

TUGAS AKHIR – TL184834

ANALISIS PENGARUH VARIASI KUAT ARUS LISTRIK ELECTRIC ARC FURNACE PADA PROSES SMELTING PASIR MONASIT TERHADAP KOMPOSISI SENYAWA DAN GRADE ThO₂

KAISAR AKBAR PURWANTO NRP. 02511840000023

Dosen Pembimbing Fakhreza Abdul, S.T., M.T. NIP. 199102172015041002 Sungging Pintowantoro, S.T., M.T., Ph.D.Eng. NIP. 196809302000031001

Program Studi Teknik Material Departemen Teknik Material dan Metalurgi Fakultas Teknologi Industri dan Rekayasa Sistem Institut Teknologi Sepuluh Nopember Surabaya 2022



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FINAL PROJECT – TL184834

ANALYSIS ON EFFECT OF VARIATION ELECTRIC ARC FURNACE CURRENT IN SMELTING PROCESS OF MONAZITE SAND ON COMPOUND COMPOSITION AND GRADE OF ThO $_2$

KAISAR AKBAR PURWANTO NRP. 02511840000023

Advisor Fakhreza Abdul, S.T., M.T. NIP. 199102172015041002 Sungging Pintowantoro, S.T., M.T., Ph.D.Eng. NIP. 196809302000031001

Study Program of Materials Engineering Departement of Materials and Metallurgical Engineering Faculty of Industrial Technology and Systems Engineering Institut Teknologi Sepuluh Nopember Surabaya 2022 (This page is intentionally blank)

LEMBAR PENGESAHAN

ANALISIS PENGARUH VARIASI KUAT ARUS LISTRIK *ELECTRIC ARC* FURNACE PADA PROSES SMELTING PASIR MONASIT TERHADAP KOMPOSISI SENYAWA DAN GRADE THO2

TUGAS AKHIR

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Oleh : KAISAR AKBAR PURWANTO NRP. 02511840000023

Disetujui oleh Tim Penguji Tugas Akhir :

- 1. Fakhreza Abdul, S.T., M.T.
- 2. Sungging Pintowantoro, S.T., M.T., Ph.D.Eng.
- 3. Mavindra Ramadhani, S.T., M.T.
- 4. Dian Mughni Fellicia, S.T., M.Sc.



SURABAYA Juli, 2022





APPROVAL SHEET

ANALYSIS ON EFFECT OF VARIATION ELECTRIC ARC FURNACE CURRENT IN SMELTING PROCESS OF MONAZITE SAND ON COMPOUND COMPOSITION AND GRADE OF ThO₂

FINAL PROJECT

Submitted to fulfill one of the requirements for obtaining a degree of bachelor of engineering at Undergraduate Study Program of Materials Engineering Departement of Materials and Metallurgical Engineering Faculty of Industrial Technology and Systems Engineering Institut Teknologi Sepuluh Nopember

> By : KAISAR AKBAR PURWANTO NRP. 02511840000023

Approved by Final Project Examiner Team :

KEBUDA

- 1. Fakhreza Abdul, S.T., M.T.
- 2. Sungging Pintowantoro, S.T., M.T., Ph.D.Eng.
- 3. Mavindra Ramadhani, S.T., M.T.
- 4. Dian Mughni Fellicia, S.T., M.Sc.

Advisor

SURABAYA July, 2022

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PERNYATAAN ORISINALITAS

Yang bertanda tangan di bawah ini:

Nama mahasiswa/NRP	: Kaisar Akbar Purwanto/02511840000023
Departemen	: Teknik Material dan Metalurgi FTIRS-ITS
Dosen Pembimbing/NIP	: Fakhreza Abdul, S.T., M.T./ 199102172015041002

Dengan ini menyatakan bahwa Tugas Akhir dengan judul "ANALISIS PENGARUH VARIASI KUAT ARUS LISTRIK *ELECTRIC ARC FURNACE* PADA PROSES *SMELTING* PASIR MONASIT TERHADAP KOMPOSISI SENYAWA DAN *GRADE* ThO₂" adalah hasil karya sendiri, bersifat orisinal, dan ditulis dengan mengikuti kaidah penulisan ilmiah.

Bilamana di kemudian hari ditemukan ketidaksesuaian dengan pernyataan ini, maka saya bersedia menerima sanksi sesuai dengan ketentuan yang berlaku di Institut Teknologi Sepuluh Nopember.

Surabaya, 1 Juli 2022

Mengetahui Dosen Pembimbing

(Fakhreza Abdul, S.T., M.T.) NIP. 199102172015041002 Mahasiswa

(Kaisar Akbar Purwanto) NRP. 02511840000023



STATEMENT OF ORIGINALITY

The undersigned below:

Name of student/NRP: Kaisar Akbar Purwanto/02511840000023 : Materials and Metallurgical Engineering FTIRS-ITS Departement : Fakhreza Abdul, S.T., M.T./ 199102172015041002 Advisor/NIP

Hereby declare that the Final Project with the title of "ANALYSIS ON EFFECT OF VARIATION ELECTRIC ARC FURNACE CURRENT IN SMELTING PROCESS OF VARIATING PROCESS OF MONAZITE SAND ON COMPOUND COMPOSITION AND GRADE OF ThO₂" is the result of my own work, is original, and is written by following the rules of scientific writing.

If in the future there is a discrepancy with this statement, then I am willing to accept sanctions in accordance with the provisions that apply at Institut Teknologi Sepuluh Nopember.

Surabaya, 1st July 2022

Acknowledged Advisor

(Fakhreza Abdul, S.T., M.T.) NIP. 199102172015041002

Student

(Kaisar Akbar Purwanto) NRP.02511840000023



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ANALISIS PENGARUH VARIASI KUAT ARUS LISTRIK *ELECTRIC ARC FURNACE* PADA PROSES *SMELTING* PASIR MONASIT TERHADAP KOMPOSISI SENYAWA DAN *GRADE* ThO₂

Nama Mahasiswa / NRP Departemen Dosen Pembimbing : Kaisar Akbar Purwanto/02511840000023 : Teknik Material dan Metalurgi FTIRS-ITS : Fakhreza Abdul, S.T., M.T.

Abstrak

Pembangkit Listrik Tenaga Nuklir (PLTN) Indonesia ditargetkan akan mulai beroperasi pada tahun 2027. Indonesia memiliki kandungan torium sebesar 130.974 ton. Bahkan torium memiliki sifat yang lebih baik daripada uranium. Salah satu mineral yang mengandung torium dan terletak di Indonesia adalah pasir monasit di Bangka Belitung. Tujuan penelitian ini adalah untuk menganalisis pengaruh variasi kuat arus listrik Electric Arc Furnace (EAF) pada proses smelting pasir monasit terhadap senyawa yang terbentuk, komposisi senyawa utama beserta recovery, dan grade ThO₂. Smelting dilakukan pada temperatur 1850°C selama 287 detik dan tegangan sebesar 40 V. Variasi kuat arus listrik yang digunakan adalah 50 A, 60 A, 70 A, 80 A, dan 90 A. Bahan yang digunakan terdiri atas pasir monasit sebagai material feed, CaCO₃ sebagai aditif, serbuk karbon sebagai reduktor, SiO₂ sebagai *flux*. Setelah *smelting*, dilakukan karakterisasi melalui pengujian X-Ray Diffraction (XRD) untuk mengetahui senyawa yang terkandung dan X-Ray Fluorosence (XRF) untuk mengetahui komposisi senyawa yang terkandung. Melalui analisis hasil pengujian XRD terdapat senyawa baru, yaitu calcium titanium oxide (CaTiO₃) pada semua variasi, hatrurite (Ca₃SiO₅) hanya pada 50 A dan 60 A, dan *fayalite* (Fe₂SiO₄) pada semua variasi, kecuali pada 50 A. Kemudian, melalui analisis hasil pengujian XRF didapatkan Fe₂O₃ dengan grade terendah (10,95%) pada 70 A dan recovery terendah (10,54%) pada 50 A, serta TiO₂ dengan grade terendah (22,95%) dan recovery terendah (6,47%) pada 50 A. Sementara itu, ThO₂ dengan grade tertinggi (0,45%) dan recovery tertinggi (38,29%) didapatkan pada 80 A. Melalui perhitungan separation efficiency (S.E.) didapatkan kuat arus listrik yang paling efisien adalah 80 A, dimana S.E. Fe₂O₃, TiO₂, dan ThO₂ berturut-turut sebesar 11,62%, 4,02%, dan 38,19%. Meskipun begitu, pasir monasit hasil smelting masih memiliki banyak sekali senyawa pengotor. Oleh karena itu, diperlukan metode ekstraksi ThO₂ lebih lanjut agar lebih optimal, contohnya menggunakan metode hidrometalurgi.

Kata Kunci: Kuat Arus Listrik, Pasir Monasit, Smelting, ThO2

ANALYSIS ON EFFECT OF VARIATION ELECTRIC ARC FURNACE CURRENT IN SMELTING PROCESS OF MONAZITE SAND ON COMPOUND COMPOSITION AND GRADE OF ThO₂

Student Name / NRP	: Kaisar Akbar Purwanto/02511840000023
Departement	: Materials and Metallurgical Engineering FTIRS-ITS
Advisor	: Fakhreza Abdul, S.T., M.T.

Abstract

Indonesia's nuclear power plant (PLTN) is targeted to start operating in 2027. Indonesia contains 130,974 tons of thorium. Even thorium has better properties than uranium. One of the minerals containing thorium and located in Indonesia is monazite sand in Bangka Belitung. The purpose of this study was to analyze the effect of variations in Electric Arc Furnace (EAF) electric current on the monazite sand smelting process on the compounds formed, the composition of the main compounds and their recovery, and the grade of ThO₂. Smelting was carried out at a temperature of 1850°C for 287 seconds and a voltage of 40 V. The variations of the electric current used were 50 A, 60 A, 70 A, 80 A, and 90 A. The materials used consisted of monazite sand as feed material, CaCO₃ as additive material. additive, carbon powder as reducing agent, SiO₂ as flux. After smelting, characterization was carried out through X-Ray Diffraction (XRD) testing to determine the compounds contained and X-Ray Fluorosence (XRF) to determine the composition of the compounds contained. Through the analysis of the XRD test results there were new compounds, namely calcium titanium oxide (CaTiO₃) in all variations, hatrurite (Ca₃SiO₅) only at 50 A and 60 A, and fayalite (Fe₂SiO₄) in all variations, except at 50 A. Then, through analysis XRF test results obtained Fe₂O₃ with the lowest grade (10.95%) at 70 A and the lowest recovery (10.54%) at 50 A, and TiO₂ with the lowest grade (22.95%) and the lowest recovery (6.47%). at 50 A. Meanwhile, ThO₂ with the highest grade (0.45%) and the highest recovery (38.29%) was found at 80 A. Through the calculation of separation efficiency (S.E.) the most efficient electric current was found to be 80 A, where S.E. Fe₂O₃, TiO₂, and ThO₂ were 11.62%, 4.02%, and 38.19%, respectively. Even so, the smelted monazite sand still contains a lot of impurities. Therefore, further ThO₂ extraction methods are needed to be more optimal, for example using the hydrometallurgical method.

Keywords: Current, Monazite Sand, Smelting, ThO₂

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BAB I PENDAHULUAN

1.1 Latar Belakang

Pada tahun 2020 tercatat kapasitas terpasang pembangkit listrik di Indonesia mencapai 72.750,72 MW. Dimana sebesar 43.186,53 MW merupakan pembangkit PLN dan 29.564,19 MW merupakan non PLN. Sedangkan pada tahun 2019 kapasitas terpasang pembangkit listrik masih di angka 69.678,85 MW. Hal ini mengindikasikan semakin tingginya pembangunan infrastruktur pemasok kebutuhan listrik Indonesia. Dari 43.186,53 MW, sekitar 40% dipasok oleh Pembangkit Listrik Tenaga Uap (PLTU) (Kementrian Energi dan Sumber Daya Mineral Direktrat Jenderal Keteragalistrikan, 2021). Dari data tersebut dapat dilihat bahwa Indonesia dalam memenuhi kebutuhan listriknya masih bertumpu pada PLTU dengan bahan bakar utamanya adalah batu bara yang termasuk bahan bakar fosil.

Energi Baru dan Terbarukan (EBT) merupakan alternatif yang dapat digunakan sebagai bahan bakar pembangkit listrik masa depan. Salah satunya adalah bahan bakar nuklir. Penggunaan nuklir sebagai pembangkit listrik sudah dimulai sejak tahun 1955. Hingga pada awal tahun 2016 terdapat sebanyak 441 buah reaktor Pembangkit Listrik Tenaga Nuklir (PLTN) berhasil didirikan dengan total kapasitas 382,9 GW atau setara 11% total produksi dunia. Selain itu, diperkirakan pada tahun 2031 kapasitas PLTN akan menjadi 150-300 GW (Suhaemi, 2017). Total negara di dunia yang telah menggunakan PLTN sebanyak 33 negara. USA merupakan negara dengan unit PLTN terbanyak di dunia, yaitu 158 buah reaktor riset dan 103 buah reaktor nuklir (Suhariyomo, 2006).

Indonesia memiliki mimpi yang besar untuk membangun PLTN. Menurut studi yang dilakukan oleh Badan Tenaga Nuklir Nasional (BATAN), PLTN Indonesia direncanakan akan beroperasi pada tahun 2027. Indonesia memiliki potensi yang sangat besar dalam dunia nuklir. Hal ini dikarenakan Indonesia memiliki kandungan uranium yang cukup besar di dalam tanah. Uranium merupakan unsur terpenting dalam bahan bakar nuklir. Terdapat tiga isotop uranium di alam, yaitu U-234, U-235, dan U-238. Dimana sekitar 99,3% dari total uranium berbentuk U-238. Hasil studi yang dilakukan oleh Pusat Pengembangan Geologi Nuklir (PPGN) – BATAN menyatakan bahwa Indonesia memiliki cadangan uranium sekitar 70.000 ton U₃O₈ (*yellow cake*). Dari 70.000 ton uranium tersebut terbagi ke dalam 1.608 ton kategori terukur, 6.456 ton kategori terindikasi, 2.648 ton kategori tereka, dan 59.288 ton kategori hipotetik. Namun, ketika dilakukan perhitungan matematis, apabila sebanyak 1.608 ton cadangan uranium terukur digunakan seluruhnya pada PLTN dengan kapasitas 2x1.000 MW, maka hanya dapat bertahan selama 3 tahun. Oleh karena itu, diperlukan diperlukan bahan bakar nuklir alternatif lainnya untuk menjalankan PLTN, salah satunya adalah torium (Badan Tenaga Nuklir Nasional, 2021).

Torium merupakan logam yang bersifat radioaktif dan memiliki waktu paruh yang sangat panjang, yaitu sekitar 14,05 juta tahun. Salah satu kelebihan dari torium dibanding uranium adalah keberadaannya di alam yang lebih melimpah, yaitu sekitar 6,6-7,4 juta ton di seluruh dunia. Sedangkan Indonesia diperkirakan memiliki cadangan torium sebesar 130.974 ton yang tersebar di beberapa wilayah, seperti Pulau Singkep, Bangka Belitung, Kalimantan Barat, dan Mamuju. Selain itu, efektifitas torium sebagai bahan bakar nuklir mencapai 90% dari total berat daripada uranium yang hanya sebesar 3-5% dari total berat (Mubarok et al., 2017). Torium dapat ditemui pada beberapa mineral, yaitu *thorite* (ThSiO₄), *thorianite* (ThO₂), *monazite* [(Ce,La,Nd,Th,U)PO₄], *bastnaesite* [(Ce,La)CO₃F], dan *thorogummite* [ThSiO₄)_{1-x}(OH)_{4-x}] (René, 2017). Di Indonesia, banyak ditemukan pasir monasit yang merupakan hasil samping dari penambangan timah. Pasir monasit ini memiliki kandungan torium sebesar 2,5-3,6%.



Untuk digunakan sebagai bahan bakar nuklir, torium haruslah memiliki kemurnian sebesar 87,42%. Penelitian yang dilakukan oleh Prassanti dan Pudjianto terkait ekstraksi torium dari monasit bangka dengan metode *Solvent Impregnated Resin* (SIR) menghasilkan *recovery* torium sebesar 81,13% (Prassanti & Pudjianto, 2018). Hal ini dapat dikatakan bahwa proses ekstraksi belum didapatkan *recovery* yang mencukupi. Selain melalui hidrometalurgi, ekstraksi monasit juga dapat dilakukan melalui pirometalurgi. Penelitian yang dilakukan oleh Wienar terkait penambahan *flux* SiO₂ pada *smelting* pasir monasit menggunakan *Electric Arc Furnace* (EAF) berhasil menghasilkan *recovery* torium sebesar 90,2% (Wienar, 2021).

Metode EAF dipilih dalam *smelting* pasir monasit dikarenakan beberapa kelebihannya, yaitu menghasilkan produk dengan kualitas yang tinggi, menghasilkan pengotor yang relative sedikit, dan kemudahan dalam pengendalian kerja. Mekanisme panas pada EAF muncul ketika busur terbentuk di antara dua elektroda tanpa adanya kontak dengan material *feed*. Busur ini terbentuk disebabkan adanya resistensi atau tahanan ketika saat arus listrik mengalir (Sarangi & Sarangi, n.d.). Kuat arus listrik berhubungan dengan jumlah elektron yang mengalir dalam satuan waktu. Lebih lanjut lagi, elektron yang mengalir akan mempengaruhi laju pemanasan (Sagita et al., 2020). Dimana, panas yang dihasilkan ini akan digunakan untuk reduksi oksida-oksida pengotor yang tidak diinginkan. Untuk mendapatkan panas yang optimal untuk reduksi, maka arus listrik yang digunakan dalam EAF harus disesuaikan.

Oleh karena itu, berdasarkan uraian diatas akan dilakukan penelitian tentang variasi arus listrik EAF pada *smelting* pasir monasit untuk meningkatkan komposisi senyawa dan *grade* ThO₂.

1.2 Rumusan Masalah

Berikut merupakan rumusan masalah dalam penelitian ini.

- 1. Bagaimana pengaruh variasi kuat arus listrik *Electric Arc Furnace* pada *smelting* pasir monasit terhadap senyawa yang terbentuk pada produk hasil *smelting*.
- 2. Bagaimana pengaruh variasi kuat arus listrik *Electric Arc Furnace* pada *smelting* pasir monasit terhadap komposisi senyawa utama pada pasir monasit.
- 3. Bagaimana pengaruh variasi kuat arus listrik *Electric Arc Furnace* pada *smelting* pasir monasit terhadap *grade* ThO₂ pada pasir monasit.
- 4. Bagaimana pengaruh variasi kuat arus listrik *Electric Arc Furnace* pada *smelting* pasir monasit terhadap *recovery* senyawa utama pada produk hasil *smelting*.

1.3 Batasan Masalah

Dalam penelitian ini diberikan beberapa batasan masalah sebagai berikut.

- 1. Komposisi serbuk karbon, pasir monasit, serbuk CaCO₃, dan serbuk SiO₂ dianggap homogen pada semua variasi.
- 2. Reaksi yang menyebabkan degradasi elektroda grafit pada saat pembentukan busur listrik diabaikan.
- 3. Serbuk SiO₂ dianggap sama untuk semua variasi.
- 4. Tegangan power suppy dan waktu smelting dianggap sama untuk semua variasi.
- 5. Posisi elektroda selama proses *smelting* berlangsung dianggap stabil.

1.4 Tujuan Penelitian

Tujuan dilakukan penelitian ini adalah sebagai berikut.

- 1. Menganalisis pengaruh variasi kuat arus listrik *Electric Arc Furnace* pada *smelting* pasir monasit terhadap senyawa yang terbentuk pada produk hasil *smelting*.
- 2. Menganalisis pengaruh variasi kuat arus listrik *Electric Arc Furnace* pada *smelting* pasir monasit terhadap komposisi senyawa utama pada produk hasil *smelting*.



- 3. Menganalisis pengaruh variasi kuat arus listrik *Electric Arc Furnace* pada *smelting* pasir monasit terhadap *grade* ThO₂ pada pasir monasit.
- 4. Menganalisis pengaruh variasi kuat arus listrik *Electric Arc Furnace* pada *smelting* pasir monasit terhadap *recovery* senyawa utama pada produk hasil *smelting*.

1.5 Manfaat Penelitian

Penelitian ini diharapkan dapat memberikan informasi empiris mengenai parameter variasi kuat arus listrik *Electric Arc Furnace* pada smelting pasir monasit terhadap komposisi senyawa dan grade ThO₂ pada pasir monasit. Sehingga diperoleh parameter proses yang optimal demi kemajuan riset serta teknologi khususnya dalam penelitian pengolahan mineral tanah jarang yang ada di Departemen Teknik Material dan Metalurgi ITS dan Indonesia.





BAB II TINJAUAN PUSTAKA

2.1 Pasir Monasit

Monasit merupakan mineral hasil samping dari pengolahan timah yang memiliki kandungan 0,298% uranium (U), 4,147% torium (Th), 23,712% fosfat (PO₄), dan 58,97% LTJ Oksida (LTJ₂O₃) (Novriyanisti et al., 2021). Kandungan dalam monasit ini memiliki nilai guna yang sangat besar dalam kehidupan manusia. Uranium dan torium digunakan sebagai bahan bakar nuklir, LTJ oksida digunakan sebagai bahan baku dalam industri nuklir, elektronika, dan otomotif. Sedangkan fosfat digunakan sebagai bahan baku dalam pembuatan pupuk kimia (L.N et al., 2009). Untuk memanfaatkan unsur atau senyawa yang terdapat pada monasit perlu dilakukan proses pemisahan terlebih dahulu. Metode yang biasa dilakukan adalah metode basa dan metode asam dan basa. Metode asam dilakukan menggunakan larutan H₂SO₄(Prassanti, 2012). Sedangkan metode basa dilakukan menggunakan larutan NaOH (Sumarni et al., 2004). Monasit secara fisik berwarna kuning atau oranye kecokelatan dengan kekerasan tinggi, serta berkilau (Widodo et al., 2019). Wujud pasir monasit ditunjukkan pada Gambar 2.1 sebagai berikut.



Gambar 2.1 Pasir Monasit (Dokumentasi Pribadi, 2022)

Monasit memiliki tiga senyawa dengan rumus kimia yang berbeda. Namun karena perbedaannya yang tidak signifikan, dirujuk menjadi satu mineral, yaitu monasit. Ketiga senyawa tersebut diantaranya adalah (Ce, La, Nd, Th, Y) PO4, (La, Ce, Nd) PO4, (Nd, La, Ce) PO4. Perbedaan rumus senyawa tersebut menunjukkan kandungan unsur tertentu di dalamnya. Unsur yang ditulis pertama kali merupakan unsur dengan persentase terbesar (Widodo et al., 2019). Kandungan pasir monasit ditunjukkan Tabel 2.1 sebagai berikut.



Senyawa	Kandungan Unsur (%)	Kandungan Oksida (%)
La	11,34	19,10
Ce	18,27	30,67
Nd	8,64	14,33
Pr	0,54	0,91
Th	6,47	10,00
Lainnya Si, Zr, Sn, Y, Gd, Dy, U)	-	24,99

Tabel 2.1 Kandungan Unsur Beserta Oksida Pada Pasir Monasit (Rodliyah et al., 2015)

2.2 Torium

Torium adalah salah satu logam aktinida yang bersifat radioaktif dan paragmanetik dengan lambing Th dan nomor atom 90. Torium umumnya berwarna putih keperakan dan bertekstur agak lunak. Ketika terkontaminasi oksida, torium akan berubah warna menjadi keabu-abuan dan akhirnya berwarna hitam (Widodo et al., 2019). Sifat torium ditunjukkan pada Tabel 2.2 berikut.

Tabel 2.2 Sifat Torium (Widodo et al., 2019)		
Sifat Umum		
Nama, simbol	torium, Th	
Warna	keperakan	
Nomor atom (Z)	90	
Kategori unsur	aktinida	
Massa atom (Ar)	232,0381	
Titik leleh	1750° C	
Titik didih	4788° C	

Torium memiliki isotop sebanyak 25 buah dengan rata-rata kestabilan sangat rendah. Isotop torium dengan kestabilan tinggi adalah Th-232 dengan waktu paruh selama 14,05 milyar tahun (Dewita et al., 2012). Th-232 memili kemampuan untuk dikonversi menjadi neutron termal menjadi isotop U-232. Torium diklaim lebih aman daripada uranium karena tidak menghasilkan plutonium-240 hasil reaksi dari uranium-235 dan uranium-238 yang digunakan sebagai senjata nuklir. Reaksi Th-232 menjadi U-232 ditunjukkan pada Persamaan (2.1) sebagai berikut (Wickleder et al., 2018).

$$^{232}Th(n,\gamma) \rightarrow ^{232}Th \xrightarrow{\beta^{-}}{232}Pa \xrightarrow{\beta^{-}}{232}U$$
(2.1)

Torium dapat ditemukan pada sebagian besar mineral. Namun, torium biasanya bercampur dengan uranium, LTJ, niobium, dan tantalum, entah itu dalam bentuk oksida



maupun tidak. Monasit menjadi salah satu mineral logam tanah jarang torium-fosfat dengan kadar torium oksida sebesar 12%. Kandungan torium pada masing-masing mineral juga bergantung dengan lokasi. Namun, umumnya memiliki kadar torium sebesar 6-7%. Mineral yang mengandung torium ditunjukkan pada Tabel 2.3 sebagai berikut.

Table 2.3 Minicial Lang Terkandung Tonuni (Dewna et al., 2012	Tabel 2.3 Mineral	Yang T	erkandung	Torium	(Dewita et a	I., 2012)
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Mineral	Rumus Kimia
Thorite	$(Th, U)SiO_4$
Thrianite	$(ThO_2 + UO_2)$
Thorogummite	$Th(ThSiO_4)_{1-x}(OH)_{4x}$
Monazite	$(Ce, La, Y, Th)PO_4$
Brocktite	$(Ca, Th, Ce)(PO_4)H_2O$
Xenotime	$(Y, Th)PO_4$
Euxenite	$(Y, Ca, Ce, U, Th)(Nb, Ta, Ti)_2O_6$
Bijih Besi	Fe + REE + Th apatit

Torium di alam berbentuk sebagai oksida, yaitu ThO₂ atau disebut *thoria*. Senyawa ini berwarna putih padat, tidak berbau, serta tidak larut dalam air. *Thoria* memiliki titik leleh yang tinggi yaitu sekitar 3300°C (Widodo et al., 2019). Sifat dari ThO₂ selengkapnya ditunjukkan pada Tabel 2.4 sebagai berikut.

Sifat Umum			
Nama IUPAC	Thorium dioxide		
Rumus kimia	ThO_2		
Warna	Putih		
Massa molar	264,04 g/mol		
Densitas	10 g/cm^3		
Titik lebur	3.300°C		
Titik didih	4.400°C		

 Tabel 2.4 Sifat Senyawa Torium Oksida (Balakrishna, 2012)

2.3 Flux SiO₂

Flux merupakan senyawa yang ditambahkan ke dalam mineral selama proses *smelting* yang digunakan untuk mengikat unsur-unsur pengotor dari mineral utama (Kokal & Ranade, 1985). Salah satu *flux* yang sering digunakan dalam metode pirometalurgi adalah SiO₂. SiO₂ atau silika merupakan senyawa penyusun dari kerak bumi dengan persentase terbesar, yaitu 60,6%. Silika dapat ditemukan dalam pasir, batuan atau tanah silika, limbah kaca, dan bahan organik seperti abu sekam padi dan abu tebu. Silika biasanya digunakan dalam bentuk bermacam-macam, antara lain gelas, kristal, gel, aerogel, *fumed* silika, dan aerosol. Silika



memiliki sifat ketahanan terhadap abrasi yang baik, isolator listrik yang baik, dan stabilitas termal yang tinggi (Dyana & Triwikantoro, 2017). Sifat silika ditunjukkan pada Tabel 2.5 sebagai berikut.

Tabel 2.5 Sifat Silika (Dyana & Triwikantoro, 2017)		
Sifat Umum		
Nama IUPAC	Silicon dioxide	
Rumus kimia	SiO_2	
Warna	Padat transparan (amorf) Putih/kuning keputihan (serbuk atau pasir)	
Massa molar	60,08 g/mol	
Densitas	2,648 g/cm ³ (quartz) 2,196 g/cm ³ (amorf)	
Titik lebur	1.713°C	
Titik didih	2.950°C	

Silika dapat mengikat pengotor menjadi *slag* pada temperatur sekitar 1550°C. Salah satu oksida yang dapat diikat pada temperatur tersebut adalah *titania* (TiO₂) dengan mengikat Ca dan Ti menjadi *titanite* (CaTiSiO₅) sesuai dengan Persamaan (2.2) sebagai berikut (Woermann et al., 1969).

$$CaO + SiO_2 + TiO_2 \rightarrow CaTiSiO_5 \tag{2.2}$$

Selain *titania*, *magnesia* (MgO) juga merupakan oksida yang dapat diikat oleh silika, tepatnya pada temperatur 1100-1400°C dan membentuk *forsterite* (Mg₂SiO₄) sesuai dengan Persamaan (2.3) sebagai berikut (Brindley & Hayami, 1965).

$$2Mg0 + SiO_2 \to Mg_2SiO_4 \tag{2.3}$$

2.4 Reduktor Karbon

Pirometalurgi identik dengan fenomena reduksi dari oksida mineral. Sehingga untuk mereduksi diperlukan agen pereduksi atau reduktor selama proses berlangsung. Reduktor pada umumnya berbasis karbon atau disebut material *carbonaceous*, seperti batu bara, kokas, karbon, grafit, dan arang. Penggunaan material ini sebagai reduktor karena mampu meningkatkan permeabilitas pada *burden*, sehingga mampu meningkatkan distribusi gas yang ada (Sahajwalla et al., 2016).

Peran reduktor dalam berbagai reaksi reduksi dalam melalui:

- Gasifikasi reduktor menjadi gas CO yang dapat bereaksi di dalam furnace
- Pelarutan karbon dalam logam cair
- Reaksi karbon terlarut dengan *slag* saat logam selama proses pemurnian
- Reaksi reduksi langsung dari karbon padat dengan *slag*

Pemilihan reduktor harus disesuaikan dengan kebutuhan industri, antara lain terkait *softening, swelling, fusion*, dan porositas dalam pembuatan kokas dan arang, serta reaktivitas atau konsumsi karbon dari reduktor karbon untuk digunakan dalam berbagai proses (Falcon et al., 2004). Dalam perannya sebagai reduktor pada proses reduksi oksidasi, material karbon



memungkinkan untuk mengalami reaksi seperti pada Persamaan (2.4), (2.5), dan (2.6) sebagai berikut (Sahajwalla et al., 2016).

$$C + O_2 \to CO_2 \tag{2.4}$$

$$2C + O_2 \to 2CO \tag{2.5}$$

$$2CO + O_2 \rightarrow 2CO_2 \tag{2.6}$$

Pada reaksi pertama (pembentukan CO₂) hampir tidak ada perubahan entropi, yaitu $\Delta S^{\circ}=$ 0 dan oleh karena itu ΔG° tetap hampir sama dengan kenaikan temperatur dan ΔG° tidak tergantung pada temperatur. Pada reaksi kedua (pembentukan CO), terjadi peningkatan entropi (ΔS positif) oleh karena itu, ΔG° menjadi lebih negatif dengan kenaikan temperatur. Namun, pada reaksi ketiga, terjadi penurunan entropi (ΔS negatif) dan oleh karena itu, ΔG° menjadi tidak lebih negatif dengan kenaikan temperatur (Sahajwalla et al., 2016). Sifat reduksi tersebut ditunjukkan pada Gambar 2.2 sebagai berikut.



Gambar 2.2 Diagram Ellingham Reduksi Karbon (National Council of Educational Research and Training, 2021)

2.5 Electric Arc Furnace (EAF)

Electric Arc Furnace (EAF) merupakan salah satu teknologi modern yang umum dan populer untuk digunakan dalam industri metalurgi. Sumber panas utama dari EAF adalah busur listrik. Busur listrik ini akibat dari loncatan elektron dari katoda yang dapat digerakkan dan anoda permanen, serta dipisahkan dengan penumpukkan gas. Mekanisme transfer panas yang utama pada kondisi ini adalah reaksi radiasi. Perubahan energi listrik menjadi energi panas terjadi melalui arus dalam busur listrik yang terionisasi, dimana temperatur busur listrik dapat mencapai 6000°C (Khodabandeh et al., 2017).

EAF dapat diklasifikasikan berdasarkan proses transfer panas dari busur, yaitu pemanasan langsung dan pemanasan tidak langsung. Pemanasan tidak langsung terjadi ketika busur listrik terbentuk antara dua elektroda tanpa kontak dengan material *feed* atau dengan kata lain transfer panas terjadi hanya melalui radiasi dan konveksi. Sedangkan pemanasan langsung terjadi ketika



busur listrik terbentuk antara dua elektroda dan kontak dengan material *feed*, sehingga transfer panas terjadi melalui konduksi, radiasi, dan konveksi (Grzella et al., 1923). Komponen EAF secara umum ditunjukkan pada Gambar 2.3 sebagai berikut.



Gambar 2.3 Komponen *Electric Arc Furnace* (Grzella et al., 1923)

2.6 Penggunaan Kuat Arus Listrik Electric Arc Furnace

Arus listrik yang digunakan dalam EAF dapat berasal dari arus listrik searah (*direct current*) maupun arus listrik bolak-balik (*alternating current*). Namun, dalam skala industri arus listrik yang digunakan adalah arus bolak-balik dengan elektroda berupa grafit. Arus listrik melewati elektroda pertama akan menjangkau material *feed* melalui busur listrik, kemudian arus listrik tersebut dari material *feed* melewat elektroda lainnya melalui busur listrik, begitu seterusnya. Umumnya digunakan arus listrik dengan 3 fasa (Hernández et al., 2005).

EAF dapat menghasilkan panas melalui prinsip adanya tahanan (resistansi) saat arus listrik mengalir. Logam atau bahan pengumpanan yang dimuatkan dalam tanur yang akan memberikan tahanan terhadap arus listrik. Terak yang terbentuk saat logam mencair juga dapat memberikan tahanan pada aliran arus listrik. Elektroda harus diangkat sehingga hanya menyentuh permukaan terak agar pemberian panas terus bertahan. Panas yang dihasilkan oleh loncatan elektron (busur api) dengan aliran listrik akan menimbulkan aliran induksi dalam cairan yang akan menyebabkan terjadinya gerak cairan, sehingga homogenisasi cairan dapat terjadi (Hernández et al., 2005).

Keberadaan elektroda pada EAF berfungsi untuk mengalirkan arus busur listrik menuju bahan peleburan. Karbon atau grafit biasanya dimanfaatkan sebagai elektroda karena lebih tahan terhadap temperatur tinggi. Ujung bawah dari elektroda akan semakin pendek ketika digunakan karena panas yang terjadi pada titik tersebut. Elektroda dapat diturunkan atau dinaikkan baik secara otomatis maupun manual agar bersentuhan dengan logam saat operasi peleburan berlangsung. Ketika elektroda sudah mulai memendek, diperlukan penggantian agar proses peleburan tetap optimal (Madias, 2014).

2.7 Waktu Smelting Electric Arc Furnace

Waktu dalam pelaksanaan proses EAF biasa disebut dengan istilah *tap to tap time* yang dapat diartikan sebagai waktu yang digunakan dalam proses EAF meliputi *charging, smelting* dan *tapping. Tap to tap* dalam industri pengolahan logam yang menggunakan proses EAF berpengaruh terhadap efisiensi proses yang digunakan. Dalam dunia industri logam, EAF


beroperasi sebagai proses peleburan yang dilakukan per *batch* yang menghasilkan baja likuid. Siklus pengoperasian EAF biasa disebut dengan *tap to tap* yang terdiri dari proses pengisian tungku, proses pelelehan, fase *refining* dan penuangan baja cair. Waktu *tap to tap* normalnya dilakukan kurang dari 60 menit untuk EAF modern, sedangkan beberapa operasi tungku kembar hanya membutuhkan waktu sekitar 35-40 menit (Stalhed, 1957).

Proses peleburan merupakan proses inti dari pengoperasian EAF. EAF berkembang menjadi alat peleburan yang efisien dan memiliki desain yang modern difokuskan untuk memaksimalkan kapasitas proses peleburan. Peleburan dilakukan dengan cara memberikan energi ke dalam tungku dimana energi ini berasal dari energi listrik. Energi listrik disalurkan melalui elektroda grafit yang merupakan kontributor utama dalam proses peleburan. Mulanya, tegangan menegah diumpankan sampai elektroda masuk ke dalam material *scrap*. Banyak operasi EAF yang baru saja mengembangkan *heat balances* untuk tungkunya. Keseimbangan ini didasarkan pada total energi masuk dan keluar ke tungku selama siklus *tap to tap* berlangsung. Analisis keseimbangan tersebut menunjukkan bahwa ada variasi kebutuhan energi yang luas dan efisiensi transfer energi di EAF. Waktu selama proses peleburan sampai terjadinya *refining* antara logam dengan pengotornya bisa didefinisikan waktu *holding* peleburan (Pretorius & Oltmann, 2002).

2.8 Diagram Bouduard-Gaussnerr

Diagram Bouduard-Gaussnerr merupakan diagram yang menggambarkan kesetimbangan antara unsur dan oksida besi yaitu besi, hematit, magnetit, wustit, karbon padat, karbon monoksida, dan karbon dioksida dalam proses reduksi langsung besi oleh karbon. Reaksi bouduard terjadi di temperatur tinggi dikarenakan reaksi bouduard merupakan reaksi endotermis. Diagram ini ditunjukkan pada Gambar 2.4, diketahui garis kesetimbangan pada temperatur 1000°C terdapat 100% gas CO. Agar gas CO terurai menjadi CO₂ dan C, temperatur harus diturunkan sehingga kesetimbangan tidak tercapai. Hal ini dapat mengurangi gas CO sebagai reduktor. Pada daerah sebelah kanan garis kesetimbangan, gas CO₂ akan mengalami reaksi bouduard menjadi gas CO. Berdasarkan diagram Bouduard-gausnerr, perbandingan gas CO/CO₂ dan temperatur operasi merupakan faktor yang mempengaruhi terbentuknya senyawa (Sarangi & Sarangi, n.d.).





Gambar 2.4 Diagram Bouduard-Gaussner (Sarangi & Sarangi, n.d.)

Berdasarkan diagram di atas, terdapat kesetimbangan antara besi oksida dengan CO/CO₂ ditunjukkan oleh Persamaan (2.7), (2.8), (2.9), dan (2.10) sebagai berikut.

1. Garis kesetimbangan Boudouard:

$$CO_2 + C \to 2CO \tag{2.7}$$

2. Garis kesetimbangan:

 $3Fe_2O_3 + CO \rightarrow 2Fe_3O_4 + CO_2$ (2.8)

3. Garis kesetimbangan:

$$Fe_3O_4 + CO \rightarrow 3FeO + CO_2 \tag{2.9}$$

4. Garis kesetimbangan:

$$FeO + CO \rightarrow Fe + CO_2$$
 (2.10)

Pada temperatur 700°C senyawa yang stabil dengan perbandingan CO/CO₂ adalah 60:40 adalah wustit (FeO). Di mana magnetit (Fe₃O₄) akan tereduksi menjadi wustit, sedangkan Fe akan mengalami oksidasi menjadi wustit. Terjadi perpotongan antara garis kesetimbangan FeO/Fe dan garis kesetimbangan boudouard pada temperatur 700°C. Hal tersebut menjadi Fe. Selain itu, juga terjadi perpotongan antara garis kesetimbangan magnetit/wustit dan garis kesetimbangan boudouard pada temperatur 650°C. Hal tersebut menunjukkan bahwa 650°C merupakan temperatur 650°C. Hal tersebut menjadi wustit. Kedua temperatur minimum yang dibutuhkan untuk mereduksi magnetit menjadi wustit. Kedua temperatur tersebut merupakan pada tekanan 1 atmosfer. Ketika dibawah temperatur tersebut, karbon monoksida akan terurai menjadi karbon dioksida. Hal ini akan membuat reaksi tidak akan terjadi (Komarudin, 2008).

2.9 Termodinamika Reduksi

Diagram Ellingham merupakan diagram yang berisi energi bebas sebuah reaksi yang kemudian diplot ke dalam suatu grafik dengan parameter energi bebas dengan temperatur. Pada



diagram Ellingham, logam yang aktif secara kimia memiliki energi bebas yang paling tinggi (negatif) dalam membentuk oksida terletak pada diagram di bagian paling bawah. Sedangkan untuk logam yang memiliki energi afinitas bebas terkecil (positif) dalam membentuk oksida terletak pada diagram di bagian paling atas. Nilai ΔG° untuk reaksi oksidasi merupakan ukuran kimia suatu logam terhadap oksigen. Semakin negatif nilai ΔG° suatu logam menunjukkan logam tersebut semakin stabil dalam bentuk oksida. Dapat diketahui temperatur minimal yang dibutuhkan agar terjadi. Hal tersebut dapat ditunjukkan oleh perpotongan antara kurva oksida dan garis pembentukan CO (Lee, 1999). Diagram ellingham untuk beberapa oksida ditunjukkan pada Gambar 2.5 sebagai berikut.



Gambar 2.5 Diagram Ellingham Berbagai Oksida (Lee, 1999)

Termodinamika hanya dapat digunakan untuk menentukan apakah suatu reaksi dapat berjalan spontan atau tidak pada temperatur tertentu berdasarkan energi bebas yang dimiliki. Namun, tidak dapat digunakan untuk menentukan laju reaksi. Perpotongan antara garis reaksi oksida dan reduksi secara termodinamika menunjukkan bahwa reaksi tersebut berjalan pada



temperatur tertentu (Lee, 1999). Sebagai contoh reduksi dari besi oksida dapat digambarkan dengan skema berikut.

- a) $T > 570^{\circ}C: Fe_2O_3 \rightarrow Fe_3O_4 \rightarrow FeO \rightarrow Fe$
- b) $T < 570^{\circ}C: Fe_2O_3 \rightarrow Fe_3O_4 \rightarrow Fe$
- c) $T < 570^{\circ}C: 4FeO \rightarrow Fe_3O_4 + Fe$

2.10 Grade, Recovery, dan Basisitas

Proses pengolahan mineral memiliki tujuan utama untuk memisahkan mineral yang berharga dengan mineral pengotor. Terdapat dua cara yang dapat kita lakukan untuk mengukur keberhasilan proses pengolahan mineral yaitu dengan mengukur kadar/grade dan pemulihan recovery (Napier-Munn & Wills, 2005).

Kadar/grade adalah persentase yang jumlah atau kandungan persentase logam atau mineral berharga dalam suatu *ore*. Pada beberapa jenis *ore* dengan kandungan logam yang sangat rendah, kandungan logamnya dinyatakan dalam satuan *part per million* atau ppm. Namun, beberapa logam dijual dalam bentuk oksidanya atau tidak sebagai logam utuh. Sehingga dalam kondisi seperti ini menyatakan persentase oksidanya (Napier-Munn & Wills, 2005).

Recovery adalah persentase dari total logam atau mineral yang terkandung dalam bijih yang berhasil diubah ke dalam konsentrat. Sebagai contoh, nilai *recovery* sebesar 90% menyatakan bahwa 90% dari logam yang ada di dalam bijih berhasil diperoleh kembali ke dalam konsentrat, namun 10% lainnya akan terbuang ke dalam *tailing*. *Recovery* dilambangkan dengan simbol *R* dengan Persamaan seperti yang ditunjukkan dalam Persamaan (2.11) sebagai berikut (Pintowantoro et al., 2021).

$$Recovery (\%) = \frac{W_{p \cdot c}}{W_{f \cdot f}} X \ 100\%$$
(2.11)

dengan W_p sebagai massa dari produk, W_f sebagai massa dari *feed*/umpan, *c* sebagai kadar mineral di dalam produk, dan *f* sebagai kadar dari mineral di dalam *feed*/umpan (Pintowantoro et al., 2021).

Kadar dan *recovery* adalah ukuran yang paling umum digunakan untuk menjelaskan efisiensi dari proses ekstraksi. Jika ingin mencapai kadar dari produk yang tinggi, maka hasil *tailing* akan lebih banyak dan *recovery* menjadi rendah. Namun jika ingin mencapai nilai *recovery* logam yang tinggi, akan ada lebih banyak *gangue* dalam konsentrat sehingga kadar logam akan menurun (Napier-Munn & Wills, 2005).

Nilai *recovery* suatu logam atau mineral juga dapat dipengaruhi oleh basisitas *slag*. Basisitas merupakan rasio senyawa yang bersifat basa terhadap senyawa yang bersifat asam yang ada pada *slag* atau produk hasil pemurnian (Pintowantoro & Abdul, 2020). Terdapat tiga definisi basisitas *slag*, yaitu B₁, B₂, dan B₃ ditunjukkan oleh Persamaan (2.12), (2.13), dan (2.14) sebagai berikut.

$$B_1 = \frac{Ca0}{SiO_2} \tag{2.12}$$

$$B_2 = \frac{CaO + MgO}{SiO_2} \tag{2.13}$$

$$B_3 = \frac{CaO + MgO}{SiO_2 + Al_2O_3} \tag{2.14}$$



2.11 Penelitian Sebelumnya

2.11.1 Ekstraksi Monasit

Trinopiawan dkk. pada 2011 melakukan pemisahan uranium dari torium dalam larutan hasil pelarutan endapan dengan H_2SO_4 melalui metode ekstraksi pelarut dengan campuran dari alamin-336, kerosin, dan isodekanol. Hasil penelitian menunjukkan kondisi optimal ekstraksi pada pH umpan 1,5 dengan perbandingan O/A = 5 dan waktu ekstraksi 5 menit, dan diperoleh U sebesar 100%, tetapi Th ikut terekstrak 32,44%. Dari hasil ini dapat disimpulkan bahwa pada kondisi optimal tersebut, Th dapat terpisah dari U sebesar 67,56%. Hasil ini ditunjukkan oleh Gambar 2.6 sebagai berikut (Trinopiawan et al., 2011).



Gambar 2.6 Grafik Pengaruh Waktu Ekstraksi Terhadap Persentase Unsur Terekstraksi (Trinopiawan et al., 2011)

Selanjutnya, Trinopiawan dkk. pada 2012 melakukan penelitian lebih lanjut. Proses ini dilakukan dengan memisahkan Th dari U pada pasir monasit sehingga dapat ditentukan kondisi optimal menggunakan metode pengendapan dengan reagen H₂SO₄. Tahapan proses terdiri dari penggerusan monasit, dekomposisi, pelarutan parsial, pelarutan total, dan pengendapan Th dengan H₂SO₄. Larutan umpan yang digunakan untuk pengendapan berasal dari pelarutan total dengan dua reagen berbeda, yaitu H₂SO₄ dan HCl. Hasil optimal *recovery* pengendapan pada larutan umpan sulfat, yaitu Th sebesar 96,99% dan U sebesar 18,26% dengan konsumsi H₂SO₄ 20 ml dan waktu pengendapan 30 menit. Hasil optimal *recovery* pengendapan pada larutan umpan klorida yaitu Th sebesar 98,05% dan U 25,03% dengan konsumsi H₂SO₄ 20 ml dan waktu pengendapan 20 menit. Hasil ini ditunjukkan oleh Gambar 2.7 sebagai berikut. (Trinopiawan & Sumiarti, 2012).





Gambar 2.7 Grafik Pengaruh Waktu Pengendapan Terhadap *Recovery* U, Th, dan RE (Trinopiawan & Sumiarti, 2012)

Nurly dkk. pada 2015 melakukan dekomposisi fosfat pasir monasit, sebagai *pre-treatment* sebelum tahapan ekstraksi. *Pre-treatment* dilakukan dengan *roasting* yang ditambahkan NaOH padat selama 120 menit. Pelarutan kalsin hasil *roasting* dilakukan untuk melarutkan fosfat dengan akuades pada temperatur 80°C selama 60 menit. Hasil percobaan menunjukkan bahwa persen dekomposisi fosfat paling baik adalah pada temperatur 400°C dengan klasifikasi ukuran butir -200 dengan persen kadar LTJ adalah 65,52%. Semakin kecil ukuran partikel dan semakin tinggi temperatur fosfat terdekomposisi semakin tinggi dan terjadi peningkatan kadar kandungan LTJ (Nurly et al., 2015).



Gambar 2.8 Pengaruh Ukuran Butir *Feed* Terhadap Persentase Kadar Pada Temperatur 400°C (Nurly et al., 2015)

Marisi dkk. pada 2018 melakukan pemisahan unsur radioaktif dan logam tanah jarang pasir monasit PLUTHO yang mengandung torium dan uranium. Penelitian ini dilakukan untuk menurunkan kadar torium dan radioaktivitas dalam limbah cair menggunakan koagulan ferosulfat. Pilot *plant* PLUTHO merupakan suatu fasilitas untuk memisahkan uranium, torium, dan logam tanah jarang (LTJ) dari mineral monasit dan mineral lainnya dalam skala pilot. Perlakuan variasi yang dilakukan pada penelitian adalah kadar koagulan dan pH. Hasil penelitian menunjukkan kondisi optimum koagulasi pada pH 8,0 dengan dosis koagulan FeSO₄



225 mg/L yang dapat menurunkan kadar torium sebesar 45,20% dari nilai kadar awal 0,40 mg/L. Hasil ini ditunjukkan oleh Gambar 2.9 sebagai berikut. (Marisi et al., 2018).



Gambar 2.9 Grafik Pengaruh Dosis Koagulan Terhadap Kadar Torium (Marisi et al., 2018) Teixeira dkk. pada 2019 melakukan ekstraksi unsur tanah jarang, torium, dan besi dalam melalui proses ekstraksi selektif bijih. Didapatkan bahwa monasit yang mengandung tanah jarang dapat diproses secara selektif untuk memisahkan besi dan torium dari unsur tanah jarang. Mineral yang digunakan adalah *bebedourite*, *flogopitite*, dan *foscorite*. Sedangkan, variasi dilakukan pada temperatur *roasting* berkisar antara 200-800°C. Ekstraksi REE maksimal didapatkan pada temperatur 700°C dengan rentang 73-82%. Hasil ini ditunjukkan oleh Gambar 2.10 sebagai berikut (Teixeira et al., 2019).



Gambar 2.10 Grafik Pengaruh Temperatur *Roasting* Terhadap Kadar Th dan Fe (Teixeira et al., 2019)

2.11.2 Penggunaan Kuat Arus Listrik Electric Arc Furnace

Supriyatna dan Shofie pada tahun 2013 membuat rancangan mengenai EAF satu fasa dengan diameter dalam *furnace* sebesar 150 mm dan tinggi 200 mm yang memiliki kapasitas



5-10 kg yang dapat digunkan untuk proses *smelting*. Pada rancangan ini, dilakukan *smelting* ferromangan dengan komposisi bahan sebanyak 6000 gr bijih mangan dan 560 gr bijih besi. *Smelting* dilakukan pada kuat arus listrik 350 A dan waktu 120 menit. Variasi yang dilakukan adalah temperatur *smelting*. Tungku busur listrik hasil rancang bangun akan membutuhkan waktu proses lebih cepat ketika arus listrik yang digunakan bertambah dan temperatur leleh dari bahan baku relatif tidak begitu tinggi. Hasil optimal didapatkan pada temperatur sekitar 1700°C dengan kandungan Fe 14,23% dan Mn 76,12% pada ferromangan. Variasi temperatur *smelting* beserta hasil ditunjukkan oleh Gambar 2.11 dan 2.12 sebagai berikut (Supriyatna & Shofie, 2013).



Gambar 2.11 Variasi Temperatur Smelting (Supriyatna & Shofie, 2013)

	Produk (%)									
Unsur	FeMn 1	FeMn 2	FeMn 3	FeMn 4	FeMn 5	FeMn 6				
Fe	84,59	96,9	83,48	80,12	16,34	14,23				
Mn	8,19	7,59	11,51	10,92	74,52	76,12				
C	5,88	4,66	4,77	4,54	4,86	4,95				
Si	0,34	0,002	4,49	5,49	0,46	0,43				
Р	0,14	0,19	0,06	0,05	0,07	0,03				
S	0,003	0,0001	0,009	0,002	0,003	0,001				

Gambar 2.12 Komposisi Kimia Setiap Variasi Temperatur *Smelting* (Supriyatna & Shofie, 2013)

Supriyatna dkk. pada tahun 2014 membuat rancang bangun EAF satu fase untuk *smelting* konsentrat mangan dan besi menjadi feromangan dengan kapasitas 10 kg. Energi yang dibutuhkan adalah sebesar 32,016 kJ. Uji coba dilakukan dengan variasi waktu dan temperatur *smelting* sebesar 126 menit-1739°C, 138 menit-1646°C, dan 222 menit-1497°C. Sedangkan untuk daya 35 kVA dan arus 300 A. Dengan arus yang tetap, maka waktu dan temperatur akan coba disesuaikan agar dapat memenuhi energi yang dibutuhkan. Didapatkan komposisi ferromangan yang optimal pada variasi waktu dan temperatur *smelting* ke-3, yaitu 222 menit-1497°C. Hasil ini ditunjukkan oleh Gambar 2.13 (Supriyatna et al., 2014).



Linour		Produk FeMn (%)						
Unsur	Ujicoba-1	Ujicoba-2	Ujicoba-3					
Fe	80,12	16,34	14,23					
Mn	10,92	74,52	76,12					
С	4,54	4,86	4,95					
Si	5,49	0,46	0,43					
Р	0,05	0,07	0,03					
S	0,002	0,003	0,001					

Gambar 2.13 Komposisi Kimia Setiap Variasi Waktu dan Temperatur *Smelting* (Supriyatna et al., 2014)

Pada tahun 2018, Wijaya melakukan penelitian terhadap pengaruh variasi arus listrik EAF pada *smelting Direct Reduced Iron* terhadap kandungan Fe total dan *recovery* Fe dalam pembuatan *pig iron*. Pada penelitian ini digunakan variasi arus listrik sebesar 140 A, 160 A, 180 A, dan 200 A dengan variabel tetap berupa tegangan sebesar 16,2 V, waktu *smelting* selama 360 detik. Dalam perhitungan neraca panas diperoleh energi yang dibutuhkan adalah sebesar 119,96 kJ. Hasil yang berhasil didapatkan adalah arus listrik sebesar 180 A didapatkan energi sebesar 1049,76 kJ. Dimana output panas tersebut merupakan nilai yang paling mendekati dengan energi yang dibutuhkan. Namun, pada penelitian ini tidak ditemukan penjelasan terkait efisiensi *power supply* yang digunakan. Hasil ini ditunjukkan oleh Gambar 2.14 sebagai berikut (Wijaya, 2018a).





Wienar pada 2021 melakukan ekstraksi torium melalui *smelting* pasir monasit dengan *flux* SiO₂ dengan menggunakan metode EAF. *Smelting* dilakukan pada temperatur 1850°C selama 5 menit. dengan arus listrik EAF sebesar 60 A dan tegangan sebesar 40 V. Hal ini untuk memenuhi energi yang dibutuhkan sebesar 378705,33 J. Didapatkan *recovery* yang tinggi dari ThO₂, yaitu sebesar 90,2%. Hasil ini ditunjukkan oleh Gambar 2.15 sebagai berikut (Wienar, 2021).





Gambar 2.15 Grafik Pengaruh Penambahan *Flux* SiO₂ Terhadap *Recovery* Senyawa Utama Pasir Monasit (Wienar, 2021)

Untuk memudahkan membandingkan penelitian sebelumnya, maka disusun dalam bentuk tabel perbandingan. Tabel perbandingan penelitian sebelumnya ditunjukkan oleh Tabel 2.6 sebagai berikut.

Metode	Material	Variabel	Hasil	Peneliti					
Ekstraksi Pelarut	Pasir Monasit	pH, waktu	pH=1,5 O/A=5 Waktu ekstraksi 5 menit Th =32,44%	Trinopiawan dkk. (2011)					
Pengendapan dengan Larutan	Pasir Monasit	Volume dan waktu	Umpan Sulfat: H_2SO_4 20 ml waktu 30 menit Th = 96,99% Umpan klorida: H_2SO_4 20 ml waktu 20 menit Th = 98,05%	Trinopiawan dkk. (2012)					
Roasting	Pasir Monasit	Temperatur dan ukuran butir	T=400°C Ukuran -200 Recovery 65,52%	Nurly dkk. (2015)					
Koagulasi	Limbah Pasir Monasit	Kadar koagulan dan pH	pH 8,0 Jumlah FeSO4 225 mg/L Kadar torium 45,20%	Marisi dkk. (2018)					



Ekstraksi Selektif dan <i>Roasting</i>	Pasir Monasit	Temperatur	<i>recovery</i> tanah jarang antara 70 dan 80%, konsumsi asam antara 0,21 kg dan 0,34 kg asam untuk 1 kg bijih	Teixeira dkk. (2019)
Smelting	Mangan dan bijih besi	Temperatur	T=+1500°C Mn=76,12%	Supriyatna dan Shofie (2013)
Smelting	Konsentrat mangan dan besi	Waktu dan temperatur	t=222 menit T=1497°C Fe=80,12% Mn=10,92%	Supriyatna, dkk. (2014)
Smelting	Direct Reduced Iron (DRI)	Kuat arus listrik	I=180 A <i>Recovery</i> Fe=98,78% Kadar Fe=91,585%	Wijaya (2018)
Smelting	Pasir Monasit	Jumlah SiO ₂	SiO ₂ =9% <i>Recovery</i> ThO ₂ =90,2% Kadar ThO ₂ =0,46%	Wienar (2022)



(Halaman ini sengaja dikosongkan)



BAB III METODOLOGI PENELITIAN

3.1 Diagram Alir







Gambar 3.1 Diagram Alir Penelitian

3.2 Bahan Penelitian

Bahan-bahan yang dibutuhkan dalam penelitian ini yaitu sebagai berikut.

3.2.1 Pasir Monasit

Pasir monasit yang digunakan dalam penelitian ini berasal dari Bangka Belitung, Indonesia. Pasir monasit dilakukan preparasi terlebih dahulu sebelum dilakukan proses *smelting*. Pasir monasit ditunjukkan oleh Gambar 3.2 sebagai berikut.





Gambar 3.2 Pasir Monasit (Dokumentasi Pribadi, 2022)

3.2.2 *Flux* SiO₂

Flux yang digunakan dalam penelitian ini adalah silika dioksida *analytical grade* dengan rumus senyawa SiO₂, yang memiliki kemurnian hingga 99%. *Flux* SiO₂ ditunjukkan oleh Gambar 3.3 sebagai berikut.



Gambar 3.3 *Flux* SiO₂ (Dokumentasi Pribadi, 2022)

3.2.3 Serbuk Karbon

Serbuk karbon digunakan sebagai reduktor. Serbuk karbon yang digunakan merupakan karbon analitik dengan kemurnian 99%. Serbuk karbon ditunjukkan oleh Gambar 3.4 sebagai berikut.



Gambar 3.4 Serbuk Karbon (Dokumentasi Pribadi, 2022)



3.2.4 Serbuk CaCO₃

Serbuk CaCO₃ digunakan untuk menyuplai kebutuhan gas CO₂ dalam proses *smelting*. Serbuk CaCO₃ yang digunakan merupakan *analytical grade* yang memiliki kemurnian 99%. Serbuk CaCO₃ ditunjukkan oleh Gambar 3.5 sebagai berikut.



Gambar 3.5 Serbuk CaCO₃ (Dokumentasi Pribadi, 2022)

3.2.5 Akuades

Akuades pada penelitian ini digunakan sebagai media pencucian pasir monasit dalam menghilangkan pengotor. Akuades ditunjukkan oleh Gambar 3.6 sebagai berikut.



Gambar 3.6 Air Akuades (Dokumentasi Pribadi, 2022)

3.2.6 Elektroda Grafit

Elektroda grafit digunakan sebagai bahan yang berfungsi untuk mengalirkan arus listrik dengan kandungan karbon sebesar 99,9%. Elektroda grafit ditunjukkan oleh Gambar 3.7 sebagai berikut.



Gambar 3.7 Elektroda Grafit (Dokumentasi Pribadi, 2022)



3.3 Alat Penelitian

Alat-alat yang digunakan dalam penelitian ini yaitu sebagai berikut.

3.3.1 Neraca Analitik

Neraca analitik yang digunakan dalam penelitian ini berfungsi untuk menimbang bahan baku yang akan digunakan sesuai neraca massa. Neraca analitik ditunjukkan oleh Gambar 3.8 sebagai berikut.



Gambar 3.8 Neraca Analitik (Dokumentasi Pribadi, 2022)

3.3.2 Ayakan

Ayakan yang digunakan dalam penelitian ini berfungsi untuk mendapatkan ukuran butir bahan baku yang diinginkan dan homogen. Ayakan yang digunakan berukuran 50 *mesh*. Ayakan ditunjukkan oleh Gambar 3.9 sebagai berikut.



Gambar 3.9 Ayakan 50 Mesh (Dokumentasi Pribadi, 2022)

3.3.3 Termometer *Infrared*

Termometer *infrared* yang digunakan dalam penelitian ini berfungsi untuk mendeteksi temperatur di dalam *Electric Arc Furnace* saat proses *smelting*, sehingga dapat mengontrol temperatur. Termometer *infrared* ditunjukkan oleh Gambar 3.10 sebagai berikut.



Gambar 3.10 Termometer Infrared (Dokumentasi Pribadi, 2022)



3.3.4 Oven

Oven yang digunakan dalam penelitian ini berfungsi untuk menghilangkan *moisture content* dan mengeringkan pasir monasit setelah proses pencucian. Oven ditunjukkan oleh Gambar 3.11 sebagai berikut.



Gambar 3.11 Oven (Dokumentasi Pribadi, 2022)

3.3.5 Alat Tumbuk

Alat ini berfungsi untuk menghancurkan bahan baku untuk mendapatkan ukuran yang homogen yaitu 50 *mesh*. Alat tumbuk ditunjukkan oleh Gambar 3.12 sebagai berikut.



Gambar 3.12 Alat Tumbuk (Dokumentasi Pribadi, 2022)

3.3.6 Power Supply

Power supply dalam penelitian ini berfungsi sebagai penyuplai energi listrik sebagai sumber energi utama untuk pada *Electric Arc Furnace. Power supply* ditunjukkan oleh Gambar 3.13 sebagai berikut.



Gambar 3.13 Power Supply (Dokumentasi Pribadi, 2022)



3.3.7 Crucible

Crucible digunakan berbahan dasar SiC yang digunakan sebagai tempat berlangsungnya proses *smelting* pasir monasit dengan *Electric Arc Furnace*. *Crucible* beserta dimensinya ditunjukkan oleh Gambar 3.14 dan 3.15 sebagai berikut.



Gambar 3.14 Crucible (Dokumentasi Pribadi, 2022)



Gambar 3.15 Dimensi Crucible



3.3.8 Magnet Neodimium

Magnet neodimium digunakan untuk memisahkan pasir monasit dari unsur pengotor, *magnetic*, dan *non-magnetic portion* sebelum dan sesudah proses *smelting*. Magnet neodimium ditunjukkan oleh Gambar 3.16 sebagai berikut.



Gambar 3.16 Magnet Neodimium (Dokumentasi Pribadi, 2022)

3.4 Metode Penelitian

Berikut merupakan langkah percobaan yang perlu dilakukan dalam penelitian ini.

3.4.1 Persiapan Material

Berikut merupakan langkah-langkah yang dilakukan dalam melakukan preparasi material sebelum dilanjutkan ke proses *smelting*.

- 1. Dilakukan proses penghancuran (grinding) pasir monasit untuk mendapatkan ukuran yang homogen.
- 2. Pasir hasil *grinding* dilakukan *screening* melalui proses pengayakan hingga didapatkan ukuran yang homogen yaitu 50 *mesh*.
- 3. Dilakukan proses pencucian (*washing*) pasir monasit menggunakan media akuades hingga bersih.
- 4. Pasir monasit dipisahkan menggunakan metode *magnetic separation* untuk memisahkan kandungan magnetik dan non-magnetik.
- 5. Dilakukan kembali proses pencucian (*washing*) menggunakan media akuades hingga bersih.
- 6. Dilanjutkan dengan proses pengeringan spesimen pasir monasit di dalam oven pada temperatur 120°C selama 1 jam.
- 7. Sampel yang telah dikeringkan kemudian diuji karakterisasi menggunakan alat XRD dan XRF.
- 8. Dilakukan proses penimbangan massa pasir monasit, serbuk karbon, CaCO₃, dan SiO₂ sesuai perhitungan neraca massa sebelum dilanjutkan ke proses *smelting* menggunakan EAF.

3.4.2 Proses Smelting Menggunakan Electric Arc Furnace

Adapun langkah-langkah yang perlu dilakukan dalam melakukan proses *smelting* menggunakan EAF yaitu sebagai berikut.

- 1. Sampel yang telah dipreparasi sebelumnya dilakukan pencampuran antara pasir monasit, serbuk karbon, CaCO₃, dan SiO₂ sesuai dengan variasi yang digunakan.
- 2. Campuran sampel dimasukkan ke dalam *crucible* dan diposisikan merata pada seluruh bagian dasar.
- 3. Elektroda grafit kemudian dihubungkan dengan power supply.
- 4. *Power supply* dihubungkan ke sumber listrik dan diatur parameter arus sesuai dengan variasi dan tegangan pada 40 volt.



5. Proses *smelting* dilakukan selama 287 detik pada temperatur 1850°C dengan menghubungkan kutub positif pada material dan kutub negatif pada *crucible* seperti pada Gambar 3.17 sebagai berikut.



Gambar 3.17 Skema Proses Smelting

3.4.3 Perlakuan Setelah Proses Smelting

Berikut merupakan perlakuan yang diberikan kepada sampel setelah proses smelting.

- 1. Produk hasil *smelting* didinginkan hingga temperatur ruang di dalam *crucible*.
- 2. Dilakukan proses penghancuran (grinding) untuk produk hasil smelting.
- 3. Selanjutnya dilakukan *magnetic separation* untuk memisahkan magnetik dan nonmagnetik *portion*.
- 4. Produk dicuci menggunakan akuades dan dikeringkan dalam oven pada temperatur 120°C selama 1 jam.
- 5. Produk ditimbang untuk mengetahui massa setelah proses smelting.
- 6. Dilakukan pengujian XRD dan XRF terhadap produk *smelting* untuk dianalisis hasilnya.

3.5 Pengujian

Berikut merupakan pengujian yang dilakukan dalam penelitian ini.

3.5.1 Pengujian X-Ray Diffraction (XRD)

Pengujian XRD diperlukan untuk mengetahui senyawa secara kualitatif dan struktur kristalnya pada spesimen uji. Sampel spesimen uji dipreparasi terlebih dahulu dengan cara dihancurkan sebelum dilakukan uji XRD. Sinar X merupakan radiasi elektromagnetik yang memiliki energi yang tinggi. Interaksi antara berkas elektron eksternal dengan elektron pada kulit atom dan menghasilkan radiasi elektromagnetik. Radiasi tersebut merupakan sinar X dengan energi yang tinggi sekitar 200 eV sampai 1 MeV. Spektrum sinar X memiliki panjang gelombang 10⁻³ - 10 nm, berfrekuensi 1017 - 1020 Hz dan memiliki energi 10³-10⁶ eV. Panjang gelombang sinar X memiliki orde yang sama dengan jarak antar atom sehingga dapat digunakan sebagai sumber difraksi kristal suatu senyawa atau unsur.

Dalam pengujian ini digunakan alat XRD yang digunakan adalah XRD PAN Analytical yang ada di Departemen Teknik Material dan Metalurgi ITS. Hasil dari pengujian XRD akan didapatkan sebuah spektrum yang kemudian dianalisis menggunakan bantuan software HighScore Plus dilanjutkan dengan pengolahan data menggunakan software Origin Pro. Selama proses analisa berlangsung, data yang diperoleh disesuaikan dengan ICDD-JCPDS Card yang diperoleh melalui database PDF-Number. Perangkat alat XRD ditunjukkan oleh Gambar 3.18 sebagai berikut.





Gambar 3.18 Perangkat Alat XRD (Dokumentasi Pribadi, 2022)

3.5.2 Pengujian X-Ray Fluorescene (XRF)

Pengujian XRF dilakukan untuk mengetahui komposisi unsur dan senyawa oksida pada material hasil penelitian. Prinsip kerja XRF hampir sama dengan XRD akan tetapi perbedaannya adalah fluoresensi yang digunakan untuk analisis. Material yang diuji dihancurkan terlebih dahulu menjadi serbuk, kemudian dimasukkan ke dalam alat pengujian.

Hasil pengujian XRF lebih akurat dibandingkan XRD secara kuantitatif. XRF mampu memberikan data baik dalam bentuk unsur maupun oksida. Analisisnya relatif cepat karena simultan (beberapa elemen atau oksida bisa dianalisis sekaligus dalam sekali *running*). Hasil analisis XRF memiliki keakuratan yang baik serta membutuhkan sedikit sampel pada tahap preparasinya.

Dalam penelitian ini dilakukan pengujian XRF di Laboratorium Energi dan Lingkungan DRPM-ITS. Hasil pengujian XRF akan didapatkan berupa daftar senyawa dan unsur yang terkandung pada material beserta komposisinya. Perangkat alat XRF ditunjukkan oleh Gambar 3.19 sebagai berikut.



Gambar 3.19 Perangkat Alat XRF (Dokumentasi Pribadi, 2022)



3.6 Perhitungan

Dalam penelitian ini dilakukan beberapa perhitungan sebagai berikut.

3.6.1 Perhitungan Neraca Massa dan Energi

Perhitungan neraca massa dan energi merupakan hal paling penting yang menentukan keberhasilan dari *smelting* pasir monasit Perhitungan dilakukan dengan menghitung massa dari setiap komponen untuk mendapatkan neraca massa berdasarkan perbandingan mol dari reaksi-reaksi yang terjadi. Temperatur *smelting* 1850°C akan didapatkan pada parameter-parameter *power supply* melalui perhitungan neraca energi yang kemudian dijadikan sebagai dasar perkiraan reaksi dan perilaku termal untuk menghitung massa dari semua bahan mulai dari pasir monasit, serbuk karbon, CaCO₃, dan SiO₂.

Dengan menggunakan reaksi Boudouard sebagai acuan, massa serbuk karbon yang dibutuhkan dapat diperoleh melalui perhitungan kebutuhan gas karbon monoksida (CO) sebagai redukto untuk proses reduksi Fe₂O₃ menjadi logam Fe. Energi untuk dekomposisi CaCO₃ dan SiO₂ juga diperhitungkan melalui parameter termodinamika dalam neraca energi. Perbandingan komposisi massa tiap bahan disajikan pada Tabel 3.1 sebagai berikut.

 Tabel 3.1 Komposisi Massa Smelting Pasir Monasit

SiO ₂	Pasir Monasit	Serbuk Karbon	CaCO ₃	Massa Total
(gram)	(gram)	(gram)	(gram)	(gram)
0,99	10	0,47	0,85	12,31

Adapun parameter proses *smelting* berdasarkan perhitungan neraca energi disajikan pada Tabel 3.2 sebagai berikut.

Tabel 5.2 Spesifikasi EAF Pada Smelling									
Energi yang Dibutuhkan (J)	Tegangan (V)	Waktu (s)	Kuat Arus (A)	Energi EAF (J)					
			50	574.000					
			60	688.800					
801.566,04	40	287	70	803.600					
			80	918.400					
			90	1.033.200					

3.6.2 Perhitungan Recovery dan Separation Efficiency (S.E.)

Recovery merupakan persentase dari total logam atau mineral terkandung dalam bijih yang berhasil diubah ke dalam konsentrat. Perhitungan *recovery* didasarkan pada Persamaan (3.1) sebagai berikut (Pintowantoro & Abdul, 2020).

$$Recovery(\%) = \frac{W_{p \cdot c}}{W_{f \cdot f}} X \ 100\%$$
(3.1)

dengan W_p sebagai massa dari produk, W_f sebagai massa dari *feed*/umpan, *c* sebagai kadar mineral di dalam produk, dan *f* sebagai kadar dari mineral di dalam *feed*/umpan (Pintowantoro & Abdul, 2020).



Untuk membandingkan kualitas antara produk dengan *grade* dan *recovery* dapat dilakukan melalui perhitungan *separation efficiency* (S.E.) sesuai Persamaan (3.2) sebagai berikut (Wills & Finch, 2015).

$$S.E. = \frac{100 \cdot C \cdot m \cdot (c-f)}{(m-f) \cdot f}$$
(3.2)

dengan *m* sebagai persentase logam berharga dalam mineral berharga dan *C* sebagai rasio antara massa produk dan massa umpan (W_p/W_f) (Pintowantoro & Abdul, 2020).

3.6.3 Perhitungan Basisitas

Basisitas merupakan rasio senyawa yang bersifat basa terhadap senyawa yang bersifat asam yang ada pada *slag* atau produk hasil pemurnian yang menentukan banyak karakteristik *slag*, seperti temperatur likuidus *slag*, viskositas *slag*, karakteristik termodinamika *slag*, dan lain sebagainya. Terdapat tiga definisi basisitas *slag*, yaitu B₁, B₂, dan B₃ sesuai dengan senyawa oksida yang cenderung terbentuk pada *slag* atau produk. Perhitungan basisitas dilakukan sesuai Persamaan (3.3), (3.4), dan (3.5) sebagai berikut (Pintowantoro & Abdul, 2020).

$$B_1 = \frac{CaO}{SiO_2} \tag{3.3}$$

$$B_2 = \frac{CaO + MgO}{SiO_2} \tag{3.4}$$

$$B_3 = \frac{CaO + MgO}{SiO_2 + Al_2O_3}$$
(3.5)

3.7 Rancangan Penelitian

Berikut merupakan rancangan penelitian yang dilakukan dalam proses *smelting* pasir monasit dengan variasi arus listrik. Rancangan penelitian ditunjukkan oleh Tabel 3.3 sebagai berikut.

Variasi	Pengujian				
Kuat Arus Listrik (A)	XRD	XRF			
50	v	v			
60	v	v			
70	v	v			
80	v	v			
90	v	v			



3.8 Jadwal Penelitian

Berikut merupakan rencana *timeline* yang akan dilaksanakan dalam penelitian ini. Jadwal penelitian ditunjukkan oleh Tabel 3.4 sebagai berikut.

		Bulan																	
No	Kegiatan	Februari Maret				April				Mei			Juni						
		3	4	1	2	3	4	1	2	3	4	1	2	3	4	1	2	3	4
1	Studi Literatur																		
2	Bimbingan																		
2	Preparasi Alat dan																		
5	Bahan																		
4	Pengujian																		
4	Komposisi Awal																		
5	Proses Smelting																		
6	Pengujian																		
0	Komposisi Akhir																		
7	Penyusunan																		
	Laporan Akhir																		

Tabel 3.4 Jadwal Penelitian



(Halaman ini sengaja dikosongkan)



BAB IV ANALISIS DATA DAN PEMBAHASAN

4.1 Karakterisasi Pasir Monasit

Dalam penelitian ini, bahan utama yang digunakan adalah pasir monasit yang berasal dari Bangka Belitung, Indonesia. Untuk mengetahui komposisi oksida yang terdapat dalam pasir monasit dilakukan pengujian karakterisasi komposisi kimia menggunakan X-Ray Fluoresence (XRF). Pengujian XRF dilakukan di Laboratorium Energi dan Lingkungan DRPM-ITS. Komposisi oksida pada pasir monasit ditunjukkan oleh Tabel 4.1. Berikut merupakan komposisi oksida yang terkandung dalam pasir monasit.

Tabel 4.1 Komposisi Oksida Pasir Monasit (%)									
TiO ₂	ZrO ₂	Fe ₂ O ₃	SnO ₂	SO ₃	SiO ₂	P ₂ O ₅	Y2O3	MnO	HfO ₂
40,80	14,70	13,80	12,10	8,90	4,60	1,00	0,92	0,83	0,66
V ₂ O ₅	Nb ₂ O ₅	ThO ₂	CaO	WO ₃	PbO	U ₃ O ₈	Bi ₂ O ₃	As ₂ O ₃	
0,42	0,42	0,25	0,20	0,16	0,09	0,08	0,04	0,02	

Berdasarkan Tabel 4.1 didapatkan informasi bahwa grade ThO₂ dalam pasir monasit sebesar 0,25%. Sementara itu, tiga oksida yang mendominasi pasir monasit adalah TiO₂ sebesar 40,8%, ZrO₂ sebesar 14,7%, dan Fe₂O₃ sebesar 13,8%. Kemudian data ini akan digunakan untuk perhitungan neraca massa dan energi dalam penelitian.

Sedangkan untuk mengetahui fasa, senyawa dan struktur kristal yang terdapat pada pasir monasit dilakukan pengujian X-Ray Differaction (XRD). Pengujian XRD dilakukan di Divisi Karakterisasi Departemen Teknik Material dan Metalurgi FTIRS-ITS. Parameter pengujian XRD yang digunakan adalah panjang gelombang Cu-Kα 1,5406 Å, energi x-ray 8,04 keV, waktu difraksi 10 detik, dan sudut yang digunakan 20-90°. Dari pengujian XRD akan didapatkan data yang berisikan intensitas dan sudut yang terdeteksi. Kemudian diolah ke dalam bentuk grafik menggunakan software Origin Pro. Selain itu, untuk melakukan identifikasi fasa dan senyawa digunakan software Highscore yang sudah dilengkapi database ICDD-JCPDS. Grafik hasil pengujian XRD pasir monasit ditunjukkan oleh Gambar 4.1 sebagai berikut.





Berdasarkan Gambar 4.1 dapat dilihat bahwasannya terdapat banyak *peak* yang muncul. *Peak* dengan intensitas tinggi menandakan fasa tersebut mendominasi pada pasir monasit. Dapat dilihat bahwasannya ThO₂ dalam fasa *Thoria* tidak dominan pada pasir monasit dikarenakan memiliki *grade* yang sangat kecil. Fasa yang dominan pada pasir monasit ditunjukkan pada Tabel 4.2. Berikut merupakan fasa yang dominan pada pasir monasit.

	Label 4.2 Fasa Dominan Pasir Monasit										
No	Fasa	Senyawa	Struktur Kristal	Reference Code							
1	Hematite	Fe ₂ O ₃	Rhombohedral	01-073-0603							
2	Magnetite	Fe ₃ O ₄	Cubic	96-900-5842							
3	Wuestite	FeO	Cubic	01-079-1969							
4	Cassiterite	SnO ₂	Tetragonal	01-077-0449							
5	Anatase	TiO ₂	Tetragonal	96-900-8217							
6	Rutile	TiO ₂	Tetragonal	00-034-0180							
7	Ilmenite	FeTiO ₃	Hexagonal	96-901-0916							
8	Titanomaghemite	Fe ₂ TiO ₄	Cubic	01-084-1595							
9	Thoria	ThO ₂	Cubic	03-065-0293							
10	Copper Oxide	CuO	Monoclinic	03-065-2309							



4.2 Pengaruh Variasi Kuat Arus Listrik *Electric Arc Furnace* Terhadap Fasa Pada Pasir Monasit Hasil *Smelting*

Untuk mengetahui fasa yang terbentuk pada pasir monasit hasil *smelting* dilakukan pengujian karakterisasi fasa menggunakan *X-Ray Diffraction* (XRD). Pengujian XRD dilakukan di Divisi Karakterisasi Departemen Teknik Material dan Metalurgi FTIRS-ITS. Pengujian XRD hanya dilakukan pada *non-magnetic portion* karena ThO₂ bersifat *diamagnetic* (Belle, 1984). Pasir monasit hasil *smelting* yang telah dilakukan *separation magnetic* ditunjukkan oleh Gambar 4.2 sebagai berikut.



Gambar 4.2 Pasir Monasit Hasil Smelting (a) Magnetic Portion, (b) Non-magnetic Portion

Parameter pengujian XRD yang digunakan adalah panjang gelombang Cu-Kα 1,5406 Å, energi *x-ray* 8,04 keV, waktu difraksi 10 detik, dan sudut yang digunakan 20-90°. Dari pengujian XRD akan didapatkan data yang berisikan intensitas dan sudut yang terdeteksi. Kemudian diolah ke dalam bentuk grafik menggunakan *software Origin Pro*. Selain itu, untuk melakukan identifikasi fasa dan senyawa digunakan *software Highscore* yang sudah dilengkapi *database* ICDD-JCPDS. Fasa pada pasir monasit hasil *smelting* ditunjukkan pada Gambar 4.3 sebagai berikut.





Gambar 4.3 Fasa Pada Pasir Monasit Hasil Smelting

Dapat dilihat pada Gambar 4.3 bahwa pasir monasit hasil *smelting* memiliki beberapa fasa baru. Fasa baru terbentuk dikarenakan bereaksi dengan SiO₂ sebagai *flux* dan/atau senyawa pengotor lainnya. Bahkan, ThO₂ dalam fasa *Thoria* menjadi salah satu fasa yang cukup dominan. Untuk mempermudah menganalisa perlu dilakukan perbandingan fasa yang terbentuk. Perbandingan fasa yang terbentuk pada masing-masing variasi ditunjukkan pada Tabel 4.3. Berikut data perbandingan fasa yang terbentuk pada masing-masing variasi.



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Tab	Tabel 4.3 Perbandingan Fasa Pada Masir Monasit Hasil Smelting										
No	Fasa	Senyawa	Variasi Kuat Arus Listrik (A)								
			50	60	70	80	90				
1	Rutile	TiO ₂	v	v	v	v	v				
2	Ilmenite	FeTiO ₃	v	v	-	-	-				
3	Hematite	Fe ₂ O ₃	v	v	v	v	v				
4	Calcium Titanium Oxide	CaTiO ₃	v	v	v	v	v				
5	Hatrurite	Ca ₃ SiO ₅	v	v	-	-	-				
6	Thoria	ThO ₂	v	v	v	v	v				
7	Fayalite	Fe ₂ SiO ₄	-	v	v	v	v				
8	Copper Oxide	CuO	v	v	v	v	v				
9	Cassiterite	SnO_2	v	v	v	v	v				

Dari Tabel 4.3 dapat dilihat bahwa terdapat beberapa fasa baru yang terbentuk pada hasil *smelting* pasir monasit, yaitu *calcium titanium oxide* (CaTiO₃), *hatrurite* (Ca₃SiO₅), dan *fayalite* (Fe₂SiO₄). CaTiO₃ terbentuk melalui reaksi CaO hasil dekomposisi CaCO₃ yang berikatan dengan TiO₂. CaTiO₃ terdapat pada semua variasi. Hal ini dikarenakan pembentukan CaTiO₃ cukup mudah. Dimana CaO didapatkan pada temperatur 750°C dan membentuk CaTiO₃ pada temperatur 1300°C. Sedangkan temperatur *smelting* mencapai 1850°C. Pembentukan CaTiO₃ ditunjukkan pada Persamaan (4.1) dan (4.2) sebagai berikut (Song et al., 2021).

$$CaCO_3 \rightarrow CaO + CO_2 \tag{4.1}$$
$$\Delta G = -95.010 \text{ J pada } T = 750^{\circ} \text{C}$$

$$TiO_2 + CaO \rightarrow CaTiO_3$$

$$\Delta G = -85.000 \text{ J pada } T = 1.300^{\circ}\text{C}$$

$$(4.2)$$

Kemudian, Ca₃SiO₅ terbentuk akibat CaCO₃ yang saling bereaksi dengan SiO₂. Reaksi ini terjadi pada rentang 605,2-1.600°C. Oleh karena itu, Ca₃SiO₅ hanya terjadi pada variasi 50 A dan 60 A. Dikarenakan pada kuat arus listrik yang lebih tinggi, laju pemanasan semakin tinggi sehingga mengakibatkan CaCO₃ terdekomposisi dan SiO₂ bereaksi dengan senyawa lainnya (Sagita et al., 2020). Pembentukan Ca₃SiO₅ ditunjukkan pada Persamaan (4.3) sebagai berikut (Kolesnikov et al., 2022).

$$3CaCO_3 + SiO_2 \rightarrow Ca_3SiO_5 + 3CO_2$$
 (4.3)
 $\Delta G = -432.500 \text{ J pada } T = 1.600^{\circ}\text{C}$

Sedangkan SiO₂ sebagai *flux* berperan untuk mengikat logam pengotor pada pasir monasit. Salah satunya adalah FeO hasil reduksi Fe₂O₃ dan membentuk Fe₂SiO₄. Alhasil FeO tidak terjadi pada semua variasi. Namun, pada 50 A Fe₂SiO₄. Hal ini dikarenakan pada 50 A laju pemanasan sangat lambat, sehingga belum mencukupi energi yang dibutuhkan untuk



pembentukan Fe₂SiO₄. Reaksi ini terjadi pada temperatur 1.210°C. Pembentukan Fe₂SiO₄ ditunjukkan pada Persamaan (4.4) sebagai berikut (Gupta, 2003).

$$2FeO + SiO_2 \rightarrow Fe_2SiO_4 \tag{4.4}$$

$$\Delta G = -1.672.000 \text{ J pada } T = 1.210^{\circ}\text{C}$$

Sementara itu, terdapat beberapa fasa yang hilang, yaitu *magnetite* (Fe₃O₄), *wustite* (FeO), dan *titanomaghemite* (Fe₂TiO₄). Fe₃O₄ dan FeO merupakan hasil reduksi dari Fe₂O₃. Awalnya Fe₂O₃ akan tereduksi menjadi Fe₃O₄ pada temperatur 700°C. Kemudian Fe₃O₄ akan tereduksi menjadi FeO pada temperatur 800°C. Dan pada akhirnya FeO akan tereduksi menjadi Fe pada temperatur 1.127°C. Kemungkinan paling tepat adalah Fe₂O₃ sudah berhasil tereduksi Fe, serta tidak menyisakan Fe₃O₄ dan FeO dikarenakan reaksi reduksi Fe₂O₃ ke Fe berlangsung sangat cepat. Reduksi Fe₂O₃ menjadi Fe ditunjukkan pada Persamaan (4.5), (4.6), dan (4.7) sebagai berikut (Chen et al., 2017).

$$3Fe_2O_3 + CO \rightarrow 2Fe_3O_4 + CO_2$$
 (4.5)
 $\Delta G = -145.000 \text{ J pada } T = 700^{\circ}\text{C}$

$$Fe_3O_4 + CO \rightarrow 3FeO + CO_2 \tag{4.6}$$
$$\Delta G = -51.600 \text{ J pada } T = 800^{\circ}\text{C}$$

$$FeO + CO \rightarrow Fe + CO_2$$

$$\Delta G = -1.630 \text{ J pada } T = 1.127^{\circ}\text{C}$$

$$(4.7)$$

Sedangkan Fe_2TiO_4 hilang dikarenakan bereaksi dengan CaO menjadi CaTiO₃ dan Fe pada temperatur 1.000°C. Reaksi Fe_2TiO_4 dengan CaO membentuk CaTiO₃ dan Fe ditunjukkan pada Persamaan (4.8) sebagai berikut (Zhao et al., 2019).

$$Fe_2TiO_4 + CaO + 2CO \rightarrow CaTiO_3 + 2Fe + 2CO_2$$
(4.8)
$$\Delta G = -50.000 \text{ J pada } T = 1.000^{\circ}\text{C}$$

Selain terdapat fasa yang baru dan hilang, juga terdapat fasa yang hanya terjadi pada beberapa variasi saja, yaitu *ilmenite* (FeTiO₃). FeTiO₃ hanya terjadi pada 50 A dan 60 A karena laju pemanasan yang lambat menghambat FeTiO₃ bereaksi dengan CaO membentuk CaTiO₃ dan Fe pada temperatur 1.200°C. Reaksi FeTiO₃ bereaksi dengan CaO membentuk CaTiO₃ dan Fe ditunjukkan pada Persamaan (4.9) sebagai berikut (Zhao et al., 2019).

$$FeTiO_3 + CaO + CO \rightarrow CaTiO_3 + Fe + CO_2$$

$$\Delta G = -100.000 \text{ J pada } T = 1.200^{\circ}\text{C}$$
(4.9)

4.3 Pengaruh Variasi Kuat Arus Listrik *Electric Arc Furnace* Terhadap Komposisi Senyawa Utama Pasir Monasit Hasil *Smelting*

Untuk mengetahui komposisi senyawa pasir monasit hasil *smelting* dilakukan pengujain XRF. Pengujian XRF dilakukan di Laboratorium Energi dan Lingkungan DRPM-ITS. Pasir monasit hasil *smelting* yang diuji adalah *non-magnetic portion* dikarenakan logam berharga, yaitu ThO₂ bersifat *diamagnetic* (Belle, 1984). Komposisi oksida pada pasir monasit hasill *smelting* ditunjukkan oleh Tabel 4.4. Berikut merupakan komposisi senyawa pasir monasit hasil *smelting*.



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Ta	Tabel 4.4 Komposisi Senyawa Pasir Monasit Hasil Smelting								
NIa	Voriosi	Grade (%)							
INU	v ariasi	ThO ₂	Fe ₂ O ₃	TiO ₂	CaO	SiO ₂	Lainnya		
1	Pasir Monasit	0,25	13,8	40,8	0,2	4,6	40,32		
2	50 A	0,28	12,65	22,95	4,66	9,05	50,41		
3	60 A	0,37	17,3	35,4	6,2	8,15	32,58		
4	70 A	0,44	10,95	43,95	6,89	8,8	28,97		
5	80 A	0,45	11,1	41,9	7,27	9,9	29,38		
6	90 A	0,43	16,05	42,7	6,64	8,25	25,93		

Dapat dilihat pada Tabel 4.4 bahwa terjadi perbedaan komposisi senyawa seiring dengan perubahan kuat arus listrik pada *smelting* pasir monasit. Pada pembahasan ini berfokus pada dua senyawa utama, yaitu Fe₂O₃ dan TiO₂, serta satu senyawa berharga, yaitu ThO₂. Perubahan *grade* Fe₂O₃ pada pasir monasit hasil *smelting* ditunjukkan oleh Gambar 4.4 sebagai berikut.



Gambar 4.4 Grade Fe₂O₃ Dalam Pasir Monasit Hasil Smelting

Gambar 4.4 menunjukkan bahwa pengaruh variasi kuat arus listrik terhadap *grade* Fe_2O_3 memiliki pola yang fluktuatif. Dimana *grade* Fe_2O_3 mengalami penurunan pada 50 A (12,65%), 70 A (10,95%), dan 80 A (11,1%). Sedangkan mengalami peningkatan pada 60 A (17,3%) dan 90 A (16,05%).

Semakin tinggi kuat arus listrik, maka laju pemanasan semakin tinggi (Sagita et al., 2020). Hal ini mempercepat peningkatan kelarutan SiO₂ selaku *flux* dalam *molten slag* dan mengurangi viskositas dari *slag* (Heo & Park, 2022). Hal ini akan menghalangi reduksi Fe₂O₃ menjadi Fe. Bahkan dalam bentuk FeO akan cenderung bereaksi dengan SiO₂ membentuk senyawa baru, yaitu Fe₂SiO₄ melalui Persamaan (4.10) sebagai berikut (Gupta, 2003).



$$2FeO + SiO_2 \rightarrow Fe_2SiO_4 \tag{4.10}$$
$$\Delta G = -1.672.000 \text{ J pada } T = 1210^{\circ}\text{C}$$

Di lain sisi, semakin tinggi kuat arus listrik, maka memungkinkan energi panas yang berlebih yang mengakibatkan Fe hasil reduksi Fe₂O₃ mengalami oksidasi. Sehingga, Fe akan kembali lagi ke dalam bentuk senyawa oksida pada temperatur 1.000°C. Persamaan oksidasi Fe ditunjukkan oleh Persamaan (4.11), (4.12), dan (4.13) sebagai berikut (Henpristian et al., 2014).

$$2Fe + O_2 \rightarrow 2FeO$$
 (4.11)
 $\Delta G = -395.000 \text{ J pada } T = 1.000^{\circ}\text{C}$

$$6FeO + O_2 \rightarrow 2Fe_3O_4$$
 (4.12)
 $\Delta G = -375.000 \text{ J pada } T = 1.000^{\circ}\text{C}$

$$4Fe_3O_4 + O_2 \to 6Fe_2O_3$$
(4.13)
$$\Delta G = -220.000 \text{ J pada } T = 1.000^{\circ}\text{C}$$

Faktor utama yang mengakibatkan *grade* Fe_2O_3 mengalami penurunan adalah reduksi Fe_2O_3 menjadi Fe. Fe merupakan unsur *paramagnetic*, sehingga akan terpisahkan ketika dilakukan *magnetic separation*. Proses reduksi Fe_2O_3 menjadi Fe ditunjukkan oleh Persamaan (4.14), (4.15), dan (4.16) sebagai berikut (Chen et al., 2017).

$$3Fe_2O_3 + CO \rightarrow 2Fe_3O_4 + CO_2$$
 (4.14)
 $\Delta G = -145.000 \text{ J pada } T = 700^{\circ}\text{C}$

$$Fe_3O_4 + CO \rightarrow 3FeO + CO_2$$

$$\Delta G = -51.600 \text{ J pada } T = 800^{\circ}\text{C}$$

$$(4.15)$$

$$FeO + CO \rightarrow Fe + CO_2$$
 (4.16)
 $\Delta G = -1.630 \text{ J pada } T = 1.127^{\circ}\text{C}$

Perlu diingat bahwa *grade* Fe_2O_3 akan turun ketika Fe sudah tidak dalam bentuk senyawa oksida. Namun, ketika Fe_2O_3 tereduksi namun belum mencapai Fe, maka akan tetap teridentifikasi Fe_2O_3 . Hal ini juga berlaku untuk Fe_2SiO_4 dan senyawa baru lainnya yang berbasis oksida Fe. Sehingga akan menyebabkan *grade* Fe_2O_3 mengalami kenaikan.

Selain Fe₂O₃, terdapat pula TiO₂ sebagai senyawa pengotor utama dalam pasir monasit. TiO₂ memiliki *grade* terbesar dalam pasir monasit, yaitu sebesar 40,8%. Senyawa ini cenderung stabil dalam bentuk oksida dikarenakan posisinya yang berada di bagian bawah pada diagram ellingham (Lee, 1999). Perubahan *grade* TiO₂ pada pasir monasit hasil *smelting* ditunjukkan oleh Gambar 4.5 sebagai berikut.

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Gambar 4.5 Grade TiO₂ Dalam Pasir Monasit Hasil Smelting

Gambar 4.5 menunjukkan bahwa pengaruh variasi kuat arus listrik terhadap *grade* TiO₂ memiliki pola meningkat. Dimana pada 50 A *grade* TiO₂ mengalami penurunan dari 40,8% ke 22,95%. Kemudian berangsur naik ke 35,4% pada 60 A dan 43,95% pada 70 A. Selanjutnya turun ke 41,9% pada 80 A dan naik kembali ke 42,7% pada 90 A.

CaTiO₃ terbentuk karena bereaksinya FeTiO₃ dan Fe₂TiO₄ dengan CaO pada temperatur 1.000°C dan 1.200°C. CaTiO₃ merupakan senyawa *diamagnetic*, sehingga sulit dipisahkan melalui *magnetic separation* (Pal et al., 2018). Reaksi ini ditunjukkan pada Persamaan (4.17) dan (4.18) sebagai berikut (Zhao et al., 2019).

$$FeTiO_3 + CaO + CO \rightarrow CaTiO_3 + Fe + CO_2$$

$$\Delta G = -100.000 \text{ J pada } T = 1200^{\circ}\text{C}$$

$$(4.17)$$

$$Fe_2TiO_4 + CaO + 2CO \rightarrow CaTiO_3 + 2Fe + 2CO_2$$

$$\Delta G = -50.000 \text{ J pada } T = 1.000^{\circ}\text{C}$$

$$(4.18)$$

Sedangkan *grade* TiO₂ mengalami peningkatan dikarenakan reduksi FeTiO₃ menjadi FeTi₂O₅ yang kemudian tereduksi lagi menjadi TiO₂. Reduksi FeTiO₃ menjadi FeTi₂O₅ terjadi pada temperatur 1.500°C. Sedangkan reduksi FeTi₂O₅ menjadi TiO₂ terjadi pada temperatur 400°C. Reduksi FeTiO₃ menjadi TiO₂ ditunjukkan oleh Persamaan (4.19) dan (4.20) sebagai berikut (He et al., 2021; Zhao et al., 2019).

$$2FeTiO_3 + CO \rightarrow Fe + FeTi_2O_5 + CO_2$$

$$\Delta G = -20.000 \text{ J pada } T = 1.500^{\circ}\text{C}$$

$$(4.19)$$

$$FeTi_2O_5 + CO \rightarrow Fe + TiO_2 + CO_2$$

$$\Delta G = -2.000 \text{ J pada } T = 400^{\circ}\text{C}$$

$$(4.20)$$

Sementara itu, senyawa berharga yang dicari, yaitu ThO₂ mengalami peningkatan *grade* seiring bertambahnya kuat arus listrik dari 50 A sampai dengan 80 A. Setelah itu mengalami



penurunan *grade* pada 90 A. Perubahan *grade* ThO₂ pada pasir monasit hasil *smelting* ditunjukkan oleh Gambar 4.6 sebagai berikut.



Gambar 4.6 Grade ThO₂ Dalam Pasir Monasit Hasil Smelting

Berdasarkan Gambar 4.6 dapat memberikan informasi bahwasannya kenaikan kuat arus listrik dapat membantu meningkatkan *grade* ThO₂. *Grade* ThO₂ tertinggi didapatkan pada 80 A. Kenaikan ini disebabkan oleh jumlah pengotor yang turun. Jumlah pengotor ini turun akibat terpisahkan melalui *separation magnetic*. Sebagai contoh, Fe dari hasil reduksi Fe₂O₃, pembentukan CaTiO₃ dari FeTiO₃ atau Fe₂TiO₄, dan reduksi FeTiO₃. Dimana Fe merupakan unsur *paramagnetic*. Kenaikan kuat arus listrik menyebabkan laju pemanasan meningkat, sehingga menyebabkan reduksi Fe₂O₃ menjadi Fe cepat terjadi (Sagita et al., 2020). Sehingga, mengahasilkan Fe yang cukup banyak.

Sangat diperlukan proses lebih lanjut melalui metode hidrometalurgi untuk dapat melakukan ekstraksi Th dari pasir hasil *smelting*. Hal ini karena sangat sulit apabila tetap dilakukan melalui *smelting*, dimana temperatur leleh ThO₂ sangat tinggi, yaitu 3.377°C (Ghosh et al., 2016). Selain itu, pada pasir monasit hasil *smelting* juga masih terdapat banyak oksida REE dengan temperatur leleh sangat tinggi (Teixeira et al., 2019).

4.4 Pengaruh Variasi Kuat Arus Listrik *Electric Arc Furnace* Terhadap *Recovery* Senyawa Utama Pasir Monasit Hasil *Smelting*

Dalam *smelting*, tujuan utama yang ingin dicapai adalah memisahkan senyawa berharga dengan senyawa pengotor melalui mengikat senyawa pengotor dengan *flux* dalam senyawa baru yang dapat dipisahkan melalui metode separasi. Salah satu indikator untuk mengetahui keberhasilan *smelting* adalah *recovery*. *Recovery* didapatkan melalui perhitungan dengan cara membandingkan antara massa produk dikalikan *grade* senyawa dan massa sampel dikalikan *grade* senyawa pada sampel (Pintowantoro & Abdul, 2020). Produk yang dimaksud adalah *non-magnetic portion* dikarenakan senyawa berharga, yaitu ThO₂ bersifat *diamagnetic* (Belle, 1984). Sedangkan *recovery* yang dibahas hanya pada senyawa utama pasir monasit hasil *smelting*, yaitu Fe₂O₃, TiO₂, dan ThO₂. Grafik *recovery* senyawa utama pasir monasit hasil *smelting* ditunjukkan oleh Gambar 4.7 sebagai berikut.




Gambar 4.7 Recovery Senyawa Utama Pasir Monasit Hasil Smelting

Gambar 4.7 menunjukkan bahwasannya *recovery* ThO₂ memiliki tren yang naik seiring kenaikan kuat arus listrik. *Recovery* tertinggi didapatkan sebesar 85,68% pada variasi kuat arus listrik 80 A. Namun, kemudian turun pada 90 A secara cukup signifikan. Walaupun pada 90 A terdapat selisih *grade* yang sangat kecil. Hal ini dikarenakan massa produk yang didapatkan juga berpengaruh terhadap perhitungan *recovery* (Pintowantoro & Abdul, 2020).

Sementara itu, *recovery* Fe₂O₃ dan TiO₂ memiliki tren yang naik. Hal ini dikarenakan terdapat senyawa baru yang teridentifikasi sebagai Fe₂O₃ dan TiO₂ walaupun tidak memiliki rumus kimia yang sama, yaitu Fe₂SiO₄ dan CaTiO₃. Selain itu, juga terdapat TiO₂ dari hasil reduksi FeTiO₃ (He et al., 2021; Zhao et al., 2019). Dimana Fe₂SiO₄ merupakan hasil reaksi antara FeO dan SiO₂ sebagai *flux* (Gupta, 2003). Sedangkan, CaTiO₃ merupakan hasil reaksi antara CaO dan TiO₂ (Song et al., 2021). Variasi kuat arus listrik 50 A memiliki *recovery* Fe₂O₃ dan TiO₂ terkecil masing-masing sebesar 10,54% dan 6,47%.

Recovery juga dipengaruhi oleh basisistas dari *slag* yang terbentuk pada hasil *smelting*. Basisitas adalah perbandingan antara senyawa basa dan senyawa asam yang terdapat pada produk hasil *smelting* (Pintowantoro & Abdul, 2020). Dimana pada produk hasil *smelting* yang dimaksud senyawa basa adalah CaO, sedangkan senyawa asam adalah SiO₂. Basisitas pada pasir monasit hasil *smelting* ditunjukkan pada Gambar 4.8 sebagai berikut.





Gambar 4.8 Basisitas Pasir Monasit Hasil Smelting

Pada Gambar 4.8 menunjukkan bahwa basisitas pasir monasit hasil *smelting* relatif mengalami kenaikan seiring meningkatnya kuat arus listrik. Basisitas yang rendah atau semakin mendekati 0 menunjukkan bahwa konsentrat bersifat asam. Sebaliknya, basisitas yang tinggi atau semakin menjauhi 0 menunjukkan bahwa konsentrat bersifat basa. Keasaman konsentrat berpengaruh pada sifat reduktibilitas dari senyawa pengotor. Semakin asam konsentrat akan meningkatkan viskositas *molten metal* dan *slag*, sehingga akan mengurangi reduktibiltas senyawa pengotor dan cenderung bereaksi dengan *flux*. Begitupun sebaliknya apabila keasaman konsentrat rendah akan meningkatkan temperatur leleh dari *slag* (Pintowantoro & Abdul, 2020).

Dapat dilihat bahwasannya ketika nilai basisitas pada titik tertinggi sebesar 0,8, maka *grade* dan *recovery* Fe_2O_3 dan TiO_2 relatif pada titik tertingginya. Hal ini dikarenakan meningkatnya temperatur leleh dari *slag*, sehingga memungkinkan proses reduksi senyawa kompleks $FeTiO_3$ dapat dengan mudah terjadi. Sedangkan pada titik terendahnya, yaitu sebesar 0,51, *grade* dan *recovery* Fe_2O_3 dan TiO_2 relatif pada titik terendahnya juga. Hal ini disebabkan Fe_2O_3 dan TiO_2 cenderung untuk bereaksi dengan logam lain maupun dengan *flux*.

Selain itu, *recovery* juga dipengaruhi oleh *magnetic separation* pasir monasit hasil *smelting*. Hal ini dikarenakan pada perhitungan *recovery* yang dianggap sebagai massa produk adalah *non*-magnetic *portion*. *Non-magnetic portion* pada pasir monasit hasil *smelting* ditunjukkan oleh Gambar 4.9 sebagai berikut.





Gambar 4.9 Non-magnetic Portion Pasir Monasit Hasil Smelting

Gambar 4.9 menunjukkan bahwa seiring meningkatnya kuat arus listrik, maka nonmagnetic portion cenderung meningkat hingga pada 90 A mengalami penurunan. Non-magnetic portion terbanyak didapatkan pada 80 A sebesar 59%. Sebaliknya, didapatkan non-magnetic portion terendah sebesar 15% pada 50 A. Persentase non-magnetic portion dapat dijadikan salah satu indikator keberhasilan smelting. Hal ini tujuan smelting adalah mereduksi senyawa pengotor atau mengikatnya dengan *flux* menjadi senyawa kompleks. Kuat arus listrik yang semakin tinggi berdampak pada laju pemanasan yang tinggi pula, sehingga reaksi reduksi maupun pembentukan senyawa kompleks terjadi secara cepat dan memberikan waktu yang cukup untuk menghasilkan jumlah yang besar (Sagita et al., 2020). Selain itu, ThO₂ memiliki sifat diamagnetic yang sangat sulit untuk ditarik oleh magnet. Sehingga ThO₂ sebagian besar berada di non-magnetic portion (Belle, 1984). Oleh karena itu, semakin besar non-magnetic portion dengan grade ThO₂ yang sama, maka jumlah ThO₂ pun semakin besar.

4.5 Pengaruh Variasi Kuat Arus Listrik *Electric Arc Furnace* Terhadap *Separation Efficiency* (S.E.) Senyawa Utama Pasir Monasit Hasil *Smelting*

Dalam menentukan variasi kuat arus listrik EAF yang terbaik, diperlukan suatu parameter dengan memperhitungan *grade* dan *recovery* senyawa utama pasir monasit hasil *smelting*. Parameter ini selanjutnya disebut dengan *separation efficiency* (S.E.). Perhitungan S.E. dilakukan sebagaimana pada Persamaan (3.2) (Pintowantoro & Abdul, 2020). Grafik perbandingan S.E. senyawa utama pasir monasit hasil *smelting* ditunjukkan oleh Gambar 4.10. sebagai berikut.





Electric Current (A)

Gambar 4.10 Grafik Perbandingan S.E. Senyawa Utama Pasir Monasit Hasil Smelting

Gambar 4.10 menunjukkan S.E. senyawa utama pasir monasit hasil *smelting* memiliki tren yang berbeda. Dimana, S.E. ThO₂ dan Fe₂O₃ mengalami peningkatan seiring meningkatnya kuat arus listrik kemudian turun pada 90 A. Sementara itu, S.E. TiO₂ memiliki tren yang fluktuatif dengan didapatkan S.E. tertinggi sebesar 15,76% pada 50 A dan terendah sebesar 4,02% pada 80 A.

Penggunaan kuat arus listrik dalam *smelting* pasir monasit adalah untuk memproduksi energi panas yang mencukupi untuk reduksi senyawa pengotor atau mengikat senyawa pengotor dengan *flux* menjadi senyawa kompleks. Seiring meningkatnya kuat arus listrik, maka laju pemanasan akan meningkat. Sehingga, mengakibatkan ketercapaian termodinamika reaksi yang lebih cepat (Sagita et al., 2020). Oleh karena itu, reduksi senyawa pengotor dan pembentukan senyawa kompleks akan signifikan dalam segi jumlah. Namun, konsekuensinya adalah terdapat reduksi yang menghasilkan senyawa pengotor, sehingga menambah *grade* dari senyawa pengotor.

Berdasarkan sub-bab yang telah dibahas terkait *grade*, *recovery*, dan S.E. senyawa utama pasir monasit hasil *smelting*, variasi kuat arus listrik yang paling efektif didapatkan pada 80 A. Pertimbangan paling kuat adalah pada S.E. ThO₂ berada pada titik tertinggi sebesar 38,19% dan TiO₂ berada pada titik terendah sebesar 4,02%. Walaupun, Fe₂O₃ memiliki S.E. tertinggi sebesar 11,62% disebabkan ikut teridentifikasinya senyawa kompleks Fe₂SiO₄ sebagai Fe₂O₃. (Gupta, 2003; He et al., 2021; Zhao et al., 2019).



BAB V KESIMPULAN DAN SARAN

5.1 Kesimpulan

Berdasarkan analisis data dan pembahasan yang telah dilakukan, penelitian ini didapatkan kesimpulan sebagai berikut.

- 1. *Smelting* pasir monasit dengan variasi kuat arus listrik membentuk senyawa baru, yaitu *calcium titanium oxide* (CaTiO₃) pada semua variasi, *hatrurite* (Ca₃SiO₅) hanya pada 50 A dan 60 A, dan *fayalite* (Fe₂SiO₄) pada semua variasi, kecuali pada 50 A.
- 2. Grade Fe₂O₃ mengalami fluktuatif pada semua variasi kuat arus listrik dengan grade terendah sebesar 10,95% pada 70 A dan tertinggi sebesar 17,3% pada 60 A. Penurunan grade Fe₂O₃ diakibatkan oleh teroksidasinya Fe menjadi senyawa oksida dan reduksi Fe₂O₃ menjadi Fe, sedangkan peningkatan diakibatkan oleh terbentuknya senyawa kompleks Fe₂SiO₄ yang teridentifikasi sebagai Fe₂O₃. Sedangkan grade TiO₂ relatif mengalami peningkatan dengan grade tertinggi sebesar 43,95% didapatkan pada 80 A. Peningkatan grade TiO₂ diakibatkan oleh reduksi FeTiO₃ menjadi TiO₂.
- 3. Peningkatan kuat arus listrik pada *smelting* pasir monasit mengakibatkan peningkatan *grade* ThO₂ sebagai senyawa berharga. *Grade* ThO₂ pada pasir monasit hasil *smelting* dengan variasi kuat arus listrik 50 A, 60 A, 70 A, 80 A, dan 90 A secara berurutan sebesar 0,28%, 0,37%, 0,44%, 0,45%, dan 0,43%.
- 4. *Recovery* ThO₂ tertinggi sebesar 85,68% pada 80 A, *recovery* Fe₂O₃ dan TiO₂ terendah secara berurutan sebesar 10,54% dan 6,47% didapatkan pada 50 A. Dengan menggunakan perhitungan *separation efficiency* (S.E.) didapatkan kuat arus listrik paling efektif adalah 80 A.

5.2 Saran

Berdasarkan penelitian yang telah dilakukan, terdapat beberapa saran untuk penelitian selanjutnya sebagai berikut.

- 1. Melakukan ekstraksi lebih lanjut untuk memperoleh *grade* ThO₂ sebagai senyawa berharga menggunakan metode hidrometalurgi.
- 2. Melakukan studi terkait desain pada proses *smelting* untuk mengoptimalkan homogenitas saat reaksi berlangsung
- 3. Melakukan studi terkait *magnetic separation* lebih lanjut karena senyawa utama pasir monasit memiliki sifat magnetik yang spesifik



(Halaman ini sengaja dikosongkan)



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LAMPIRAN

1. Perhitungan neraca massa

Pada proses reduksi, berikut merupakan kesetimbangan Persamaan reaksi stoikiometri reduksi senyawa yang terkandung dalam pasir monasit.

$$\begin{array}{c} 3Fe_2O_3+CO\rightarrow 2Fe_3O_4+CO_2\\ Fe_3O_4+CO\rightarrow 3FeO+CO_2\\ FeO+CO\rightarrow Fe+CO_2\\ CaCO_3\rightarrow CaO+CO_2\\ CO_2+C\rightarrow 2CO \end{array}$$

Berdasarkan hasil pengujian XRF didapatkan komposisi senyawa utama yang terkandung dalam pasir monasit, yaitu sebagai berikut:

- Hematit (Fe_2O_3) = 16,50%
- Titanium dioksida (TiO₂) = 36,05%
- Silika dioksida (SiO₂) = 4,50%
- Toirum dioksida (ThO₂) = 0,22%

Apabila diasumsikan sampel percobaan sebesar 100 gram pasir monasit maka:

•	Mol Hematit (FeaOa)	<u>massa hematit</u> $16,5 gram = 0.1025$ mol
•	Wor Hemath (10203)	<i>Mr hematit</i> 161 gram/mol - 0,1025 III01
•	Mol Titanium dioksida	$\frac{massa TiO2}{2} = \frac{36.05 gram}{2} = 0.4563 mol$
•	WOI I Italiiulli uloksiua	$\frac{-1}{Mr TiO2} - \frac{-1}{79 gram/mol} = 0,4505 \text{ IIIOI}$
•	Mol Silika dioksida	$\underline{-massa\ SiO2}$ $\underline{-4,5\ gram}$ $\underline{-0.075\ mol}$
•	WOI SIIIKa Uloksida	$\frac{-1}{Mr SiO2} = \frac{-1}{60 gram/mol} = 0.073 \text{ mor}$
•	Mol Torim diaksida	$-\frac{massa ThO2}{2} - \frac{16,5 gram}{2} - 0.00083 mol$
•	WOT TOTTIL UIOKSIUA	$\frac{-1}{Mr hematit} = \frac{-1}{161 gram/mol} = 0,00085 \text{ III01}$

• Serbuk karbon yang digunakan memiliki kemurnian 99,99%

• Kalsium karbonat yang digunakan memiliki kemurnian 99,99%

I. Reaksi Reduksi Hematit

a.	Reaksi 1		~ ~				~ ~
	$3Fe_2O_3$	+	CO	\rightarrow	$2Fe_3O_4$	+	CO_2
	0,1025 mol		0,0342 mol		0,0684 mol		0,0342 mol

 CO_2 hasil dekomposisi $\mathrm{Ca}\mathrm{CO}_3$ yang dibutuhkan untuk bereaksi dengan serbuk karbon.

CO_2	+	С	\rightarrow	2CO	
0,0171 mol		0,0171mol		0,0342 mol	

Reaksi CO2 hasil dari reaksi 1 dengan serbuk karbon.

	CO_2	+	С	\rightarrow	2CO		
	0,0342 mol		0,0342 mol		0,0684 mol		
b.	Reaksi 2						
	Fe ₃ O ₄	+	CO	\rightarrow	3FeO	+	CO_2
	0,0684 mol		0,0684mol		0,2052 mol		0,0684 mol



	CO ₂ hasil reaksi serbuk karbon	dekomposisi	CaC	O ₃ yang	dibutuhkan	untuk	bereaksi	dengan
	CO ₂ +	С		\rightarrow 20	CO			
	0 mol	0 mol		0 mol				
	Reaksi CO ₂ hasil	dari reaksi 2 d	engai	n serbuk l	karbon.			
	$CO_2 + 0.0684 + 1$	C		$\rightarrow 20$				
C	0,0684 mol Reaksi 3	0,0684 mol		0,136	8 mol			
U.	FeO +	CO		→ Fe	+	CC		
	0,2052 mol	0,2052 mol		0,2052 m	ol	0,2052	2 mol	
	CO ₂ hasil reaksi serbuk karbon.	dekomposisi	CaC	O ₃ yang	dibutuhkan	untuk	bereaksi	dengan
	CO ₂ +	С	\rightarrow	2CO				
	0,0684 mol	0,0684 mol		(0,20	52-0,1368) n	nol		
	0,0684 mol	0,0684 mol		0,068	4 mol			
	Reaksi CO ₂ hasil CO ₂ $+$	dari reaksi 3 d	engaı →	n serbuk k 2CO	karbon.			
	0.2052 mol	0.2052 mol	,	0.410	4 mol			
	,	,		,				
Pe To	rhitungan Kebutu tal mol C yang dib	han Serbuk I utuhkan = (0,0 = 0,39	Xarb 171 + 33 m	on ⊢ 0,0342 - nol	+ 0,0684 + 0	,0684 +	- 0,2052)	mol
Ma	assa C yang dibutul	hkan = total = $0,39$ = $4,71$	l mol 933 m 96 gi	x Ar C nol x 12 g r	r/mol			
Pe	rhitungan Kebutu	ihan CaCO ₃	171.	0.0004	1			
10	tal CO ₂ yang dibut	= (0,0) = 0,08	171 + 55 m	+ 0,0684) 101	mol			
Са	$CO_2 \rightarrow$	CaO	+	CO_2				
0.0	855 mol	0.0855 mol	,	0.0855 m	ol			
Ma	ussa CaCO ₃ yang d	ibutuhkan = t	otal 1	mol x Mr	CaCO ₃			
		= (0,085	5 mol x 1	00 gr/mol			
		= 8	8,55 g	gr	0			
a 1		1 1'						
Sel	hingga didapatkan	perbandingan	sebag	gai beriku	t.			
Pas	100 :	4,7196	:	CaCO ₃ 8,55				
Pe	rhitungan Kehuti	ıhan <i>Flur</i> SiO) -					
M	$TiO_2 = mol SiO_2$		2					
M	$TiO_2 = 0.4563 \text{ m}$	ol						
M	$s_1 = 0, 1503 = 0$	0.075 = 0.3813	s mol					
1,1(-5.52 - 0,1000	0,0,0 = 0,0010						

II.

III.

IV.



Massa *flux* SiO_2 yang ditambahkan = mol x Mr SiO_2 $= 0,3813 \times 60 \text{ gr/mol}$ = 22,878 gram

Maka perbandingan massa yang diperoleh sebesar Pasir monasit : Fluks SiO₂ 100 22,878 : Penambahan fluks SiO₂ optimal = 18,61%

Pada kesempatan kali ini menggunakan fluks SiO₂ sebesar 9% atau sebesar 9,99 gr. Hal ini sesuai dengan penelitian yang telah dilakukan oleh Wienar pada tahun 2022.

V. Perhitungan Mass Balance Proses Smelting

Massa *input*

- = 12,32 gram
- Pasir monasit = 10 gram • •
- Flux SiO₂ = 0,99 gram
- Serbuk Karbon = 0,47 gram •
- CaCO₃ = 0,86 gram •

Massa *output*

•	Varias	i 50 A	= 7,66 gram
	0	Magnetic portion	= 6,51 gram
	0	Non-magnetic portion	= 1,15 gram
	0	Mass loss	= 4,66 gram
•	Varias	i 60 A	= 8,08 gram
	0	Magnetic portion	= 6,40 gram
	0	Non-magnetic portion	= 1,68 gram
	0	Mass loss	= 4,24 gram
•	Varias	i 70 A	= 8,26 gram
	0	Magnetic portion	= 4,43 gram
	0	Non-magnetic portion	= 3,83 gram
	0	Mass loss	= 4,06 gram
•	Varias	si 80 A	= 7,88 gram
	0	Magnetic portion	= 3,12 gram
	0	Non-magnetic portion	= 4,76 gram
	0	Mass loss	= 4,44 gram
•	Varias	si 90 A	= 7,15 gram
	0	Magnetic portion	= 3,14 gram
	0	Non-magnetic portion	= 4,01 gram
	0	Mass loss	= 5,17 gram

2. Perhitungan Neraca Energi (Heat Balance)

a) Data Mol

Berdasarkan data XRF raw material dan perhitungan neraca massa, digunakan data mol material sebagai berikut.



Senyawa	Mol
Fe ₂ O ₃	0,1025
TiO ₂	0,4563
CaO	0,02
SiO ₂	0,075
CaCO ₃	0,1537

b) Data Entalpi Pembentukan Standar (AHf)

Berikut merupakan data entalpi pembentukan standar senyawa pada 298 K.

Senyawa	∆Hf 298 (kJ/mol)
Fe ₂ O ₃	-824,2
Fe ₃ O ₄	-1.118
FeO	-272
Fe	0
Fe ₂ SiO ₄	39,33
FeTiO ₃	151,71
TiO ₂	-944,7
CaO	-635,09
SiO_2	-910,86
CaCO ₃	-1.207,6
CO_2	-393,509
CO	-110,525
С	0

c) Data *Heat Content* (H_T-H₂₉₈)

Berikut merupakan data heat content senyawa dan unsur, yang dihitung dengan Persamaan: 、 、

$$H_T-H_{298} = aT + bT^2 + cT^{-1} + d$$



Senyawa	a	b	c	d
Fe ₂ O ₃	98,658	0,03906	1.491.000	-37.888,2
Fe ₃ O ₄	91,896	0,01008	0	-36.397,2
FeO	48,972	0,0042	281.400	-15.918
Fe	12,768	0,015918	-252.000	-4.376,4
Fe	41,034	0,0084	0	-2.814
Fe ₂ SiO ₄	40,71	0,00338	977.000	15.715
FeTiO ₃	27,87	0,00218	479.000	10.111
TiO ₂	75,474	0,00588	1.827.000	-28.681,8
CaO	49,014	0,02268	655.200	-17.014,2
SiO ₂	166,228	0,42782	892.910	47.390
SiO ₂	65,277	0,0028	1.846.300	-24.310
CaCO ₃	104,916	0,011004	2.604.000	-40.992
CO_2	44,394	0,00441	865.200	-16.543,8
СО	28,518	0,02058	462.000	-8.841
С	16,926	0,02394	856.800	-8.131,2
CaTiO ₃	127,974	0,002856	2.809.800	-47.833,8

d) Perhitungan Entalpi Reaksi

Entalpi reaksi dihitung berdasarkan data di atas dengan Persamaan:

$\Delta \mathbf{H} = \sum \mathbf{H} \operatorname{produk} - \sum \mathbf{H} \operatorname{reaktan}$

Dengan temperatur target 1850°C atau 2123 K, didapat:

i) $3Fe_2O_3 + CO \rightarrow 2Fe_3O_4 + CO_2$	ΔH=11.382,73 J
ii) $Fe_3O_4 + CO \rightarrow 3FeO + CO_2$	∆H= -61.818,13 J
iii) $FeO + CO \rightarrow Fe + CO_2$	ΔH= -13.810,27 J
iv) $Fe \rightarrow Fe$	∆H= 3.615,97 J
v) $2FeO + SiO_2 \rightarrow Fe_2SiO_4$	∆H= 127.099,64 J
vi) $FeO + TiO_2 \rightarrow FeTiO_3$	∆H= 79.388,18 J
vii) $CaCO_3 \rightarrow CaO + CO_2$	∆H= 51.559,47 J
viii) $CO_2 + C \rightarrow 2CO$	∆H= 49.637,30 J
ix) $SiO_2 \rightarrow SiO_2$	∆H= 154.864,67 J
x) $CaO + TiO_2 \rightarrow CaTiO_3$	∆H= 326.776,83 J
Total papas reaksi yang dibutuhkan adalah 728696 4 Joule	

Total panas reaksi yang dibutuhkan adalah 728696,4 Joule

e) Perhitungan Energi Input Proses Smelting

Spesifikasi Power Supply yang digunakan adalah sebagai berikut.



Spesifikasi	Nilai
Tegangan output	40 V
Efisiensi	90%

Berdasarkan spesifikasi diatas, maka didapatkan energi yang dibutuhkan sebagai berikut.

E input = E outputE input = E reaksi x (100% + (100% - efisiensi)) E input = 728696,4 J x 110% E input = 801566,04 J

Panas yang dihasilkan dari EAF dengan menggunakan Persamaan energi listrik adalah sebagai berikut.

Variasi Kuat Arus Liastrik (A)	Tegangan (V)	Waktu (s)	Energi (J)
50			574.000
60	40		688.800
70		287	803.600
80			918.400
90			1.033.200

3. Perhitungan *Recovery*

Recovery senyawa utama pasir monasit hasil *smelting* didapatkan melalui membandingkan jumlah senyawa pada produk dan *feed* dengan perhitungan sebagai berikut.

Recovery (%) =
$$\frac{W_p.c}{W_f.f} x100\%$$

I. *Recovery* ThO₂

Data massa *feed* dan *non-magnetic portion* beserta *grade* Fe₂O₃ di dalamnya yang digunakan untuk menghitung *recovery* Fe₂O₃ disajikan dalam tabel berikut.



No	Variasi Kuat Arus Listrik (A)	W _f (gram)	f (%)	W _p (gram)	c (%)
1	50			1,15	0,28
2	60			1,68	0,37
3	70	10	0,25	3,83	0,44
4	80			4,76	0,45
5	90			4,01	0,43

• Variasi 50 A

Recovery ThO_2 , 50 $A = \frac{1,15 \times 0,28}{10 \times 0,25} \times 100\%$ Recovery ThO_2 , 50 A = 12,88%

• Variasi 60 A

Recovery ThO_2 , 60 $A = \frac{1,68 \times 0,37}{10 \times 0,25} \times 100\%$ Recovery ThO_2 , 60 A = 24,86%

• Variasi 70 A

Recovery ThO_2 , 70 $A = \frac{3,83 \times 0,44}{10 \times 0,25} \times 100\%$ Recovery ThO_2 , 70 A = 67,41%

• Variasi 80 A

$$\begin{aligned} & Recovery \ ThO_2, 80 \ A = \frac{4,76 \ x \ 0,45}{10 \ x \ 0,25} x 100\% \\ & Recovery \ ThO_2, 80 \ A = 85,68\% \end{aligned}$$

Variasi 90 A

$$\begin{aligned} Recovery \ ThO_2, 90 \ A &= \frac{4,01 \ x \ 0,43}{10 \ x \ 0,25} x 100\% \\ Recovery \ ThO_2, 90 \ A &= 68,97\% \end{aligned}$$

II. Recovery Fe₂O₃

Data massa *feed* dan *non-magnetic portion* beserta *grade* Fe₂O₃ di dalamnya yang digunakan untuk menghitung *recovery* Fe₂O₃ disajikan dalam tabel berikut.

No	Variasi Kuat Arus Listrik (A)	W _f (gram)	f (%)	W _p (gram)	c (%)
1	50			1,15	12.65
2	60			1,68	17.3
3	70	10	13,8	3,83	10.95
4	80			4,76	11.1
5	90			4,01	16.05



Variasi 50 A •

Recovery
$$Fe_2O_3$$
, 50 $A = \frac{1,15 \times 12,65}{10 \times 13,8} \times 100\%$
Recovery Fe_2O_3 , 50 $A = 10,54\%$

Variasi 60 A •

Recovery
$$Fe_2O_3$$
, 60 $A = \frac{1,68 \times 17,3}{10 \times 13,8} \times 100\%$
Recovery Fe_2O_3 , 60 $A = 21,06\%$

Variasi 70 A •

Recovery
$$Fe_2O_3$$
, 70 $A = \frac{3,83 \times 10,95}{10 \times 13,8} \times 100\%$
Recovery Fe_2O_3 , 70 $A = 30,39\%$

Variasi 80 A

Recovery
$$Fe_2O_3$$
, 80 $A = \frac{4,76 \times 11,1}{10 \times 13,8} \times 100\%$
Recovery Fe_2O_3 , 80 $A = 38,29\%$

. . .

Variasi 90 A •

Recovery
$$Fe_2O_3$$
, 90 $A = \frac{4,01 \times 16,05}{10 \times 13,8} \times 100\%$
Recovery Fe_2O_3 , 90 $A = 46,64\%$

III. Recovery TiO₂

Data massa feed dan non-magnetic portion beserta grade TiO2 di dalamnya yang digunakan untuk menghitung recovery TiO₂ disajikan dalam tabel berikut.

No	Variasi Kuat Arus Listrik (A)	W _f (gram)	f (%)	Wp (gram)	с (%)
1	50			1,15	22.95
2	60			1,68	35.4
3	70	10	40,8	3,83	43.95
4	80			4,76	41.9
5	90			4,01	42.7

Variasi 50 A

Recovery
$$TiO_2$$
, 50 $A = \frac{1,15 \times 22,95}{10 \times 40,8} \times 100\%$
Recovery TiO_2 , 50 $A = 6,47\%$

Variasi 60 A •

Recovery
$$TiO_2$$
, 60 $A = \frac{1,68 \times 35,4}{10 \times 40,8} \times 100\%$
Recovery TiO_2 , 60 $A = 14,58\%$

Variasi 70 A

<i>Recovery TiO</i> 70 $A = \frac{3,83 \times 4}{2}$	13,95 ×100%
10 x 4	0,8
Recovery TiO_2 , 70 $A = 4$	1,26%



• Variasi 80 A

$$Recovery TiO_{2}, 80 A = \frac{4,76 \times 41,9}{10 \times 40,8} \times 100\%$$
$$Recovery TiO_{2}, 80 A = 48,88\%$$

• Variasi 90 A

$$\begin{aligned} & \textit{Recovery TiO}_2, 90 \ \textit{A} = \frac{4,01 \ x \ 42,7}{10 \ x \ 40,8} \ x100\% \\ & \textit{Recovery TiO}_2, 90 \ \textit{A} = 41,97\% \end{aligned}$$

4. Perhitungan Separation Efficiency (S.E.)

S.E. senyawa utama pasir monasit hasil *smelting* didapatkan dengan meninjau *grade* dan *recovery* masing-masing melalui perhitungan sebagai berikut.

$$S.E.(\%) = \frac{100 \cdot C \cdot m \cdot (c-f)}{(m-f) \cdot f} x 100\%$$

I. S.E. ThO₂

Berikut data yang digunakan untuk menghitung S.E. ThO₂ pasir monasit hasil *smelting*.

No	Variasi Kuat Arus Listrik (A)	W _f (gram)	W _p (gram)	C (%)	m (%)	с (%)	f (%)
1	50		1,15	0,115		0,28	
2	60		1,68	0,168		0,37	
3	70	10	3,83	0,383	87,88	0,44	0,25
4	80		4,76	0,476		0,45	
5	90		4,01	0,401		0,43	

• Variasi 50 A $S.E. ThO_{2}, 50 A (\%) = \frac{100 \cdot 0,115 \cdot 87,88 \cdot (0,28 - 0,25)}{(0,28 - 0,25) \cdot 0,25} x100\%$ $S.E. ThO_{2}, 50 A (\%) = 1,38\%$ • Variasi 60 A $S.E. ThO_{2}, 60 A (\%) = \frac{100 \cdot 0,168 \cdot 87,88 \cdot (0,37 - 0,25)}{(0,37 - 0,25) \cdot 0,25} x100\%$ $S.E. ThO_{2}, 60 A (\%) = 8,09\%$ • Variasi 70 A $S.E. ThO_{2}, 70 A (\%) = \frac{100 \cdot 0,383 \cdot 87,88 \cdot (0,44 - 0,25)}{(0,44 - 0,25) \cdot 0,25} x100\%$ $S.E. ThO_{2}, 70 A (\%) = \frac{100 \cdot 0,476 \cdot 87,88 \cdot (0,45 - 0,25)}{(0,45 - 0,25)} x100\%$ • Variasi 80 A $S.E. ThO_{2}, 80 A (\%) = \frac{100 \cdot 0,476 \cdot 87,88 \cdot (0,45 - 0,25)}{(0,45 - 0,25) \cdot 0,25} x100\%$



• Variasi 90 A

S.E.
$$ThO_2$$
, 90 $A(\%) = \frac{100 \cdot 0.401 \cdot 87.88 \cdot (0.43 - 0.25)}{(0.43 - 0.25) \cdot 0.25} x100\%$
S.E. ThO_2 , 90 $A(\%) = 28.95\%$

II. S.E. Fe₂O₃

Berikut data yang digunakan untuk menghitung S.E. Fe_2O_3 pasir monasit hasil smelting.

No	Variasi Kuat Arus Listrik (A)	Variasi Kuat Arus Listrik (gram) (gram) (%) (A)		C (%)	m (%)	c (%)	f (%)
1	50		1,15	0,115		12.65	
2	60		1,68	0,168		17.3	
3	70	10	3,83	0,383	69,56	10.95	13,8
4	80		4,76	0,476		11.1	
5	90		4,01	0,401		16.05	

• Variasi 50 A $S.E. Fe_2O_3, 50 A (\%) = \frac{100 \cdot 0,115 \cdot 69,56 \cdot (12,65 - 13,8)}{(12,65 - 13,8) \cdot 13,8} x100\%$ $S.E. Fe_2O_3, 50 A (\%) = 1,2\%$ • Variasi 60 A $S.E. Fe_2O_3, 60 A (\%) = \frac{100 \cdot 0,168 \cdot 69,56 \cdot (17,3 - 13,8)}{(17,3 - 13,8) \cdot 13,8} x100\%$ $S.E. Fe_2O_3, 60 A (\%) = 5,32\%$ • Variasi 70 A $S.E. Fe_2O_3, 70 A (\%) = \frac{100 \cdot 0,383 \cdot 69,56 \cdot (10,95 - 13,8)}{(10,95 - 13,8) \cdot 13,8} x100\%$ $S.E. Fe_2O_3, 70 A (\%) = \frac{100 \cdot 0,476 \cdot 69,56 \cdot (11,1 - 13,8)}{(11,1 - 13,8) \cdot 13,8} x100\%$ • Variasi 80 A $S.E. Fe_2O_3, 80 A (\%) = \frac{100 \cdot 0,476 \cdot 69,56 \cdot (11,1 - 13,8)}{(11,1 - 13,8) \cdot 13,8} x100\%$ $S.E. Fe_2O_3, 80 A (\%) = \frac{100 \cdot 0,476 \cdot 69,56 \cdot (11,1 - 13,8)}{(11,1 - 13,8) \cdot 13,8} x100\%$

$$S.E. Fe_2O_3, 90 A (\%) = \frac{100 \cdot 0,401 \cdot 69,56 \cdot (16,05 - 13,8)}{(16,05 - 13,8) \cdot 13,8} x100\%$$

S.E. Fe_2O_3, 50 A (%) = 8,16%

III. S.E. TiO₂

Berikut data yang digunakan untuk menghitung S.E. Fe_2O_3 pasir monasit hasil *smelting*.



No	Variasi Kuat Arus Listrik (A)	W _f (gram)	W _p (gram)	C (%)	m (%)	с (%)	f (%)
1	50		1,15	0,115		22.95	
2	60		1,68	0,168		35.4	
3	70	10	3,83	0,383	59,93	43.95	40,8
4	80		4,76	0,476		41.9	
5	90		4,01	0,401		42.7	

- Variasi 50 A
 S.E. TiO₂, 50 A (%) = 100 . 0,115 . 59,93 . (22,95 40,8) / (22,95 40,8) . 40,8 / (22,95 40,8) / (22,95 4
- $S.E. TiO_2, 60 A (\%) = \frac{100 \cdot 0,168 \cdot 59,93 \cdot (35,4 40,8)}{(35,4 40,8) \cdot 40,8} x100\%$ S.E. TiO₂, 50 A (%) = 6,97%
- Variasi 70 A $S.E. TiO_2, 70 A (\%) = \frac{100 \cdot 0.383 \cdot 59.93 \cdot (43.95 - 40.8)}{(43.95 - 40.8) \cdot 40.8} x100\%$ $S.E. TiO_2, 70 A (\%) = 9.26\%$
- Variasi 80 A $S.E. TiO_2, 80 A (\%) = \frac{100 \cdot 0,476 \cdot 59,93 \cdot (41,9 - 40,8)}{(41,9 - 40,8) \cdot 40,8} x100\%$ $S.E. TiO_2, 80 A (\%) = 4,02\%$

• Variasi 90 A

$$S.E. TiO_2, 90 A (\%) = \frac{100 \cdot 0,401 \cdot 59,93 \cdot (42,7 - 40,8)}{(42,7 - 40,8) \cdot 40,8} x100\%$$

 $S.E. TiO_2, 90 A (\%) = 5,85\%$

5. Perhitungan Basisitas

Basisitas didapatkan melalui membandingkan grade SiO₂ dan CaO pasir monasit hasil smelting.

$$Basisitas = \frac{CaO}{SiO_2}$$

Berikut data *grade* CaO dan SiO₂ pada masing-masing variasi kuat arus listrik untuk menghitung basisitas pasir monasit hasil *smelting*.



No	Variasi Kuat Arus Listrik (A)	CaO (%)	SiO2 (%)
1	50	4,66	9,05
2	60	6,2	8,15
3	70	6,89	8,8
4	80	7,27	9,9
5	90	6,64	8,25

• Variasi 50 A

		$Basisitas, 50 A = \frac{4,66}{9,05}$
•	Variasi 60 A	Basisitas, 50 A = 0,51
		Basisitas, 60 A = $\frac{6,2}{8,15}$
_	Variaci 70 A	Basisitas, 60 A = 0,76
•	Vallasi 70 A	Basisitas, 70 $A = \frac{6,89}{88}$
•	Variasi 80 A	Basisitas, 70 A = 0,78
•	Vallasi ou A	<i>Basisitas</i> , 80 $A = \frac{7,27}{9,9}$
•	Variasi 90 A	Basisitas, 80 A = 0,73
		$Basisitas, 90 A = \frac{6,64}{8,25}$ $Basisitas, 90 A = 0,8$



LAPORAN TUGAS AKHIR DEPARTEMEN TEKNIK MATERIAL FI-ITS

6. Hasil	Peng Pasir	gujia Mor	an <i>X-Ra</i> j nasit	y Fluor	esence	e (XRF))						
Sample I	EL-1	63	(Pasir	Monas	it S	melti	ng O%	- No	on M	agne	tik 2) Ok	sida
ident		1.1.1			+ + + + + + + + + + + + + + + + + + + +	11111		1111	141				11114
Uispiay	aii 50 🕨	H			Seq.: Time:	1/1 28-okt-2	Pc 021 13	IS: 3 33:46					
Compound	Conc	Unit											
Si02	4.1	%											
P205	1	%											
CaO	6.89	%											
TiO2	43,2	%											
V205	0.41	%											
MnO	1,48	%											
Fe203	15,8	%											
NiO	0,02	%											
Y203	1,70	%											
Zr02	16,1	%											
Nb205	0,44	%											
Sn02	7,66	%											
HfO2	0,42	%											
W03	0,18	%											
ThO2	0,37	%											
U308	0,09	%											
Sample [EL-1	63	(Pasir	Monas	sit S	Smelti	ng Oʻ	k – N	on M	lagne	tik 2	2) 01	csida 2
_ ident E					+ 1 1		1+11		1141				
	a⊪ 61 ▶	H	e E		Seq.: Time:	1/1 28-okt-2	Pi 2021 13	os: 3 t.36:25					
Compound	Conc	Unit											
Si02	4.2	1%	1										
P205	1	%											
CaO	6,92	%											
TiO2	43,1	%											
V205	0,42	%											
MnO	1,47	%											
Fe203	15,7	%											
NiO	0.02	%											
Y203	1,69	%											
Zr02	16,0	%											
Nb205	0,45	%											
SnD2	7,81	%											
HfO2	0,44	%											
W03	0,20	%											
Th02	0,36	%											
U308	0.08	%											



b)	Varias	si 50) A
Sample	EL-2:	19	(Smelting Pasir Monasit Kode 50 Ampere) Oksida
ident			···*··································
Display	all	E	(%) (m) (m) (Seq.: 1/1 Pos: 1
I I I 131	08		😂 🗉 🔛 📟 Time: 23-mei-2022 14:34:31
Compound	d Conc	Unit	
Al203	0,5	%	
Si02	8,8	%	
P205	0,9	%	
<u>S03</u>	10,9	%	
CaO	4,64	%	
102	23,0	%	
V205	0,28	%	
MnU	12.7	76 */	
Fe203	17.5	76 97	
A=20.2	6.22	10 9/	
X203	1 11	*	
7:02	10.1	2	
Nb205	0.27	2	
Sn02	2.0	%	
Th02	0.27	%	
Sample D	1		- (Gwolting Desig Weyesit Vede 50 Juneye) Oksida 2
Sample I	EL-21	9,((Smelting Pasir Monasit Kode 50 Ampere) Oksida 2
Sample] ident _	EL-21 all	9 ((Smelting Pasir Monasit Kode 50 Ampere) Oksida 2
Sample I ident Display	EL-21 all	우.(이 ((Smelting Pasir Monasit Kode 50 Ampere) Oksida 2 Seq.: 1/1 Pos: 1 Time: 23-mei-2022 14:40:49
Sample ident	all D9	9 (이 ((Smelting Pasir Monasit Kode 50 Ampere) Oksida 2 Seq: 1/1 Pos: 1 Time: 23-mei-2022 14:40:49
Sample 1 ident Display I 1310 Compound Al203	EL-21 all D9 ▶ ♪ Conc 0,5	9 (1 6 Unit	(Smelting Pasir Monasit Kode 50 Ampere) Oksida 2 Seq: 1/1 Pos: 1 Time: 23-mei-2022 14:40:49
Sample 1 ident Display I 1310 Compound Al203 Si02	all 09 • • Conc 0,5 9,3	9 (1 d	(Smelting Pasir Monasit Kode 50 Ampere) Oksida 2 Seq: 1/1 Pos: 1 Time: 23-mei-2022 14:40:49
Sample 1 ident Display I 1310 Compound Al203 Si02 P205	EL-21 all 09 ▶ ▶ 0,5 9,3 1	9 (Unit	(Smelting Pasir Monasit Kode 50 Ampere) Oksida 2
Sample 1 ident Display I ◀ 1310 Compound Al2O3 SiO2 P2O5 SO3	all 09 ▶ 1 Conc 0.5 9,3 1 10,9	9 (Unit % %	(Smelting Pasir Monasit Kode 50 Ampere) Oksida 2 Seq: 1/1 Pos: 1 Time: 23-mei-2022 14:40:49
Sample 1 ident 1 Display I ■ 1310 Compound Al203 Si02 P205 S03 Ca0	EL-21 all 09 ▶ 1 0.5 9,3 1 10,9 4,67	9 (Unit % % %	(Smelting Pasir Monasit Kode 50 Ampere) Oksida 2 Seq: 1/1 Pos: 1 Time: 23-mei-2022 14:40:49
Sample 1 ident Display I ■ 1311 Compound Al2O3 SiO2 P2O5 SO3 CaO TiO2	EL-21 all 09 ▶ 1 0.5 9.3 1 10,9 4,67 22,9	9 (Unit % % %	(Smelting Pasir Monasit Kode 50 Ampere) Oksida 2
Sample 1 ident Display I ◀ 1310 Compound Al203 Si02 P205 S03 Ca0 Ti02 V205	EL-21 all 09 ▶ ■ Conc 0.5 9.3 1 10,9 4,67 22,9 0,28	9 (Unit 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	(Smelting Pasir Monasit Kode 50 Ampere) Oksida 2 Seq: 1/1 Pos: 1 Time: 23-mei-2022 14:40:49
Sample 1 ident 1 Display I ■ 1310 Compound Al203 Si02 P205 S03 Ca0 Ti02 V205 Mn0	EL-21 all 03 ▶ ↓ 0,5 9,3 1 10,9 4,67 22,9 0,28 0,776	9 (Unit 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	(Smelting Pasir Monasit Kode 50 Ampere) Oksida 2 Seq: 1/1 Pos: 1 Time: 23-mei-2022 14:40:49
Sample 1 ident Display I ■ 1311 Compound Al203 Si02 P205 S03 Ca0 Ti02 V205 Mn0 Fe203	EL-21 all 09 ▶ 1 Conc 0.5 9.3 1 10.9 4,67 22,9 0,28 0,776 12,6	9 (Unit 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	(Smelting Pasir Monasit Kode 50 Ampere) Oksida 2
Sample 1 ident 1 Display I ■ 1310 Compound Al203 Si02 P205 S03 Ca0 Ti02 V205 Mn0 Fe203 Cu0	EL-21 all 09 ▶ 1 Conc 0.5 9.3 1 10,9 4,67 22,9 0,28 0,776 12,6 17,3 0,27	9 (Unit 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	(Smelting Pasir Monasit Kode 50 Ampere) Oksida 2 Seq: 1/1 Pos: 1 Time: 23-mei-2022 14:40:49
Sample 1 ident 1 Display ■ 1310 Compound Al203 Si02 P205 S03 Ca0 Ti02 V205 Mn0 Fe203 Cu0 As203 V202	EL-21 all 03 ▶ 1 Conc 0.5 9.3 1 10,9 4,67 22,9 0,28 0,776 12,6 17,3 6,17 1.10	9 (Unit 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	(Smelting Pasir Monasit Kode 50 Ampere) Oksida 2
Sample 1 ident Display I ■ 1311 Compound Al203 Si02 P205 S03 Ca0 Ti02 V205 Mn0 Fe203 Cu0 As203 Y203	all 09 ▶ 1 Conc 0.5 9,3 1 10,9 4,67 22,9 0,28 0,776 12,6 17,3 6,17 1,10 9,05	9 (Unit 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	(Smelting Pasir Monasit Kode 50 Ampere) Oksida 2
Sample 1 ident 1 Display I ■ 1310 Compound Al203 Si02 P205 S03 Ca0 Ti02 V205 Mn0 Fe203 Cu0 As203 Y203 Zr02 Nb205	all Conc 0.5 9.3 1 10.9 4,67 22,9 0,28 0,776 12,6 17,3 6,17 1,10 9,95 0,28	9 (Unit 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	(Smelting Pasir Monasit Kode 50 Ampere) Oksida 2
Sample 1 ident 1 Display I ■ 1310 Compound Al203 Si02 P205 S03 Ca0 Ti02 V205 Mn0 Fe203 Cu0 As203 Y203 Zr02 Nb205 Sc02	EL-21 all 03 ▶ 1 0,5 9,3 1 10,9 4,67 22,9 0,28 0,776 12,6 17,3 6,17 1,10 9,95 0,28 1,28 1,20 1	9 (Unit 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	(Smelting Pasir Monasit Kode 50 Ampere) Oksida 2
Sample 1 ident Display I ■ 1311 Compound Al203 Si02 P205 S03 Ca0 Ti02 V205 Mn0 Fe203 Cu0 As203 Y203 Zr02 Nb205 Sn02 Tb02	all Conc 0.5 9,3 1 10,9 4,67 22,9 0,28 0,776 12,6 17,3 6,17 1,10 9,95 0,28 1,9 0,29 0,29	9 (Unit 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	(Smelting Pasir Monasit Kode 50 Ampere) Oksida 2



V205

MnO Fe2O3

CuO

Y203

Zr02

Nb205

Sn02 W03

ThO2

0,42 % 1,43 %

17,3 %

5,29 %

1,63 %

13,0 %

0,44 % 4,5 %

0,22 %

0,36 %

As203 1,77 %

LAPORAN TUGAS AKHIR DEPARTEMEN TEKNIK MATERIAL FI-ITS

c)	Varia	si 6) A								
Sample	EL-2	39	(Smelting	Pasir	Monasit	Kode	60A	nm)	Oksida		
ident	<u> </u>										
I Displa	ayall	and I	alm 🗖	Seq.:	1/1	Pos: 2	2				
	145			Time:	30-mei-2022	2 12:25:3	0				
Compour	nd Conc	Unit									
Si02	8,2	%									
P205	1	%									
S03	2,9	%									
CaO	6,17	%									
Ti02	35,3	%									
V205	0,42	%									
MnO	1,43	%									
Fe203	17,3	%									
CuO	5,27	%									
As203	1,77	%									
Y203	1,64	%									
Zr02	12,8	%									
Nb205	0,43	%									
Sn02	4,5	%									
W03	0,20	%									
ThO2	0,38	%									
-											
Sample	EL-2	39	(Smelting	Pasir	Monasit	Kode	60A	nmì	Oksida	2	
ident			********								
🗌 Displa	y all			Seq.:	1/1	Pos:	2				
▲ 13	146 🕨	M		😐 Time:	30-mei-2022	2 12:28:2	2				
Compour	nd Conc	Unit									
Si02	8,1	%									
P205	0,8	%									
S03	3,0	%									
CaO	6,22	%									
TiO2	35.5	%									



d)) Var	iasi 7	'0 A		
	Sample	EL-	208	Pasir Monasit Hasi.	1 Smelting Kode 70A, 287S) Oksida
	ident	<u></u>			
	Displ	ay all		simulation Seq. 1.	/1 Pos: 3
		3100		🔊 💷 🔛 📟 Time: 17-m	ei-2022 16:00:50
	Compou	nd Con	ic Un		
	Al203	1	2		
	Si02	8,7	7 %		
	CaO	6,8	9 %		
	TiO2	44,	0 %		
	V205	0,4	8 %		
	MnO	1,5	8 %		
	Fe203	3 11,	0 %		
	NiO	0,0	2 %		
	CuO	0,43	33 %		
	As203	3 0,09	36 %		
	Y203	1,8	9 %		
	Zr02	18,	9 %		
	Nb205	5 0,5	4 %		
	Sn02	3,9	3 %		
	W03	0,07	73 %		
	0s04	0,0	7 %		
	P60	0,0	1 %		
	Th02	0,4	5 %		
	Sample F	EL-20	8 (sir Monasit Hasil	Smelting Kode 70A, 2875) Oksida2
	ident E		i.,	·····	**************************************
Г	Display	all		Seq.: 1/1	Pos: 3
1	1310	01	H C	🗉 🔛 📟 Time: 17-mei-	2022 16:03:34
0	Compound	Conc	Unit		
	Al203	1	%		
	SiO2	8,9	%		
	CaO	6,89	%		
	TiO2	43,9	%		
	V205	0,45	%		
	MnO	1,59	%		
	Fe203	10,9	%		
	NiO	0,03	%		
	CuO	0,444	%		
	As203	0,091	%		
	Y203	1,89	%		
	Zr02	18,8	%		
	Nb205	0,54	%		
	Sn02	3,8	%		
	W03	0,083	%		
	0s04	0,07	%		
	Pb0	0,02	%		
	ThO2	0,43	%		



e) Variasi 80 A

A											
Sample I	EL-20	8	(Pasir Monasit Hasil Smelting Kode 80A) Oksida								
ident 占											
Display all Seq.: 1/1 Pos: 2											
K < 13096 ► F 😂 🖽 🔤 Time: 17-mei-2022 15:48:16											
Compound	Conc	Unit									
Al203	1,0	%									
Si02	10	%									
S03	1,2	%									
CaO	7,24	%									
TiO2	41,8	%									
V205	0,48	%									
MnO	1,53	%									
Fe203	11,1	%									
NiO	0,02	%									
CuO	1,43	%									
As203	0,35	%									
Y203	1,99	%									
Zr02	18,2	%									
Nb205	0,52	%									
Sn02	2,3	%									
W03	0.080	%									
0s04	0.04	%									
РЬО	0.01	%									
Th02	0,45	%									

Sample I	EL-20	8	(Pasir Monasit Hasil Smelting Kode 80A) Oksida 2						
Display all Seq.: 1/1 Pos: 2									
K ◀ 13097 ▶ ▶ 🖨 🖽 🔤 Time: 17-mei-2022 15:50:52									
Compound	Conc	Unit							
Al203	1	%							
Si02	9,8	%							
S03	1,2	%							
CaO	7,29	%							
TiO2	42,0	%							
V205	0,50	%							
MnO	1,54	%							
Fe203	11,1	%							
NiO	0,02	%							
CuO	1,43	%							
As203	0,36	%							
Y203	1,99	%							
Zr02	18,2	%							
Nb205	0,52	%							
SnO2	2,4	%							
W03	0,076	%							
0s04	0,02	%							
PbO	0,02	%							
ThO2	0,45	%							



f)	Varia	nsi 9(0 A
Sample	EL-2	39	(Smelting Pasir Monasit Kode 90A nm) Oksida
ident		1	···•··································
Displ	ay all		Calma Seq.: 1/1 Pos: 3
	3149 🕨		😂 🗉 🕍 📟 Time: 30-mei-2022 12:52:21
Compou	nd Conc	Unit	
Si02	8,0] %	
CaO	6,66	%	
TiO2	42,8	%	
V205	0,44	%	
MnO	1,61	%	
Fe203	3 16,1	%	
CuO	0,11	%	
As203	3 0,02	%	
Y203	1,90	%	
Zr02	16,5	%	
Nb205	5 0,53	%	
Sn02	4,4	%	
Hf02	0,35	%	
W03	0,11	%	
РЬО	0,01	%	
Th02	0,44	%	
Sample	EL-2	39	(Smelting Pasir Monasit Kode 90A nm) Oksida 2
iden			····*·································
	ay all	(sul	A PP Seq.: 1/1 Pos: 3
	3150		Time: 30-mei-2022 12:55:08
Compou	ind Con	c Uni	it
SiO2	8,5	%	
CaO	6,61	1 %	
Ti02	42,6	5 %	
V205	5 0,50] %	
MnO	1,60] %	
Fe20	3 16,0	JX	
CuO L CuO	0,11	1 76	
As20	3 0,01		
7203	1,8	1 %	
Zr02	16,4	1 76	
Nb20	5 0,5	0 %	
5002	4,3	76	
HIU2	0,3	7 %	
W03	0,09	1 %	
PBU	0,03	3 %	
1602	0,42	2 76	



7. Hasil Pengujian X-Ray Diffraction (XRD)a) Pasir Monasit



b) Variasi 50 A













8. Database *Reference* ICDD-JCPDS

a) Fe₂O₃

Date: 6/14/2022 Time: 1:53:09 F	PM File: Sampel Pasir Monasit	User: LENOVO
Name and formula		
Reference code:	01-073-0603	
Mineral name:	Hematite, syn	
Compound name:	Iron Oxide	
Common name:	Iron(III) oxide - alpha	
ICSD name:	Iron Oxide	
Empirical formula:	Fe ₂ O ₃	
Chemical formula:	Fe ₂ O ₃	
Crystallographic paran	<u>ieters</u>	
Crystal system:	Rhombohedral	
Space group:	R-3c	
Space group number:	167	
a (Å):	5.0342	
b (Å):	5.0342	
c (Å):	13.7483	
Alpha (°):	90.0000	
Beta (°);	90.0000	
Gamma (°):	120.0000	
Calculated density (g/cm^3):	5.27	
Volume of cell (10^6 pm^3):	301.75	
Z:	6.00	
RIR:	0.06	
Subfiles and Quality		
Subfiles:	Alloy, metal or intermetalic	
	Corrosion	
	ICSD Pattern	
	Inorganic	
	Mineral	
	Pharmaceutical	
Quality:	Calculated (C)	
<u>Comments</u>		
IC5D collection code:	022505	
Creation Date:	1/1/1970	
Modification Date:	1/1/1970	
	ADDE05	
ICSD Collection Code:	022505	
ICSD Collection Code: Temperature Factor:	022505 ATF. The Electron Density Distribution in Hematite, Fe2 O3 al	pha, from Precision X-Ray

References

Primary reference:	Calculated from ICSD using POWD-12++, (1997)
Structure:	Antipin, M.Y., Tzirelson, V.G., Flugge, M.P., Gerr, R.G., Struchkov, Y.T., Ozerov, R.P.,
	10[2

Date: 6/14/2022 Time: 1:53:09 PM	File: Sampel Pasir Monasit	User: LENOVO
1	lokl. Akad. Nauk SSSR, 281, 854, (1985)	

Peak list

No.	h	1c	1	d [A]	2Theta[deg] I [%]
1	0	1	2	3.68171	24,154	2.6
z	1	0	4	2,69915	33.164	0.1
3	1	1	0	2.51710	35.640	100.0
4	1	1	3	2.20622	40.871	0.1
5	z	0	2	2.07790	43.519	0.1
6	0	2	4	1.84086	49.473	0.1
7	2	1	1	1.63612	56,174	0.1
8	1	2	2	1.60243	57.463	0.1
9	0	1	8	1.59881	57,606	0.1
10	з	0	D	1,45325	64.018	0.1
11	2	0	8	1.34958	69.608	0.1
12	1	0	10	1.31118	71,958	0.1
13	1	1	9	1.30591	72.294	0.1
14	2	2	0	1.25855	75.476	0.1
15	z	z	з	1.21362	78.797	0.1
16	1	3	1	1.20453	79.509	0.1
17	з	1	2	1,19089	80.606	0.1
18	1	3	4	1.14065	84.957	0.1
19	3	1	5	1.10688	88,201	0.1



b) Fe₃O₄

Date: 6/14/2022 Time: 1:55:31 PM File: Sampel Pasir Monasit

User: LENOVO

Name and formula

Reference code:	96-900-0140
Mineral name: Compound name: Common name:	Hematite Hematite Hematite
Chemical formula:	Fe _{12.00} O _{18.00}

Crystallographic parameters

Crystal system:	Hexagonal
Space group:	R-3 c
Space group number:	167
a (Â):	5.0380
b (Â):	5.0380
c (Å):	13.7720
Alpha (°):	90.0000
Beta (°):	90.0000
Gamma (º):	120.0000
Calculated density (g/cm^3):	5.26
Volume of cell (10^6 pm^3):	302.72
RIR:	3.32

Subfiles and Quality

Subfiles:

Quality:

User Inorganic User Mineral None ()

Comments

 Creation Date:
 10/

 Modification Date:
 10/

 Publication title:
 Ref

 COD database code: 9000139

10/25/2014 6:49:36 PM 10/25/2014 6:49:36 PM Refinement of the hematite structure

References

Structure:

Blake, R. L., Hessevick, R. E., Zoltai, T., Finger, L. W., American Nineralogist, 51, 123 - 129, (1966)

No.	h	k	1	d [A]	2Theta[deg]	I [%]
1	0	1	2	3.68552	24.128	29.0
2	1	0	4	2.70280	33.118	100.0
3	1	1	0	2,51900	35.612	71.3
4	0	0	6	2.29533	39.217	2.0
5	1	1	3	2.20838	40.829	20.0
6	2	0	2	2.07965	43.480	1.9

							1 Of 2
Date: 6	/14/2022	Tim	e: 1:55:3	1 PM	File: Sampel Pasir Monasit		User: LENOVC
7	0	2	4	1.84276	49.419	37.7	
8	1	1	6	1.69662	54,004	46.1	
9	z	1	1	1.63738	56.127	0.6	
10	1	2	2	1.60373	57.412	2.2	
11	0	1	в	1.60136	57.505	B.7	
12	2	1	4	1.48728	62.386	29.8	
13	0	3	0	1,45435	63.964	14.4	
14	1	2	5	1.41488	65.971	0.2	
15	2	0	8	1.35140	69.501	3.1	
16	1	0	10	1.31333	71.822	11.4	
17	1	1	9	1.30782	72.171	2.0	
18	2	1	7	1.26383	75.106	0.2	
19	z	z	D	1.25950	75.409	6.4	
20	0	3	6	1.22851	77.662	1.2	
21	2	2	3	1.21461	78,720	1.1	
22	1	3	1	1.20544	79.437	0.1	
23	3	1	2	1.19183	80.529	1.5	
24	1	z	в	1,19085	80.609	4.2	
25	0	2	10	1.16455	82.822	5.6	
26	0	0	12	1,14767	84.318	0.2	
27	1	3	4	1.14163	84.867	8.0	
28	3	1	5	1,10789	88,100	0.0	
29	z	Z	6	1,10419	88,472	7.7	



c) FeO

Date: 6/14/2022 Time: 1:54:41 F	PM File: Sampel Pasir Monasit User: LEN	NOVO
Name and formula		
Reference code:	01-079-1969	
Mineral name:	Wuestite, syn	
Compound name:	Iron Oxide	
ICSD name:	Iron Oxide	
Empirical formula:	Fe _{0.92} D	
Chemical formula:	Fe _{.920} 0	
Crystallographic param	<u>ieters</u>	
Crystal system:	Cubic	
Space group:	Fm-3m	
Space group number:	225	
a (Å):	4.3611	
b (Â):	4.3611	
c (Å):	4.3611	
Alpha (°):	90.0000	
Beta (°):	90.0000	
Gamma (°):	90.0000	
Calculated density (g/cm^3):	5.39	
Volume of cell (10^6 pm^3):	82.94	
Z;	4.00	
RIR:	3.73	
Status, subfiles and gu	ality	
Chalter	Diffraction data collected at non-ambiant temperature	
Subfiles:	Alloy, metal or intermetalic	
Sabries.	Corrosion	
	ICSD Pattern	
	Inorganic	
	Mineral	
Quality:	Calculated (C)	
Comments		
ICSD collection code:	067199	
Creation Date:	1/1/1970	
Modification Date:	1/1/1970	
ICSD Collection Code:	067199. Rietveld profile refinement applied	
Temperature of Data Collection:	REM TEM 1050 C. Published data has been corrected through correspondence wit author	h the
Temperature Factor:	ITF See DDE 01-070-1050, Daint defect diviters in Williamthe In a (DM2-M), AV	
Auditional Fatterns:	see For ot ovartada, Foint delect clusters in woestite, b a (FM3-M), AX,	

<u>References</u>

Primary reference:	Calculated from ICSD using POWD-12++, (1997)	
		1 Of 2
Date: 6/14/2022 Time: 1:54:41 PM	File: Sampel Pasir Monasit	User: LENOVO

Date: 0/14/2022 11/16: 1.04.41114	r File, Gamper Fasir Monasit	USEL LENOV
Structure:	Radler, M.J., Cohen, J.B., Faber, J., J. Phys. Chem. Solids, 51, 217, (1990))

No.	h	k	1	d [A]	2Theta[deg]	I [%]
1	1	1	1	2.51788	35.628	64.8
2	2	0	0	2.18055	41.374	100.0
3	2	2	0	1.54188	59,945	36.7
4	з	1	1	1.31492	71.721	10.4
5	2	2	2	1.25894	75.449	7.2
6	4	0	0	1.09028	89.904	2.1



SnO₂ d)

Name and formula Reference code: 01-077-0449 Mineral name: Cassiterite, syn Compound name: Tin Oxide Common name: Tin Oxide Common name: Tin Oxide Empirical formula: O_2Sn Chemical formula: O_2Sn Crystallographic parameters Crystal system: Tetragonal Space group: F42/mnm Space group number: 136 a (Å): 4.7421 c (Å): 4.7421 c (Å): 4.7421 c (Å): 3.1901 Alpha (°): 90.0000 Gamma (°): 90.0000 Calculated density (g/cm^3): 6.97 Volume of cell (10^6 pm^3): 71.74 Z: 2.00 RIR: 9.74 Status: Diffraction data collected a Subfiles: Diffraction data collected a	
Reference code: 01-077-0449 Mineral name: Cassilerite, syn Compound name: Tin Oxide Common name: Tin Oxide CSD name: Tin Oxide Empirical formula: 0_2 Sn Chemical formula: 0_2 Sn Crystallographic parameters Crystal system: Tetragonal Space group: P42/mnm Space group: 136 a (Å): 4.7421 b (Å): 4.7421 c (Å): 3.1901 Alpha (°): 90.0000 Gamma (°): 90.0000 Calculated density (g/cm^3): 6.97 Volume of cell (10^6 pm^3): 71.74 Z: 2.00 RIR: 9.74 Status: Diffraction data collected a Subfiles: Diffraction data collected a	
Mineral name: Cassiterite, syn Compound name: Tin Oxide Common name: Tin Oxide ICSD name: Tin Oxide Empirical formula: O_2Sn Chemical formula: SnO_2 Crystal system: Tetragonal Space group: F42/mnm Space group: F42/mnm Space group number: 136 a (Å): 4.7421 c (Å): 4.7421 c (Å): 3.1901 Alpha (°): 90.0000 Gamma (°): 90.0000 Calculated density (g/cm^3): 6.97 Volume of cell (10^6 pm^3): 71.74 Z: 2.00 RIR: 9.74 Status: Subfiles: Diffraction data collected a Subfiles: Diffraction data collected a	
Compound name: Tin Oxide Common name: Tin(IV) oxide - at 615 K CSD name: Tin(Oxide Empirical formula: O_2Sn Chemical formula: SnO_2 Crystallographic parameters Crystal system: Tetragonal Space group: P42/mnm Space group number: 136 a (Å): 4.7421 c (Å): 4.7421 c (Å): 4.7421 c (Å): 4.7421 c (Å): 3.1901 Alpha (°): 90.0000 Gamma (°): 90.0000 Calculated density (g/cm^3): 6.97 Volume of cell (10^6 pm^3): 71.74 Z: 2.00 RiR: 9.74 Status: Diffraction data collected a Subfiles: Diffraction data collected a	
Common name: Tin(IV) oxide - at 615 K ICSD name: Tin Oxide Empirical formula: O ₂ Sn chemical formula: SnO ₂ Crystal lographic parameters Crystal system: Tetragonal Space group: P42/mnm Space group number: 136 a (Å): 4.7421 b (Å): 4.7421 c (Å): 4.7421 c (Å): 90.0000 Beta (°): 90.0000 Gamma (°): 90.0000 Calculated density (g/cm^3): 6.97 Volume of cell (10^6 pm^3): 71.74 Z: 2.00 RIR: 9.74 Status, subfiles and quality Status: Diffraction data collected a Subfiles: Alloy, metal or intermetalia Corrosion	
ICSD name: Tin Oxide Empirical formula: O ₂ Sn Chemical formula: SnO ₂ Crystallographic parameters SnO ₂ Crystallographic parameters Space group: F42/mnm Space group: F42/mnm Space group: a (Å): 4.7421 c (Å): b (Å): 4.7421 c (Å): c (Å): 3.1901 Alpha (°): Beta (°): 90.0000 Beta (°): 90.0000 Gamma (°): 90.0000 Calculated density (g/cm^3): 6.97 Volume of cell (10^6 pm^3): 71.74 Z: 2.00 RIR: 9.74 Status, subfiles and quality Status: Diffraction data collected a Subfiles:	
Empirical formula: O25n Chemical formula: SnO2 Crystal lographic parameters Crystal system: Tetragonal Space group: F42/mm Space group: F42/mm Space group: F42/mm Space group: Space group: F42/mm F42/mm Alpha (%): Space group: Space group: F42/mm Gamma (*): Space group: Space group: F42/mm Colculated density (g/cm^3): 6.97 F42/mm F42/mm Status: Space group: Space group: F42/mm F42/mm Subfiles: Space group:	
Chemical formula: SnO2 Crystal lographic parameters Crystal system: Tetragonal Space group: F42/mm Space group number: 136 a (Å): 4.7421 c (Å): 4.7421 c (Å): 4.7421 c (Å): 3.1901 Alpha (°): 90.0000 Gamma (°): 90.0000 Calculated density (g/cm^3): 6.97 Volume of cell (10^6 pm^3): 71.74 Z: 2.00 RiR: 9.74 Status: Diffraction data collected a Subfiles: Diffraction data collected a	
Crystallographic parameters Crystal system: Tetragonal Space group: F42/mm Space group: 136 a (Å): 4.7421 b (Å): 4.7421 c (Å): 3.1901 Alpha (°): 90.0000 Beta (°): 90.0000 Gauma (°): 90.0000 Calculated density (g/cm^3): 6.97 Volume of cell (10^6 pm^3): 71.74 Z: 2.00 RIR: 9.74 Status, subfiles and quality Status: Diffraction data collected a Subfiles: Diffraction idata collected a	
Crystal system: Tetragonal Space group: P42/mnm Space group number: 136 a (Å): 4.7421 b (Å): 4.7421 c (Å): 3.1901 Alpha (°): 90.0000 Gamma (°): 90.0000 Calculated density (g/cm^3): 6.97 Volume of cell (10^6 pm^3): 71.74 Z: 2.00 RIR: 9.74 Status: Diffraction data collected a Subfiles: Diffraction data collected a	
Space group: P42/mm Space group number: 136 a (Å): 4.7421 b (Å): 4.7421 c (Å): 3.1901 Alpha (°): 90.0000 Gamma (°): 90.0000 Calculated density (g/cm^3): 6.97 Volume of cell (10^6 pm^3): 71.74 Z: 2.00 RIR: 9.74 Status, subfiles and quality Status: Diffraction data collected a Subfiles: Alloy, metal or intermetatic Corresion	
Space group number: 136 a (Å): 4.7421 b (Å): 4.7421 c (Å): 3.1901 Alpha (°): 90.0000 Beta (°): 90.0000 Gamma (°): 90.0000 Calculated density (g/cm^3): 6.97 Volume of cell (10^6 pm^3): 71.74 Z: 2.00 RIR: 9.74 Status: Diffraction data collected a Subfiles: Diffraction intermetatic Corrosion	
a (Å): 4.7421 b (Å): 4.7421 c (Å): 3.1901 Alpha (°): 90.0000 Beta (°): 90.0000 Gamma (°): 90.0000 Calculated density (g/cm^3): 6.97 Volume of cell (10^6 pm^3): 71.74 Z: 2.00 RIR: 9.74 Status, subfiles and quality Status: Diffraction data collected a Subfiles: Alloy, metal or intermetatio Corrosion	
b (Å): 4.7421 c (Å): 3.1901 Alpha (°): 50.0000 Beta (°): 90.0000 Gamma (°): 90.0000 Calculated density (g/cm^3): 6.97 Volume of cell (10^6 pm^3): 71.74 Z: 2.00 RIR: 9.74 Status: Diffraction data collected a Subfiles: Alloy, metal or intermetation Corrorsion	
c (Å): 3.1901 Alpha (°): 90.0000 Beta (°): 90.0000 Gamma (°): 90.0000 Calculated density (g/cm^3): 6.97 Volume of cell (10^6 pm^3): 71.74 Z: 2.00 RIR: 9.74 Status, subfiles and quality Status: Diffraction data collected a Subfiles: Diffraction data collected a	
Alpha (°): \$0.0000 Beta (°): \$0.0000 Gamma (°): \$0.0000 Calculated density (g/cm^3): 6.97 Volume of cell (10^6 pm^3): 71.74 Z: 2.00 RIR: 9.74 Status, subfiles and quality Status: Diffraction data collected a Subfiles: Alloy, metal or intermetation Corrosion	
Beta (*): 90.0000 Gamma (*): 90.0000 Calculated density (g/cm^3): 6.97 Volume of cell (10^6 pm^3): 71.74 Z: 2.00 RIR: 9.74 Status: Diffraction data collected a Subfiles: Diffraction data collected a	
Gamma (*): 90.0000 Calculated density (g/cm^3): 6.97 Volume of cell (10^6 pm^3): 71.74 Z: 2.00 RIR: 9.74 Status, subfiles and quality Status: Diffraction data collected a Subfiles: Alloy, metal or intermetatio Corrosion	
Calculated density (g/cm^3): 6.97 Volume of cell (10^6 pm^3): 71.74 Z: 2.00 RIR: 9.74 Status, subfiles and quality Status: Diffraction data collected a Subfiles: Alloy, metal or intermetation Corrosion	
Volume of cell (10 ⁻⁶ pm ⁻³): 71.74 Z: 2.00 RIR: 9.74 Status, subfiles and quality Status: Diffraction data collected a Subfiles: Alloy, metal or intermetation Corrosion	
Z: 2.00 RIR: 9.74 Status, subfiles and quality Status: Diffraction data collected a Subfiles: Alloy, metal or intermetation Corrosion	
RIR: 9.74 Status, subfiles and guality Status: Diffraction data collected a Subfiles: Alloy, metal or intermetatio Corrosion	
Status, subfiles and quality Status: Diffraction data collected a Subfiles: Alloy, metal or intermetation Corrosion Corrosion	
Status: Diffraction data collected a Subfiles: Alloy, metal or intermetalic Corrosion	
Subfiles: Alloy, metal or intermetalic Corrosion	t non ambient temperature
Corrosion	
ICSD Pattern	
Inorganic	
Mineral Overline Coloridated (C)	
Quality. Calculated (C)	
Comments	
ICSD collection code: 039175	
Creation Date: 1/1/1970	
Modification Date: 1/1/1970	
ICSD Collection Code: 039175	
Temperature Factor: ATF	
remperature of Data Collection: REM TEM 342 C	

039175
1/1/1970
1/1/1970
039175
ATE
REM TEM 342 C
See PDF 01-077-0452. High temperature structures of the rutile-type oxides, TLO2 and Sn O2. f a (P42/MIM). AX2.

References

		1 Of 3
Date: 6/14/2022 Time: 8:14:37 PI	A File: Sampel Pasir Monasit	User: LENOVO
Primary reference: Structure:	Calculated from ICSD using POWD-12++, (1997) Seki, H., Ishizawa, N., Mizutani, N., Kato, M., Yogyo Kyokarshi (J. 219, (1984)	Ceram. Assoc. Jpn.), 92,

No.	h	k	1	d [A]	2Theta[deg] I [%]
1	1	1	0	3.35317	26.562	100.0
2	1	0	1	2.64691	33.838	76.7
3	z	0	D	2.37105	37.916	20.9
4	1	1	1	2.31124	38,936	3.4
5	2	1	0	2.12073	42.597	1.2
6	2	1	1	1.76609	51.718	54.5
7	2	2	0	1.67659	54,703	12.5
8	0	0	2	1.59505	57.754	6.1
9	3	1	0	1,49958	61,818	11.2
10	z	2	1	1.48410	62.535	0.1
11	1	1	2	1.44039	64.659	11.4
12	3	0	1	1,41636	65.893	13.9
13	3	1	1	1.35712	69.166	0.2
14	2	0	2	1.32345	71,188	5.5
15	z	1	z	1.27474	74.354	0.2
16	3	2	1	1.21594	78.618	8.2
17	4	0	0	1.18552	81.047	2.6
18	2	2	2	1.15562	83.606	5.3
19	4	1	0	1,15013	84.096	0.2
20	з	3	0	1.11772	87.129	2.4
21	3	1	2	1.09256	89.666	6.3



e) TiO₂ Anatase

Date: 6/14/2022 Time: 8:15:54 P	M File: Sampel Pasir Monasit	User: LENC
Name and formula		
Reference code:	96-900-8217	
Mineral name:	Anatase	
Compound name:	Anatase	
Common name:	Anatase	
Chemical formula:	TI _{4.00} O _{8.00}	
Crystallographic param	eters	
Crystal system:	Tetragonal	
Space group:	I 41/a m d	
Space group number:	141	
a (Â):	3.8040	
b (Å):	3.8040	
c (Å):	9.6140	
Alpha (°):	90.0000	
Beta (°):	90.0000	
Gamma (º):	90.0000	
Calculated density (g/cm^3):	3.81	
Volume of cell (10^6 pm^3):	139.12	
RIR:	4.92	
Subfiles and Quality		
Subfiles:	User Inorganic	
	User Mineral	
Quality:	None ()	
<u>Comments</u>		
Creation Date:	10/25/2014 7:04:41 PM	
Modification Date:	10/25/2014 7:04:41 PM	
Structure TIDY:	TRANS Origin 0 3/4 5/8	
Structure TIDY: REMARK Transfo Publication title: Refinement of th	rmed from non-centrosymmetric setting. e structure of anatase at several temperatures. Sample: T = 8	00 C Locality: Legenbach
COD database code: 9008216	quarry, Binnatal, Switzerland	

Structure:

Horn, M., Schwerdtfeger, C. F., Meagher, E. P., Zeitschrift fur Kristallographie, 136, 273 - 281, (1972)

No.	h	k	1	d [A]	2Theta[deg]	I (%)
1	0	1	1	3.53718	25.156	100.0
2	0	1	3	2.45087	36.637	6.4
3	0	0	4	2.40350	37.385	19.4

1 Of 2							
User: LENOVO	l Pasir Monasit	File: Sampe	4 PM	e: 8:15:5	22 Time	5/14/202	Date: 6
	7.7	38.314	2.34733	2	1	1	4
	25.3	97.78Z	1.90200	D	2	0	5
	0.0	51,640	1.76859	2	2	0	6
	16.0	53.344	1.71603	5	1	0	7
	15.6	54.753	1.67518	1	2	1	8
	2.8	61.680	1,50261	3	2	1	9
	11.5	62.191	1.49149	4	2	0	10
	5.2	68.052	1.37659	6	1	1	11
	5.3	69.884	1.34492	D	z	z	12
	0.5	73.210	1.29181	7	1	0	13
	8.0	74.397	1.27411	5	2	1	14
	2.2	75.578	1.25711	1	з	0	15
	0.0	77.893	1.22544	6	2	0	16
	0.4	79.730	1.20175	8	0	0	17
	0.6	01.004	1.17906	3	3	0	10
	3.8	82.040	1.17367	4	2	2	19
	1.8	82.615	1,16695	z	3	1	20


User: LENOVO

f) TiO₂ Rutile

Date: 6/14/2022 Time: 1:53:29 PM	File: Sampel Pasir Monasit

Name and formula

Reference code:	00-034-0180
Mineral name:	Rutile, syn
Compound name:	Titanium Oxide
PDF index name:	Titanium Oxide
Empirical formula:	0 ₂ TI
Chemical formula:	TIO ₂

Crystallographic parameters

Crystal system:	Tetragonal
Space group:	F42/mnm
Space group number:	136
a (Å):	4.5930
b (Å):	4.5930
c (Å):	2.9590
Alpha (°):	90.0000
Beta (°):	90.0000
Gamma (°):	90.0000
Calculated density (g/cm^3);	4.25
Volume of cell (10^6 pm^3);	62.42
Z:	2.00
RIR:	9.96

Status, subfiles and quality

Status:	Marked as deleted by ICDD
Subfiles:	Alloy, metal or intermetalic
	Inorganic
	Mineral
	Pharmaceutical
Quality:	Calculated (C)

Comments

Creation Date: 1/1/1970 Modification Date: 1/1/1970 Cell parameters at 25 C. Deleted Or Rejected By: Deleted: something wrong, 22-1176 shows this pattern incorrect.

References

Primary	reference.	

Smith, Zolensky, Dept. Geol. Sciences, Penn State Univ., University Park, PA, USA., *ICDD Grant-In-Aid*, (1979) Meagher, E., Lager., *Can. Mineral.*, **17**, 77, (1979)

Unit cell: <u>Peak list</u>

1.0							
User: LENO	l Pasir Monasit	File: Sampe	9 PM	: 1:53:2	22 Time	5/14/20	Date: (
	1 1 181	Al 2Thetaideo	d (A)	1	k	h	No.
	100.0	4800 27.438	3.24800	0	1	1	1
	15.0	8700 36.086	2.48700	1	0	1	2
	27.0	9700 39,188	2.29700	0	0	2	3
	7.0	8740 54.323	1.68740	1	1	2	4
	6.0	2390 56.634	1.62390	0	2	2	5
	6.0	5240 64.060	1,45240	0	1	3	6
	1.0	5980 69.010	1.35980	1	0	з	7
	1.0	4640 69.796	1.34640	z	1	1	8
	1.0	7000 82.352	1.17000	1	2	3	9
	1.0	4820 84.269	1.14820	0	0	4	10
	1.0	8260 90.719	1.08260	0	3	3	11
	1.0	4250 95.275	1.04250	1	1	4	12
	1.0	2700 97.189	1.02700	D	2	-	13
	1.0	6430 106.035	0.96430	3	0	1	14
	1.0	0080 117.548	0.90080	0	1	5	15
	1.0	8910 120.082	0.88910	3	1	2	16



g) FeTiO₃

	32 PM File: Sampel Pasir Monasit	User: LE
Name and formula	·	
Reference code:	01-075-1210	
Mineral name:	Ilmenite, syn	
Compound name:	Iron Titanium Oxide	
Common name:	Iron titanate	
ICSD name:	Iron Titanium Oxide	
Empirical formula:	FeO ₃ TI	
Chemical formula:	FeTiO ₃	
Crystallographic par	ameters	
Crystal system:	Rhombohedral	
Crystal system: Space group:	Rhombohedral R-3	
Crystal system: Space group: Space group number:	Rhombohedral R-3 148	
Crystal system: Space group: Space group number: a (Å):	Rhombohedral R-3 148 5.0691	
Crystal system: Space group: Space group number: a (Å); b (Å);	Rhombohedral R-3 148 5.0691 5.0691	
Crystal system: Space group: Space group number: a (Å): b (Å): c (Å):	Rhombohedral R-3 148 5.0691 5.0691 13.8849	
Crystal system: Space group: Space group number: a (Å): b (Å): c (Å): Alpha (°):	Rhombohedral R-3 148 5.0691 5.0691 13.9849 90.0000	
Crystal system: Space group: Space group number: a (Å): b (Å): c (Å): Alpha (°): Bete (°):	Rhombohedral R-3 148 5.0691 5.0691 13.9849 90.0000 90.0000	
Crystal system: Space group: Space group number: $a(\hat{A}):$ $c(\hat{A}):$ $c(\hat{A}):$ $c(\hat{A}):$ Alpha (°): Beta (°): Gamma (°):	Rhombohedral R-3 148 5.0691 5.0691 13.9849 90.0000 90.0000 120.0000	
Crystal system: Space group: Space group number: a(A): b(A): c(A): c(A): Beta (°): Beta (°): Calculated density (a/cm^{3})	Rhombohedral R-3 148 5.0691 5.0691 13.9849 50.0000 90.0000 120.0000 : 4.86	
Crystal system: Space group: Space group number: a (Å): b (Å): c (Å): c (Å): Apha (°): Beta (°): Gamma (°): Calculated density (g/cm^3) Volume of cell (10°6 pm°3)	Rhombohedral R-3 148 5.0691 5.0691 13.5849 90.0000 90.0000 120.0000 : 4.86 : 311.21	
Crystal system: Space group: Space group number: a (Å): b (Å): c (Å): Alpha (°): Beta (°): Gamma (°): Calculated density (g/cm^3) Volume of cell (10 ⁻⁶ pm^1) Z:	Rhombohedral R-3 148 5.0691 5.0691 13.5849 90.0000 90.0000 120.0000 : 4.86 : 311.21 6.00	

Status, subfiles and quality

Status: Subfiles:	Diffraction data Corrosion ICSD Pattern Inorganic Mineral	a collected at non ambient pressure
Quality:	Calculated (C)	
<u>Comments</u>		
ICSD collection code:	030671	
Creation Date:	1/1/1970	
Modification Date:	1/1/1970	
ICSD Collection Code:	030671	
Calculated Pattern Original Reman	ks: REM	PRE 25.4 kbar
Temperature Factor:	ΠF	
Calculated Pattern Original Reman	ks: REM	TEM Mentioned
Additional Patterns:	See PDF 01-07	75-1212. Crystal structure of ilmenite (Fe TI O3) at high temperature and
	high pressure.	f c2 (R3-H). ABX3.

References

bits 1 1 2 27:32 PM File: Sampel Pasir Monasit U imary reference: Calculated from XCD using POWD-12++, (1997)	
imary reference: Calculated from RSD using POWD-12++, (1997) Wechsler, 8.A., Prewitt, C.T., Am. Mineral, 09, 176, (1984) eak list b. h k 1 d [A] 2Theta [deg] T [5] 1 0 0 3 4.66143 19.023 0.2 2 1 0 1 4.18846 21.195 0.3 3 0 1 2 3.71797 23.915 35.4 4 1 0 4 2.73487 32.718 100.0 5 1 1 0 2.55485 35.386 68.6 6 0 1 5 2.35889 38.115 0.1 7 0 0 6 2.33062 39.596 1.7 8 1 1 -3 2.23614 40.478 22.7 8 1 1 -3 2.23614 40.478 22.7 9 0 2 1 2.16644 41.78 22.7 9 0 2 1 2.16644 41.78 22.7	ier: LENOV
nucture: Wechsler, 8.A., Prewitt, C.T., Am. Mineral, 69, 176, (1984) eak list b. h l 0 3 4.66163 1 0 4 1 1 0 3 1.2 3.71797 23.81 5 1 1 0 2.53455 35.4 4 1 0 2.53455 35.86 6 1 5 1 1 0 2.53689 38.11 0 6 2.3062 305.556 1.7 8 1 1 -3 2.2671 40.478 22.7 9 2 2 2 2 2 3.11 -3 2.22671 40.478 22.7 2 2 2 2 2 2 2 3 4	
k 1 d [A] 2Thets[deg] I [%] 1 0 0 3 4.66163 15.023 0.2 2 1 0 1 4.66163 15.023 0.2 2 1 0 1 4.66163 15.023 0.2 3 0 1 2 3.71797 23.915 35.4 4 1 0 4 2.73487 32.718 100.0 5 1 1 0 2.53485 35.366 66.6 6 0 1 5.33062 36.556 1.7 8 1 1 -3 2.22671 40.478 22.7 9 0 2 1.2 2.09433 43.162 1.6 1 -3 2.22671 40.478 22.7 53.66 0 2 1 2.09433 43.162 1.6	
b. h k 1 d [A] 2Theta[deg] T [4] 1 0 0 3 4.66163 19.023 0.2 1 0 1 4.18846 21.195 0.3 3 0 1 2 3.71797 23.915 35.4 4 1 0 4 2.73487 32.718 100.0 5 1 1 0 2.53455 38.386 68.6 6 0 1 5 2.35889 38.119 0.1 7 0 0 6 2.33062 36.596 1.7 8 1 1 -3 2.22671 40.478 22.7 9 0 2 1 2.16644 41.615 1.2 0 2 0 2 1 2.16644 41.615 1.2 0 2 0 2 4 2.09433 43.162 1.6	
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9 0 2 1 2.16044 41.615 1.2 0 2 0 2 2.09423 43.162 1.6 1 0 2 1 1 0.000 40 000 1.0	
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1 0 2 1 1.00000 30.000 30.0	
12 1 0 7 1.81839 50.126 0.5	
3 2 0 5 1.72675 52.987 0.8	
14 1 1 -6 1.71565 53.357 43.7	
15 2 1 1 1.64770 55.744 0.7	
16 0 1 8 1.62408 56.627 7.2	
17 2 1 -2 1.61442 56.997 2.5	
8 0 0 9 1.55388 59.435 0.1	
9 1 2 -4 1.49901 61.844 25.1	
0 0 2 7 1.47748 62.847 0.2	
1 3 0 0 1.46332 63.526 24.9	
2 2 1 -5 1.42704 65.339 0.4	
3 0 3 3 1.39615 66.972 0.1	
4 2 0 5 1.36744 68.571 1.9	
5 1 0 10 1.33251 70.632 8.8	
1 1 -9 1.344/3 /1.109 1.9	
., <u> </u>	
10 a a 0 1.aurar 73.007 0.a	
30 2 2 -3 1 22286 78 086 1 0	
1 1 3 1 1 1 21297 78 848 0 1	
12 2 1 -8 1.20346 79.594 2.9	
3 3 1 2 1 10051 70 000 1.0	
15 0 0 12 1-16541 82.748 0.2	
16 3 1 -4 1.14983 84.123 6.0	
37 2 2 -6 1,11335 87,558 5,7	
88 2 0 11 1.10014 88.883 0.1	
19 4 0 1 1.09413 89.502 0.1	



Fe₂TiO₄ h)

Date: 6/14/2022 Time: 2/26/16/5	DM File: Carned Basis Massait	Lines LENOVO
Name and formula	-M File, Samper Fasir Monasit	USER. LENOVO
Name and formula		
Reference code:	01-084-1595	
Mineral name:	Maghemite, titanian	
Compound name:	Iron Titanium Oxide	
Common name:	Iron iron	
ICSD name:	Iron Titanium Oxide	
Empirical formula:	Fe2 1804Tl0.42	
Chemical formula:	Fe 23 (Fe1 05 Ti 42) 04	
	120 1130 1127 1	
Contallererebierere		
Crystallographic paran	neters	
Crystal system:	Cubic	
Space group:	P4332	
Space group number:	212	
a (Å):	8.3410	
b (Å):	8.3410	
c (Å):	8.3410	
Alpha (°):	90.0000	
Beta (°):	90.0000	
Gamma (°):	90.0000	
Calculated density (g/cm^3):	4.70	
Volume of cell (10^6 pm^3):	580.30	
Z:	B.00	
RIR:	4.14	
Subfiles and Quality		
SubBlace	Corracion	
outries.	ICSD Pattern	
	Inorganic	
	Mineral	
Quality:	Calculated (C)	

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Comments

ICSD collection code:	202597
Creation Date:	1/1/1970
Modification Date:	1/1/1970
ICSD Collection Code:	202597
Temperature Factor:	ATF
Sample Source or Locality:	Specimen from Petoria, South Africa. Studies of the crystal structure and crystal chemistry of titanomaghemite. e d c2 b (P4332). A21X32.

References

Primary reference:	Calculated from ICSD using POWD-12++, (1997)
Structure:	Collyer, S., Grimes, N.W., Vaughan, D.J., Longworth, G., Am. Mineral., 73 , 153, (1988)

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Jate: (6/14/20 c list	22 Tim	e: 3:25:1	16 PM	File: Samp	ei Pasir Monasit	User: LENO
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No.	h	k	1	d [A]	2Theta[de	2] I [8]	
1	1	1	D	5.89798	15.009	3.9	
2	1	1	1	4.81568	18.409	3.2	
3	2	1	0	3.73021	23.835	3.8	
4	2	1	1	3.40520	26.148	4.3	
5	2	2	0	2.94899	30.284	36.5	
6	2	2	1	2.78033	32.169	1.0	
1	-	1		2.63766	33.960	1.6	
8	3	1	1	2.51491	35.672	100.0	
	2	2	z	2.40784	37.315	2.9	
10	3	2		2.31338	38.899	0.0	
11	3	2	1	2.22923	40,430	0.3	
12				2.08525	43.358	17.0	
13		1	0	2.02299	99.763	0.3	
14	-	1	1	1.96599	46.135	0.2	
15	3	3	1	1.91356	47.475	0.1	
16		2	1	1.82016	50.074	1.3	
17	3	3	2	1.77831	51.337	0.1	
18	9	2	2	1.70260	53.799	10.8	
19	1	3		1.66820	55.001	0.6	
20	5	1	0	1.63580	56.186	0.4	
21	5	1	1	1.60523	57.354	26.4	
22	-	2		1.54888	59.647	0.7	
23	5	2	1	1.52285	60.773	1.5	
24	1	4		1.47449	62.989	35.9	
25	9	9	1	1.45198	69.081	0.5	
26	5	3		1.43047	65.162	0.5	
27	5	3	÷	1.40989	66.235	0.2	
28	9	4	2	1.39017	67.298	0.1	
29		1		1.37125	68.354	0.3	
30	5	3	2	1.35309	69.401	0.5	
31	0	2		1.31883	71.976	3.5	
32		4	-	1.30265	72.503	0.4	
33	2	-	-	1.28704	73.526	0.1	
37	-	2	2	1.2/199	71.512	0.5	
35	-	2	-	1.25745	75.554	1.1	
36	5	9	2	1.24340	76.561	0.3	
37	6	3	1	1.22981	77.564	0.1	
38	-	9	9	1.20392	79.558	1.5	
39	6	3	2	1.19157	80.550	0.3	
=0	7	1	0	1.17960	81.539	0.1	
91	5	5	1	1.16797	82.527	0.1	
92	6	4		1.15669	83.511	0.1	
93	7	2	0	1.14572	89.494	0.1	
11	5	5	2	1.13507	85.474	0.4	
95	6	4	2	1.11461	87.434	3.2	
96	2	2	Z	1,10479	88,411	0.1	
97	7	3	0	1.09523	89.388	0.2	



i) ThO₂

Date: 0/30/2022 Time: 10.56.20	PM Pile: Sampel Pasir Monasit	User: LENO
<u>Name and formula</u>		
Reference code:	03-065-0292	
Mineral name:	Thoria, syn	
Compound name:	Thorium Oxide	
PDF index name:	Thorium Oxide	
Empirical formula:	O ₂ Th	
Chemical formula:	ThO ₂	
Crystallographic param	<u>ieters</u>	
Crystal system:	Cubic	
Space group:	Fm-3m	
Space group number:	225	
a (Å):	5.7210	
b (Â):	5.7210	
c (Å):	5,7210	
Alpha (°):	90.0000	
Beta (°):	90.0000	
Gamma (º):	90.0000	
Calculated density (g/cm^3):	9.36	
Volume of cell (10^6 pm^3):	187.25	
Ζ:	4.00	
RIR:	22.52	
Charles and Charles and an	- 11	
<u>Status, subriles and qu</u>	aiity	
Status:	Diffraction data collected at non ambient temperature	
Subfiles:	Alloy, metal or intermetalic	
	Inorganic	
	Mineral	
	NIST Pattern	
Quality:	Calculated (C)	
<u>Comments</u>		
Creation Date:	1/1/1970	
Modification Date:	1/1/1970	
N 23225 21560. Temperatu	re of Data Collection: 2000	
Torona da Canada da C	No TE share for other 0-1.0 serviced	

References

Primary reference: Structure: Calculated from NIST using POWD-12++ K.Clausen, W.Hayes, J.E.Macdonald, P.Schnabel, M.T.Hutchings & J.KKjems, High Temp. High Pressures, 15, 383-3, (1983)

Peak list

1 Of 2 User: LENOVO	l Pasir Monasit	2 Time: 10:58:20 PM File: Sampel Pasir Monasit					Date: (
	[\$] I [8]	2Theta[deg	d [A]	1	k	h	No.
	100.0	26.972	3.30302	1	1	1	1
	34.4	31.244	2.86050	D	0	z	2
	43.3	44.770	2.02268	0	2	2	3
	37.1	53.047	1.72495	1	1	3	4
	7.9	55.605	1.65151	2	2	2	5
	5.5	65.174	1,43025	0	0	4	6
	12.3	71.875	1.31249	1	3	з	7
	8.9	74.048	1.27925	D	2	4	8
	9.3	82.542	1.16779	2	2	4	9
	B.0	88.795	1,10101	1	1	5	10
	2.7	99.222	1.01134	0	4	4	11
	7.8	105.607	0,96703	1	3	5	12
	3.9	107.776	0.95350	D	0	6	13
	3.9	116.765	0.90457	0	2	6	14
	3.1	123.994	0.87244	з	3	s	15
	2.6	126.538	0.86247	2	2	6	16
	1.1	137.765	0.82576	4	4	4	17
	5.6	148.121	0.80110	1	1	7	18



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k) CaTiO₃

Date: 6	a 30/20	22 IIM	a. 10:51:	15 11/10	FI	e. JUA		Usef: LEN
Nam	e and	forn	nula					
Refere	nce coc	le:		00-040-01	03			
Compo	ound na	me:		Calcium T	itanium Oxide			
PDF in	idex na	me:		Calcium T	itanium Oxide			
Empirio	cal form	nula:		Ca ₂ O ₆ Ti ₂				
Chemic	cal form	nula:		Ca ₂ TI ₂ O ₆				
<u>Cryst</u>	tallog	raph	ic para	meters				
Crystal	l system	1:		Cubic				
Space	group:			F				
a (Å):				9.953	0			
b (Â):				9,953	0			
c (Â):				9,953	0			
Alpha ((°);			90,000	0			
Beta (*	1			90,000	0			
Gamma	a (º):			90.000	a			
Volume	e of cell	(10^6	pm^3):	985.97				
Z:				B.00				
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~ 10		1.0						
Subr	iles a	nd Q	uality					
Subfile	s:			Corrosion				
Quality	:			Inorganic Calculated	(C)			
<u>Com</u>	ment	s						
Creatio	on Date			1/1/1970				
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<u>Refe</u>	rence	<u>s</u>						
Priman	y refere	ence:		Ball, C., W	/hite, T., <i>J. Soli</i> (d State Chem	a, 65 , 148, (1986)	
	<u>c list</u>							
<u>Peak</u>		k	1	d [A]	2Theta[de	J] [8]		
Peak	h		2	2.87320	31.102	100.0		
Peak	<u>h</u> 2	2		2.48830	36.066	20.0		
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Peak	h 2 4 4	2 0 4	0	1.75950	51.927	40.0		
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l) Ca₃SiO₅

Reference	e code:		96-900-83	67				
Mineral na	ame:		Hatrurite					
Compoun	d name:		Hatrurite					
Common	name:		Hatrurite					
Chemical	formula:		Ca _{108.00} 5i	36.00 ⁰ 180.00				
Crystal	llograp	hic para	ameters					
Crystal sy	stem:		Monodinic					
Space gro	oup:		C 1 m 1					
Space gro	oup numbe	en:	8					
a (Â):			33.0830	1				
b (Â):			7.0270	3				
c (Å):			18,4990)				
Alpha (°):	:		90.0000)				
Beta (°):			94.1200	1				
Gamma (•):		90.0000	3				
Calculated								
	a aensity (Q/Cm^3):	3.18					
Volume o	a aensity (f cell (10^	g/cm^3): 6 pm^3):	3.18 4289.43					
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8	2	0	2	7.01657	11.311	0.1	
9	4	0	-1	7.74104	11,422	0.4	
11	1	1	Ô	6.87289	12.870	0.2	
12	1	1	-1	6.47234	13.670	0.4	
13	1	1	1	6.40929	13.806	0.0	
14	4	0	-2	6.38150	13,866	0.1	
16	4	ő	2	5.94103	14.900	5.9	
17	3	1	0	5,92169	14,949	12.4	
18	2	0	-3	5.90349	14.995	0.0	
20	3	1 0	-1	5.70297	15.525	0.1	
21	3	1	1	5.57601	15.551	0.1	
22	1	1	-2	5,55150	15,952	0.1	
23	6	0	0	5.49958	16.103	1.4	
24	-	-	-1	5.47247	16.104	3.1	
26	6	ŏ	1	5.16976	17.138	0.1	
27	4	0	-3	5.10987	17.340	0.0	
28	3	1	-2	5.07343	17.466	0.2	
30	6	ō	-2	4.88066	18.162	0.1	
31	5	1	0	4.81059	18.428	0.1	
32	4	0	3	4.76934	18.589	0.0	
33	5	1	-1	4.71566	18.803	0.0	
35	0	ō	4	4.61280	19.226	0.1	
36	5	1	1	4.59658	19.294	0.2	
37	6	0	2	4.58137	19.359	0.0	
38	2	1	-4	4.59950	19,996	0.1	
40	2	ŏ	4	4.36192	20.343	0.1	
41	5	1	-2	4.36016	20.351	0.3	
42	3	1	-3	4.35074	20.396	0.4	
43	3	1	-3	4.18570	20.863	0.1	
45	5	1	2	4.17678	21.255	0.3	
46	4	0	-4	4.15530	21.366	0.5	
47	8	0	0	4.12469	21.527	0.0	
48	8	0	-1	1.08836 3.96514	22,404	0.2	
50	6	ŏ	3	3,96069	22,429	0.1	
51	7	1	D	3,91469	22.696	0.1	
52	4	0	4	3.90828	22.734	0.1	
53	2	1	-3	3.88932	22,922	0.2	
55	8	ō	-2	3.87052	22,959	3.9	
56	1	1	-4	3.85692	23.041	6.2	
57	1	1	4	3.80387	23.367	0.3	
59	á	1	-4	3.70925	23.992	0.0	
60	5	1	3	3,69641	24.056	0.0	
61	0	0	5	3.69024	24.097	0.1	
62	7	1	-2	3.68357	24,141	0.1	
62	8	•	2	3.66955	24,242	0.2	
63 64	8	0	2 -4	3.66855 3.66628	24,242	0.2	
63 64 65	8 2	0	2 -4 -5	3.66855 3.66628 3.65767	24.242 24.257 24.315	0.2	
63 64 65 66	8 6 2 3	0 0 1	2 -4 -5 4	3.66855 3.66628 3.65767 3.57265	24.242 24.257 24.315 24.903	0.2 0.3 0.1 0.4	
63 64 65 66	8 2 3	0 0 1	2 -4 -5 4	3.66855 3.66628 3.65767 3.57265	24,242 24,257 24,315 24,903	0.2 0.3 0.1 0.4	20(3
63 64 65 66 Date:	8 2 3 6/18/20	0 0 1 22 Tim	2 -4 -5 4 ie: 9:17	3.66855 3.66628 3.65767 3.57265	24,242 24.257 24,315 24.903	0.2 0.3 0.1 0.4	2 Of 3 User: LENOVO
63 64 65 66 Date: 67 60	8 2 3 6/18/20 2 5	0 0 1 22 Tim 0 0	2 -4 -5 4 e: 9:17 5 -3	3.66855 3.66628 3.65767 3.57265 :37 AM 3.54738 3.54738 3.54552	24,242 24,257 24,315 24,903 Fi 25,083 25,096	0.2 0.3 0.1 0.4 ile: 50A 0.4 0.4	2 Of 3 User: LENOVO
63 64 65 66 Date: 67 69	8 2 3 6/18/20 2 7	0 0 1 22 Tim 0 1	2 -4 -5 4 we: 9:17 5 -3 2	3.66855 3.65628 3.65767 3.57265 :37 AM 3.54738 3.54738 3.54532 3.52876	24,242 24,257 24,315 24,903 Fi 25,083 25,096 25,217	0.2 0.3 0.1 0.4 ile: 50A 0.4 0.4 0.4 4.8	2 Of 3 User: LENOVO
63 64 65 66 Date: 67 69 70	8 2 3 6/18/20 2 7 7 0	0 0 1 22 Tim 0 0 1 2	2 -4 -5 4 e: 9:17 5 -3 2 0	3.66855 3.66628 3.65767 3.57265 :37 AM 3.54738 3.54738 3.5452 3.52876 3.51350	24.242 24.257 24.315 24.903 Fi 25.083 25.096 25.217 25.329	0.2 0.3 0.1 0.4 1e: 50A 0.4 0.4 4.8 2.7	2 OF 3 User: LENOVO
63 64 65 66 Date: 67 69 70 71	8 2 3 6/18/20 2 7 0 4	0 0 1 22 Tim 0 0 1 2 0	2 -4 -5 4 e: 9:17 5 -3 2 0 -5	3.66855 3.66628 3.65767 3.57265 3.54738 3.54738 3.54552 3.55276 3.51350 3.46256	24.242 24.257 24.315 24.903 25.083 25.083 25.096 25.217 25.329 25.708	0.2 0.3 0.1 0.4 1e: 50A 0.4 0.4 0.4 0.4 2.7 0.2 2.7	2 Of 3 User: LENOVO
63 64 65 66 Date: 67 69 70 71 72 73	8 2 3 6/18/20 2 7 0 4 0 2	0 0 1 22 Tim 0 0 1 2 0 2 2	2 -4 -5 4 e: 9:17 5 -3 2 0 -5 1 0	3.666855 3.66628 3.65767 3.57265 3.57265 3.54738 3.54738 3.54552 3.52876 3.51350 3.46256 3.45148 3.43644	24.242 24.257 24.315 24.903 25.083 25.096 25.217 25.329 25.708 25.702 25.907	0.2 0.3 0.1 0.4 1e: 50A 0.4 0.4 4.8 2.7 0.2 0.1 0.0	2 OF 3 User: LENOVO
63 64 65 66 0 70 70 71 72 73 74	8 2 3 6/18/20 2 7 0 4 0 2 5	0 0 1 22 Tim 0 0 1 2 0 2 2 1	2 -4 -5 4 -5 -3 2 0 -5 1 0 -4	3.66855 3.66628 3.65767 3.57265 3.57265 3.54738 3.54738 3.54532 3.52876 3.51350 3.46256 3.45148 3.43644 3.42015	24.242 24.257 24.315 24.903 25.083 25.096 25.217 25.329 25.708 25.708 25.702 25.907 26.032	0.2 0.3 0.1 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.2 0.1 0.2 0.1 0.0 0.0	2 Of 3 User: LENOVO
63 64 65 66 0 0 1 70 71 72 73 74 75	8 6/18/20 2 7 0 4 0 2 5 6	0 0 1 22 Tim 0 0 1 2 0 2 2 1 0	2 -4 -5 4 5 -3 2 0 -5 1 0 -4 4	3.66855 3.66628 3.65767 3.57245 3.57245 3.52453 3.524738 3.524738 3.524738 3.52476 3.51350 3.46256 3.45148 3.43644 3.43015 3.41545	24.242 24.257 24.315 24.903 25.083 25.096 25.217 25.329 25.708 25.708 25.702 25.907 26.032 26.069	0.2 0.3 0.1 0.4 0.4 0.4 4.8 2.7 0.2 0.1 0.0 0.3 0.1	2 Of 3 User: LENOVO
63 64 65 66 0 70 71 72 73 74 75 76 77	8 6/18/20 2 7 0 4 0 2 5 6 7 2	0 0 1 22 Tim 0 1 2 0 2 2 1 0 2 2 1 0 1 2	2 -4 -5 4 e: 9:17 5 -3 2 0 -5 1 0 -4 -4 -3 -1	3.66855 3.66628 3.57265 3.57265 3.57265 3.57265 3.54738 3.54738 3.54738 3.54758 3.54876 3.45148 3.43044 3.43054 3.41545 3.41545 3.41545 3.33552 3.83766	24.242 24.257 24.315 24.903 25.083 25.096 25.217 25.329 25.708 25.708 25.702 25.907 26.032 26.069 26.224 26.228	0.2 0.3 0.1 0.4 0.4 0.4 0.4 0.4 4.8 2.7 0.2 0.1 0.0 0.3 0.1 0.0 0.3 0.1 0.0	2 OF 3 User: LENOVO
63 64 65 66 70 70 71 72 73 74 75 76 77 78	8 6/18/20 2 7 0 4 0 2 5 6 7 2 2 2	0 0 1 22 Tim 0 1 2 0 2 2 1 0 2 2 1 0 2 2 2 1 0 2 2 2	2 -4 -5 4 e: 9:17 5 -3 2 0 -5 1 0 -4 4 -3 -1 1	3.66855 3.66628 3.65767 3.57265 3.57265 3.57265 3.5127 3.52876 3.51350 3.64256 3.45128 3.45256 3.45148 3.43015 3.41545 3.33749 3.36529 3.36529	24.242 24.257 24.315 24.903 Fi 25.083 25.085 25.217 25.329 25.708 25.702 25.907 26.082 26.069 26.224 26.288 26.432	0.2 0.3 0.1 0.4 0.4 0.4 4.8 2.7 0.2 0.1 0.0 0.3 0.1 0.1 0.1 0.2 0.0	2 OF 3 User: LENOVO
63 64 65 66 70 71 72 73 74 75 76 77 77 78 79	8 6/18/20 2 7 0 4 0 2 5 6 7 2 2 8	0 0 1 22 Tim 0 1 2 0 1 2 2 1 0 1 2 2 0	2 -4 -5 4 0 -3 2 0 -5 1 0 -4 4 -3 -1 3	3.66855 3.66628 3.65767 3.57265 3.57265 3.57265 3.52876 3.52876 3.52876 3.52876 3.46256 3.45148 3.46256 3.43148 3.46215 3.43552 3.38552 3.38529 3.31718	24,242 24,257 24,315 24,903 Fi 25,083 25,086 25,217 25,329 25,708 25,708 25,217 26,322 26,082 26,082 26,082 26,224 26,282 26,432 26,655	0.2 0.3 0.1 0.4 1e: 50A 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.2 0.1 0.1 0.1 0.2 0.1 0.2 0.2 0.1 0.2	2 Of 3 User: LENOVO
63 64 65 66 70 71 72 73 74 75 76 77 78 79 80	8 6/18/20 2 7 0 4 0 2 5 6 7 2 2 8 10	0 0 1 22 Tim 0 1 2 0 2 2 1 0 1 2 2 0 0 0 0 1 2 0 0 0 1 2 0 0 0 1 2 0 0 0 1 2 0 0 0 1 2 0 0 0 1 2 0 0 0 1 2 0 0 0 0	2 -4 -5 4 -5 -3 2 0 -5 1 0 -4 -3 -1 1 3 0 -1	3.66855 3.66628 3.65747 3.57245 3.57245 3.57245 3.57245 3.52876 3.54738 3.54738 3.54738 3.545738 3.54505 3.46226 3.45148 3.42015 3.42015 3.42041 3.420453.42045 3.42045 3.420453.420	24,242 24,257 24,315 24,315 24,903 75,083 25,085 25,083 25,083 25,085 25,083 25,085 25,085 25,085 25,085 25,085 25,085 25,085 25,085 25,085 25,085 25,085 25,085 25,085 25,085 26,085 27,000	0.2 0.3 0.1 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	2 OF 3 User: LENOVO
63 64 65 66 07 67 69 70 71 72 73 74 75 76 77 80 80 82	8 6/18/20 2 7 0 4 0 2 5 6 7 2 2 8 10 10 0	0 0 1 22 Tim 0 0 1 2 2 2 1 0 1 2 2 0 0 0 2 2 2 0 0 0 2 2 2 0 0 0 2 2 2 0 0 0 2 2 2 0 0 0 2 2 2 0 0 0 2 2 2 0 0 0 0 2 2 0 0 0 0 2 2 0 0 0 0 2 2 0 0 0 0 2 2 0	2 -4 -5 4 (e: 9:17) 5 -3 2 0 -5 1 0 -4 4 -3 -1 1 3 0 -1 2	3.66855 3.66628 3.65767 3.57265 3.57265 3.517265 3.517265 3.51726 3.51350 3.64525 3.45126 3.45126 3.45126 3.45128 3.45252 3.35729 3.36525 3.41545 3.41545 3.41545 3.35749 3.36525 3.35726 3.29975 3.29975 3.29975	24,242 24,257 24,315 24,903 Fi 25,008 25,008 25,207 25,327 25,320 25,700 25,327 25,327 26,059 26,224 26,052 26,432 26,432 26,432 26,435 26,432 26,435 26,432 26,435 26,432 26,435 26,432 26,435 26,435 27,136	0.2 0.3 0.1 0.4 1e: 50A 0.4 0.4 0.4 0.4 0.4 0.2 0.1 0.2 0.1 0.0 0.3 0.1 0.1 0.2 0.0 0.0 0.2 0.0 0.1 0.1 0.1 0.2 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	2 Of 3 User: LENOVO
63 64 65 66 Date: 67 67 69 70 71 72 73 74 75 76 77 80 81 82 83	8 6/18/20 2 7 0 4 0 2 5 6 7 2 2 8 10 10 10 0 4	0 0 1 22 Tim 0 0 1 2 2 1 0 1 2 2 1 0 1 2 2 0 0 0 2 2 0 0 0 2 2 0 0 0 2 2 0 0 0 1	2 -4 -5 4 : : : : : : : : : : : : : : : : : :	3.66855 3.66628 3.65767 3.57265 3.57265 3.57265 3.52876 3.54738 3.54738 3.54752 3.52876 3.51380 3.46256 3.45148 3.43015 3.43644 3.43015 3.43645 3.43645 3.43645 3.33719 3.32925 3.32943 3.28344 3.28345	24,242 24,257 24,315 24,903 Fi 25,086 25,086 25,217 25,329 25,208 25,702 25,702 25,907 26,082 26,082 26,082 26,082 26,082 26,082 26,082 26,082 26,082 26,082 26,082 26,082 27,006 27,150	0.2 0.3 0.1 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	2 Of 3 User: LENOVO
63 64 65 66 67 67 69 70 71 72 73 74 75 77 78 80 81 83 84	8 6/18/20 2 7 7 4 0 2 5 6 7 2 2 8 10 10 10 0 4 1	0 0 1 22 Tim 0 0 1 2 2 1 0 1 2 2 1 0 0 1 2 2 0 0 0 2 2 1 0 0 1 2 2 1 0 0 1 2 2 1 0 0 1 2 2 1 0 0 1 2 2 1 0 0 1 2 2 1 0 0 0 1 1 2 2 0 0 1 1 2 2 0 0 1 1 2 2 0 0 1 1 2 2 0 0 1 1 2 2 0 0 1 1 2 2 0 0 1 1 2 2 0 0 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 1 1 2 2 2 1 1 2 2 2 1 1 2 2 2 1 1 2 2 2 1 1 2 2 2 1 2 2 2 2 2 1 2	2 -4 -5 4 : : : : : : : : : : : : : : : : : :	3.66855 3.66628 3.65747 3.57245 3.57245 3.57245 3.57245 3.57245 3.57245 3.52476 3.51350 3.46226 3.45145 3.42015 3.42045 3.42045 3.42045 3.38749 3.38749 3.38749 3.28945 3.28945 3.28945 3.28182 2.27170	24,242 24,257 24,315 24,903 Fi 25,083 20,096 25,217 25,229 25,702 25,702 25,702 26,052 26,055 26,055 26,055 26,055 26,055 26,055 26,055 27,000 27,136 27,136 27,236	0.2 0.3 0.4 10.4 1e: 50A 1e: 50A 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.2 0.1 0.0 0.3 0.1 0.2 0.2 0.1 0.2 0.2 0.1 0.2 0.3 0.1 0.2 0.3	2013 User: LENOVO
63 64 65 66 70 72 73 74 75 77 78 90 82 84 85 84 85	8 6/18/20 2 5 6 7 2 2 2 8 7 7 4 0 2 5 5 6 7 2 2 8 10 10 10 10 9 5	0 0 1 22 Tim 0 0 1 2 2 2 1 0 1 2 2 0 0 0 2 2 1 2 0 0 0 1 2 2 1 0 0 1 2 2 1 0 0 1 2 2 1 0 0 0 1 1 0 0 0 0	2 -4 -5 4 -5 -3 2 0 -3 2 0 -3 -3 2 0 -4 4 -3 -1 3 0 -1 2 5 -5 -3 2 0 -5 1 0 -2 -5 -5 -3 2 0 -5 -5 -3 2 0 -5 -5 -5 -3 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5	3.66855 3.66628 3.65767 3.57265 3.57265 3.57265 3.51265 3.51265 3.51265 3.51265 3.51265 3.51265 3.45126 3.32765 3.32765 3.32755 3.32755 3.32975 3.32975 3.32975 3.22943 3.22944 3.22054	24.242 24.257 24.315 24.305 25.063 25.056 25.217 25.325 25.708 25.708 25.708 25.225 25.708 25.708 25.225 25.055 26.055 26.255 26.255 27.136 27.136 27.136 27.136	0.2 0.3 0.1 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	2 Of 3 User: LENOVO
63 64 65 65 66 70 72 73 75 76 77 75 76 77 78 79 80 82 83 84 85 86 85 86	8 6/18/20 2 7 7 4 0 4 0 2 5 5 6 7 2 2 8 10 10 0 4 1 9 5 5	0 0 1 22 Tim 0 0 1 2 2 2 1 0 1 2 2 0 0 0 2 2 0 0 0 2 2 1 2 0 0 0 1 2 2 1 2 1	2 -4 -5 -5 -3 2 0 -5 1 0 -4 4 -3 -1 3 0 -1 2 5 -0 4 -2 -5 0 4 -2 -5	3.66855 3.66628 3.65767 3.57265 3.57265 3.57265 3.52876 3.52876 3.52876 3.52876 3.46256 3.45128 3.46256 3.45128 3.46256 3.45128 3.38522 3.38525 3.31710 3.28545 3.28545 3.22943 3.28545 3.22170 0.25054 3.225056 3.225056 3.255056 3.255056 3.255056 3.255056 3.255056 3.255056 3.255056 3.255056 3	24.242 24.257 24.315 24.903 25.068 25.068 25.068 25.072 25.327 25.327 25.327 25.907 26.085 26.042 26.055 26.026 26.288 26.432 26.055 27.000 27.286 27.150 27.286 27.150	0.2 0.3 0.4 0.4 1e: 50A 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	20/3 User: LENOVO
63 64 65 66 67 70 71 72 73 74 75 77 77 78 80 81 82 83 84 85 86 87 88	8 6/18/20 2 7 0 4 0 2 5 6 7 2 2 8 10 0 4 1 9 5 2 4	0 0 1 22 Tim 0 1 2 0 1 2 2 1 0 1 2 2 2 1 0 1 2 2 0 0 2 2 1 0 0 2 2 1 2 0 0 1 2 2 1 0 0 1 2 2 1 2 0 0 1 2 0 0 1 2 0 0 1 2 0 0 1 2 0 0 1 1 0 0 1 2 0 0 1 2 0 0 1 2 0 0 1 1 2 0 0 1 1 0 0 1 2 2 2 1 0 0 1 1 0 0 1 1 2 2 2 1 0 0 1 1 2 2 2 2	2 -4 -5 4 :e: 9:17 5 -3 2 0 -5 1 0 -4 4 -3 -5 -5 1 0 -1 2 5 -5 0 -1 2 5 -5 -0 -2 -5 -1 0 -2 5 -3 2 0 0 -5 -5 -3 2 0 -5 -5 -1 -5 -5 -5 -1 -5 -5 -1 -5 -5 -1 -1 -1 -5 -5 -1 -1 -1 -1 -1 -2 -5 	3.66855 3.66628 3.65745 3.57245 3.57245 3.57245 3.57245 3.57245 3.5474 3.54738 3.54743 3.54753 3.5474 3.45145 3.45145 3.45145 3.38574 3.28544 3.28544 3.28544 3.28544 3.28544 3.24544 3.24564 3.24564	24,242 24,257 24,315 24,315 25,063 25,063 25,086 25,217 25,329 26,096 25,702 26,097 26,032 26,063 26,063 26,082 26,082 26,082 26,082 26,082 26,082 26,082 26,083 26,083 26,084 27,086 26,084 27,086 26,085 27,08627,086 27	0.2 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	20/3 User: LENOVO
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55	3	3	2	1.40626	66,428	0.1	
6	1	2	3	1.40117	66.701	0.5	
7	- 2	0	1	1.39684	66.934	8.7	
68 66	2	4	1	1.38915	67.354	0.0	
70	5	2	2	1.38381	67.649	0.1	
71	5	3	1	1.37529	68.125	3.0	
72	2	2	3	1.36326	68,811	7.8	
73	7	1	1	1.36102	68.940	0.2	
74	4	0	3	1.35625	69.216	0.7	
75	•	1	2	1.35391	69.354	3.9	
22	4	1	3	1.32340	70.853	5.6	
78	4	3	2	1.32142	71.314	1.0	
79	3	z	3	1.30638	72.263	0.1	
80	4	4	0	1.30138	72.585	2.7	
81	6	3	0	1.30119	72.598	5.3	
82	0	4	2	1.27952	74.030	5.2	
83	8	0	0	1.27750	74.166	2.0	
85	-	-	1	1.26901	74.808	1.0	
86	6	2	2	1.26236	75.209	5.4	
87	5	0	3	1.26007	75.370	0.5	
88	4	4	1	1.25606	75.652	0.7	
89	6	3	1	1.25588	75.665	0.0	
90	0	3	3	1.25350	75.834	0.4	
91	8	1	0	1.24993	76.089	0.2	
92	7	0	2	1.24740	76.271	0.5	
5.5 64	2	4	2	1.24120	76.301	0.1	
95	4	2	3	1.23753	76,991	0.0	
96	8	ō	1	1.23454	77.211	0.0	
97	5	1	3	1.23359	77.282	0.7	
98	5	3	2	1.23198	77,401	1.7	
99	7	1	2	1.22169	78.177	0.4	
00	2	3	3	1.21741	78.505	0.3	
02	ő	ò	4	1.20025	79.850	3.8	
03	3	4	2	1,19782	80.045	0.1	
04	1	0	4	1.19206	80.510	0.5	
05	5	4	1	1.17850	81,631	1.1	
90	z	5	0	1.17726	81.736	0.8	
.07	8	2	0	1.17683	81.772	0.1	
00		5	1	1.17313	82 085	2.0	
10	1	1	đ	1 16956	82 390	0.9	
11	z	ō	4	1.16845	82.485	0.1	
12	6	0	3	1.16632	82.669	0.0	
13	1	5	1	1.16547	82.742	1.0	
14	5	2	3	1.16316	82.943	6.7	
15	7	2	2	1.15317	83.823	1.6	
16	7	3	1	1.14823	84.267	0.2	
18	6	1	3	1.14/24	84.539	0.3	
9	4	4	z	1.14407	84.644	5.5	
20	6	3	2	1.14394	84.656	2.1	
21	2	5	1	1.14338	84.707	0.0	
22	8	2	1	1.14299	84.743	1.0	
23	3	0	4	1.13204	85.758	0.0	
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5	8	0	2	1.12775	86.164	2.4	
26	4	3	3	1.12536	86.391	4.1	
27	0	2	9	1.11501	67.335	0.0	
28	3	5	1	1,10920	87.969	3.8	
30	1	2	ā.	1.10903	87.986	2.6	
31	8	1	2	1.10864	88.025	2.6	
32	9	Ó	1	1.10507	88.384	0.3	
33	6	4	1	1,10075	88.822	0.2	
4	4	5	0	1.09342	89.576	0.4	
5	1	4	3	1.09284	89,636	1.6	
16	2	- 4	7	1.08994	89.940	4.6	



9. Dokumentasi Penelitian





UCAPAN TERIMA KASIH

Terdapat sebuah kebanggaan, ketika dapat menyelesaikan penelitian tugas akhir ini. Terdapat sebuah kesedihan pula, ketika menyadari sudah habis kesempatan untuk menjalani hidup bersama di perkuliahan. Untuk mengenang jasa-jasa orang baik yang senantiasa turut beperan dalam penelitian tugas akhir ini, penulis ingin mengucapkan terimakasih sebanyakbanyaknya kepada:

- 1. Kedua orang tua penulis yaitu Bapak Diono Purwanto dan Ibu Nurul Farida Hidayati, serta kakak penulis, yaitu Sofia Rizky Purwanto yang senantiasa memberikan do'a terbaik, motivasi yang berarti, dan semangat yang hangat.
- 2. Seluruh dosen Departemen Teknik Material dan Metalurgi yang telah memberikan ilmu dan nasihat selama masa perkuliahan berlangsung.
- 3. Sahabat penulis, yaitu Silvia Mutimmatus Syaadah yang menjadi tempat mencurahkan isi hati dan pikiran, serta senantiasa memberikan do'a terbaik dan semangat yang hangat.
- 4. Lodeh Asem Kunci, yaitu Wafiq dan Erika sebagai tempat bercerita dan bercanda selama masa perkuliahan
- 5. Kabinet HMMT Kontribusi 2021 yang lain, yaitu Feby, Ipeh, Safa, Lula, Karim, Arga, Fergi, Fernanda, Aldi, Ega, Serly, Ezra, Denby, dan Sabam yang membersamai ketika mengabdikan diri untuk HMMT.
- 6. Keluarga besar MT20 yang selalu ada menemani selama proses perkuliahan ini.
- 7. SMELTING ASYUUUUIK terdiri dari Raihan dan Ojil sebagai partner penelitian tugas akhir yang saling membantu dalam pelaksanaan penelitian,
- 8. Anggota Laboratorium Pengolahan Mineral dan Material yang lain, yaitu Zafi, Fadhlan, Rachmat, Yulindarika, Ganang, Edric, dan Jojo yang selalu menemani dan memberikan dukungan ketika melaksanakan penelitian tugas akhir di laboratorium.
- 9. Grader Metalurgi, Grader Perlakuan Panas, dan Grader Pengolahan Mineral dan Material, serta praktikan penulis yang memberikan pengalaman berharga.
- 10. Keluarga "Matahati Family" yang menjadi tempat bercerita selama masa perkuliahan.
- 11. Keluarga "Kos Family", yaitu Yuslam, Darel, Syarief, Rikza, Byan, Fatah, dll yang menjadi teman dalam menghabiskan waktu senggang bersama.
- 12. Tendik Solid Team, yaitu Cak Bas, Cak Indro, Cak Dayat, dan Cak Natsir yang menjadi tempat bersenda gurau ketika beristirahat selama penelitian tugas akhir.
- 13. Serta semua pihak yang tidak bisa penulis sebutkan satu persatu.

Pada akhirnya, kebaikan akan terbalas lebih baik dengan kebaikan yang lain. Oleh karena itu, penulis senantiasa berdo'a agar diberikan waktu dan kesempatan suatu saat nanti untuk sejenak bercerita. Akhir kata, semoga penelitian tugas akhir ini dapat membawa manfaat untuk kehidupan manusia kedepannya.

Surabaya, 1 Juli 2022 Penulis

Kaisar Akbar Purwanto



(Halaman ini sengaja dikosongkan)





BIODATA PENULIS

Nama lengkap penulis adalah Kaisar Akbar Purwanto. Penulis merupakan anak kedua dari dua bersaudara dari pasangan Bapak Diono Purwanto dan Ibu Nurul Farida Hidayati. Dilahirkan di Kabupaten Magetan, Jawa Timur pada tanggal 12 April 2000. Penulis telah menempuh pendidikan formal di SDIT Al-Furqon Maospati (2006-20012), SMPN 1 Magetan (2012-2015), dan SMAN 1 Magetan (2015-2018). Kemudian melanjutkan studi sarjana di Departemen Teknik Material dan Metalurgi FTIRS-ITS, Surabaya, melalui jalur penerimaan mahasiswa baru SNMPTN pada tahun 2018. Selama menjalani masa perkuliahan, penulis aktif dalam kegiatan akademik sebagai Grader Metalurgi 2019-2021, Grader Perlakuan Panas 2020/2021, dan Grader Pengolahan Mineral dan Material 2021/2022. Selain itu, penulis juga pernah mendapatkan penghargaan sebagai Finalist Top 10 Lomba

Karya Tulis Ilmiah oleh Omah Karya Indonesia. Penulis juga turut aktif dalam kegiatan nonakademik sebagai Ketua HMMT FTI-ITS 2021 dan Staf Departemen Pengembangan Sumber Daya Mahasiswa HMMT FTI-ITS 2019/2020. Sebagai persiapan dalam bekerja, penulis melaksanakan kerja praktik selama 2 bulan di Departemen Inspeksi Teknik PT. Petrokimia Gresik. Sementara itu, untuk menyelesaikan studi sarjana, penulis melakukan penelitian tugas akhir dalam bidang keprofesian Metalurgi Ekstraksi dengan judul "Analisis Pengaruh Variasi Kuat Arus Listrik *Electric Arc Furnace* Pada Proses *Smelting* Pasir Monasit Terhadap Komposisi Senyawa dan *Grade* ThO₂". Apabila terdapat hal yang ingin ditanyakan, penulis dapat dihubungi melalui alamat email: kaisarakbar14@gmail.com, nomor *handphone*: +6281615511275, dan profil *linkedin*: linkedin.com/in/kaisarakbar/.