 | 53 | 50.05 | 7.4 | 54 | 13.09 | 26.800 | 0.01212 | 0.066 |
| 0.5 | 49 | 48.05 | 8.1 | 50 | 12.05 | 16.201 | 0.01212 | 0.049 |
| 1 | 43 | 40.05 | 9.1 | 44 | 10.48 | 9.100 | 0.01212 | 0.037 |
| 2 | 38 | 33.05 | 10.2 | 37 | 8.85 | 5.100 | 0.01212 | 0.027 |
| 3 | 29 | 28.05 | 11.4 | 30 | 6.81 | 3.800 | 0.01212 | 0.024 |
| 4 | 27 | 24.05 | 11.7 | 28 | 6.29 | 2.925 | 0.01212 | 0.021 |
| 8 | 24 | 21.05 | 12.2 | 25 | 5.51 | 1.525 | 0.01212 | 0.015 |
| 16 | 23 | 20.05 | 12.4 | 24 | 5.24 | 0.775 | 0.01212 | 0.011 |
| 30 | 21 | 18.05 | 12.7 | 22 | 4.72 | 0.425 | 0.01212 | 0.008 |
| 50 | 20 | 17.05 | 12.9 | 21 | 4.48 | 0.215 | 0.01212 | 0.008 |
| 100 | 16 | 13.05 | 13.5 | 17 | 3.41 | 0.115 | 0.01212 | 0.004 |
| 200 | 13 | 10.05 | 14.5 | 11 | 3.1 | 0.010 | 0.01212 | 0.001 |
| 24 hrs | 15 | 7.05 | - | - | - | - | - | - |

Bore/depth : BH-20 / -10.00 s/d -11.00 m LWS



Visual description : Sand and coral/shells, gray, trace silt, trace clay
Soil classification (USCS) : SM

GRAIN SIZE DISTRIBUTION

Project : Pengembangan Pelatungan Benoa Bali

Location : Pelabuhan Benoa Bali

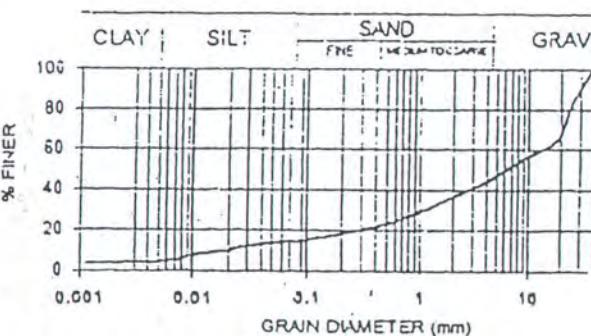
Sieve Analysis

| Sieve opening No. | mean (mm) | mean weight gr | % retained | Cumulative % retained | % finer |
|------------------------|--------------|----------------------|---------------|--------------------------|------------|
| 1.5* | 33.100 | 0.00 | 0.00 | 0.0 | 100.00 |
| 1.0* | 25.400 | 246.10 | 16.14 | 16.14 | 83.86 |
| 0.4 | 13.000 | 192.10 | 19.62 | 34.76 | 65.34 |
| 0.8 | 9.500 | 148.90 | 9.03 | 44.03 | 55.71 |
| 4 | 4.750 | 142.34 | 9.31 | 53.34 | 46.40 |
| 8 | 2.360 | 127.20 | 8.04 | 57.34 | 38.06 |
| 15 | 1.180 | 113.30 | 7.47 | 62.77 | 30.59 |
| 30 | 0.600 | 73.10 | 6.10 | 73.10 | 24.48 |
| 50 | 0.300 | 31.00 | 4.02 | 77.12 | 20.48 |
| 100 | 0.150 | 54.00 | 3.59 | 82.12 | 16.07 |
| 200 | 0.075 | 35.60 | 2.33 | 85.46 | 14.54 |
| TOTAL | | 1303.34 | 35.6 | - | - |
| TOTAL SAMPLE gr | | 1525 | - | - | - |

Hydrometer

| Time (min) | Actual Hyd. (F1) | Corr. Hyd. (Fc) | Effective depth L (cm) | Hyo. Corr only for meniscus (R) | % finer | L1 | K | D, mm |
|---------------|---------------------|--------------------|------------------------------|---------------------------------------|---------|--------|---------|-------|
| 0.25 | 53 | 50.05 | 7.4 | 54 | 14.43 | 26.800 | 0.01204 | 0.066 |
| 0.5 | 51 | 48.05 | 8.1 | 52 | 13.86 | 15.600 | 0.01204 | 0.048 |
| 1 | 47 | 44.05 | 8.4 | 46 | 12.73 | 8.400 | 0.01204 | 0.035 |
| 2 | 41 | 41.05 | 9.9 | 45 | 11.24 | 4.450 | 0.01204 | 0.025 |
| 3 | 38 | 37.05 | 9.8 | 41 | 10.68 | 3.200 | 0.01204 | 0.022 |
| 4 | 37 | 34.05 | 10.1 | 39 | 9.82 | 2.525 | 0.01204 | 0.019 |
| 8 | 34 | 31.05 | 10.5 | 35 | 9.05 | 1.315 | 0.01204 | 0.014 |
| 16 | 30 | 27.05 | 11.2 | 31 | 7.80 | 0.700 | 0.01204 | 0.010 |
| 30 | 24 | 21.05 | 12.2 | 25 | 6.07 | 0.405 | 0.01204 | 0.008 |
| 50 | 20 | 17.05 | 12.9 | 21 | 4.92 | 0.215 | 0.01204 | 0.006 |
| 100 | 17 | 14.05 | 13.0 | 16 | 4.05 | 0.115 | 0.01204 | 0.004 |
| 200 | 15 | 10.05 | 13.7 | 14 | 3.47 | 0.010 | 0.01204 | 0.001 |
| 24 hrs | - | - | - | - | - | - | - | - |

Bore/depth : BH-21 / -0.00 s/d -1.00 m LWS



Visual description : Coral/shells and sand, grey, trace silt, trace clay
Soil classification (USCS) : GM



JURUSAN TEKNIK KELAUTAN
FAKULTAS TEKNOLOGI KELAUTAN ITS

DATA KOLAM

KEDALAMAN RENCANA = 11.0000 m SLOPE = 1:3.0 - 1:6.0
KEDALAMAN EKSISTING = 9 m
LUAS KOLAM = 255000 m² DRAFT/SARAT KAPAL MAX= 10 m

ADDITIONAL DATA

HARGA BBM/LT = Rp 1000
HARGA PELUMAS/LT = Rp 15000
GAJI KRU = Rp 6000000

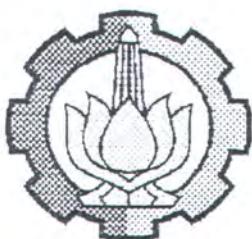
KAPAL KERUK

NAMA KAPAL : KALIMANTAN II
LOA : 109 m B : 18 m T : 6.33 m
DREDGING DEPTH: 20 m
HARGA BELI = Rp 500000000000
DAYA POMPA = 1796 hp
PRODUKTIVITAS= 200 m³/jam
JUMLAH KRU= 10 ORANG

JENIS PENGGERUKAN:
CAPITAL DREDGING

HASIL PERHITUNGAN:

| No. | Output Item | NILAI | UNIT |
|-----|------------------------|-------------------|----------------|
| 1 | DIKERUK | 2 | m |
| 2 | VOLUME KERUKAN | 1481995.00 | m ³ |
| 3 | SEDIMENTASI | 0.062413226651 | m/tahun |
| 4 | TIPE KAPAL YANG SESUAI | TSHD | |
| 5 | BIAYA/M3 | 6,779.02 | Rp |
| 6 | BIAYA TOTAL | 10,046,474,842.67 | Rp |



JURUSAN TEKNIK KELAUTAN
FAKULTAS TEKNOLOGI KELAUTAN ITS

DATA KOLAM

KEDALAMAN RENCANA = 11.0000 m SLOPE = 1:3.0 - 1:6.0
KEDALAMAN EKSISTING = 9 m
LUAS KOLAM = 255000 m² DRAFT/SARAT KAPAL MAX= 10 m

ADDITIONAL DATA

HARGA BBM/LT = Rp 1000
HARGA PELUMAS/LT = Rp 15000
GAJI KRU = Rp 6000000

KAPAL KERUK

NAMA KAPAL : MUSI 30
LOA : 41.4 m B : 13.4 m T : 2.9 m
DREDGING DEPTH: 17.6 m
HARGA BELI = Rp 25000000000
DAYA POMPA = 3600 hp
PRODUKTIVITAS= 200 m³/jam
JUMLAH KRU= 10 ORANG

JENIS PENGERUKAN:

CAPITAL DREDGING

HASIL PERHITUNGAN:

| No. | Output Item | NILAI | UNIT |
|-----|------------------------|-------------------|----------------|
| 1 | DIKERUK | 2 | m |
| 2 | VOLUME KERUKAN | 1481995.00 | m ³ |
| 3 | SEDIMENTASI | 0.062413226651 | m/tahun |
| 4 | TIPE KAPAL YANG SESUAI | CSD | |
| 5 | BIAYA/M3 | 6,752.75 | Rp |
| 6 | BIAYA TOTAL | 10,007,534,875.16 | Rp |

```

unit Main;

interface

uses Windows, SysUtils, Classes,
Graphics,      Forms,      Controls,
Menus,
type
  TMainForm = class(TForm)
    MainMenul: TMainMenu;
    Filel: TMenuItem;
    FileNewItem: TMenuItem;
    FileOpenItem: TMenuItem;
    FileCloseItem: TMenuItem;
    Windowl: TMenuItem;
    Help1: TMenuItem;
    N1: TMenuItem;
    FileExitItem: TMenuItem;
    WindowCascadeItem:
    TMenuItem;
    WindowTileItem: TMenuItem;
    WindowArrangeItem:
    TMenuItem;
    HelpAboutItem: TMenuItem;
    OpenDialog: TOpenDialog;
    Edit1: TMenuItem;
    CutItem: TMenuItem;
    CopyItem: TMenuItem;
    PasteItem: TMenuItem;
    WindowMinimizeItem:
    TMenuItem;
    StatusBar: TStatusBar;
    ActionList1: TActionList;
    EditCut1: TEditCut;
    EditCopy1: TEditCopy;
    EditPaste1: TEditPaste;
    FileNew1: TAction;
    FileSave1: TAction;
    FileExit1: TAction;

procedure
FileNew1Execute(Sender:
 TObject);
procedure
FileOpen1Execute(Sender:
 TObject);
procedure
HelpAbout1Execute(Sender:
 TObject);
procedure
FileExit1Execute(Sender:
 TObject);
procedure
FileClose1EXECUTE(Sender:
 TObject);

StdCtrls,   Dialogs,   Buttons,
Messages,  ExtCtrls,   ComCtrls,
StdActns,
ActnList, ToolWin, ImgList;

FileOpen1: TAction;
FileSaveAs1: TAction;
WindowCascade1:
TWindowCascade;
WindowTileHorizontal1:
TWindowTileHorizontal;
WindowArrangeAll1:
TWindowArrange;
WindowMinimizeAll1:
TWindowMinimizeAll;
HelpAbout1: TAction;
FileClose1: TWindowClose;
WindowTileVertical1:
TWindowTileVertical;
WindowTileItem2: TMenuItem;
ToolBar2: TToolBar;
ToolButton1: TToolButton;
ToolButton2: TToolButton;
ToolButton3: TToolButton;
ToolButton4: TToolButton;
ToolButton5: TToolButton;
ToolButton6: TToolButton;
ToolButton9: TToolButton;
ToolButton7: TToolButton;
ToolButton8: TToolButton;
ToolButton10: TToolButton;
ToolButton11: TToolButton;
ImageList1: TImageList;
SaveDialog1: TSaveDialog;
APA1: TMenuItem;
Simpan1: TMenuItem;

procedure APA1Click(Sender:
 TObject);

private
  { Private declarations }
  procedure
CreateMDIChild(const           Name:
string);
  public
    { Public declarations }
  end;

var
  MainForm: TMainForm;

implementation

```

```

{$R *.DFM}

uses ChildWinrev, About;

procedure
TMainForm.CreateMDIChild(const
Name: string);
var
  Child: TMDIChild;
begin
  { create a new MDI child
window }
  Child := TMDIChild.Create(Application);
  Child.Caption := Name;
end;

procedure
TMainForm.FileNew1Execute(Sender
: TObject);
begin
  CreateMDIChild('ANALISA');
end;

procedure
TMainForm.FileOpen1Execute(Sender
: TObject);
begin
  if OpenDialog.Execute then
    CreateMDIChild(OpenDialog.FileName);
end;

procedure
TMainForm.HelpAbout1Execute(Sender
: TObject);
begin
  AboutBox.ShowModal;
end;

type
  TMDIChild = class(TForm)
    PG: TPageControl;
    TabSheet1: TTabSheet;
    TabSheet2: TTabSheet;
    TabSheet3: TTabSheet;
    Panel1: TPanel;
    BitBtn1: TBitBtn;
    BitBtn4: TBitBtn;
    BitBtn5: TBitBtn;
    SGTEK: TStringGrid;
    TabSheet4: TTabSheet;
    Label6: TLabel;
    CMAT: TComboBox;
    CAIR: TComboBox;
    CBUANG: TComboBox;
  
```

```

procedure
TMainForm.FileExit1Execute(Sender
: TObject);
begin
  IF
    (APPLICATION.MESSAGEBOX ('KELUAR
PROGRAMINI?', 'KELUAR', MB_YESNO
OR
MB_ICONQUESTION)=IDYES) THEN
    Close;
end;
procedure
TMainForm.FileCLOSE1Execute(Sender
: TObject);
begin
  CLOSE;
end;

procedure
TMainForm.APAlClick(Sender:
 TObject);
begin
  APPLICATION.HELPFILE:='MYHELPER.
HLP';
  APPLICATION.HELPJUMP('');
end;
end.

unit childwinrev;

interface

uses Windows, Classes, Graphics,
Forms, Controls, StdCtrls,
Buttons,
ExtCtrls, ComCtrls,
Grids, MATH, SYSUTILS, DIALOGS,
DBGrids, Db, DBTables, QUICKRPT;

CVOLUM: TComboBox;
CTRASF: TComboBox;
BitBtn2: TBitBtn;
BitBtn3: TBitBtn;
Label5: TLabel;
Label10: TLabel;
SGCAP: TStringGrid;
BitBtn7: TBitBtn;
CMA: TComboBox;
CAI: TComboBox;
CBUAK: TComboBox;
CISI: TComboBox;
CLALU: TComboBox;
BitBtn6: TBitBtn;
TabSheet5: TTabSheet;
DSCSD: TDataSource;

```

```
TABELCSD: TTable;
DSTSHD: TDataSource;
TSHD: TTable;
DBCSD: TDBGrid;
Label37: TLabel;
Label38: TLabel;
DBTSHD: TDBGrid;
Label39: TLabel;
GroupBox3: TGroupBox;
Label1: TLabel;
Edit1: TEdit;
Label2: TLabel;
Edit2: TEdit;
Label3: TLabel;
Edit4: TEdit;
Label4: TLabel;
Edit6: TEdit;
Label140: TLabel;
Label41: TLabel;
Label142: TLabel;
Label143: TLabel;
BitBtn13: TBitBtn;
BitBtn12: TBitBtn;

GroupBox4: TGroupBox;
SELOP: TComboBox;
Label44: TLabel;
Edit8: TEdit;
Label45: TLabel;
Label46: TLabel;
Edit21: TEdit;
Label47: TLabel;
Label48: TLabel;
Label49: TLabel;
Label50: TLabel;
Label51: TLabel;
Label52: TLabel;
Label11: TLabel;
Label153: TLabel;
Label154: TLabel;
Label155: TLabel;
Edit22: TEdit;
DSGRAB: TDataSource;
TabGRAB: TTable;
DBGGRAB: TDBGrid;
GRAB: TLabel;
DSBUKET: TDataSource;
TabBUCKET: TTable;
DBGGrid1: TDBGrid;
Label58: TLabel;
dsvolker: TDataSource;
volker: TTable;
DBVOLKER: TDBGrid;
SED: TTable;
DSSED: TDataSource;
DBSED: TDBGrid;
Label60: TLabel;

DateTimePicker2:
TDateTimePicker;
CATATAN: TMemo;
TabSheet6: TTabSheet;
GroupBox6: TGroupBox;
GroupBox7: TGroupBox;
Label7: TLabel;
Label8: TLabel;
Label9: TLabel;
Label59: TLabel;
Label61: TLabel;
Label62: TLabel;
Label63: TLabel;
Label64: TLabel;
Label65: TLabel;
Label66: TLabel;
Label67: TLabel;
Label68: TLabel;
Label69: TLabel;
CBTIPE: TComboBox;
Edit25: TEdit;
PMP: TEdit;
Edit27: TEdit;
BELI: TEdit;
Edit7: TEdit;
PROD: TEdit;
KPL: TEdit;
LOA: TEdit;
B: TEdit;
T: TEdit;
DEPTH: TEdit;
Edit24: TEdit;
GroupBox8: TGroupBox;
Label70: TLabel;
Label71: TLabel;
Label72: TLabel;
Label73: TLabel;
Label74: TLabel;
Label75: TLabel;
Label76: TLabel;
Label77: TLabel;
Label78: TLabel;
Label79: TLabel;
Label80: TLabel;
Label81: TLabel;
Edit9: TEdit;
Edit10: TEdit;
Edit12: TEdit;
Edit13: TEdit;
Edit14: TEdit;
Edit11: TEdit;
Edit17: TEdit;
Edit18: TEdit;
Edit19: TEdit;
Edit20: TEdit;
BitBtn10: TBitBtn;
Edit15: TEdit;
```

```

Edit16: TEdit;
BitBtn11: TBitBtn;
BitBtn14: TBitBtn;
Label82: TLabel;
BAYAR: TEdit;
Label83: TLabel;
Edit23: TEdit;
Label16: TLabel;
Label17: TLabel;
GroupBox1: TGroupBox;
R1: TRadioButton;
R2: TRadioButton;
R3: TRadioButton;

procedure      FormClose(Sender:
TObject;      var      Action:
TCloseAction);
procedure
BitBtn1Click(Sender: TObject);
procedure
BitBtn4Click(Sender: TObject);
procedure
BitBtn5Click(Sender: TObject);
procedure      FormCreate(Sender:
TObject);
procedure      CAIRChange(Sender:
TObject);
procedure
CBUANGChange(Sender: TObject);
procedure
CVOLUMChange(Sender: TObject);
procedure
CTRAFChange(Sender: TObject);
procedure
BitBtn2Click(Sender: TObject);
procedure      CMACChange(Sender:
TObject);
procedure      CAIChange(Sender:
TObject);
procedure
CBUAKChange(Sender: TObject);
procedure      CISICChange(Sender:
TObject);
procedure
CLALUChange(Sender: TObject);
procedure
BitBtn7Click(Sender: TObject);
procedure
BitBtn3Click(Sender: TObject);
procedure
BitBtn6Click(Sender: TObject);
procedure      CMATChange(Sender:
TObject);
procedure      BTOKClick(Sender:
TObject);
procedure
BitBtn20Click(Sender: TObject);

Edit3: TEdit;
GroupBox2: TGroupBox;
Label14: TLabel;
Edit5: TEdit;
Label13: TLabel;
Label12: TLabel;
cbalat: TComboBox;
M2: TMemo;
Panel2: TPanel;
Image2: TImage;
Image1: TImage;

procedure
BitBtn9Click(Sender: TObject);
procedure
BitBtn13Click(Sender: TObject);
procedure
BitBtn12Click(Sender: TObject);
procedure
SELOPChange(Sender: TObject);
procedure
CBTIPEChange(Sender: TObject);
procedure
DBVOLKERKeyPress(Sender:
TObject; var Key: Char);
procedure
DBSEDKeyPress(Sender:      TObject;
var Key: Char);
procedure
cbalatChange(Sender: TObject);
procedure      R1Click(Sender:
TObject);
procedure      R2Click(Sender:
TObject);
procedure      R3Click(Sender:
TObject);

private
  { Private declarations }
public
  { Public declarations }

ST,LT,CSD,CS,GH,GP,HOE,KET,DIP,B
AR,STAN,LET,CD,CL,HOP,PON,HO,KE,
DI,BA:STRING;
BBM,OLI,PIPA,KPS,DIAM,KUAT,HARGA
,SISA,FAKTOR,AKHIR,TOTALAN:DOUBL
E;
EKS,PLAN:single;
THN,KRU:INTEGER;
TJUMLAH:SINGLE;

```

```

Tjuml:double;
end;

implementation
USES RPT;
{$R *.DFM}

procedure
TMDIChild.FormClose(Sender:
TObject; var Action:
TCloseAction);
begin
Action := caFree;
end;

procedure
TMDIChild.BitBtn1Click(Sender:
TObject);
begin
IF PG.ACTIVEPAGE=TABSHEET2 THEN
PG.ACTIVEPAGE:=TABSHEET1
ELSE IF PG.ACTIVEPAGE=TABSHEET3
THEN PG.ACTIVEPAGE:=TABSHEET2
ELSE IF PG.ACTIVEPAGE=TABSHEET4
THEN PG.ACTIVEPAGE:=TABSHEET3
ELSE IF PG.ACTIVEPAGE=TABSHEET5
THEN PG.ACTIVEPAGE:=TABSHEET4
ELSE IF PG.ACTIVEPAGE=TABSHEET6
THEN PG.ACTIVEPAGE:=TABSHEET5
begin
CATATAN.ENABLED:=FALSE;
EDIT3.ENABLED:=FALSE;
WITH SGTEK DO
BEGIN
CELLS [0,0]:='KONDISI';
CELLS [0,1]:='MATERIAL';
CELLS [0,2]:='PERAIRAN';
CELLS [0,3]:='PEMBUANGAN';
CELLS [0,4]:='VOLUME';
CELLS [0,5]:='TRAFIC';
cells [0,6]:='JUMLAH';

WITH SGCAP DO
CELLS [0,0]:='KONDISI';
CELLS [0,1]:='MATERIAL';
CELLS [0,2]:='PERAIRAN';
CELLS [0,3]:='PEMBUANGAN';
CELLS [0,4]:='VOLUME';
CELLS [0,5]:='TRAFIC';
cells [0,6]:='JUMLAH';
CELLS [1,0]:='STANDART
TRAILLER';

CELLS [2,0]:='LIGHT TRAILLER';
CELLS [3,0]:=' CSD';
CELLS [4,0]:=' CLAMPSHELL';
CELLS [5,0]:=' GRAB HOPPER';
CELLS [6,0]:=' GRAB PONTOON';
CELLS [7,0]:='BACKHOE';
CELLS [8,0]:='BUCKET';
CELLS [9,0]:='DIPPER';
CELLS [10,0]:='BARGE';

BEGIN

CELLS [2,0]:='LIGHT TRAILLER';
CELLS [3,0]:=' CSD';
CELLS [4,0]:=' CLAMPSHELL';
CELLS [5,0]:=' GRAB HOPPER';
CELLS [6,0]:=' GRAB PONTOON';
CELLS [7,0]:='BACKHOE';
CELLS [8,0]:='BUCKET';
CELLS [9,0]:='DIPPER';
CELLS [10,0]:='BARGE';

CTRAF.ENABLED:=FALSE;
CMA.ENABLED:=FALSE;
CAI.ENABLED:=FALSE;
CBUAK.ENABLED:=FALSE;

```

```

CISI.ENABLED:=FALSE;
CLALU.ENABLED:=FALSE;
BITBTN2.ENABLED:=FALSE;
BITBTN3.ENABLED:=FALSE;
BITBTN6.ENABLED:=FALSE;
BITBTN7.ENABLED:=FALSE;
SGTEK.ENABLED:=FALSE;
SGCAP.ENABLED:=FALSE;
EDIT4.ENABLED:=FALSE;
EDIT4.COLOR:=CLINFOBK;
EDIT6.ENABLED:=FALSE;
EDIT6.COLOR:=CLINFOBK;
EDIT7.ENABLED:=FALSE;
EDIT7.COLOR:=CLINFOBK;
EDIT8.ENABLED:=FALSE;
EDIT8.COLOR:=CLINFOBK;
EDIT9.ENABLED:=FALSE;
EDIT9.COLOR:=CLINFOBK;
EDIT10.ENABLED:=FALSE;
EDIT10.COLOR:=CLINFOBK;
EDIT11.ENABLED:=FALSE;
EDIT11.COLOR:=CLINFOBK;

SELOP.Items.APPEND('STIFF
CLAY');
SELOP.Items.APPEND('FIRM CLAY');
SELOP.Items.APPEND('SANDY
CLAY');

CBTIPE.ITEMS.APPEND('CSD');
CBTIPE.ITEMS.APPEND('TSHD');

cbalat.items.append('TSHD');
cbalat.items.append('CSD');
cbalat.items.append('BACKHOE');
cbalat.items.append('GRAB');
cbalat.items.append('BUCKET');
cbalat.items.append('DIPPER');
end;
CMAT.Items.APPEND('LOOSE SILT');
CMAT.Items.APPEND('COHESIVE
SILT');
CMAT.Items.APPEND('FINE SAND');
CMAT.Items.APPEND('MEDIUM
SAND');
CMAT.Items.APPEND('COARSE
SAND');

CAIR.Items.APPEND('PERAIRAN
TERTUTUP');
CAIR.Items.APPEND('PERAIRAN
TERLINDUNG');
CAIR.Items.APPEND('PERAIRAN
TERBUKA');

EDIT12.ENABLED:=FALSE;
EDIT12.COLOR:=CLINFOBK;
EDIT14.ENABLED:=FALSE;
EDIT14.COLOR:=CLINFOBK;
EDIT17.ENABLED:=FALSE;
EDIT17.COLOR:=CLINFOBK;
EDIT18.ENABLED:=FALSE;
EDIT18.COLOR:=CLINFOBK;
EDIT19.ENABLED:=FALSE;
EDIT19.COLOR:=CLINFOBK;
EDIT20.ENABLED:=FALSE;
EDIT20.COLOR:=CLINFOBK;
EDIT21.ENABLED:=TRUE;
TJUMLAH:=0;
EDIT22.ENABLED:=TRUE;
TJUML:=0;
EDIT22.TEXT:=FORMAT('%10.12F', [T
JUML]);
bayar.ENABLED:=FALSE;
bayar.COLOR:=CLINFOBK;
EDIT23.ENABLED:=FALSE;
EDIT23.COLOR:=CLINFOBK;

SELOP.Items.APPEND('MEDIUM
SAND');
SELOP.Items.APPEND('COARSE
SAND');
SELOP.Items.APPEND('FINE SAND');
SELOP.Items.APPEND('MUD');
CBTIPE.ITEMS.APPEND('GRAB');
CBTIPE.ITEMS.APPEND('BUCKET');

CBUANG.Items.APPEND('BUANG PANTAI'); DI
CBUANG.Items.APPEND('BUANG TIDE'); DI
CBUANG.Items.APPEND('BUANG LAUT'); DI

CBUAK.Items.APPEND('BUANG PANTAI'); DI
CBUAK.Items.APPEND('BUANG TIDE'); DI
CBUAK.Items.APPEND('BUANG LAUT'); DI

CVOLUM.Items.APPEND('VOLUME <100.000 m3');
CVOLUM.Items.APPEND('VOLUME <250.000 m3');
CVOLUM.Items.APPEND('VOLUME <500.000 m3');
CVOLUM.Items.APPEND('VOLUME >500.000 m3');

CISI.Items.APPEND('VOLUME <100.000 m3');

```

```

SGTEK.CELLS[8, 2]:=KET;
SGTEK.CELLS[9, 2]:=DIP;
SGTEK.CELLS[10, 2]:=BAR;
IF CAIR.TEXT='PERAIRAN TERBUKA'
THEN
ST:='3';
LT:='2';
CSD:='1';
CS:='1';
GH:='1';
GP:='0';
HOE:='1';
KET:='1';
DIP:='0';
BAR:='0';

SGTEK.CELLS[1, 2]:=ST;

procedure
TMDIChild.CBUANGChange(Sender:
TObject);
ST:='2';
LT:='2';
CSD:='3';
CS:='3';
GH:='0';
GP:='2';
HOE:='2';
KET:='2';
DIP:='0';
BAR:='3';

SGTEK.CELLS[1, 3]:=ST;

IF CBUANG.TEXT='BUANG DI TIDE'
THEN
ST:='3';
LT:='3';
CSD:='3';
CS:='0';
GH:='0';
GP:='0';
HOE:='0';
KET:='0';
DIP:='0';
BAR:='0';

SGTEK.CELLS[1, 3]:=ST;
IF CBUANG.TEXT='BUANG DI LAUT'
THEN
BEGIN
ST:='3';
LT:='3';
CSD:='0';
CS:='0';
GH:='3';
GP:='3';

```

ITS

```

CISI.Items.APPEND('VOLUME
<250.000 m3');
CISI.Items.APPEND('VOLUME
<500.000 m3');
CISI.Items.APPEND('VOLUME
>500.000 m3');

CTRAF.Items.APPEND('TRAFIK
PADAT');
CTRAF.Items.APPEND('TRAFIK
JARANG');

CMA.Items.APPEND('LOOSE SILT');
CMA.Items.APPEND('COHESIVE
SILT');

WITH SGCAP DO
BEGIN
CELLS [0,0]:='KONDISI';
CELLS [0,1]:='MATERIAL';
CELLS [0,2]:='PERAIRAN';
CELLS [0,3]:='PEMBUANGAN';
CELLS [0,4]:='VOLUME';
CELLS [0,5]:='TRAFFIC';
cells [0,6]:='JUMLAH';
CELLS [1,0]:='STANDART
TRAILLER';
CELLS [2,0]:='LIGHT TRAILLER';
CELLS [3,0]:=' CSD';
CELLS [4,0]:=' CLAMPSHELL';
CELLS [5,0]:=' GRAB HOPPER';
CELLS [6,0]:=' GRAB PONTOON';
CELLS [7,0]:='BACKHOE';
IF CAIR.text='PERAIRAN TERTUTUP'
THEN
BEGIN
ST:='1';
LT:='2';
CSD:='3';
CS:='3';
GH:='3';
GP:='2';
HOE:='2';
KET:='2';
DIP:='0';
BAR:='3';
IF CAIR.TEXT='PERAIRAN
TERLINDUNG' THEN
ST:='3';
LT:='3';
CSD:='3';
CS:='3';
GH:='3';
GP:='3';
HOE:='3';
KET:='3';
DIP:='0';

```

```

CMA.Items.APPEND('FINE SAND');
CMA.Items.APPEND('MEDIUM SAND');
CMA.Items.APPEND('COARSE SAND');
CMA.Items.APPEND('GRAVEL');
CMA.Items.APPEND('SOFT CLAY');
CMA.Items.APPEND('MEDIUM CLAY');
CMA.Items.APPEND('BOULDERS');
CMA.Items.APPEND('ROCK');

CLALU.Items.APPEND('TRAFIK
PADAT');
CLALU.Items.APPEND('TRAFIK
JARANG');

CELLS [8,0]:='BUCKET';
CELLS [9,0]:='DIPPER';
CELLS [8,0]:='BARGE';
END;

CAI.Items.APPEND('PERAIRAN
TERTUTUP');
CAI.Items.APPEND('PERAIRAN
TERLINDUNG');
CAI.Items.APPEND('PERAIRAN
TERBUKA');
END;
END;
procedure
TMDIChild.CAIRChange(Sender:
TObject);
begin

SGTEK.CELLS[1,2]:=ST;
SGTEK.CELLS[2,2]:=LT;
SGTEK.CELLS[3,2]:=CSD;
SGTEK.CELLS[4,2]:=CS;
SGTEK.CELLS[5,2]:=GH;
SGTEK.CELLS[6,2]:=GP;
SGTEK.CELLS[7,2]:=HOE;
SGTEK.CELLS[8,2]:=KET;
SGTEK.CELLS[9,2]:=DIP;
SGTEK.CELLS[10,2]:=BAR;

END;
BEGIN
BAR:='2';

SGTEK.CELLS[1,2]:=ST;
SGTEK.CELLS[2,2]:=LT;
SGTEK.CELLS[3,2]:=CSD;
SGTEK.CELLS[4,2]:=CS;
SGTEK.CELLS[5,2]:=GH;
SGTEK.CELLS[6,2]:=GP;
SGTEK.CELLS[7,2]:=HOE;

```

```

SGTEK.CELLS[3, 3]:=CSD;
SGTEK.CELLS[4, 3]:=CS;
SGTEK.CELLS[5, 3]:=GH;
SGTEK.CELLS[6, 3]:=GP;
SGTEK.CELLS[7, 3]:=HOE;

procedure
TMDIChild.CVOLUMChange(Sender:
TObject);
IF CVOLUM.TEXT='VOLUME <100.000
m3' THEN
BEGIN
ST:='2';
LT:='3';
CSD:='3';
CS:='3';
GH:='3';
GP:='3';
HOE:='2';
KET:='3';
DIP:='0';
BAR:='3';
IF CVOLUM.TEXT='VOLUME <250.000
m3' THEN
BEGIN
ST:='3';
LT:='2';
CSD:='3';
CS:='3';
GH:='3';
GP:='2';
HOE:='3';
KET:='2';
DIP:='0';
BAR:='3';
IF CVOLUM.TEXT='VOLUME <500.000
m3' THEN
BEGIN
ST:='3';
LT:='2';
CSD:='3';
CS:='3';
GH:='3';
GP:='2';
HOE:='3';
KET:='2';
DIP:='0';
BAR:='3';
IF CVOLUM.TEXT='VOLUME >500.000
m3' THEN
BEGIN
ST:='3';
LT:='2';
CSD:='3';
CS:='3';
GH:='1';
GP:='1';

```

HOE:='3';
KET:='1';
DIP:='0';
BAR:='3';

```

SGTEK.CELLS[8, 3]:=KET;
SGTEK.CELLS[9, 3]:=DIP;
SGTEK.CELLS[10, 3]:=BAR;
END;
END;
begin
SGTEK.CELLS[1, 4]:=ST;
SGTEK.CELLS[2, 4]:=LT;
SGTEK.CELLS[3, 4]:=CSD;
SGTEK.CELLS[4, 4]:=CS;
SGTEK.CELLS[5, 4]:=GH;
SGTEK.CELLS[6, 4]:=GP;
SGTEK.CELLS[7, 4]:=HOE;
SGTEK.CELLS[8, 4]:=KET;
SGTEK.CELLS[9, 4]:=DIP;
SGTEK.CELLS[10, 4]:=BAR;

END;
BEGIN
SGTEK.CELLS[1, 4]:=ST;
SGTEK.CELLS[2, 4]:=LT;
SGTEK.CELLS[3, 4]:=CSD;
SGTEK.CELLS[4, 4]:=CS;
SGTEK.CELLS[5, 4]:=GH;
SGTEK.CELLS[6, 4]:=GP;
SGTEK.CELLS[7, 4]:=HOE;
SGTEK.CELLS[8, 4]:=KET;
SGTEK.CELLS[9, 4]:=DIP;
SGTEK.CELLS[10, 4]:=BAR;

END;
BEGIN
SGTEK.CELLS[1, 4]:=ST;
SGTEK.CELLS[2, 4]:=LT;
SGTEK.CELLS[3, 4]:=CSD;
SGTEK.CELLS[4, 4]:=CS;
SGTEK.CELLS[5, 4]:=GH;
SGTEK.CELLS[6, 4]:=GP;
SGTEK.CELLS[7, 4]:=HOE;
SGTEK.CELLS[8, 4]:=KET;
SGTEK.CELLS[9, 4]:=DIP;
SGTEK.CELLS[10, 4]:=BAR;

END;
BEGIN
SGTEK.CELLS[1, 4]:=ST;
SGTEK.CELLS[2, 4]:=LT;
SGTEK.CELLS[3, 4]:=CSD;
SGTEK.CELLS[4, 4]:=CS;
SGTEK.CELLS[5, 4]:=GH;
SGTEK.CELLS[6, 4]:=GP;
SGTEK.CELLS[7, 4]:=HOE;
SGTEK.CELLS[8, 4]:=KET;
SGTEK.CELLS[9, 4]:=DIP;
SGTEK.CELLS[10, 4]:=BAR;

```

```

SGTEK.CELLS[3, 4]:=CSD;
SGTEK.CELLS[4, 4]:=CS;
SGTEK.CELLS[5, 4]:=GH;
SGTEK.CELLS[6, 4]:=GP;
SGTEK.CELLS[7, 4]:=HOE;
SGTEK.CELLS[8, 4]:=KET;
procedure
TMDIChild.CTRAFChange(Sender:
TObject);
IF CTRAF.TEXT='TRAFIK PADAT'
THEN
BEGIN
ST:='3';
LT:='3';
CSD:='1';
CS:='1';
GH:='2';
GP:='2';
HOE:='1';
KET:='3';
DIP:='0';
BAR:='2';

IF CTRAF.TEXT='TRAFIK JARANG'
THEN
ST:='3';
LT:='2';
CSD:='3';
CS:='3';
GH:='2';
GP:='2';
HOE:='2';
KET:='1';
DIP:='0';
BAR:='2';

SGTEK.CELLS[1, 5]:=ST;
procedure
TMDIChild.CMATChange(Sender:
TObject);
IF CMAT.TEXT='LOOSE SILT' THEN
BEGIN
ST:='3';
LT:='3';
CSD:='3';
CS:='3';
GH:='2';
GP:='2';
HOE:='2';
KET:='2';
DIP:='0';
BAR:='3';

IF CMAT.TEXT='COHESIVE SILT'
THEN
ST:='3';
LT:='2';

SGTEK.CELLS[9, 4]:=DIP;
SGTEK.CELLS[10, 4]:=BAR;
END;
END;

begin
SGTEK.CELLS[1, 5]:=ST;
SGTEK.CELLS[2, 5]:=LT;
SGTEK.CELLS[3, 5]:=CSD;
SGTEK.CELLS[4, 5]:=CS;
SGTEK.CELLS[5, 5]:=GH;
SGTEK.CELLS[6, 5]:=GP;
SGTEK.CELLS[7, 5]:=HOE;
SGTEK.CELLS[8, 5]:=KET;
SGTEK.CELLS[9, 5]:=DIP;
SGTEK.CELLS[10, 5]:=BAR;

END;
BEGIN
SGTEK.CELLS[2, 5]:=LT;
SGTEK.CELLS[3, 5]:=CSD;
SGTEK.CELLS[4, 5]:=CS;
SGTEK.CELLS[5, 5]:=GH;
SGTEK.CELLS[6, 5]:=GP;
SGTEK.CELLS[7, 5]:=HOE;
SGTEK.CELLS[8, 5]:=KET;
SGTEK.CELLS[9, 5]:=DIP;
SGTEK.CELLS[10, 5]:=BAR;
END;
end;

begin
SGTEK.CELLS[1, 1]:=ST;
SGTEK.CELLS[2, 1]:=LT;
SGTEK.CELLS[3, 1]:=CSD;
SGTEK.CELLS[4, 1]:=CS;
SGTEK.CELLS[5, 1]:=GH;
SGTEK.CELLS[6, 1]:=GP;
SGTEK.CELLS[7, 1]:=HOE;
SGTEK.CELLS[8, 1]:=KET;
SGTEK.CELLS[9, 1]:=DIP;
SGTEK.CELLS[10, 1]:=BAR;

END;
BEGIN
CSD:='3';
CS:='3';

```

```

GH:='3';
GP:='3';
HOE:='2';
KET:='3';
DIP:='0';
BAR:='3';

SGTEK.CELLS[1,1]:=ST;
SGTEK.CELLS[2,1]:=LT;
IF CMAT.TEXT='FINE SAND' THEN
ST:='3';
LT:='3';
CSD:='3';
CS:='3';
GH:='2';
GP:='2';
HOE:='2';
KET:='2';
DIP:='0';
BAR:='3';

IF CMAT.TEXT='MEDIUM SAND' THEN
ST:='3';
LT:='3';
CSD:='3';
CS:='3';
GH:='2';
GP:='2';
HOE:='3';
KET:='2';
DIP:='0';
BAR:='3';

IF CMAT.TEXT='COARSE SAND' THEN
ST:='3';
LT:='2';
CSD:='3';
CS:='3';
GH:='2';
GP:='2';
HOE:='3';
KET:='2';
DIP:='0';
BAR:='3';

SGTEK.CELLS[1,1]:=ST;
procedure
TMDIChild.BitBtn2Click(Sender:
 TObject);

VAR
a,b,c,d,e,TOT:integer;
f,g,h,i,j,tet:integer;
k,l,m,n,o,tut:integer;
p,q,r,s,t,tat:integer;
u,v,w,x,y,tit:integer;
a:=strToInt(cells[1,1]);

```

```

SGTEK.CELLS[3,1]:=CSD;
SGTEK.CELLS[4,1]:=CS;
SGTEK.CELLS[5,1]:=GH;
SGTEK.CELLS[6,1]:=GP;
SGTEK.CELLS[7,1]:=HOE;
SGTEK.CELLS[8,1]:=KET;
SGTEK.CELLS[9,1]:=DIP;
SGTEK.CELLS[10,1]:=BAR;
END;
BEGIN
SGTEK.CELLS[1,1]:=ST;
SGTEK.CELLS[2,1]:=LT;
SGTEK.CELLS[3,1]:=CSD;
SGTEK.CELLS[4,1]:=CS;
SGTEK.CELLS[5,1]:=GH;
SGTEK.CELLS[6,1]:=GP;
SGTEK.CELLS[7,1]:=HOE;
SGTEK.CELLS[8,1]:=KET;
SGTEK.CELLS[9,1]:=DIP;
SGTEK.CELLS[10,1]:=BAR;
END;
BEGIN
SGTEK.CELLS[1,1]:=ST;
SGTEK.CELLS[2,1]:=LT;
SGTEK.CELLS[3,1]:=CSD;
SGTEK.CELLS[4,1]:=CS;
SGTEK.CELLS[5,1]:=GH;
SGTEK.CELLS[6,1]:=GP;
SGTEK.CELLS[7,1]:=HOE;
SGTEK.CELLS[8,1]:=KET;
SGTEK.CELLS[9,1]:=DIP;
SGTEK.CELLS[10,1]:=BAR;
END;
BEGIN
SGTEK.CELLS[2,1]:=LT;
SGTEK.CELLS[3,1]:=CSD;
SGTEK.CELLS[4,1]:=CS;
SGTEK.CELLS[5,1]:=GH;
SGTEK.CELLS[6,1]:=GP;
SGTEK.CELLS[7,1]:=HOE;
SGTEK.CELLS[8,1]:=KET;
SGTEK.CELLS[9,1]:=DIP;
SGTEK.CELLS[10,1]:=BAR;
END;
end;

z,ab,ac,ad,ae,tst:integer;
ze,ai,au,aa,ao,sts:integer;
zo,aba,aca,ada,aea,ses:integer;
zoe,abah,acah,adah,aeah,sesi:integer;
zoei,abahi,acahi,adahi,aeahi,set
an:integer;
begin
with sgtek do
begin
b:=strToInt(cells[1,2]);

```

```

c:=strtoint(cells[1,3]);
d:=strtoint(cells[1,4]);
e:=strtoint(cells[1,5]);
f:=strtoint(cells[2,1]);
g:=strtoint(cells[2,2]);
h:=strtoint(cells[2,3]);
i:=strtoint(cells[2,4]);
j:=strtoint(cells[2,5]);
k:=strtoint(cells[3,1]);
l:=strtoint(cells[3,2]);
m:=strtoint(cells[3,3]);
n:=strtoint(cells[3,4]);
o:=strtoint(cells[3,5]);
p:=strtoint(cells[4,1]);
q:=strtoint(cells[4,2]);
r:=strtoint(cells[4,3]);
s:=strtoint(cells[4,4]);
t:=strtoint(cells[4,5]);
u:=strtoint(cells[5,1]);
v:=strtoint(cells[5,2]);
w:=strtoint(cells[5,3]);
x:=strtoint(cells[5,4]);
y:=strtoint(cells[5,5]);
z:=strtoint(cells[6,1]);
ab:=strtoint(cells[6,2]);
ac:=strtoint(cells[6,3]);
ad:=strtoint(cells[6,4]);
ae:=strtoint(cells[6,5]);
ze:=strtoint(cells[7,1]);
ai:=strtoint(cells[7,2]);
cells[1,6]:=inttostr (tot);
cells[10,6]:=inttostr (setan);
cells[2,6]:=inttostr (tet);
cells[3,6]:=inttostr (tut);
cells[4,6]:=inttostr (tat);

cells[5,6]:=inttostr (tit);
cells[6,6]:=inttostr (tst);

cells[7,6]:=inttostr (sts);
cells[8,6]:=inttostr (ses);
STAN:='3';
LET:='3';
CD:='3';
CL:='3';
HOP:='2';
PON:='2';
HO:='2';
KE:='2';
DI:='1';
BA:='3';

SGCAP.CELLS[1,1]:=STAN;

IF CMA.TEXT='COHESIVE SILT' THEN
STAN:='3';
au:=strtoint(cells[7,3]);
aa:=strtoint(cells[7,4]);
ao:=strtoint(cells[7,5]);
zo:=strtoint(cells[8,1]);
aba:=strtoint(cells[8,2]);
aca:=strtoint(cells[8,3]);
ada:=strtoint(cells[8,4]);
aea:=strtoint(cells[8,5]);
zoe:=strtoint(cells[9,1]);
abah:=strtoint(cells[9,2]);
acah:=strtoint(cells[9,3]);
adah:=strtoint(cells[9,4]);
aeah:=strtoint(cells[9,5]);
zoei:=strtoint(cells[10,1]);
abahi:=strtoint(cells[10,2]);
acahi:=strtoint(cells[10,3]);
adahi:=strtoint(cells[10,4]);
aeahi:=strtoint(cells[10,5]);

TOT:=(a+b+c+d+e);
tat:=p+q+r+s+t;
tit:=u+v+w+x+y;
tet:=f+g+h+i+j;
tut:=k+l+m+n+o;
tst:=z+ab+ac+ad+ae;
sts:=ze+ai+aa+au+ao;
ses:=zo+aba+aca+ada+aea;
sesi:=zoe+abah+acah+adah+aeah;
setan:=zoei+abahi+acahi+adahi+aeahi;
cells[9,6]:=inttostr (sesi);
CATATAN.text:='PILIH LAH
PERALATAN KERUK DENGAN SKOR
BESAR !';
END;
END;
procedure
TMDIChild.CMACHange(Sender:
TOBJECT);
begin
IF CMA.TEXT='LOOSE SILT' THEN
BEGIN
SGCAP.CELLS[2,1]:=LET;
SGCAP.CELLS[3,1]:=CD;
SGCAP.CELLS[4,1]:=CL;
SGCAP.CELLS[5,1]:=HOP;
SGCAP.CELLS[6,1]:=PON;
SGCAP.CELLS[7,1]:=HO;
SGCAP.CELLS[8,1]:=KE;
SGCAP.CELLS[9,1]:=DI;
SGCAP.CELLS[10,1]:=BA;
END;
BEGIN
LET:='3';

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```

CD:='3';
CL:='3';
HOP:='3';
PON:='3';
HO:='2';
KE:='1';
DI:='1';
BA:='3';

SGCAP.CELLS[1,1]:=STAN;
IF CMA.TEXT='FINE SAND' THEN
STAN:='3';
LET:='3';
CD:='3';
CL:='3';
HOP:='2';
PON:='2';
HO:='2';
KE:='2';
DI:='1';
BA:='3';

IF CMA.TEXT='MEDIUM SAND' THEN
STAN:='3';
LET:='3';
CD:='3';
CL:='3';
HOP:='2';
PON:='2';
HO:='3';
KE:='2';
DI:='2';
BA:='3';

IF CMA.TEXT='COARSE SAND' THEN
STAN:='3';
LET:='3';
CD:='3';
CL:='3';
HOP:='3';
PON:='3';
HO:='2';
KE:='2';
DI:='3';
BA:='3';

IF CMA.TEXT='GRAVEL' THEN
STAN:='3';
LET:='2';
CD:='3';
CL:='3';
HOP:='3';
PON:='3';
HO:='3';
KE:='3';
DI:='3';
BA:='3';

SGCAP.CELLS[2,1]:=LET;
SGCAP.CELLS[3,1]:=CD;
SGCAP.CELLS[4,1]:=CL;
SGCAP.CELLS[5,1]:=HOP;
SGCAP.CELLS[6,1]:=PON;
SGCAP.CELLS[7,1]:=HO;
SGCAP.CELLS[8,1]:=KE;
SGCAP.CELLS[9,1]:=DI;
SGCAP.CELLS[10,1]:=BA;
END;
BEGIN
SGCAP.CELLS[1,1]:=STAN;
SGCAP.CELLS[2,1]:=LET;
SGCAP.CELLS[3,1]:=CD;
SGCAP.CELLS[4,1]:=CL;
SGCAP.CELLS[5,1]:=HOP;
SGCAP.CELLS[6,1]:=PON;
SGCAP.CELLS[7,1]:=HO;
SGCAP.CELLS[8,1]:=KE;
SGCAP.CELLS[9,1]:=DI;
SGCAP.CELLS[10,1]:=BA;
END;
BEGIN
SGCAP.CELLS[1,1]:=STAN;
SGCAP.CELLS[2,1]:=LET;
SGCAP.CELLS[3,1]:=CD;
SGCAP.CELLS[4,1]:=CL;
SGCAP.CELLS[5,1]:=HOP;
SGCAP.CELLS[6,1]:=PON;
SGCAP.CELLS[7,1]:=HO;
SGCAP.CELLS[8,1]:=KE;
SGCAP.CELLS[9,1]:=DI;
SGCAP.CELLS[10,1]:=BA;
END;
BEGIN
SGCAP.CELLS[1,1]:=STAN;
SGCAP.CELLS[2,1]:=LET;
SGCAP.CELLS[3,1]:=CD;
SGCAP.CELLS[4,1]:=CL;
SGCAP.CELLS[5,1]:=HOP;
SGCAP.CELLS[6,1]:=PON;
SGCAP.CELLS[7,1]:=HO;
SGCAP.CELLS[8,1]:=KE;
SGCAP.CELLS[9,1]:=DI;
SGCAP.CELLS[10,1]:=BA;
END;
BEGIN
SGCAP.CELLS[1,1]:=STAN;
SGCAP.CELLS[2,1]:=LET;
SGCAP.CELLS[3,1]:=CD;
SGCAP.CELLS[4,1]:=CL;
SGCAP.CELLS[5,1]:=HOP;
SGCAP.CELLS[6,1]:=PON;
SGCAP.CELLS[7,1]:=HO;
SGCAP.CELLS[8,1]:=KE;
SGCAP.CELLS[9,1]:=DI;
SGCAP.CELLS[10,1]:=DI;

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```

SGCAP.CELLS[10,1]:=BA;
IF CMA.TEXT='SOFT CLAY' THEN
STAN:='3';
LET:='2';
CD:='1';
CL:='3';
HOP:='3';
PON:='2';
HO:='2';
KE:='3';
DI:='2';
BA:='3';

IF CMA.TEXT='MEDIUM CLAY' THEN
STAN:='2';
LET:='1';
CD:='1';
CL:='2';
HOP:='2';
PON:='2';
HO:='3';
KE:='3';
DI:='2';
BA:='2';

IF CMA.TEXT='BOULDERS' THEN
STAN:='0';
LET:='0';
CD:='1';
CL:='1';
HOP:='1';
PON:='2';
HO:='3';
KE:='2';
DI:='3';
BA:='0';

IF CMA.TEXT='ROCK' THEN
STAN:='0';
LET:='0';
CD:='3';
CL:='1';
HOP:='0';
PON:='0';
HO:='3';
KE:='1';
DI:='3';
BA:='0';

SGCAP.CELLS[1,1]:=STAN;
procedure
TMDIChild.CAIChange(Sender:
TObject);
STAN:='0';
LET:='1';
CD:='3';
END;
BEGIN
SGCAP.CELLS[1,1]:=STAN;
SGCAP.CELLS[2,1]:=LET;
SGCAP.CELLS[3,1]:=CD;
SGCAP.CELLS[4,1]:=CL;
SGCAP.CELLS[5,1]:=HOP;
SGCAP.CELLS[6,1]:=PON;
SGCAP.CELLS[7,1]:=HO;
SGCAP.CELLS[8,1]:=KE;
SGCAP.CELLS[9,1]:=DI;
SGCAP.CELLS[10,1]:=BA;
END;
BEGIN
SGCAP.CELLS[1,1]:=STAN;
SGCAP.CELLS[2,1]:=LET;
SGCAP.CELLS[3,1]:=CD;
SGCAP.CELLS[4,1]:=CL;
SGCAP.CELLS[5,1]:=HOP;
SGCAP.CELLS[6,1]:=PON;
SGCAP.CELLS[7,1]:=HO;
SGCAP.CELLS[8,1]:=KE;
SGCAP.CELLS[9,1]:=DI;
SGCAP.CELLS[10,1]:=BA;
END;
BEGIN
SGCAP.CELLS[1,1]:=STAN;
SGCAP.CELLS[2,1]:=LET;
SGCAP.CELLS[3,1]:=CD;
SGCAP.CELLS[4,1]:=CL;
SGCAP.CELLS[5,1]:=HOP;
SGCAP.CELLS[6,1]:=PON;
SGCAP.CELLS[7,1]:=HO;
SGCAP.CELLS[8,1]:=KE;
SGCAP.CELLS[9,1]:=DI;
SGCAP.CELLS[10,1]:=BA;
END;
BEGIN
SGCAP.CELLS[2,1]:=LET;
SGCAP.CELLS[3,1]:=CD;
SGCAP.CELLS[4,1]:=CL;
SGCAP.CELLS[5,1]:=HOP;
SGCAP.CELLS[6,1]:=PON;
SGCAP.CELLS[7,1]:=HO;
SGCAP.CELLS[8,1]:=KE;
SGCAP.CELLS[9,1]:=DI;
SGCAP.CELLS[10,1]:=BA;
END;
END;
begin
IF CAI.TEXT='PERAIRAN TERTUTUP'
THEN
BEGIN
CL:='3';
HOP:='3';
PON:='3';

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HO:='3';
KE:='3';
DI:='3';
BA:='3';

SGCAP.CELLS[1,2]:=STAN;
SGCAP.CELLS[2,2]:=LET;
SGCAP.CELLS[3,2]:=CD;
IF           CAI.TEXT='PERAIRAN
TERLINDUNG' THEN
STAN:='3';
LET:='3';
CD:='3';
CL:='2';
HOP:='2';
PON:='3';
HO:='3';
KE:='2';
DI:='2';
BA:='1';

IF   CAI.TEXT='PERAIRAN    TERBUKA'
THEN
STAN:='3';
LET:='2';
CD:='1';
CL:='1';
HOP:='1';
PON:='1';
HO:='2';
KE:='1';
DI:='1';
BA:='0';

SGCAP.CELLS[1,2]:=STAN;
procedure
TMDIChild.CBUAKChange(Sender:
TObject);
IF CBUAK.TEXT='BUANG DI LAUT'
THEN
BEGIN
STAN:='3';
LET:='3';
CD:='1';
CL:='1';
HOP:='3';
PON:='3';
HO:='3';
KE:='3';
DI:='3';
BA:='0';

IF CBUAK.TEXT='BUANG DI PANTAI'
THEN
STAN:='3';
LET:='2';
CD:='3';
CL:='3';
HOP:='0';
PON:='0';
END;
END;

SGCAP.CELLS[4,2]:=CL;
SGCAP.CELLS[5,2]:=HOP;
SGCAP.CELLS[6,2]:=PON;
SGCAP.CELLS[7,2]:=HO;
SGCAP.CELLS[8,2]:=KE;
SGCAP.CELLS[9,2]:=DI;
SGCAP.CELLS[10,2]:=BA;
END;
BEGIN

SGCAP.CELLS[1,2]:=STAN;
SGCAP.CELLS[2,2]:=LET;
SGCAP.CELLS[3,2]:=CD;
SGCAP.CELLS[4,2]:=CL;
SGCAP.CELLS[5,2]:=HOP;
SGCAP.CELLS[6,2]:=PON;
SGCAP.CELLS[7,2]:=HO;
SGCAP.CELLS[8,2]:=KE;
SGCAP.CELLS[9,2]:=DI;
SGCAP.CELLS[10,2]:=BA;
END;
BEGIN

SGCAP.CELLS[2,2]:=LET;
SGCAP.CELLS[3,2]:=CD;
SGCAP.CELLS[4,2]:=CL;
SGCAP.CELLS[5,2]:=HOP;
SGCAP.CELLS[6,2]:=PON;
SGCAP.CELLS[7,2]:=HO;
SGCAP.CELLS[8,2]:=KE;
SGCAP.CELLS[9,2]:=DI;
SGCAP.CELLS[10,2]:=BA;
END;
END;

begin
SGCAP.CELLS[1,3]:=STAN;
SGCAP.CELLS[2,3]:=LET;
SGCAP.CELLS[3,3]:=CD;
SGCAP.CELLS[4,3]:=CL;
SGCAP.CELLS[5,3]:=HOP;
SGCAP.CELLS[6,3]:=PON;
SGCAP.CELLS[7,3]:=HO;
SGCAP.CELLS[8,3]:=KE;
SGCAP.CELLS[9,3]:=DI;
SGCAP.CELLS[10,3]:=BA;
END;

BEGIN
CL:='3';
HOP:='0';
PON:='0';

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```

HO:='0';
KE:='0';
DI:='0';
BA:='3';

SGCAP.CELLS[1,3]:=STAN;
SGCAP.CELLS[2,3]:=LET;
SGCAP.CELLS[3,3]:=CD;
IF CBUAK.TEXT='BUANG DI TIDE'
THEN
STAN:='3';
LET:='3';
CD:='2';
CL:='3';
HOP:='0';
PON:='0';
HO:='0';
KE:='0';
DI:='0';
BA:='0';
SGCAP.CELLS[1,3]:=STAN;

procedure
TMDIChild.CISIChange(Sender:
TObject);
BEGIN
STAN:='2';
LET:='3';
CD:='3';
CL:='3';
HOP:='3';
PON:='3';
HO:='3';
KE:='2';
DI:='3';
BA:='3';

IF CISI.TEXT='VOLUME <100.000
m3' THEN
SGCAP.CELLS[1,4]:=STAN;
SGCAP.CELLS[2,4]:=LET;
SGCAP.CELLS[3,4]:=CD;
SGCAP.CELLS[4,4]:=CL;
SGCAP.CELLS[5,4]:=HOP;
SGCAP.CELLS[6,4]:=PON;
SGCAP.CELLS[7,4]:=HO;
SGCAP.CELLS[8,4]:=KE;
SGCAP.CELLS[9,4]:=DI;
SGCAP.CELLS[10,4]:=BA;
END;

IF CISI.TEXT='VOLUME <250.000
m3' THEN
STAN:='3';
LET:='2';
CD:='3';
CL:='3';
HOP:='2';
PON:='2';
HO:='3';
KE:='3';
DI:='2';
BA:='3';

IF CISI.TEXT='VOLUME <500.000
m3' THEN
STAN:='3';
LET:='1';
CD:='3';
CL:='3';

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SGCAP.CELLS[4,3]:=CL;
SGCAP.CELLS[5,3]:=HOP;
SGCAP.CELLS[6,3]:=PON;
SGCAP.CELLS[7,3]:=HO;
SGCAP.CELLS[8,3]:=KE;
SGCAP.CELLS[9,3]:=DI;
SGCAP.CELLS[10,3]:=BA;
END;
BEGIN

SGCAP.CELLS[2,3]:=LET;
SGCAP.CELLS[3,3]:=CD;
SGCAP.CELLS[4,3]:=CL;
SGCAP.CELLS[5,3]:=HOP;
SGCAP.CELLS[6,3]:=PON;
SGCAP.CELLS[7,3]:=HO;
SGCAP.CELLS[8,3]:=KE;
SGCAP.CELLS[9,3]:=DI;
SGCAP.CELLS[10,3]:=BA;
END;
END;
begin
IF CISI.TEXT='VOLUME <100.000
m3' THEN
SGCAP.CELLS[1,4]:=STAN;
SGCAP.CELLS[2,4]:=LET;
SGCAP.CELLS[3,4]:=CD;
SGCAP.CELLS[4,4]:=CL;
SGCAP.CELLS[5,4]:=HOP;
SGCAP.CELLS[6,4]:=PON;
SGCAP.CELLS[7,4]:=HO;
SGCAP.CELLS[8,4]:=KE;
SGCAP.CELLS[9,4]:=DI;
SGCAP.CELLS[10,4]:=BA;
END;

BEGIN
SGCAP.CELLS[1,4]:=STAN;
SGCAP.CELLS[2,4]:=LET;
SGCAP.CELLS[3,4]:=CD;
SGCAP.CELLS[4,4]:=CL;
SGCAP.CELLS[5,4]:=HOP;
SGCAP.CELLS[6,4]:=PON;
SGCAP.CELLS[7,4]:=HO;
SGCAP.CELLS[8,4]:=KE;
SGCAP.CELLS[9,4]:=DI;
SGCAP.CELLS[10,4]:=BA;
END;
BEGIN
HOP:='1';
PON:='2';
HO:='2';
KE:='3';

```

```

DI:='1';
BA:='3';
SGCAP.CELLS[1, 4]:=STAN;
SGCAP.CELLS[2, 4]:=LET;
SGCAP.CELLS[3, 4]:=CD;
SGCAP.CELLS[4, 4]:=CL;
SGCAP.CELLS[5, 4]:=HOP;

IF CISI.TEXT='VOLUME >500.000
m3' THEN
STAN:='3';
LET:='1';
CD:='3';
CL:='3';
HOP:='1';
PON:='1';
HO:='1';
KE:='3';
DI:='1';
BA:='3';
SGCAP.CELLS[1, 4]:=STAN;
SGCAP.CELLS[2, 4]:=LET;

procedure
TMDIChild.CLALUChange(Sender:
 TObject);
IF CLALU.TEXT='TRAFIK PADAT'
THEN
BEGIN
STAN:='3';
LET:='3';
CD:='3';
CL:='2';
HOP:='2';
PON:='1';
HO:='2';
KE:='1';
DI:='2';
BA:='2';

IF CLALU.TEXT='TRAFIK JARANG'
THEN
STAN:='3';
LET:='3';
CD:='3';
CL:='3';
HOP:='3';
PON:='3';
HO:='3';
KE:='3';
DI:='2';
BA:='2';
SGCAP.CELLS[1, 5]:=STAN;

procedure
TMDIChild.BitBtn7Click(Sender:
 TObject);

```

SGCAP.CELLS[6, 4]:=PON;
SGCAP.CELLS[7, 4]:=HO;
SGCAP.CELLS[8, 4]:=KE;
SGCAP.CELLS[9, 4]:=DI;
SGCAP.CELLS[10, 4]:=BA;
END;

BEGIN

SGCAP.CELLS[3, 4]:=CD;
SGCAP.CELLS[4, 4]:=CL;
SGCAP.CELLS[5, 4]:=HOP;
SGCAP.CELLS[6, 4]:=PON;
SGCAP.CELLS[7, 4]:=HO;
SGCAP.CELLS[8, 4]:=KE;
SGCAP.CELLS[9, 4]:=DI;
SGCAP.CELLS[10, 4]:=BA;
END;
END;

begin

SGCAP.CELLS[1, 5]:=STAN;
SGCAP.CELLS[2, 5]:=LET;
SGCAP.CELLS[3, 5]:=CD;
SGCAP.CELLS[4, 5]:=CL;
SGCAP.CELLS[5, 5]:=HOP;
SGCAP.CELLS[6, 5]:=PON;
SGCAP.CELLS[7, 5]:=HO;
SGCAP.CELLS[8, 5]:=KE;
SGCAP.CELLS[9, 5]:=DI;
SGCAP.CELLS[10, 5]:=BA;
END;

BEGIN

SGCAP.CELLS[2, 5]:=LET;
SGCAP.CELLS[3, 5]:=CD;
SGCAP.CELLS[4, 5]:=CL;
SGCAP.CELLS[5, 5]:=HOP;
SGCAP.CELLS[6, 5]:=PON;
SGCAP.CELLS[7, 5]:=HO;
SGCAP.CELLS[8, 5]:=KE;
SGCAP.CELLS[9, 5]:=DI;
SGCAP.CELLS[10, 5]:=BA;
END;
END;
VAR
X, Y: INTEGER;
begin
FOR X:=1 TO SGCAP.COLCOUNT DO

```

FOR Y:=1 TO SGCAP.ROWCOUNT DO
SGCAP.CELLS[X,Y]:='';
end;

procedure
TMDIChild.BitBtn3Click(Sender:
TObject);
VAR
I,J:INTEGER;
a2,b2,c2,d2,e2,TOT2:integer;
f2,g2,h2,i2,j2,tet2:integer;
k2,l2,m2,n2,o2,tut2:integer;
p2,q2,r2,s2,t2,tat2:integer;
u2,v2,w2,x2,y2,tit2:integer;
z2,ab2,ac2,ad2,ae2,tst2:integer;
ze2,ai2,au2,aa2,ao2,sts2:integer
;
begin
with sgcap do
a2:=STRTOInt(cells[1,1]);
b2:=STRTOInt(cells[1,2]);
c2:=STRTOInt(cells[1,3]);
d2:=STRTOInt(cells[1,4]);
e2:=STRTOInt(cells[1,5]);
f2:=STRTOInt(cells[2,1]);
g2:=STRTOInt(cells[2,2]);
h2:=STRTOInt(cells[2,3]);
i2:=STRTOInt(cells[2,4]);
j2:=STRTOInt(cells[2,5]);
k2:=STRTOInt(cells[3,1]);
l2:=STRTOInt(cells[3,2]);
m2:=STRTOInt(cells[3,3]);
n2:=STRTOInt(cells[3,4]);
o2:=STRTOInt(cells[3,5]);
p2:=STRTOInt(cells[4,1]);
q2:=STRTOInt(cells[4,2]);
r2:=STRTOInt(cells[4,3]);
s2:=STRTOInt(cells[4,4]);
t2:=STRTOInt(cells[4,5]);
u2:=STRTOInt(cells[5,1]);
v2:=STRTOInt(cells[5,2]);
w2:=STRTOInt(cells[5,3]);
x2:=STRTOInt(cells[5,4]);
y2:=STRTOInt(cells[5,5]);
z2:=STRTOInt(cells[6,1]);
ab2:=STRTOInt(cells[6,2]);
ac2:=STRTOInt(cells[6,3]);
ad2:=STRTOInt(cells[6,4]);
ae2:=STRTOInt(cells[6,5]);
ze2:=STRTOInt(cells[7,1]);
ai2:=STRTOInt(cells[7,2]);
au2:=STRTOInt(cells[7,3]);
aa2:=STRTOInt(cells[7,4]);
ao2:=STRTOInt(cells[7,5]);
zo2:=STRTOInt(cells[8,1]);
begin
FOR I:=1 TO SGTEK.COLCOUNT DO
FOR J:=1 TO SGTEK.ROWCOUNT DO
SGTEK.CELLS[I,J]:='';
end;
procedure
TMDIChild.BitBtn6Click(Sender:
TObject);
VAR
zo2,aba2,aca2,ada2,aea2,ses2:int
eger;
zoi2,abai2,acai2,adai2,aeai2,ses
i2:integer;
zoe2,abae2,acae2,adae2,aaee2,bru
tu2:integer;
begin
aba2:=STRTOInt(cells[8,2]);
aca2:=STRTOInt(cells[8,3]);
ada2:=STRTOInt(cells[8,4]);
aea2:=STRTOInt(cells[8,5]);
zoi2:=STRTOInt(cells[9,1]);
abai2:=STRTOInt(cells[9,2]);
acai2:=STRTOInt(cells[9,3]);
adai2:=STRTOInt(cells[9,4]);
aeai2:=STRTOInt(cells[9,5]);
zoe2:=STRTOInt(cells[10,1]);
abae2:=STRTOInt(cells[10,2]);
acae2:=STRTOInt(cells[10,3]);
adae2:=STRTOInt(cells[10,4]);
aaee2:=STRTOInt(cells[10,5]);
TOT2:=a2+b2+c2+d2+e2;
tat2:=p2+q2+r2+s2+t2;
tit2:=u2+v2+w2+x2+y2;
tet2:=f2+g2+h2+i2+j2;
tut2:=k2+l2+m2+n2+o2;
tst2:=z2+ab2+ac2+ad2+ae2;
sts2:=ze2+ai2+aa2+au2+ao2;
ses2:=zo2+aba2+aca2+ada2+aea2;
sesi2:=zoi2+abai2+acai2+adai2+ae
ai2;
brutu2:=zoe2+abae2+acae2+adae2+a
ee2;
CELLS[1,6]:=INTTOstr (tot2);
CELLS[2,6]:=INTTOstr (tet2);
CELLS[3,6]:=INTTOstr (tut2);
CELLS[4,6]:=INTTOstr (tat2);
CELLS[5,6]:=INTTOstr (tit2);
CELLS[6,6]:=INTTOstr (tst2);
CELLS[7,6]:=INTTOstr (sts2);
CELLS[8,6]:=INTTOstr (ses2);
CELLS[9,6]:=INTTOstr (sesi2);
CELLS[10,6]:=INTTOstr (brutu2);

```

```

CATATAN.text:='PILIH LAH
PERALATAN KERUK DENGAN SKOR
BESAR !';
END;
END;
procedure
TMDIChild.BTOKClick(Sender:
 TObject);
var
JAKER,HARGA,SISA,kuat,kps,bbm,ol
i,BLJ,BJ,OLJ,NSUT,SUSUT,BAIK,ASU
,GJ,gaji,OJ,volume:DOUBLE;
kru:INTEGER;
begin
HARGA:=STRTOFLOAT(beli.TEXT);
SISA:=HARGA*0.05;
KRU:=STRTOINT(EDIT27.TEXT);
JAKER:=STRTOINT(EDIT24.TEXT);
KUAT:=STRTOFLOAT(pmp.TEXT);
KPS:=STRTOFLOAT(prod.TEXT);
BBM:=STRTOFLOAT(EDIT15.TEXT);
OLI:=STRTOFLOAT(EDIT16.TEXT);
BLJ:=0.15*kuat;
BJ:=bbm*blj;
OLJ:=7*(0.0007*kuat);
OJ:=olj*oli;
GAJI:=STRTOFLOAT (EDIT13.TEXT);
GJ:=kru*gaji/(4*6*JAKER);
ASU:=0.025*harga/(6*48*JAKER);
BAIK:=FAKTOR*harga/JAKER;
SUSUT:=(harga-sisa)/30;
NSUT:=susut/(48*6*JAKER);
AKHIR:=(BJ+OJ+GJ+ASU+BAIK+NSUT) /
KPS;
CBTIPE.TEXT:='';
kpl.text:='';
b.text:='';
t.text:='';
loa.text:='';
pmp.text:='';
depth.TEXT:='';
edit25.text:='';
edit27.text:='';
procedure
TMDIChild.BitBtn9Click(Sender:
 TObject);
begin
Laporan:=TLaporan.Create(self);
WITH Laporan do
begin
LAPORAN.QRLABEL26.CAPTION:=forma
t('%5.4f',[plan]);
LAPORAN.QRLABEL25.CAPTION:=edit2
.text;
LAPORAN.QRLABEL33.CAPTION:=SED['
LKOL'];

```

```

volume:=strtofloat
(edit21.text);
TOTALAN:=AKHIR*volume;
edit7.text:=format('%12.2n',[sis
a]);
edit9.text:=format('%10.2n',[bj
]);
edit10.text:=format('%10.2n',[bj
]);
edit11.text:=format('%10.2n',[ol
j]);
edit12.text:=format('%10.2n',[oj
]);
edit14.text:=format('%10.2n',[gj
]);
edit17.text:=format('%12.2n',[as
u]);
edit18.text:=format('%12.2n',[ba
ik]);
edit19.text:=format('%12.2n',[su
sut]);
edit20.text:=format('%12.2n',[ns
ut]);
bayar.TEXT:=Format('%12.2N',[AKH
IR]);
EDIT23.TEXT:=FORMAT('%12.2N',[TO
TALAN]);
end;

procedure
TMDIChild.BitBtn20Click(Sender:
 TObject);
begin
edit15.text:='';
edit16.text:='';
beli.TEXT:='';
prod.TEXT:='';
EDIT13.TEXT:='';
EDIT24.TEXT:='';
end;

LAPORAN.QRLABEL37.CAPTION:=(EDIT
8.TEXT);
LAPORAN.QRLABEL78.CAPTION:=EDIT6
.TEXT;
LAPORAN.QRLABEL45.CAPTION:=T.TEX
T;
LAPORAN.QRLABEL19.CAPTION:=KPL.T
EXT;
LAPORAN.QRLABEL23.CAPTION:=LOA.T
EXT;
LAPORAN.QRLABEL38.CAPTION:=B.TEX
T;

```

```

LAPORAN.QRLABEL14.CAPTION:=EDIT1
.TEXT;
LAPORAN.QRLABEL83.CAPTION:=beli.
text;

LAPORAN.QRLABEL85.CAPTION:=DEPTH
.TEXT;

LAPORAN.QRLABEL94.CAPTION:=EDIT1
5.TEXT;

LAPORAN.QRLABEL101.CAPTION:=EDIT
16.TEXT;

LAPORAN.QRLABEL105.CAPTION:=EDIT
13.TEXT;

LAPORAN.QRLABEL106.CAPTION:=EDIT
27.TEXT;
LAPORAN.QRLABEL61.CAPTION:=pmp.t
ext;
LAPORAN.QRLABEL77.CAPTION:=prod.
text;
LAPORAN.QRLABEL78.CAPTION:=edit6
.TEXT;
LAPORAN.QRLABEL10.CAPTION:=FORMAT('%.20.2F',[TJUMLAH]);
LAPORAN.QRLABEL79.CAPTION:=FORMAT('%.10.12F',[TJUML]);
LAPORAN.QRLABEL80.CAPTION:=CBTIPE.TEXT;
LAPORAN.QRLABEL81.CAPTION:=Format('%.12.2N',[AKHIR]);
LAPORAN.QRLABEL109.CAPTION:=Format('%.12.2N',[TOTALAN]);
LAPORAN.QRLABEL113.CAPTION:=EDIT
3.TEXT;
end;
LAPORAN.PREVIEW;
end;

procedure
TMDIChild.BitBtn13Click(Sender:
TObject);

VAR
DRT, KERUK:SINGLE;

begin
DRT:=STRTOFLOAT (EDIT1.TEXT);
EKS:=STRTOFLOAT (EDIT2.TEXT);
PLAN:=DRT*1.1;
EDIT4.TEXT:=FLOATTOSTR (PLAN);

BEGIN
KERUK:=0;
IF EKS>=PLAN THEN
EDIT6.TEXT:=FLOATTOSTR (KERUK);
end;
BEGIN
IF EKS<PLAN THEN
KERUK:=PLAN-EKS;
EDIT6.TEXT:=FLOATTOSTR (KERUK);
end;
END;

procedure
TMDIChild.BitBtn12Click(Sender:
TObject);
begin
EDIT1.TEXT:='';
EDIT2.TEXT:='';
end;

procedure
TMDIChild.SELOPChange(Sender:
TObject);
begin
IF SELOP.text='STIFF CLAY' THEN
BEGIN
EDIT8.TEXT:='1:1.5';
end;
IF SELOP.text='FIRM CLAY' THEN
BEGIN
EDIT8.TEXT:='1:1.5 - 1:4.5';
end;
IF SELOP.text='SANDY CLAY' THEN
BEGIN
EDIT8.TEXT:='1:4.0 - 1:7.0';
end;
IF SELOP.text='COARSE SAND' THEN
BEGIN
EDIT8.TEXT:='1:3.0 - 1:6.0';
end;
IF SELOP.text='FINE SAND' THEN
BEGIN
EDIT8.TEXT:='1:4.0 - 1:10.0';
end;
IF SELOP.text='MUD' THEN
BEGIN
EDIT8.TEXT:='1:8.0 - 1:50';
end;
END;

procedure
TMDIChild.CBTIPEChange(Sender:
TObject);
BEGIN
IF CBTIPE.TEXT='TSHD' THEN
FAKTOR:=0.000135;
IF CBTIPE.TEXT='CSD' THEN
FAKTOR:=0.000140;
IF CBTIPE.TEXT='BACKHOE' THEN

```

```

FAKTOR:=0.000140;
IF CBTIPE.TEXT='GRAB' THEN
FAKTOR:=0.000130;
END;
procedure
TMDIChild.DBVOLKERKeyPress(Sender: TObject; var Key: Char);
VAR
JB:DOUBLE;
begin
IF DBVOLKER.SELECTEDINDEX=4 THEN
BEGIN
VOLKER['VOLK']:=VOLKER['JARAK']*(
VOLKER['PIAS1']+VOLKER['PIAS2'])/2;
JB:=VOLKER.FIELDS[4].ASFLOAT;
TJUMLAH:=TJUMLAH+JB;
EDIT21.TEXT:=FORMAT('%20.2F',[TJUMLAH]);
end;
END;

procedure
TMDIChild.DBSEDKeyPress(Sender: TObject; var Key: Char);
var
jsed:double;
begin
IF dbsed.SELECTEDINDEX=5 THEN
BEGIN
sed['cz]:=18*log10(12*sed['ked']/sed['r']);
end;
IF dbsed.SELECTEDINDEX=6 THEN
BEGIN
sed['cz90]:=18*log10(12*sed['ked']/sed['D90']);
end;
IF dbsed.SELECTEDINDEX=9 THEN
BEGIN
sed['miu]:=power((SED['cz']/SED['cz90']),1.5);
end;
IF dbsed.SELECTEDINDEX=10 THEN
BEGIN
sed['mio']:=(0.66*5.4)/(2*sinh(0.041*sed['ked']));
end;
IF dbsed.SELECTEDINDEX=11 THEN
BEGIN
sed['SC]:=1025*9.81*POWER(sed['arus']/SED['cz'],2);
end;
IF dbsed.SELECTEDINDEX=12 THEN
BEGIN
sed['ANOL]:=SED['mio']*9.83/6.2
8;
end;
IF dbsed.SELECTEDINDEX=13 THEN
BEGIN
sed['FW]:=exp(-5.977+(5.213*power(SED['anol']/sed['r'],-0.194)));
end;
IF dbsed.SELECTEDINDEX=14 THEN
BEGIN
sed['BJK]:=sed['CZ']*POWER((SED['FW']/(2*9.81)),0.5);
end;
IF dbsed.SELECTEDINDEX=15 THEN
BEGIN
sed['SCW]:=SED['SC']*(1+POWER((0.5*(SED['BJK'])*(SED['MIO']/sed['arus']))),2));
end;
IF dbsed.SELECTEDINDEX=16 THEN
BEGIN
sed['sb]:=5*sed['d50']*sed['arus']*POWER(9.81,0.5)/SED['CZ']*EXP(
(0.27*1.585*sed['d50']*1025*9.81)/(SED['MIU']/SED['SC']));
end;
IF dbsed.SELECTEDINDEX=17 THEN
BEGIN
sed['VS]:=POWER((SED['SCW']/1025),0.5);
end;
IF dbsed.SELECTEDINDEX=18 THEN
BEGIN
sed['ZET]:=0.16*SED['VS']*sed['ked'];
end;
IF dbsed.SELECTEDINDEX=19 THEN
BEGIN
sed['CB]:=sed['sb']/(6.34*sed['VS'])*sed['r'];
end;
IF dbsed.SELECTEDINDEX=20 THEN
BEGIN
sed['ce1]:= (sed['CB']*sed['ZET'])/(0.0325*sed['ked'])*(1-EXP(-(0.0325*sed['ked']/sed['ZET'])));
end;
IF dbsed.SELECTEDINDEX=21 THEN
BEGIN
sed['ss]:=sed['VS']*sed['CE1']*sed['ked'];
end;
IF dbsed.SELECTEDINDEX=22 THEN
BEGIN
sed['stot]:=sed['SB']+sed['SS'];

```

```

end;
IF dbsed.SELECTEDINDEX=23 THEN
BEGIN
sed['sth']:=sed['stot']*3600*24*
365;
end;

IF dbsed.SELECTEDINDEX=26 THEN
BEGIN
sed['sm']:=sed['sth']/((sed['lko
l']+sed['ldas'])/2);
end;
Jsed:=sed.fields[26].asfloat;
TJUML:=TJUML+Jsed;
EDIT22.TEXT:=FORMAT ('%10.12F',[T
JUML]);
end;

procedure
TMDIChild.cbalatChange(Sender:
TObject);
VAR
A,B,C,D,E,F,GELOM:SINGLE;
begin
GELOM:=STRTOFLOAT (EDIT5.TEXT);
BEGIN;
IF CBALAT.TEXT='TSHD' THEN
BEGIN
A:=4;
IF GELOM<=A THEN
M2.TEXT:='TIPE ALAT MEMENUHI
SYARAT BATAS'
ELSE
M2.TEXT:='TIPE ALAT TIDAK
MEMENUHI SYARAT BATAS';
end;
END;

begin
GELOM:=STRTOFLOAT (EDIT5.TEXT);
BEGIN;
IF CBALAT.TEXT='CSD' THEN
BEGIN
B:=4;
IF GELOM<=B THEN
M2.TEXT:='TIPE ALAT MEMENUHI
SYARAT BATAS'
ELSE
M2.TEXT:='TIPE ALAT TIDAK
MEMENUHI SYARAT BATAS';
end;
END;

begin
GELOM:=STRTOFLOAT (EDIT5.TEXT);
BEGIN;
IF CBALAT.TEXT='GRAB' THEN
BEGIN
C:=3.5;
IF GELOM<=C THEN
M2.TEXT:='TIPE ALAT MEMENUHI
SYARAT BATAS'
ELSE
M2.TEXT:='TIPE ALAT TIDAK
MEMENUHI SYARAT BATAS';
end;
END;

begin
GELOM:=STRTOFLOAT (EDIT5.TEXT);
BEGIN;
IF CBALAT.TEXT='BUCKET' THEN
BEGIN
D:=1.0;
IF GELOM<=D THEN
M2.TEXT:='TIPE ALAT MEMENUHI
SYARAT BATAS'
ELSE
M2.TEXT:='TIPE ALAT TIDAK
MEMENUHI SYARAT BATAS';
end;
END;

begin
GELOM:=STRTOFLOAT (EDIT5.TEXT);
BEGIN;
IF CBALAT.TEXT='BACKHOE' THEN
BEGIN
E:=0.8;
IF GELOM<=E THEN
M2.TEXT:='TIPE ALAT MEMENUHI
SYARAT BATAS'
ELSE
M2.TEXT:='TIPE ALAT TIDAK
MEMENUHI SYARAT BATAS';
end;
END;

begin
GELOM:=STRTOFLOAT (EDIT5.TEXT);
BEGIN;
IF CBALAT.TEXT='DIPPER' THEN
BEGIN
F:=0.8;
IF GELOM<=F THEN
M2.TEXT:='TIPE ALAT MEMENUHI
SYARAT BATAS'
ELSE

```

```

M2.TEXT:='TIPE      ALAT      TIDAK
MEMENUHI SYARAT BATAS';
end;
END;
END;
END;

R2.ENABLED:=FALSE;
R3.ENABLED:=FALSE;
CMA.ENABLED:=FALSE;
CAIR.ENABLED:=FALSE;
CBUAK.ENABLED:=FALSE;
CISI.ENABLED:=FALSE;
CLALU.ENABLED:=FALSE;
SGCAP.ENABLED:=FALSE;
BITBTN6.ENABLED:=FALSE;
BITBTN7.ENABLED:=FALSE;
CMAT.ENABLED:=TRUE;

procedure
TMDIChild.R2Click(Sender:
TObject);
R1.ENABLED:=FALSE;
R3.ENABLED:=FALSE;
CMAT.ENABLED:=FALSE;
CAIR.ENABLED:=FALSE;
CBUANG.ENABLED:=FALSE;
CVOLUM.ENABLED:=FALSE;
CTRAF.ENABLED:=FALSE;
SGTEK.ENABLED:=FALSE;
BITBTN2.ENABLED:=FALSE;
BITBTN3.ENABLED:=FALSE;

procedure
TMDIChild.R3Click(Sender:
TObject);
R1.ENABLED:=FALSE;
R2.ENABLED:=FALSE;
CMAT.ENABLED:=TRUE;
CAIR.ENABLED:=TRUE;
CBUANG.ENABLED:=TRUE;
CVOLUM.ENABLED:=TRUE;
CTRAF.ENABLED:=TRUE;
SGTEK.ENABLED:=TRUE;
BITBTN2.ENABLED:=TRUE;
BITBTN3.ENABLED:=TRUE;
CMA.ENABLED:=TRUE;

unit Rpt;
interface

uses      Windows,      SysUtils,
Messages,   Classes,    Graphics,
Controls,
TLAPORAN = class(TQuickRep)
  QRShape16: TQRShape;
  TitleBand1: TQRBand;
  QRLabel1: TQRLabel;
begin
procedure
TMDIChild.R1Click(Sender:
TObject);
begin
CAIR.ENABLED:=TRUE;
CBUANG.ENABLED:=TRUE;
CVOLUM.ENABLED:=TRUE;
CTRAF.ENABLED:=TRUE;
SGTEK.ENABLED:=TRUE;
BITBTN2.ENABLED:=TRUE;
BITBTN3.ENABLED:=TRUE;
EDIT3.TEXT:='MAINTENANCE
DREDGING';
end;

begin
CMA.ENABLED:=TRUE;
CAI.ENABLED:=TRUE;
CBUAK.ENABLED:=TRUE;
CISI.ENABLED:=TRUE;
CLALU.ENABLED:=TRUE;
SGCAP.ENABLED:=TRUE;
BITBTN6.ENABLED:=TRUE;
BITBTN7.ENABLED:=TRUE;
EDIT3.TEXT:='CAPITAL DREDGING';
end;
begin
CAI.ENABLED:=TRUE;
CBUAK.ENABLED:=TRUE;
CISI.ENABLED:=TRUE;
CLALU.ENABLED:=TRUE;
SGCAP.ENABLED:=TRUE;
BITBTN6.ENABLED:=TRUE;
BITBTN7.ENABLED:=TRUE;
EDIT3.TEXT:='CAPITAL
MAINTENANCE';
end;
END.

StdCtrls,      ExtCtrls,      Forms,
Quickrpt,     QRCtrls;      DAN

type
QRImage1: TQRImage;
QRShape1: TQRShape;
QRShape2: TQRShape;
QRLabel6: TQRLabel;

```

QRLLabel17: TQRLabel;
QRLLabel18: TQRLabel;
QRShape4: TQRShape;
QRShape5: TQRShape;
QRLLabel48: TQRLabel;
QRLLabel50: TQRLabel;
QRLLabel51: TQRLabel;
QRShape13: TQRShape;
QRShape14: TQRShape;
QRLLabel68: TQRLabel;
QRLLabel69: TQRLabel;
QRLLabel70: TQRLabel;
QRLLabel74: TQRLabel;
QRLLabel78: TQRLabel;
QRLLabel79: TQRLabel;
QRLLabel80: TQRLabel;
QRLLabel81: TQRLabel;
QRShape17: TQRShape;
QRShape18: TQRShape;
QRLLabel89: TQRLabel;
QRLLabel90: TQRLabel;
QRLLabel92: TQRLabel;
QRLLabel93: TQRLabel;
QRLLabel99: TQRLabel;
QRLLabel76: TQRLabel;
QRLLabel77: TQRLabel;
QRLLabel98: TQRLabel;
QRLLabel62: TQRLabel;
QRLLabel63: TQRLabel;
QRLLabel64: TQRLabel;
QRLLabel66: TQRLabel;
QRLLabel20: TQRLabel;
QRLLabel24: TQRLabel;
QRLLabel25: TQRLabel;
QRLLabel26: TQRLabel;
QRLLabel27: TQRLabel;
QRLLabel29: TQRLabel;
QRLLabel33: TQRLabel;
QRLLabel34: TQRLabel;
QRLLabel35: TQRLabel;
QRLLabel36: TQRLabel;
QRLLabel37: TQRLabel;
QRLLabel55: TQRLabel;
QRShape25: TQRShape;
QRShape26: TQRShape;
QRLLabel56: TQRLabel;
QRLLabel57: TQRLabel;
QRLLabel58: TQRLabel;
QRLLabel59: TQRLabel;
QRLLabel60: TQRLabel;
QRLLabel61: TQRLabel;
QRLLabel65: TQRLabel;
QRLLabel67: TQRLabel;
QRLLabel84: TQRLabel;
QRLLabel88: TQRLabel;
QRLLabel106: TQRLabel;
QRLLabel111: TQRLabel;
QRLLabel182: TQRLabel;
QRLLabel183: TQRLabel;
QRShape15: TQRShape;
QRLLabel28: TQRLabel;
QRLLabel12: TQRLabel;
QRLLabel14: TQRLabel;
QRLLabel15: TQRLabel;
QRLLabel10: TQRLabel;
QRLLabel11: TQRLabel;
QRLLabel13: TQRLabel;
QRLLabel14: TQRLabel;
QRLLabel15: TQRLabel;
QRLLabel16: TQRLabel;
QRLLabel17: TQRLabel;
QRLLabel18: TQRLabel;
QRLLabel19: TQRLabel;
QRLLabel21: TQRLabel;
QRLLabel22: TQRLabel;
QRLLabel23: TQRLabel;
QRLLabel30: TQRLabel;
QRLLabel31: TQRLabel;
QRLLabel32: TQRLabel;
QRLLabel38: TQRLabel;
QRLLabel39: TQRLabel;
QRLLabel40: TQRLabel;
QRLLabel41: TQRLabel;
QRLLabel44: TQRLabel;
QRLLabel45: TQRLabel;
QRLLabel47: TQRLabel;
QRLLabel49: TQRLabel;
QRLLabel71: TQRLabel;
QRLLabel85: TQRLabel;
QRLLabel86: TQRLabel;
QRLLabel87: TQRLabel;
QRLLabel91: TQRLabel;
QRLLabel94: TQRLabel;
QRLLabel95: TQRLabel;
QRLLabel96: TQRLabel;
QRLLabel97: TQRLabel;
QRLLabel100: TQRLabel;
QRLLabel101: TQRLabel;
QRLLabel102: TQRLabel;
QRLLabel103: TQRLabel;
QRLLabel104: TQRLabel;
QRLLabel105: TQRLabel;
QRLLabel107: TQRLabel;
QRLLabel108: TQRLabel;
QRLLabel109: TQRLabel;
QRShape3: TQRShape;
QRLLabel110: TQRLabel;
QRLLabel112: TQRLabel;
QRLLabel113: TQRLabel;
QRLLabel13: TQRLabel;
QRLLabel19: TQRLabel;

```
private           {  Private
declarations }

public          {  Public
declarations }

end;

var
  LAPORAN: TLAPORAN;

implementation

{$R *.DFM}
end.
```

D90: 0.0012 m D50: 0.00018 m r: 0.06

TRANSPORT SEDIMENT (titik 3)

| No | h (m) | V (m/dt) | Arah (o) | C (m/dt) | C90 (m/dt) | μ | μ_0 (m/dt) | τ_χ (N/m ²) | ao | fw | x | τ_{cw} (N/m ²) | S _b (m ³ /dt) | V* | ε | C _b | C ₁ | S _s (m ³ /dt) | Stot (m ³ /dt) |
|----|----------|-------------|-------------|-------------|---------------|-------|-------------------|------------------------------------|-------|-------|------|------------------------------------|--|-------|---------------|----------------|----------------|--|------------------------------|
| 1 | 9.00 | 0.2 | 35 | 58.595 | 89.176 | 0.533 | 4.721 | 1.17E-01 | 7.390 | 0.020 | 1.86 | 56.330 | 7.71E-06 | 0.234 | 0.338 | 9.10E-05 | 6.09E-05 | 1.28E-04 | 1.30E-04 |
| 2 | 9.00 | 0.3 | 40 | 58.595 | 89.176 | 0.533 | 4.721 | 2.64E-01 | 7.390 | 0.020 | 1.86 | 56.477 | 8.77E-06 | 0.235 | 0.338 | 1.10E-04 | 7.37E-05 | 1.56E-04 | 1.48E-04 |
| 3 | 9.00 | 0.1 | 40 | 58.595 | 89.176 | 0.533 | 4.721 | 2.93E-02 | 7.390 | 0.020 | 1.86 | 56.242 | 4.55E-06 | 0.234 | 0.337 | 5.17E-05 | 3.46E-05 | 7.29E-05 | 7.66E-05 |
| 4 | 9.00 | 0.1 | 60 | 58.595 | 89.176 | 0.533 | 4.721 | 2.93E-02 | 7.390 | 0.020 | 1.86 | 56.242 | 4.55E-06 | 0.234 | 0.337 | 5.17E-05 | 3.46E-05 | 7.29E-05 | 7.66E-05 |

Transport: Ke Utara: 0.000430600 m³/detik = 13579.407 m³/tahun

Ke Selatan: 0 m³/detik

Total: 13579.407 m³/tahun

Jika luas kolam: 255000 m³ dan luas dasar: 180200 m³ maka sedimentasi/tahun = 0.0624053 m = 6.624 cm/tahun.

PROFIL

CHEK STABILITAS kolam labuh (slope 1:4)

19 13

0. 300. 300. 300. 1
300. 300. 320. 295. 1
320. 295. 358. 293. 2
358. 293. 370. 290. 3
370. 290. 374. 289. 4
374. 289. 590. 289. 4
590. 289. 594. 290. 4
594. 290. 606. 293. 3
606. 293. 714. 295. 2
714. 295. 734. 300. 1
734. 300. 1034. 300. 1
0. 295. 320. 295. 2
714. 295. 1034. 295. 2
0. 293. 358. 293. 3
606. 293. 1034. 293. 3
0. 289. 374. 289. 4
590. 289. 1034. 289. 4
0. 289. 374. 289. 4
590. 289. 1034. 289. 4

SOIL

4

14. 14. 0. 27. 0. 0. 1
15. 15. 0. 28. 0. 0. 2
16. 16. 0. 30. 0. 0. 3
17. 17. 0. 31. 0. 0. 4

WATER

1 10.055

2

0. 302.
1034. 302.

CIRCLE

5 5

0. 300. 374. 590.
0. 1. 0. 0.

1

--SLOPE STABILITY ANALYSIS--
 SIMPLIFIED JANBU METHOD OF SLICES
 IRREGULAR FAILURE SURFACES

PROBLEM DESCRIPTION BENOA SLOPE 1:4

BOUNDARY COORDINATES

13 TOP BOUNDARIES
 19 TOTAL BOUNDARIES

| TYPE | BOUNDARY | X-LEFT | Y-LEFT | X-RIGHT | Y-RIGHT | SOIL |
|------|----------|--------|--------|---------|---------|-----------|
| | NO. | (FT) | (FT) | (FT) | (FT) | BELOW BND |
| | 1 | 00 | 300.00 | 300.00 | 300.00 | 1 |
| | 2 | 300.00 | 300.00 | 320.00 | 295.00 | 1 |
| | 3 | 320.00 | 295.00 | 358.00 | 293.00 | 2 |
| | 4 | 358.00 | 293.00 | 370.00 | 290.00 | 3 |
| | 5 | 370.00 | 290.00 | 374.00 | 289.00 | 4 |
| | 6 | 374.00 | 289.00 | 590.00 | 289.00 | 4 |
| | 7 | 590.00 | 289.00 | 594.00 | 290.00 | 4 |
| | 8 | 594.00 | 290.00 | 606.00 | 293.00 | 3 |
| | 9 | 606.00 | 293.00 | 714.00 | 295.00 | 2 |
| | 10 | 714.00 | 295.00 | 734.00 | 300.00 | 1 |
| | 11 | 734.00 | 300.00 | 1034.00 | 300.00 | 1 |
| | 12 | .00 | 295.00 | 320.00 | 295.00 | 2 |
| | 13 | 714.00 | 295.00 | 1034.00 | 295.00 | 2 |
| | 14 | .00 | 293.00 | 358.00 | 293.00 | 3 |
| | 15 | 606.00 | 293.00 | 1034.00 | 293.00 | 3 |
| | 16 | .00 | 289.00 | 374.00 | 289.00 | 4 |
| | 17 | 590.00 | 289.00 | 1034.00 | 289.00 | 4 |
| | 18 | .00 | 289.00 | 374.00 | 289.00 | 4 |
| | 19 | 590.00 | 289.00 | 1034.00 | 289.00 | 4 |

1 ISOTROPIC SOIL PARAMETERS

4 TYPE(S) OF SOIL

| SOIL | TOTAL | SATURATED | COHESION | FRICITION | PORE |
|----------|-------------|-----------|-----------|-----------|------------------|
| PRESSURE | PIEZOMETRIC | | | | |
| TYPE | UNIT WT. | UNIT WT. | INTERCEPT | ANGLE | PRESSURE |
| | | | | | CONSTANT SURFACE |

| NO. | (PCF) | (PCF) | (PSF) | (DEG) | PARAMETER | (PSF) |
|-----|-------|-------|-------|-------|-----------|-------|
|-----|-------|-------|-------|-------|-----------|-------|

| | | | | | | | |
|---|------|------|----|------|-----|----|---|
| 1 | 14.0 | 14.0 | .0 | 27.0 | .00 | .0 | 1 |
| 2 | 15.0 | 15.0 | .0 | 28.0 | .00 | .0 | 2 |
| 3 | 16.0 | 16.0 | .0 | 30.0 | .00 | .0 | 3 |
| 4 | 17.0 | 17.0 | .0 | 31.0 | .00 | .0 | 4 |

1 1 PIEZOMETRIC SURFACE(S) HAVE BEEN SPECIFIED

UNITWEIGHT OF WATER = 10.06

PIEZOMETRIC SURFACE NO. 1 SPECIFIED BY 2 COORDINATE POINTS

| POINT NO. | X-WATER (FT) | Y-WATER (FT) |
|--------------|-----------------|-----------------|
|--------------|-----------------|-----------------|

| | | |
|---|--------|--------|
| 1 | .00 | 302.00 |
| 2 | 900.00 | 302.00 |

1 A CRITICAL FAILURE SURFACE SEARCHING METHOD, USING A RANDOM

TECHNIQUE FOR GENERATING CIRCULAR SURFACES, HAS BEEN SPECIFIED.

25 TRIAL SURFACES HAVE BEEN GENERATED.

5 SURFACES INITIATE FROM EACH OF 5 POINTS EQUALLY SPACED

ALONG THE GROUND SURFACE BETWEEN X = .00 FT.
AND X = 300.00 FT.

EACH SURFACE TERMINATES BETWEEN X = 340.00 FT.
AND X = 556.00 FT.

UNLESS FURTHER LIMITATIONS WERE IMPOSED, THE MINIMUM ELEVATION

AT WHICH A SURFACE EXTENDS IS Y = .00 FT.

100 FT. LINE SEGMENTS DEFINE EACH TRIAL FAILURE SURFACE.

THE FOLLOWING ARE DISPLAYED THE TEN MOST CRITICAL OF THE TRIAL

FAILURE SURFACES EXAMINED. THEY ARE ORDERED -
MOST CRITICAL
FIRST

FAILURE SURFACE SPECIFIED BY 37 COORDINATE POINTS

| POINT NO. | X-SURF (FT) | Y-SURF (FT) |
|--------------|----------------|----------------|
| 1 | 210.00 | 300.00 |
| 2 | 210.73 | 305.31 |
| 3 | 211.49 | 310.67 |
| 4 | 212.29 | 312.07 |
| 5 | 213.13 | 314.52 |
| 6 | 213.99 | 314.01 |
| 7 | 214.88 | 315.56 |
| 8 | 215.80 | 316.16 |
| 9 | 216.74 | 316.82 |
| 10 | 217.70 | 316.53 |
| 11 | 218.67 | 316.29 |
| 12 | 219.65 | 316.12 |
| 13 | 220.64 | 312.99 |
| 14 | 221.64 | 312.93 |
| 15 | 222.64 | 312.93 |
| 16 | 223.64 | 313.98 |
| 17 | 224.63 | 316.09 |
| 18 | 225.62 | 316.26 |
| 19 | 226.59 | 316.48 |
| 20 | 227.55 | 316.76 |
| 21 | 228.50 | 316.10 |
| 22 | 229.42 | 316.49 |
| 23 | 230.31 | 318.93 |
| 24 | 231.18 | 320.42 |
| 25 | 232.02 | 320.96 |
| 26 | 232.83 | 320.55 |
| 27 | 233.60 | 320.19 |
| 28 | 234.34 | 320.87 |
| 29 | 235.03 | 322.59 |
| 30 | 235.68 | 322.35 |
| 31 | 236.28 | 322.15 |
| 32 | 236.84 | 322.98 |
| 33 | 237.35 | 323.84 |
| 34 | 237.81 | 324.75 |
| 35 | 238.21 | 325.64 |
| 36 | 238.57 | 326.58 |
| 37 | 238.75 | 327.10 |

*** 1.319 ***

FAILURE SURFACE SPECIFIED BY 31 COORDINATE POINTS

| POINT NO. | X-SURF (FT) | Y-SURF (FT) |
|--------------|----------------|----------------|
| 1 | 212.50 | 320.00 |
| 2 | 213.39 | 319.54 |
| 3 | 214.30 | 319.12 |
| 4 | 215.23 | 318.75 |
| 5 | 216.18 | 318.44 |
| 6 | 217.14 | 318.17 |
| 7 | 218.12 | 317.96 |
| 8 | 219.10 | 317.80 |
| 9 | 220.10 | 317.69 |
| 10 | 221.10 | 317.64 |
| 11 | 222.10 | 317.64 |
| 12 | 230.09 | 317.69 |
| 13 | 234.09 | 317.80 |
| 14 | 235.08 | 317.95 |
| 15 | 236.05 | 318.17 |
| 16 | 237.02 | 318.43 |
| 17 | 237.97 | 318.75 |
| 18 | 238.90 | 319.11 |
| 19 | 239.81 | 319.52 |
| 20 | 240.70 | 319.99 |
| 21 | 241.56 | 320.50 |
| 22 | 242.39 | 321.05 |
| 23 | 243.19 | 321.65 |
| 24 | 243.96 | 322.29 |
| 25 | 244.69 | 322.97 |
| 26 | 245.39 | 323.69 |
| 27 | 246.04 | 324.44 |
| 28 | 246.66 | 325.23 |
| 29 | 247.23 | 326.05 |
| 30 | 247.75 | 326.90 |
| 31 | 247.86 | 327.10 |

*** 1.350 ***

FAILURE SURFACE SPECIFIED BY 33 COORDINATE POINTS

| POINT NO. | X-SURF (FT) | Y-SURF (FT) |
|--------------|----------------|----------------|
| 1 | 200.00 | 320.00 |
| 2 | 200.94 | 319.65 |
| 3 | 210.89 | 319.33 |
| 4 | 210.85 | 319.05 |
| 5 | 210.82 | 318.81 |
| 6 | 2144.80 | 318.61 |
| 7 | 215.78 | 318.45 |
| 8 | 216.78 | 318.33 |
| 9 | 217.77 | 318.25 |
| 10 | 218.77 | 318.20 |
| 11 | 219.77 | 318.20 |
| 12 | 220.77 | 318.24 |
| 13 | 221.77 | 318.31 |
| 14 | 222.76 | 318.43 |
| 15 | 223.75 | 318.58 |
| 16 | 224.73 | 318.78 |
| 17 | 225.70 | 319.01 |
| 18 | 226.67 | 319.28 |
| 19 | 227.62 | 319.59 |
| 20 | 228.55 | 319.93 |
| 21 | 229.48 | 320.32 |
| 22 | 230.39 | 320.74 |
| 23 | 231.28 | 321.19 |
| 24 | 232.15 | 321.68 |
| 25 | 233.00 | 322.21 |
| 26 | 234.83 | 322.76 |
| 27 | 234.64 | 323.35 |
| 28 | 235.42 | 323.98 |
| 29 | 236.18 | 324.63 |
| 30 | 236.91 | 325.31 |
| 31 | 237.61 | 326.02 |
| 32 | 238.29 | 326.76 |
| 33 | 238.58 | 327.10 |

*** 1.364 ***

FAILURE SURFACE SPECIFIED BY 36 COORDINATE POINTS

| POINT NO. | X-SURF (FT) | Y-SURF (FT) |
|--------------|----------------|----------------|
| 1 | 220.00 | 320.00 |
| 2 | 220.77 | 319.36 |
| 3 | 221.57 | 318.77 |
| 4 | 222.41 | 318.22 |
| 5 | 223.27 | 317.72 |
| 6 | 224.17 | 317.26 |
| 7 | 225.08 | 316.86 |
| 8 | 226.02 | 316.51 |
| 9 | 226.97 | 316.21 |
| 10 | 227.94 | 315.96 |
| 11 | 228.92 | 315.77 |
| 12 | 229.91 | 315.63 |
| 13 | 230.91 | 315.55 |
| 14 | 231.91 | 315.52 |
| 15 | 232.91 | 315.55 |
| 16 | 233.90 | 315.63 |
| 17 | 234.89 | 315.77 |
| 18 | 235.88 | 315.97 |
| 19 | 236.84 | 316.21 |
| 20 | 237.80 | 316.51 |
| 21 | 238.75 | 316.87 |
| 22 | 239.65 | 317.27 |
| 23 | 240.54 | 317.73 |
| 24 | 241.40 | 318.23 |
| 25 | 242.24 | 318.78 |
| 26 | 243.04 | 319.38 |
| 27 | 243.81 | 320.02 |
| 28 | 244.54 | 320.70 |
| 29 | 245.34 | 321.42 |
| 30 | 245.89 | 322.18 |
| 31 | 246.50 | 322.97 |
| 32 | 247.06 | 323.79 |
| 33 | 247.58 | 324.65 |
| 34 | 248.05 | 325.53 |
| 35 | 248.47 | 326.44 |
| 36 | 248.76 | 327.10 |

*** 1.394 ***

1

FAILURE SURFACE SPECIFIED BY 29 COORDINATE POINTS

| POINT NO. | X-SURF (FT) | Y-SURF (FT) |
|--------------|----------------|----------------|
| 1 | 225.00 | 320.00 |
| 2 | 225.83 | 329.44 |
| 3 | 226.69 | 328.94 |
| 4 | 227.59 | 328.50 |
| 5 | 228.52 | 328.11 |
| 6 | 229.46 | 327.80 |
| 7 | 230.43 | 327.54 |
| 8 | 231.41 | 327.35 |
| 9 | 232.40 | 327.23 |
| 10 | 233.40 | 327.17 |
| 11 | 234.40 | 327.18 |
| 12 | 235.40 | 327.26 |
| 13 | 236.39 | 327.40 |
| 14 | 237.37 | 327.61 |
| 15 | 238.33 | 327.89 |
| 16 | 239.27 | 328.22 |
| 17 | 240.19 | 328.63 |
| 18 | 241.07 | 329.09 |
| 19 | 241.93 | 329.61 |
| 20 | 242.75 | 330.18 |
| 21 | 243.52 | 330.81 |
| 22 | 244.26 | 330.49 |
| 23 | 244.94 | 332.22 |
| 24 | 245.58 | 332.99 |
| 25 | 246.16 | 333.80 |
| 26 | 246.69 | 334.65 |
| 27 | 247.16 | 335.53 |
| 28 | 247.57 | 336.45 |
| 29 | 247.81 | 337.10 |

*** 1.431 ***

FAILURE SURFACE SPECIFIED BY 37 COORDINATE POINTS

| POINT NO. | X-SURF (FT) | Y-SURF (FT) |
|--------------|----------------|----------------|
| 1 | 210.00 | 320.00 |
| 2 | 210.73 | 319.31 |
| 3 | 211.50 | 318.67 |
| 4 | 212.30 | 318.08 |
| 5 | 213.14 | 317.53 |
| 6 | 214.00 | 317.03 |
| 7 | 214.90 | 316.59 |
| 8 | 215.82 | 316.20 |
| 9 | 216.76 | 315.86 |
| 10 | 217.72 | 315.58 |
| 11 | 218.70 | 315.35 |
| 12 | 221.68 | 315.19 |
| 13 | 222.68 | 315.08 |
| 14 | 222.67 | 315.03 |
| 15 | 222.67 | 315.03 |
| 16 | 223.67 | 315.10 |
| 17 | 224.66 | 315.22 |
| 18 | 225.65 | 315.41 |
| 19 | 226.62 | 315.65 |
| 20 | 227.57 | 315.94 |
| 21 | 228.51 | 316.29 |
| 22 | 229.42 | 316.70 |
| 23 | 230.31 | 317.16 |
| 24 | 231.17 | 317.67 |
| 25 | 232.00 | 318.23 |
| 26 | 232.79 | 318.84 |
| 27 | 233.55 | 319.49 |
| 28 | 234.27 | 320.19 |
| 29 | 234.95 | 320.2 |
| 30 | 235.58 | 321. |
| 31 | 236.16 | 322.1 |
| 32 | 236.70 | 333.35 |
| 33 | 237.18 | 324.23 |
| 34 | 237.62 | 325.13 |
| 35 | 238.00 | 326.05 |
| 36 | 238.32 | 327.00 |
| 37 | 238.35 | 327.10 |

*** 1.463 ***

1

FAILURE SURFACE SPECIFIED BY 34 COORDINATE POINTS

| POINT NO. | X-SURF (FT) | Y-SURF (FT) |
|--------------|----------------|----------------|
| 1 | 222.50 | 320.00 |
| 2 | 223.25 | 329.34 |
| 3 | 224.04 | 328.72 |
| 4 | 224.86 | 328.16 |
| 5 | 225.72 | 327.65 |
| 6 | 226.61 | 327.19 |
| 7 | 227.53 | 326.79 |
| 8 | 228.47 | 326.45 |
| 9 | 229.43 | 326.17 |
| 10 | 230.40 | 325.94 |
| 11 | 231.39 | 325.78 |
| 12 | 232.39 | 325.69 |
| 13 | 233.38 | 325.65 |
| 14 | 234.38 | 325.68 |
| 15 | 235.38 | 325.77 |
| 16 | 236.37 | 325.92 |
| 17 | 237.35 | 326.13 |
| 18 | 238.31 | 326.41 |
| 19 | 239.25 | 326.74 |
| 20 | 240.17 | 327.13 |
| 21 | 241.06 | 327.58 |
| 22 | 241.93 | 328.08 |
| 23 | 242.76 | 328.64 |
| 24 | 243.55 | 329.25 |
| 25 | 244.31 | 329.90 |
| 26 | 245.02 | 330.61 |
| 27 | 245.68 | 331.35 |
| 28 | 246.30 | 332.14 |
| 29 | 246.87 | 332.96 |
| 30 | 247.39 | 333.82 |
| 31 | 247.85 | 334.71 |
| 32 | 248.25 | 335.62 |
| 33 | 248.60 | 336.56 |
| 34 | 248.76 | 337.10 |

*** 1.471 ***

FAILURE SURFACE SPECIFIED BY 34 COORDINATE POINTS

| POINT NO. | X-SURF (FT) | Y-SURF (FT) |
|--------------|----------------|----------------|
| 1 | 252.50 | 330.00 |
| 2 | 253.23 | 333.31 |
| 3 | 253.99 | 338.67 |
| 4 | 254.80 | 338.08 |
| 5 | 255.64 | 337.54 |
| 6 | 256.52 | 337.06 |
| 7 | 257.42 | 336.63 |
| 8 | 258.35 | 336.27 |
| 9 | 259.31 | 335.96 |
| 10 | 261.28 | 335.72 |
| 11 | 271.26 | 335.54 |
| 12 | 272.25 | 335.42 |
| 13 | 273.25 | 335.37 |
| 14 | 274.25 | 335.38 |
| 15 | 275.25 | 335.45 |
| 16 | 276.24 | 335.59 |
| 17 | 277.22 | 335.79 |
| 18 | 278.18 | 336.05 |
| 19 | 279.13 | 336.38 |
| 20 | 280.05 | 336.77 |
| 21 | 280.95 | 337.21 |
| 22 | 281.81 | 337.71 |
| 23 | 282.64 | 338.27 |
| 24 | 283.44 | 338.87 |
| 25 | 284.19 | 339.53 |
| 26 | 284.90 | 340.23 |
| 27 | 285.57 | 340.98 |
| 28 | 286.18 | 341.77 |
| 29 | 286.74 | 342.60 |
| 30 | 287.25 | 343.46 |
| 31 | 287.70 | 344.35 |
| 32 | 288.10 | 345.27 |
| 33 | 288.43 | 346.21 |
| 34 | 288.68 | 347.10 |

*** 1.496 ***

1

FAILURE SURFACE SPECIFIED BY 35 COORDINATE POINTS

| POINT NO. | X-SURF (FT) | Y-SURF (FT) |
|--------------|----------------|----------------|
| 1 | 255.50 | 330.00 |
| 2 | 255.21 | 330.29 |
| 3 | 255.96 | 330.63 |
| 4 | 260.75 | 338.03 |
| 5 | 265.59 | 337.47 |
| 6 | 266.45 | 336.97 |
| 7 | 267.35 | 336.53 |
| 8 | 268.27 | 336.15 |
| 9 | 269.22 | 335.83 |
| 10 | 270.19 | 335.57 |
| 11 | 271.17 | 335.37 |
| 12 | 272.16 | 335.24 |
| 13 | 273.16 | 335.18 |
| 14 | 274.16 | 335.18 |
| 15 | 275.15 | 335.24 |
| 16 | 276.15 | 335.38 |
| 17 | 277.13 | 335.57 |
| 18 | 278.09 | 335.83 |
| 19 | 279.04 | 336.15 |
| 20 | 279.96 | 336.53 |
| 21 | 280.86 | 336.98 |
| 22 | 281.73 | 337.48 |
| 23 | 282.56 | 338.03 |
| 24 | 283.35 | 338.64 |
| 25 | 284.10 | 339.30 |
| 26 | 284.81 | 340.01 |
| 27 | 285.47 | 340.76 |
| 28 | 286.08 | 341.55 |
| 29 | 286.63 | 342.38 |
| 30 | 287.14 | 343.25 |
| 31 | 287.58 | 344.15 |
| 32 | 287.96 | 345.07 |
| 33 | 288.28 | 346.02 |
| 34 | 288.54 | 346.98 |
| 35 | 288.57 | 347.10 |

*** 1.508 ***

FAILURE SURFACE SPECIFIED BY 30 COORDINATE POINTS

| POINT NO. | X-SURF (FT) | Y-SURF (FT) |
|--------------|----------------|----------------|
|--------------|----------------|----------------|

| | | |
|-----|-----------|--------|
| 1 | 262.50 | 330.00 |
| 2 | 263.48 | 339.79 |
| 3 | 264.46 | 339.62 |
| 4 | 265.45 | 339.48 |
| 5 | 266.45 | 339.37 |
| 6 | 267.44 | 339.30 |
| 7 | 268.44 | 339.26 |
| 8 | 269.44 | 339.26 |
| 9 | 270.44 | 339.29 |
| 10 | 271.44 | 339.36 |
| 11 | 272.44 | 339.46 |
| 12 | 273.43 | 339.60 |
| 13 | 274.41 | 339.77 |
| 14 | 275.39 | 339.97 |
| 15 | 276.36 | 340.21 |
| 16 | 277.32 | 340.48 |
| 17 | 318.28 | 340.79 |
| 18 | 319.22 | 341.13 |
| 19 | 320.15 | 341.50 |
| 20 | 321.06 | 341.90 |
| 21 | 321.96 | 342.33 |
| 22 | 322.85 | 342.80 |
| 23 | 323.72 | 343.30 |
| 24 | 324.57 | 343.82 |
| 25 | 325.40 | 344.38 |
| 26 | 326.21 | 344.96 |
| 27 | 327.00 | 345.57 |
| 28 | 327.77 | 346.21 |
| 29 | 328.52 | 346.87 |
| 30 | 328.76 | 347.10 |
| *** | 1.518 *** | |

| | Y | A | X _t L | T | S | F | P |
|---|--------|------------|---------------------|--------|--------|--------|---|
| X | .00 | 129.25 | 258.50 | 387.75 | 517.00 | 646.25 | |
| | - | - | - | - | - | - | |
| | . | 161.422. | . | 114* | | | |
| | - | - | - | - | - | - | |
| | . | 9114232. | . | | | | |
| | - | - | - | - | - | - | |
| | . | 1145230. | . | | | | |
| | - | - | - | - | - | - | |
| | 9 | 9145.220.. | . | | | | |
| | - | - | - | - | - | - | |
| | . | 11455230. | . | | | | |
| | - | - | - | - | - | - | |
| | 14 | 14.52.30.. | . | | | | |
| | - | - | - | - | - | - | |
| | . | 14.523.0. | . | | | | |
| | - | - | - | - | - | - | |
| | 14 | 14.52330.* | . | | | | |
| | - | - | - | - | - | - | |
| | 14 | 14.523.0. | . | | | | |
| | - | - | - | - | - | - | |
| | 14 | 14..230.. | . | | | | |
| | - | - | - | - | - | - | |
| | 147 | 147.230.* | * | | | | |
| | - | - | - | - | - | - | |
| | 14 | 14.230. | . | | | | |
| | - | - | - | - | - | - | |
| | 147 | 147.25. | . | | | | |
| | - | - | - | - | - | - | |
| | 197250 | 197250 | | | | | |
| | - | - | - | - | - | - | |
| | 49325 | 49325 | | | | | |
| | - | - | - | - | - | - | |
| | 11732 | 11732 | | | | | |
| | - | - | - | - | - | - | |
| | 132 | 132 | | | | | |
| X | 387.75 | 387.75 | + | + | + | + | + |
| | - | - | - | - | - | - | - |
| | 113 | 113 | | | | | |

1

T 1034.00 + *
* 4 *

F 904.75 + -

775.50 + -

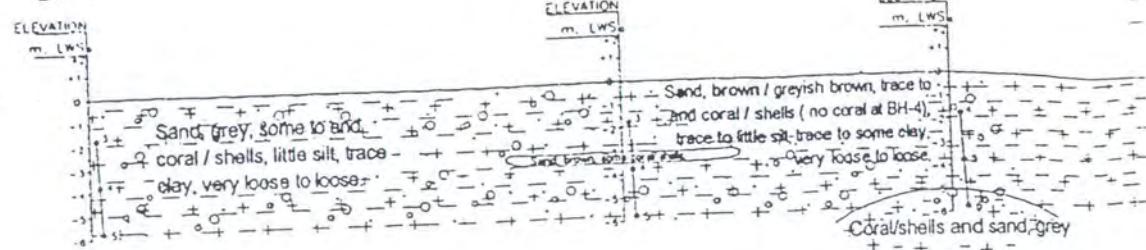
S 646.25 + -

*
**

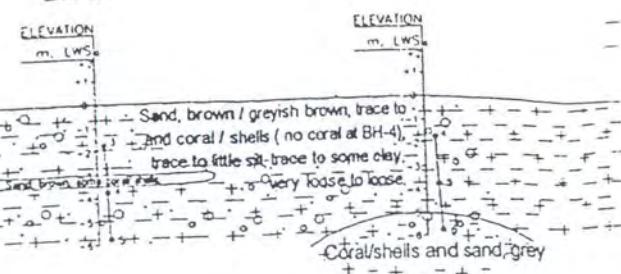
W

*

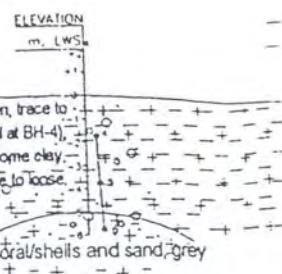
BH-1



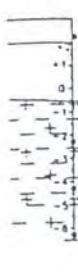
BH-2



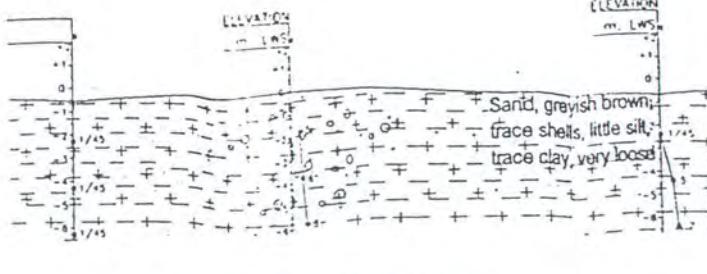
BH-3



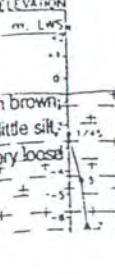
BH-4



BH-5

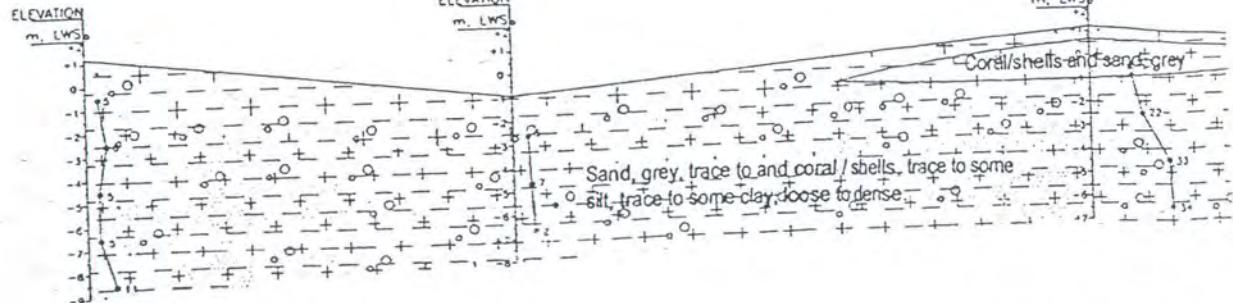


BH-6

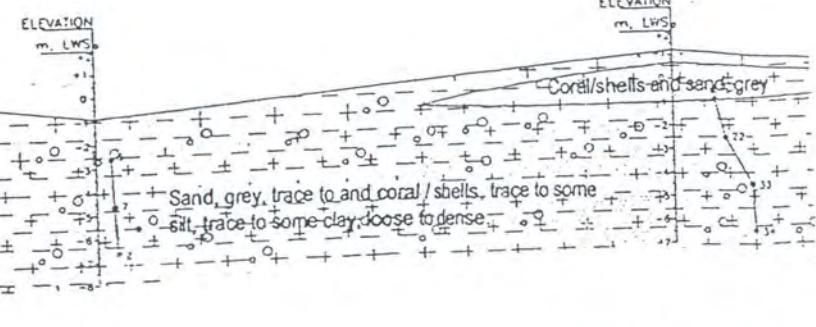


POTONGAN I-I

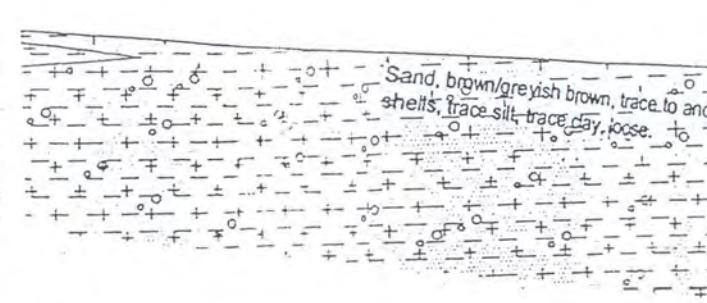
BH-14



BH-11

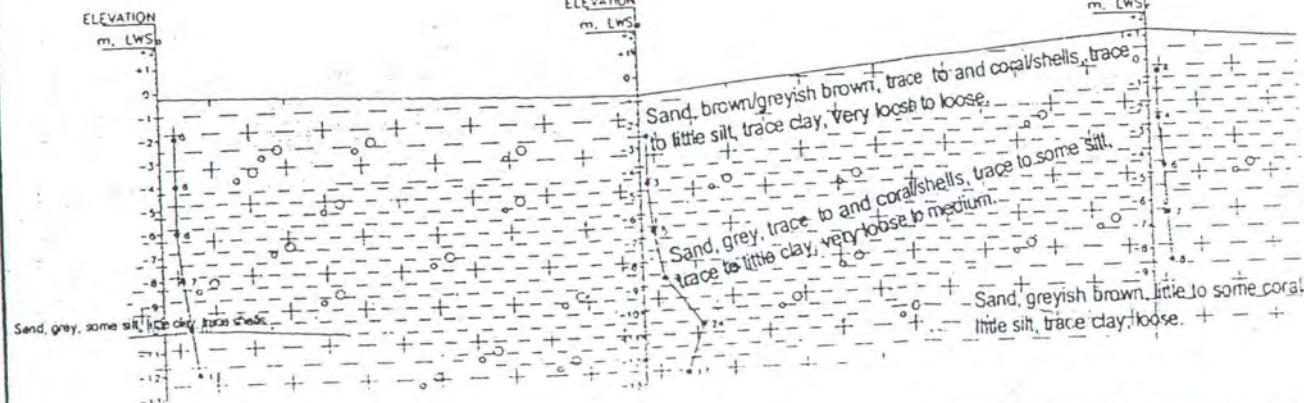


BH-21

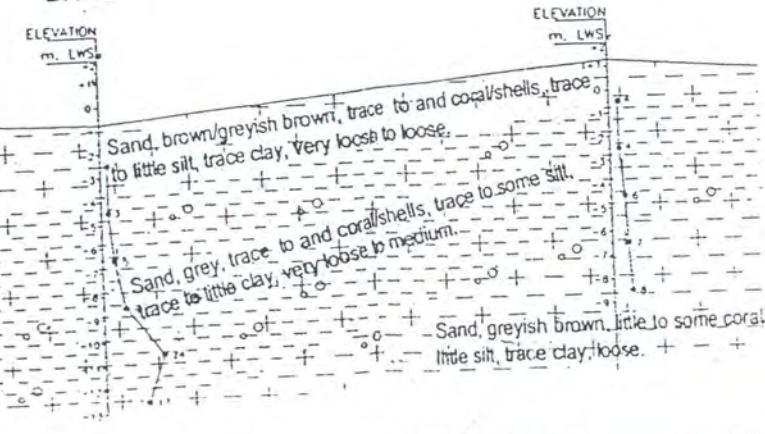


POTONGAN II-II

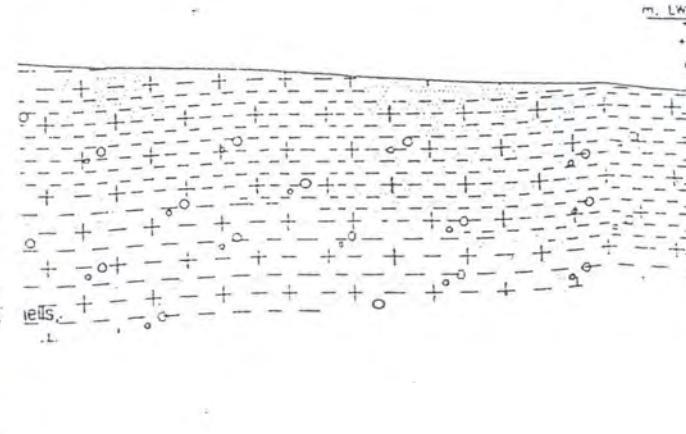
BH-15



BH-16



BH-12



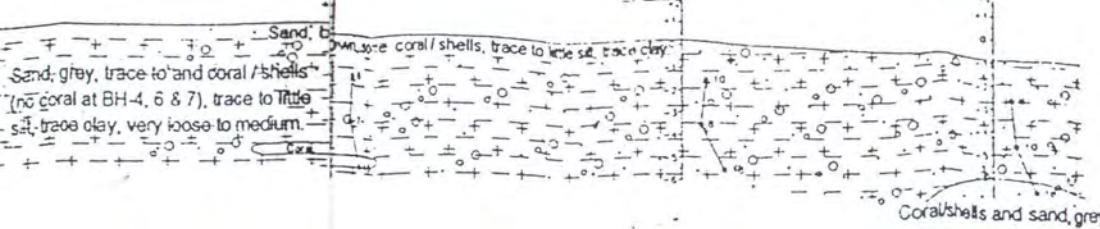
POTONGAN III-III

BH-7

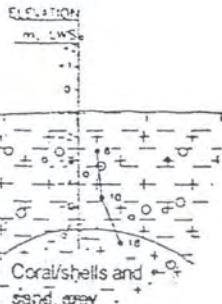
BH-8

BH-9

BH-10

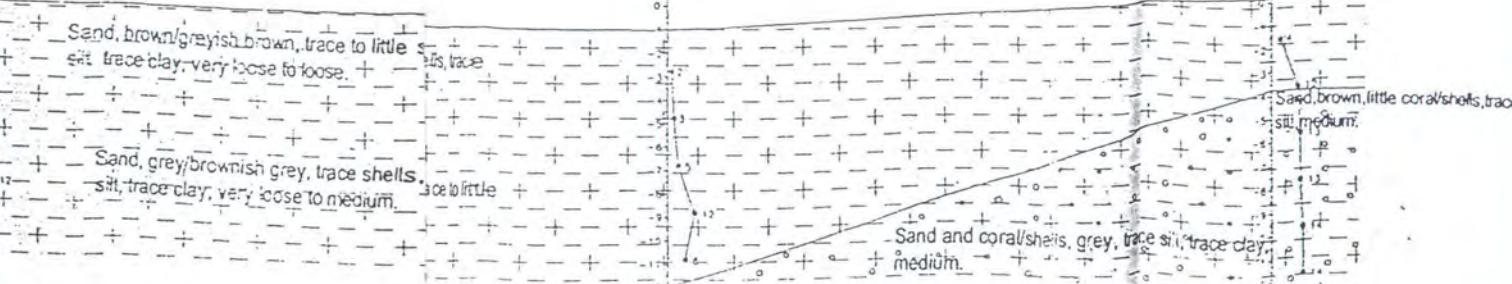


BH-10



BH-19

BH-20



POTONGAN IV-IV

PT (Persero) Pelabuhan Indonesia III

SURABAYA

NAMA PROJEK
PROJECT

**PEKERJAAN SOIL INVESTIGATION
DI PELABUHAN BENOA
UNTUK PERENCANAAN PENGERUKAN**

CATATAN
NOTE

Keterangan :

- Sand
- Clay
- Silt
- Coral



DEPARTEMEN PENDIDIKAN DAN KEBUDAYAAN
LEMBAGA PENGABDIAN KEPADA MASYARAKAT
INSTITUT TEKNOLOGI SEPULUH NOPEMBER
Kampus ITS Kemiru Simoko Glangsa Telp. (031) 5894892

MENGETAHUI/MENYETUJUI
APPROVEDDIKETAHUI
KNOWN BYDISETUJUI
APPROVED BYDIRENCANAKAN
DESIGN BYDICAMBARKAN
ACAD BYJUDUL GAMBAR
DRAWING

PERKIRAAN PROFIL TANAH

| | |
|-------------------|--------------------|
| KODE BM CIN 10 | RSP. TAHUN 2010 |
| 33 | |
| FILE | |

