

TUGAS AKHIR  
KONVERSI ENERGI

PERENCANAAN ULANG INSTALASI HEATER  
DRAIN PUMP (HDP)  
PADA PLTU UNIT 3 PT. PJB UP GRESIK

Oleh:

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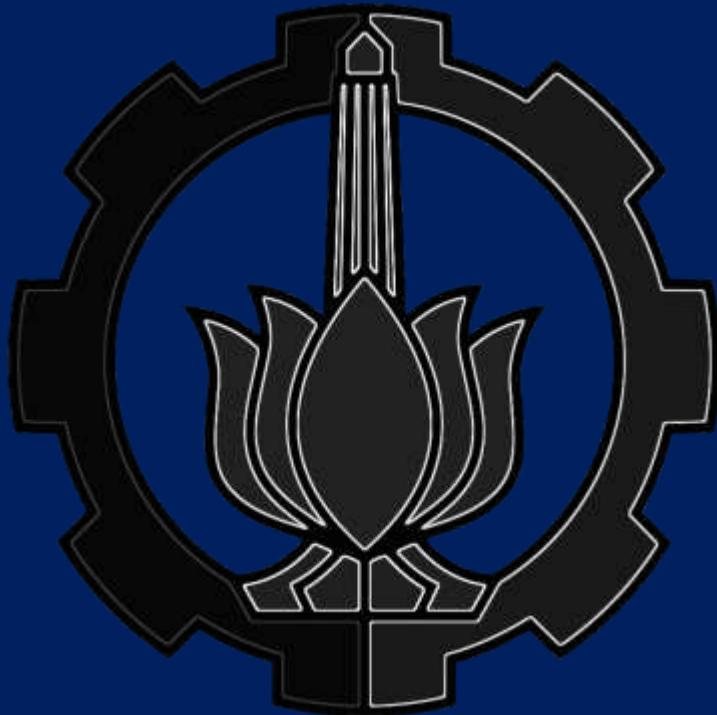
Program Studi Diploma III Kerjasama PT. PLN (Persero)

Jurusan Teknik Mesin

Fakultas Teknologi Industri

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Surabaya 2015



# PENDAHULUAN

LITERATUR SAINS

# LATAR BELAKANG

Feed Water Heater Drain System memiliki peranan yang sangat penting dalam siklus PLTU unit 3 dan 4 sebagai penambah suplai air kondensat yang menuju ke deaerator. Temperatur air yang masih tinggi di heater drain tank dapat menambah efisiensi siklus.



Terjadi backflow pada bulan maret 2015 yang menyebabkan pompa heater drain pump trip.

# PERUMUSAN MASALAH

## Sehingga permasalahannya:

Bagaimana Perencanaan Ulang Instalasi *Heater Drain Pump, Pemilihan Pompa dan Perawatan* pada Instalasi Perpipaan *Feed Water Heater Drain System* pada PLTU Unit 3 PT. PJB UP Gresik.

# BATASAN MASALAH



Analisa Pompa Heater Drain Pump Unit 3



Perhitungan Head Effektif Instalasi dimulai Dari Heater Drain Tank Sampai Pipa Air Kondensat



Tidak Ada Perpindahan Panas



Fluida Bersifat Incompressible, Alirannya Steady State, Steady Flow dan Fully Develop



Temperatur tiap Section Konstan kecuali masuk ke Heat Exchanger

# TUJUAN PENULISAN

Menghitung *Head Effektif* instalasi baik secara Analitis maupun Numerik

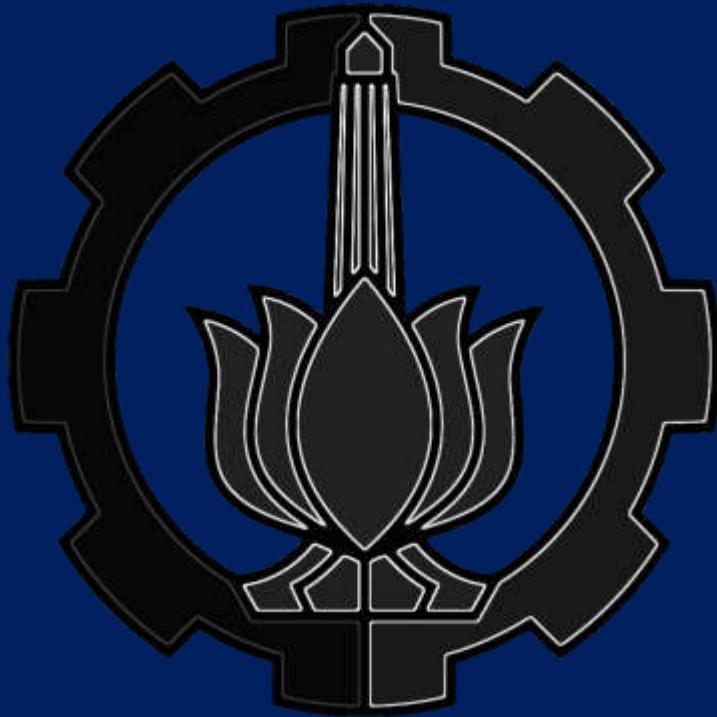
Melakukan pemilihan tipe pompa yang sesuai dengan instalasi *Feed Water Heater Drain System*

Mempelajari perawatan pompa  
*Heater Drain Pump*

# MANFAAT PENULISAN

Mengetahui besar  
nilai Head Effektif  
Instalasi

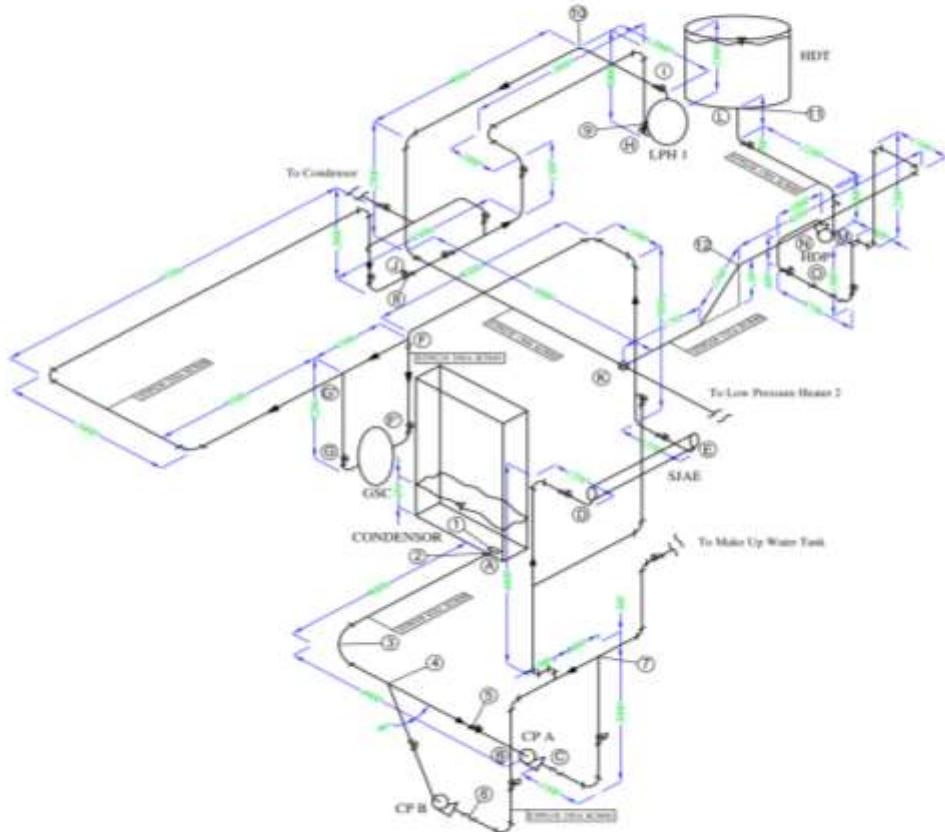
Diharapkan dengan dilakukannya  
pemilihan ulang pompa HDP ini dapat  
digunakan pedoman dalam  
mengembangkan sistem produksi pada  
PLTU UP Gresik Unit 3 secara optimal



DASAR TEORI  
DASAR TEORI

# GAMBAR INSTALASI

12	5	Elbow 30°
11	1	Pipe Entrance Rounded
10	1	Elbow 45°
9	2	Globe Valve
8	2	Control Valve
7	4	Tee Branch
6	2	Swing Check Valve
5	11	Gate Valve
4	7	Tie Through
3	36	Elbow 90°
2	4	Reducer
1	2	Strainer
NO. JUMLAH		KETERANGAN



# KOMPONEN-KOMPONEN



CONDENSOR



CONDENSATE PUMP



STEAM JET AIR EJECTOR



GLAND STEAM CONDENSOR

# KOMPONEN-KOMPONEN



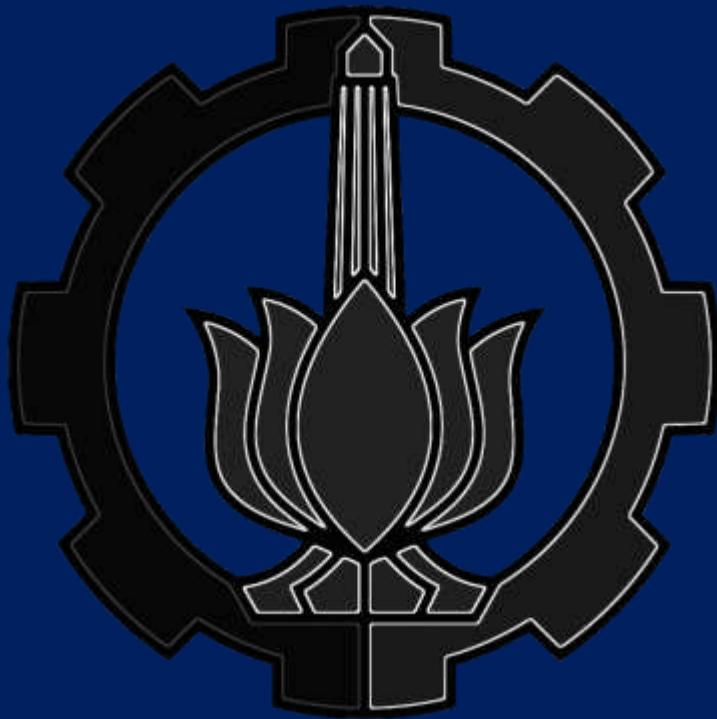
LOW PRESSURE HEATER 1



HEATER DRAIN TANK

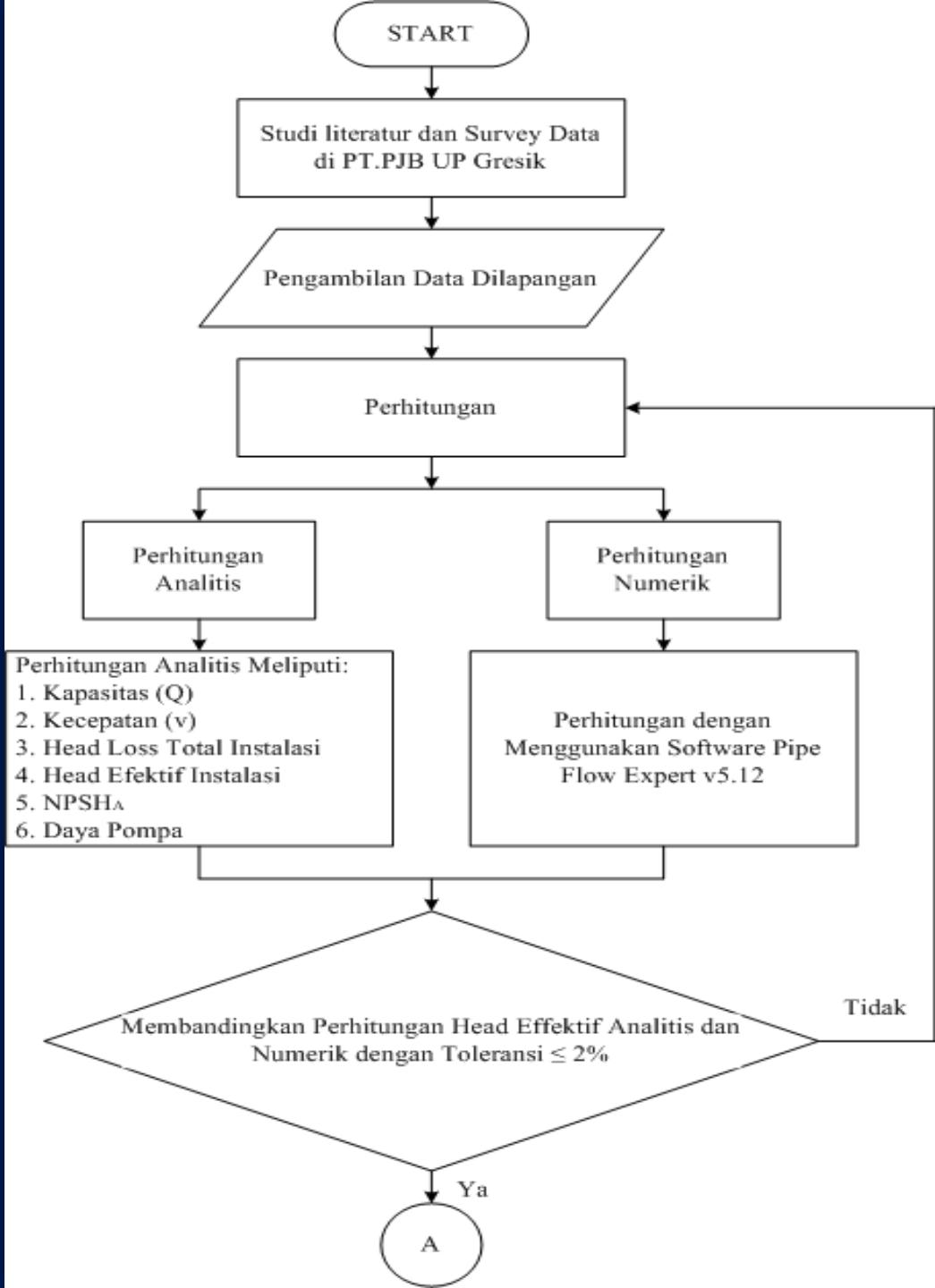


HEATER DRAIN PUMP

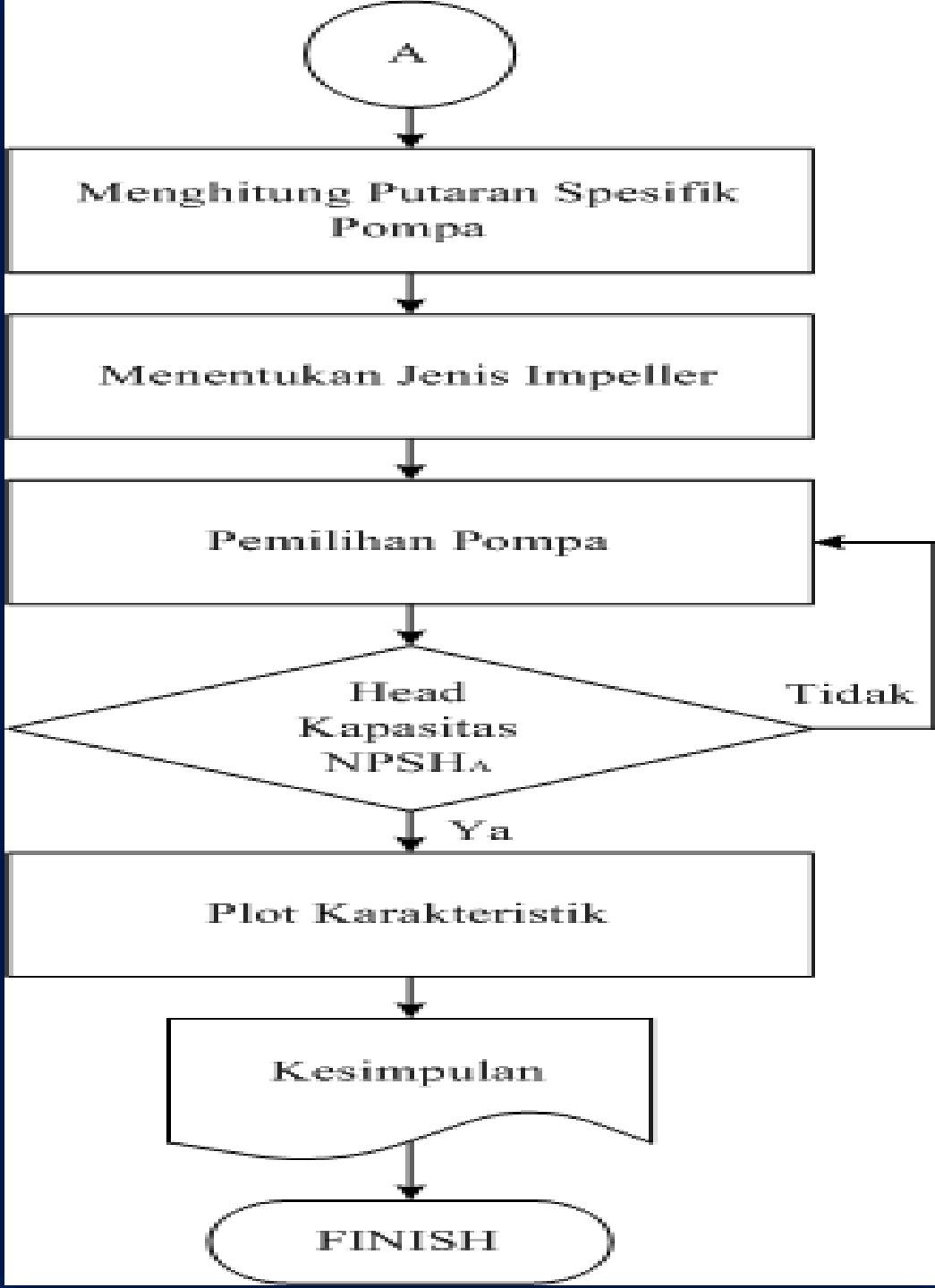


METODOLOGI  
TALE IODOFOOD

# ANALITIS



# ANALITIS



# NUMERIK

START

Pembuatan Instalsi Perpipaan dan Pompa pada Software Pipe Flow Expert v5.12 yang Terdiri Dari:

1. Perpipaan
2. Pompa
3. Suction Reservoir
4. Discharge Reservoir
5. Fitting dan Accessories

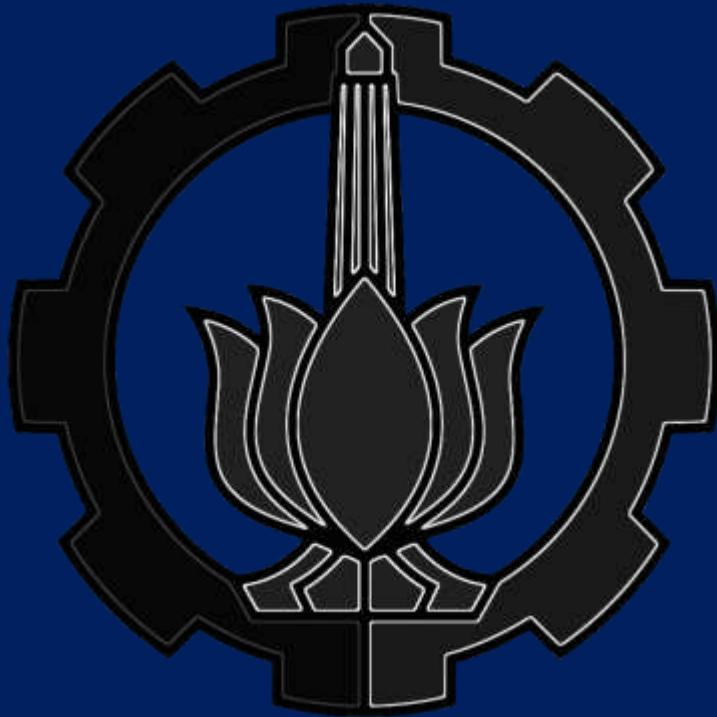
Menginput Data yang Terdiri Dari:

1. Material Pipa
2. Diameter Pipa
3. Data Pompa
4. Data Fluida
5. Nilai Koefisien Gesek Fitting dan Accessories
6. Tekanan dan Level Air di Suction Reservoir dan Discharge Reservoir

Calculate

Result

FINISH



PERHITUNGAN  
LEMBAGA

# CONDENSATE WATER SYSTEM

## Perhitungan Kapasitas Nominal Pompa:

$$\dot{m} = 432,623 \frac{\text{ton}}{\text{jam}} \times \frac{1000 \text{ kg}}{\text{ton}} \times \frac{\text{jam}}{3600 \text{ s}} \\ = 120,17 \frac{\text{kg}}{\text{s}}$$

Dari tabel B.1 (Properties of Water) (Lampiran 7), dengan  $T_1 = 43,1 \text{ }^{\circ}\text{C}$  maka di dapatkan massa jenis air sebesar:

$$\rho = 990,84 \frac{\text{kg}}{\text{m}^3}$$

$$Q = \frac{\dot{m}}{\rho} = \frac{120,17 \frac{\text{kg}}{\text{s}}}{990,84 \frac{\text{kg}}{\text{m}^3}}$$

$$= 0,12128 \frac{\text{m}^3}{\text{s}}$$

## Perhitungan Kapasitas Setiap Section:

$$Q_{(A-B)(C-D)} = \frac{\dot{m}}{\rho} \\ = \frac{120,17 \frac{\text{kg}}{\text{s}}}{990,84 \frac{\text{kg}}{\text{m}^3}} = 0,12128 \frac{\text{m}^3}{\text{s}}$$

Section	Kapasitas
A – B	0,12128
C – D	0,12128
E – F	0,12131
F – G'	0,09768
F – F'	0,02351
G – G'	0,02379
G' – H	0,12147
I – J	0,12415
J – K	0,12415

# CONDENSATE WATER SYSTEM

Perhitungan Kecepatan Setiap Section:

$$\begin{aligned}\bar{v}_{A-B} &= \frac{Q_{A-B}}{A_{A-B}} \\&= \frac{4Q_{A-B}}{\pi(D_{A-B})^2} \\&= \frac{4 \times 0,12128 \frac{m^3}{s}}{\pi(0,428650)^2 m^2} \\&= 0,840 \frac{m}{s}\end{aligned}$$

Section	Kecepatan
A – B	0,84041
C – D	2,38394
E – F	2,38394
F – G'	2,38453
F – F'	1,92005
G – G'	0,72841
G' – H	0,73709
I – J	2,38768
J – K	6,66082

# CONDENSATE WATER SYSTEM

## Perhitungan Head Loss Mayor:

$$Re = \frac{0,84041 \frac{m}{s} \times 0,428650 \text{ m}}{6,2366 \times 10^{-7} \frac{m^2}{s}} = 5,77627 \times 10^5$$

$$\frac{e}{D} = \frac{0,046 \text{ mm}}{428,650 \text{ mm}} = 0,00011$$

$$\frac{1}{\sqrt{f}} = -2 \log \left( \frac{e}{D} + \frac{2,51}{Re \sqrt{f}} \right)$$



$$f = 0,0143$$

$$Hl_{AB} = 0,0143 \times \frac{8,9 \text{ m}}{0,428650} \times \frac{0,84041^2 \frac{m^2}{s^2}}{2 \times 9,81 \frac{m}{s}} = 0,0107 \text{ m}$$

Section	Head Loss Mayor
A – B	0,0107
C – D	0,1956
E – F	0,1676
F – G'	0,0163
F – F'	0,0050
G – G'	0,0047
G' – H	0,4635
I – J	0,1419
J – K	1,1156

# CONDENSATE WATER SYSTEM

## Perhitungan Head Loss Minor:

Kerugian pada Foot Valve with Strainer Hinged Disk  $k=0,9$  pada diameter pipe size 24 inch (Lampiran 14), maka head loss minornya

$$H_{lm} = K \times \frac{\bar{v}_{AB}^2}{2g}$$
$$= 0,9 \times \frac{0,84041^2 \frac{m^2}{s^2}}{2 \times 9,81 \frac{m}{s^2}}$$

$$= 0,0324 \text{ m}$$

Section	Head Loss Minor
A – B	0,0770
C – D	1,6308
E – F	0,4898
F – G'	0,2104
F – F'	0,0279
G – G'	0,0324
G' – H	3,6118
I – J	1,7909
J – K	0,7724

# CONDENSATE WATER SYSTEM

## Perhitungan Head Loss Heat Exchanger:

$$\Delta P \text{ (Pressure Drop)} = 0,5 \text{ mAq} \\ = 4903,19 \text{ Pa}$$

$$Hl_{Steam Jet Air Ejector} = \frac{\Delta P}{\rho_{air 43,1^{\circ}C} \times g}$$

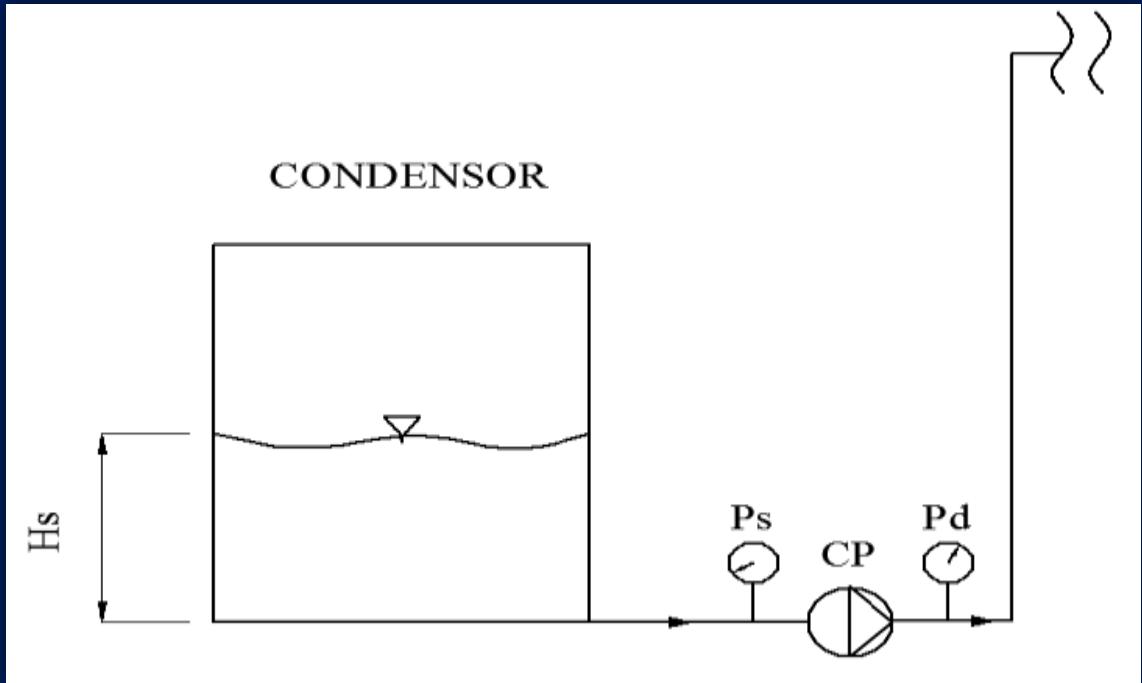
$$= \frac{4903,19 \text{ Pa}}{990,84 \frac{\text{kg}}{\text{m}^3} \times 9,81 \frac{\text{m}}{\text{s}^2}} \times \frac{\text{N}}{\text{Pa} \times \text{m}^2} \times \frac{\text{kg} \times \text{m}}{\text{N} \times \text{s}^2} \\ = 0,5044 \text{ m}$$

Heat Exchanger	Head Loss
SJAE	0,5044
GSC	3,0273
LPH 1	6,8654

$$\sum H_{loss total (C-K)} = \sum H_{loss mayor} + \sum H_{loss minor} \\ + \sum H_{loss heat exchanger} \\ = 2,1102 \text{ m} + 8,5163 \text{ m} + 10,3971 \text{ m} \\ = \mathbf{21,0236 \text{ m}}$$

# CONDENSATE WATER SYSTEM

Perhitungan Tekanan Ps:

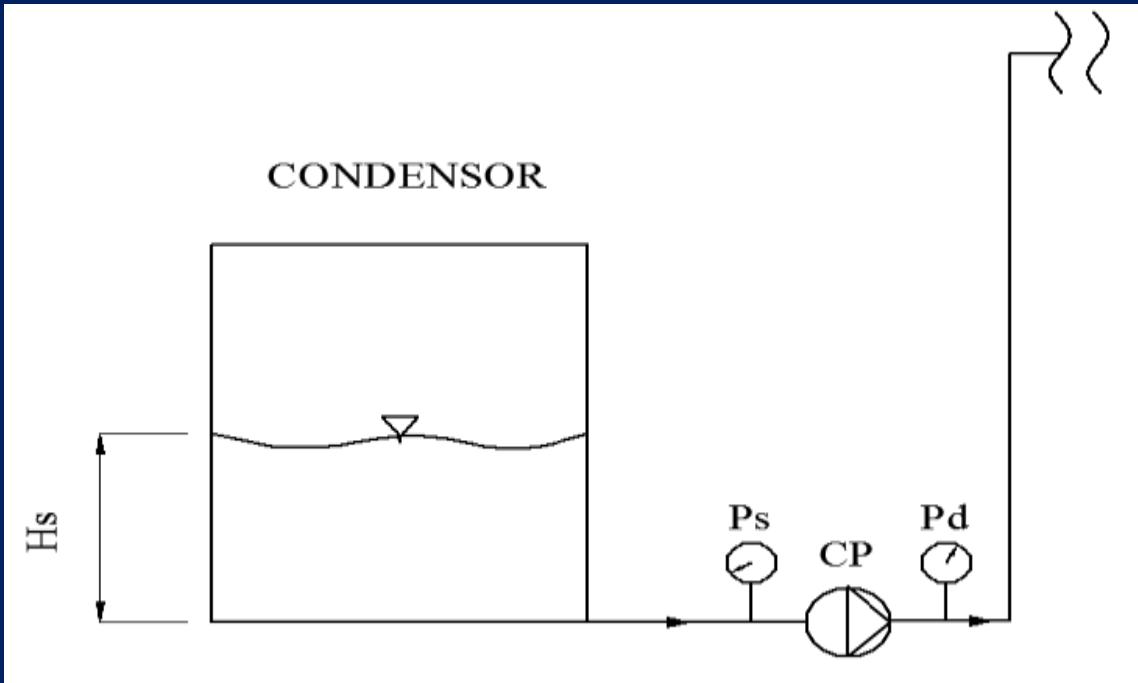


$$\begin{aligned}\frac{P_{ps}}{\gamma} &= \frac{P_{sr}}{\gamma} + \frac{\bar{v}_{sr}^2 - \bar{v}_{ps}^2}{2g} + (Z_{sr} - Z_{ps}) - \sum H_{LT(sr-ps)} \\ &= \frac{-8665,954 \text{ Pa}}{990,84 \frac{\text{kg}}{\text{m}^3} \times 9,81 \frac{\text{m}}{\text{s}^2}} + \frac{0^2 \frac{\text{m}^2}{\text{s}^2} - 0,84041^2 \frac{\text{m}^2}{\text{s}^2}}{2 \times 9,81 \frac{\text{m}}{\text{s}^2}} + 0,684 \text{ m} - 0,0877 \text{ m}\end{aligned}$$

$$P_{ps} = -3220,283 \text{ Pa}$$

# CONDENSATE WATER SYSTEM

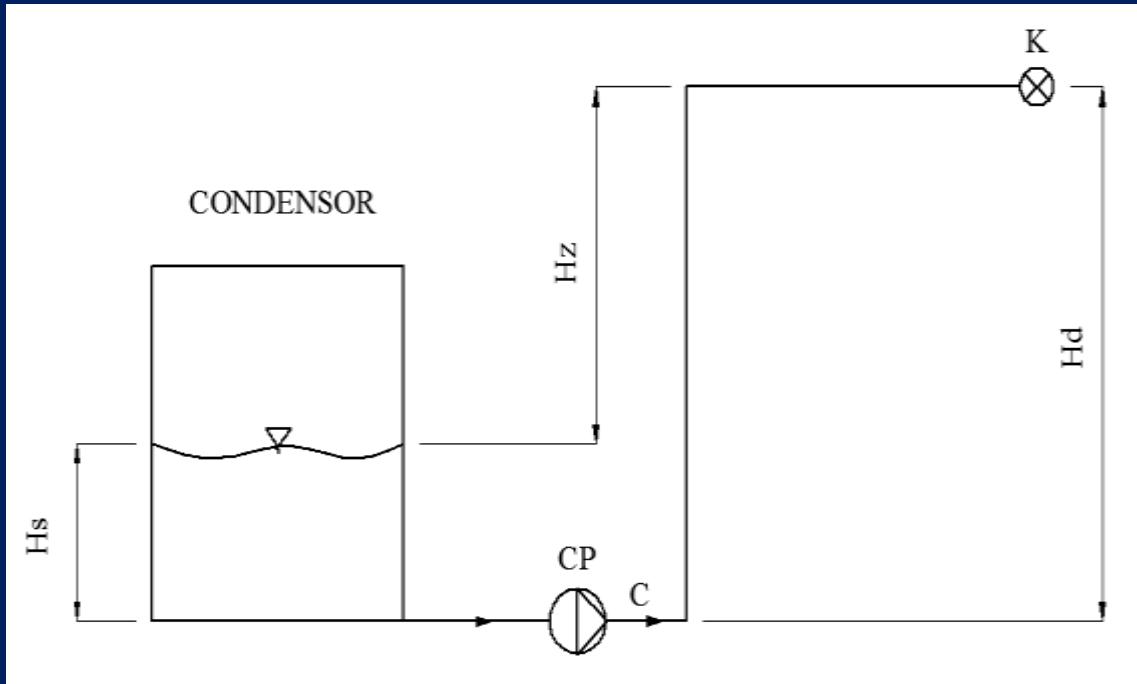
Perhitungan Tekanan Pd:



$$P_d = \left[ H_{eff} - \frac{(\bar{v}_d^2 - \bar{v}_s^2)}{2g} \right] \gamma + P_s$$
$$= \left[ 205 \text{ m} - \frac{2,38394^2 \frac{\text{m}^2}{\text{s}^2} - 0,84041^2 \frac{\text{m}^2}{\text{s}^2}}{2 \times 9,81 \frac{\text{m}}{\text{s}^2}} \right] = 1,987 \text{ Mpa}$$

# CONDENSATE WATER SYSTEM

Perhitungan Tekanan di Titik K:

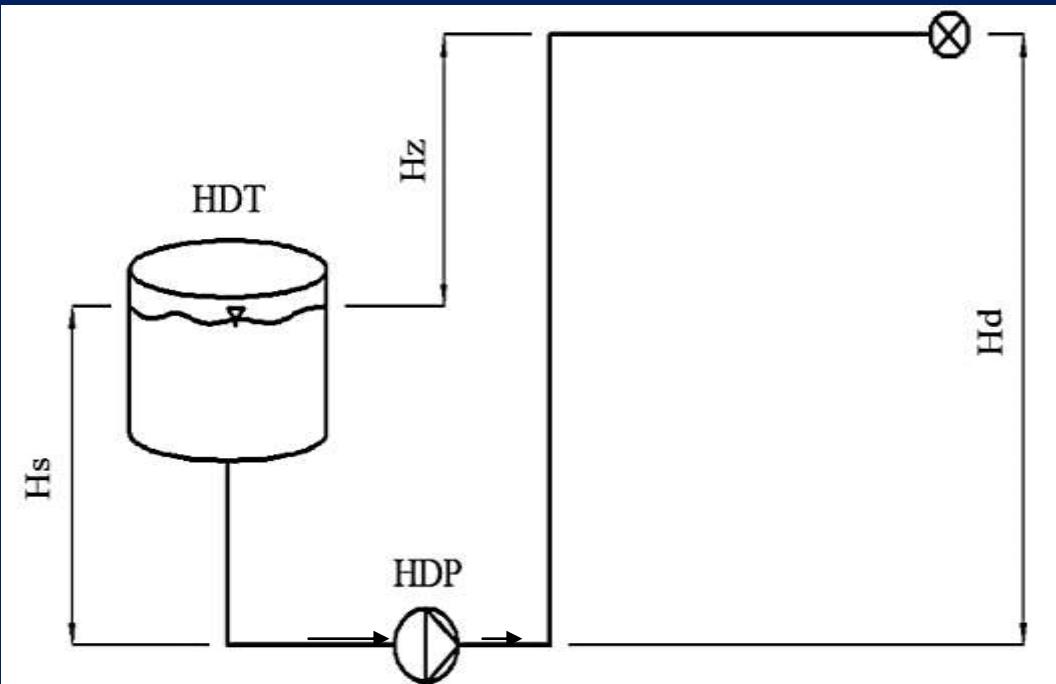


$$\frac{P_k}{\gamma} = \frac{P_c}{\gamma} + \frac{\bar{v}_c^2 - \bar{v}_k^2}{2g} + (Z_c - Z_k) - \sum H_{LT}(c-K)$$

$$P_k = \left[ \frac{1,987 \times 10^6 \text{ Pa}}{990,84 \frac{\text{kg}}{\text{m}^3} \times 9,81 \frac{\text{m}}{\text{s}^2}} \times \frac{\text{N}}{\text{Pa} \cdot \text{m}^2} \times \frac{\text{kg} \cdot \text{m}}{\text{N} \cdot \text{s}^2} \right] + (-29,0952 \text{ m}) = 1,665 \text{ Mpa}$$

# FEED WATER HEATER DRAIN SYSTEM

Perhitungan Head Statis :



$$\begin{aligned} H_{statis} &= \left[ \frac{P_{dr} - P_{sr}}{\gamma} \right] + (H_d - H_s) \\ &= \left[ \frac{1,665 \text{ Mpa} - 0,064 \text{ Mpa}}{965,85 \frac{\text{kg}}{\text{m}^3} \times 9,81 \frac{\text{m}}{\text{s}^2}} \right] + (2,313 - 3,26)m \\ &= \left[ \frac{(1,665 - 0,064) \times 10^6 \text{ pa}}{965,85 \frac{\text{kg}}{\text{m}^3} \times 9,81 \frac{\text{m}}{\text{s}^2}} \times \frac{\text{N}}{\text{Pa} \cdot \text{m}^2} \times \frac{\text{kg} \cdot \text{m}}{\text{N} \cdot \text{s}^2} \right] + (-0,947 \text{ m}) \\ &= 168,971 - 0,947 \text{ m} \\ &= 168,024 \text{ m} \end{aligned}$$

# FEED WATER HEATER DRAIN SYSTEM

## Perhitungan Kapasitas Nominal Pompa:

$$\dot{m} = 102,206 \frac{\text{ton}}{\text{jam}} \times \frac{1000 \text{ kg}}{\text{ton}} \times \frac{\text{jam}}{3600 \text{ s}} \\ = 28,39 \frac{\text{kg}}{\text{s}}$$

Dari tabel B.1 (Properties of Water) (Lampiran 7), dengan  $T_1 = 89,2 \text{ }^{\circ}\text{C}$  maka di dapatkan massa jenis air sebesar:

$$\rho = 965,85 \frac{\text{kg}}{\text{m}^3}$$

$$Q = \frac{\dot{m}}{\rho} = \frac{28,39 \frac{\text{kg}}{\text{s}}}{965,85 \frac{\text{kg}}{\text{m}^3}}$$

$$= 0,0294 \frac{\text{m}^3}{\text{s}}$$

## Perhitungan Kapasitas Setiap Section:

$$Q_{(L-K)} = \frac{\dot{m}}{\rho} \\ = \frac{28,39 \frac{\text{kg}}{\text{s}}}{965,85 \frac{\text{kg}}{\text{m}^3}} = 0,0294 \frac{\text{m}^3}{\text{s}}$$

Section	Kapasitas
L - M	0,0294
N - O	0,0294
O - K	0,0294

# FEED WATER HEATER DRAIN SYSTEM

Perhitungan Kecepatan Setiap Section:

$$\begin{aligned}\bar{v}_{L-M} &= \frac{Q_{L-M}}{A_{L-M}} \\&= \frac{4Q_{L-M}}{\pi(D_{L-M})^2} \\&= \frac{4 \times 0,0294 \frac{m^3}{s}}{\pi(0,202717)^2 m^2} \\&= 0,9109 \frac{m}{s}\end{aligned}$$

Section	Kecepatan
L - M	0,9109
N - O	1,5773
O - K	2,2778

# FEED WATER HEATER DRAIN SYSTEM

## Perhitungan Head Loss Mayor:

$$Re = \frac{0,9109 \frac{m}{s} \times 0,154051 \text{ m}}{3,2588 \times 10^{-7} \frac{m^2}{s}} = 5,6664 \times 10^5$$

$$\frac{e}{D} = \frac{0,046 \text{ mm}}{202,717 \text{ mm}} = 0,00023$$

$$\frac{1}{\sqrt{f}} = -2 \log \left( \frac{\frac{e}{D}}{3,7} + \frac{2,51}{Re \sqrt{f}} \right)$$



$$f = 0,0155$$

$$Hl_{LM} = 0,0155 \times \frac{3,9 \text{ m}}{0,202717} \times \frac{0,9109^2 \frac{m^2}{s^2}}{2 \times 9,81 \frac{m}{s}} = 0,0126 \text{ m}$$

Section	Head Loss Mayor
L – M	0,0126
N – O	0,0321
O – K	0,4862

# FEED WATER HEATER DRAIN SYSTEM

## Perhitungan Head Loss Minor:

Kerugian pada pipe entrance rounded k=0,24 pada diameter pipe size 8 inch (lampiran 11), maka head loss minornya:

$$H_{lm} = K \times \frac{\bar{v}_{LM}^2}{2g}$$

$$= 0,24 \times \frac{0,9109^2 \frac{m^2}{s^2}}{2 \times 9,81 \frac{m}{s^2}}$$

$$= 0,0101 m$$

Section	Head Loss Minor
L – M	0,0842
N – O	0,7646
O – K	1,3672

$$\sum H_{loss\ total} = \sum H_{loss\ mayor} + \sum H_{loss\ minor}$$
$$= 0,5309 m + 2,2160 m$$
$$= 2,7469 m$$

# FEED WATER HEATER DRAIN SYSTEM

Perhitungan Head Dynamis:

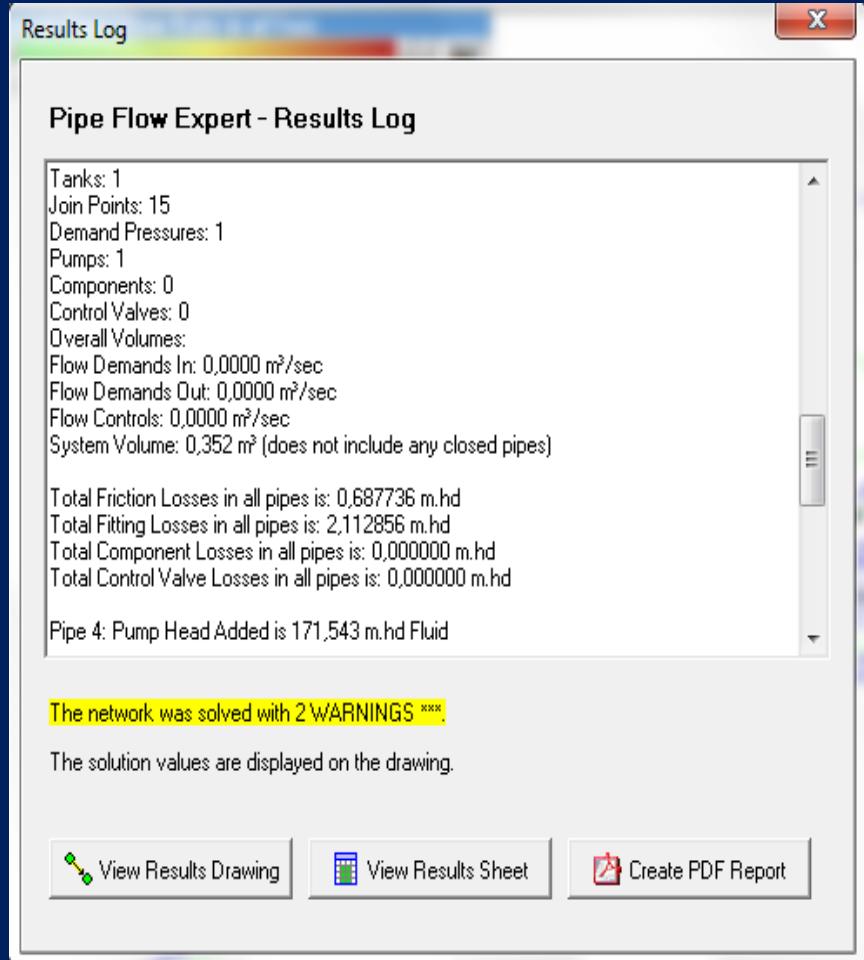
$$\begin{aligned} H_{dynamis} &= \left( \frac{\bar{v}_{dr}^2}{2g} \right) + \sum H_{loss\ total} \\ &= \left( \frac{2,2778^2 \frac{m^2}{s^2}}{2 \times 9,81 \frac{m}{s^2}} \right) + 2,7469\ m \\ &= 3,0113\ m \end{aligned}$$

**Perhitungan Head Effektif  
Instalasi**

$$\begin{aligned} H_{eff} &= H_{statis} + H_{dynamis} \\ &= 168,024\ m + 3,0113\ m \\ &= 171,0353\ m \end{aligned}$$

# FEED WATER HEATER DRAIN SYSTEM

## Head Effektif Instalasi Secara Numerik:



$$\text{Tingkat kesalahan} = \frac{H_{eff} - H_{eff\ PFE}}{H_{eff}} \times 100\%$$

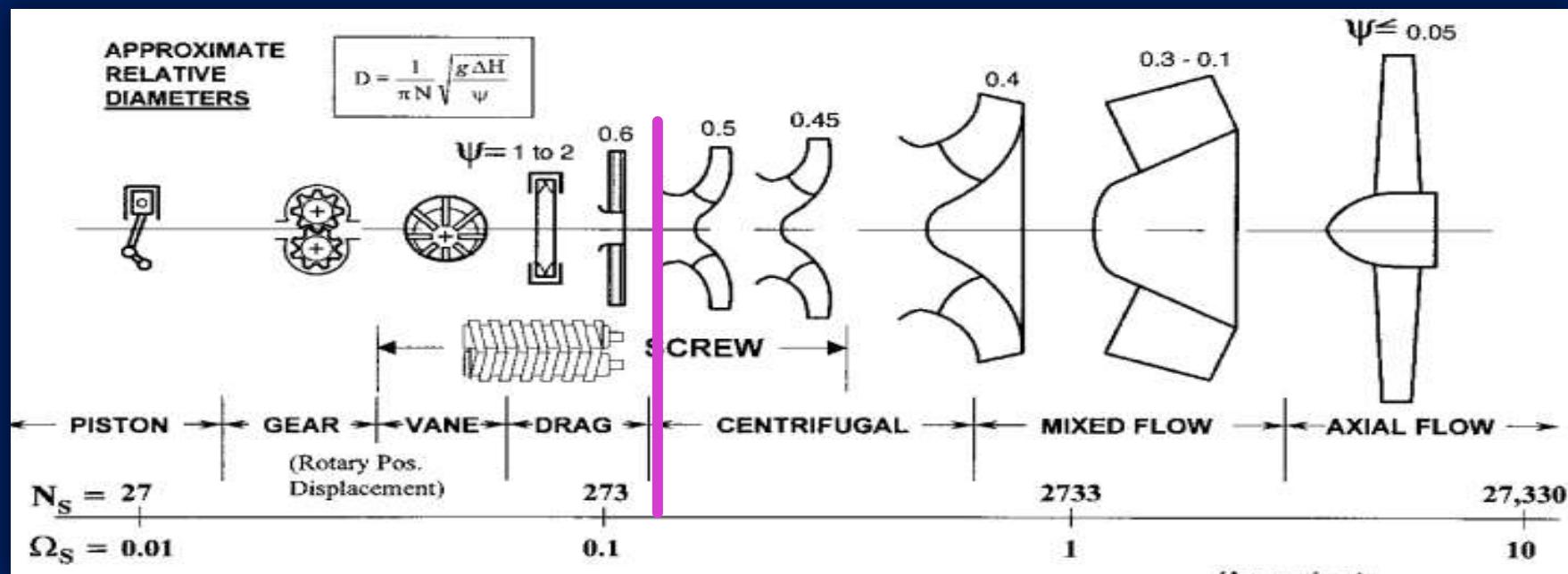
$$\text{Tingkat kesalahan} = \frac{171,0353\ m - 171,543\ m}{171,0353\ m} \times 100\%$$

$$\text{Tingkat kesalahan} = 0,3\%$$

# FEED WATER HEATER DRAIN SYSTEM

Pemilihan Pompa Berdasarkan Putaran Spesifik:

$$n_s = n \frac{\sqrt{Q}}{H_{eff}^{3/4}} = 1500 \text{ rpm} \frac{\sqrt{1,764 \frac{m^3}{min} \times \frac{gal}{3,785 \times 10^{-3} m^3}}}{\left( 171,0353 \text{ m} \times \frac{ft}{0,3048 \text{ m}} \right)^{3/4}} = 280,87$$



# FEED WATER HEATER DRAIN SYSTEM

Menentukan Jumlah Stage:

$$n_s = 3,65 \times 1500 \text{ rpm} \frac{\sqrt{0,0294 \frac{m^3}{s}}}{(171,0353 m)^{3/4}} = 19,85$$

Centrifugal pumps			Mixed-flow impeller	Axial-flow impeller
Low-speed impeller	Moderate-speed impeller	High-speed impeller		
				
$n_{s1} = 40-80$	$n_{s1} = 80-150$	$n_{s1} = 150-300$		
$\frac{D_2}{D_0} \approx 2.5$	$\frac{D_2}{D_0} \approx 2$	$\frac{D_2}{D_0} \approx 1.8-1.4$	$n_{s1} = 300-600$	$n_{s1} = 600-2000$
			$\frac{D_2}{D_0} \approx 1.2-1.1$	$\frac{D_2}{D_0} \approx 0.8$

$$N_{s1} = 85$$

$$N_s = 19,85$$

$$i = \left( \frac{n_{s1}}{n_s} \right)^{4/3} = \left( \frac{85}{19,85} \right)^{4/3} = 6,95 \approx 7 \text{ stage}$$

# FEED WATER HEATER DRAIN SYSTEM

## Perhitungan NPSHa:

$$\begin{aligned}NPSH_A &= \frac{P_a - P_v}{\gamma} + H_S - \sum H_{LT} \\&= \frac{(0,064 - 0,06817) \times 10^6 Pa}{965,85 \frac{kg}{m^3} \times 9,81 \frac{m}{s^2}} + 3,26 m - 0,0968 m \\&= -0,4401 m + 3,26 m - 0,0968 m \\&= 2,72 m\end{aligned}$$

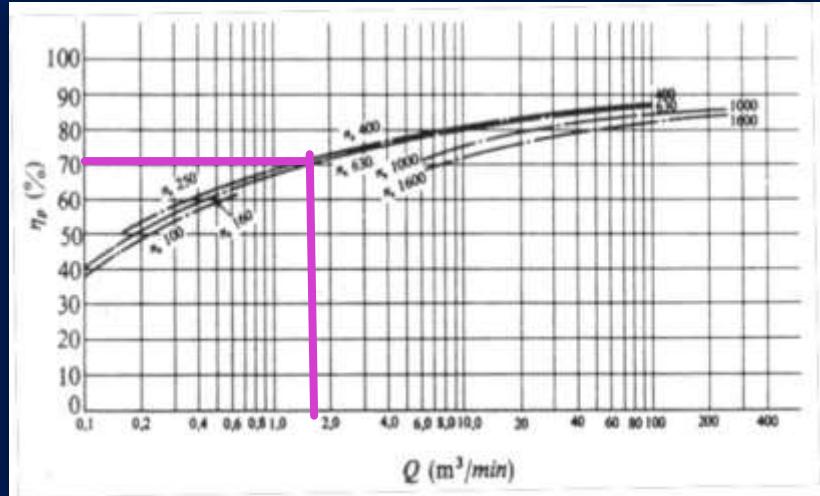
## Perhitungan WHP:

$$\begin{aligned}WHP &= \rho \times g \times Q \times H_{eff} \\WHP &= 965,85 \frac{kg}{m^3} \times 9,81 \frac{m}{s^2} \times 0,0294 \frac{m^3}{s} \times 171,0353 m \\&= 47644,39 Watt \\&= 47,644 kW\end{aligned}$$

# FEED WATER HEATER DRAIN SYSTEM

Perhitungan Pshaft:

$$P_{shaft} = \frac{WHP}{\eta_p} = \frac{47,644 \text{ kW}}{0,7} = 68,06 \text{ kW}$$



Perhitungan Pmotor:

$$\begin{aligned} P_m &= \frac{P_{shaft}(1 + \alpha)}{\eta_t} \\ &= \frac{68,06 \text{ kW}(1 + 0,2)}{1} \\ &= 81,67 \text{ kW} \end{aligned}$$

Jenis Penggerak Mula	$\alpha$
Motor Induksi	0,1 – 0,2
Motor Bakar Kecil	0,15 – 0,25
Motor Bakar Besar	0,1 – 0,2

# FEED WATER HEATER DRAIN SYSTEM

Penentuan Jenis Pompa:

## Perhitungan

- $Q = 1,764 \text{ m}^3/\text{min}$
- $H_{\text{eff}} = 171,0353 \text{ m}$
- Stage = 7
- NPSHa = 2,72 m
- $P_m = 81,67 \text{ kW}$

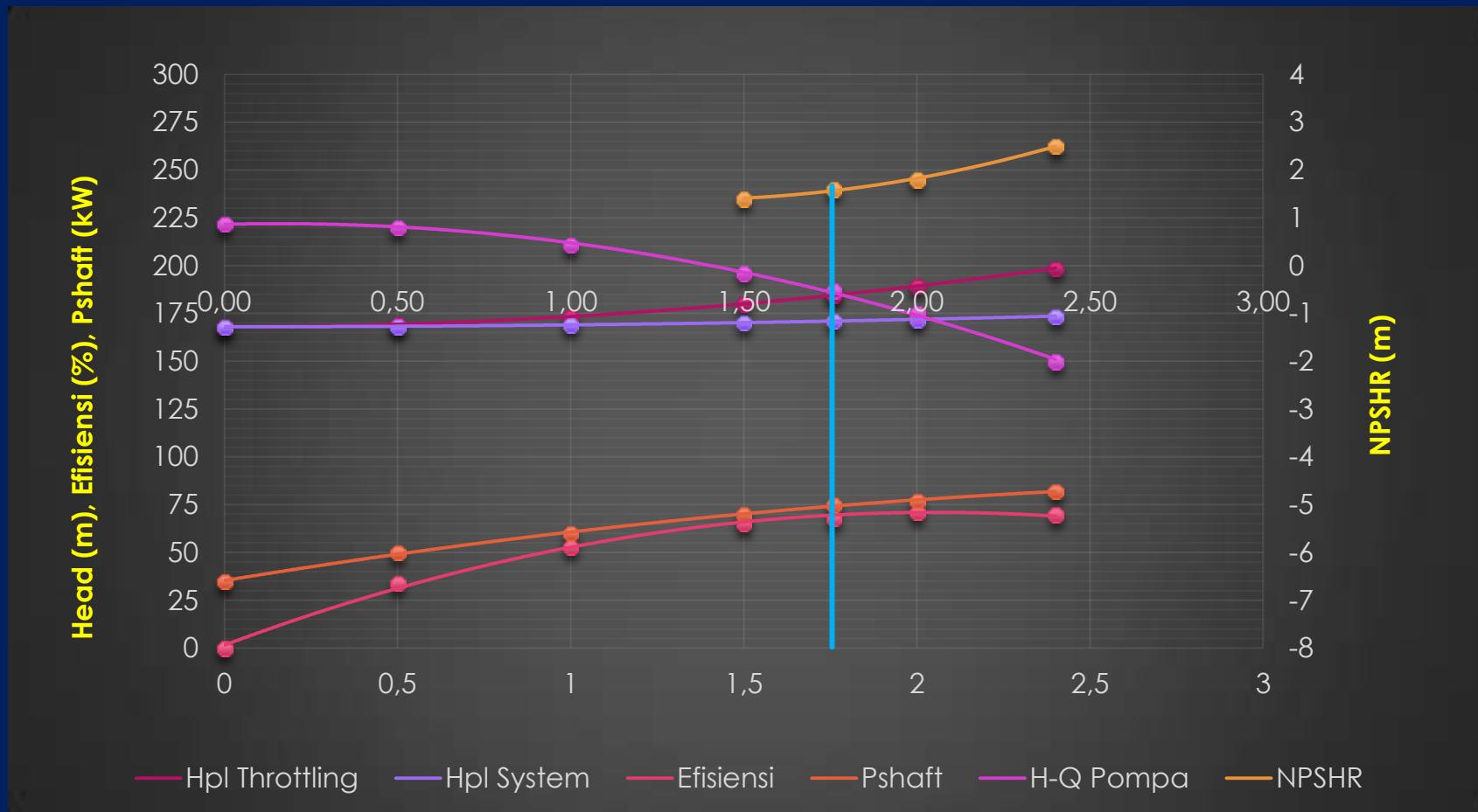
## Data Pompa

- $Q = 2 \text{ m}^3/\text{min}$
- Head = 175 m
- Stage = 7
- NPSHr = 2,1 m
- $P_m = 85 \text{ kW}$

**Pompa centrifugal multistage moderate speed impeller**

# FEED WATER HEATER DRAIN SYSTEM

## Karaktersistik Kerja Secara Analitis:



**Head Thrott = 184,59 m**

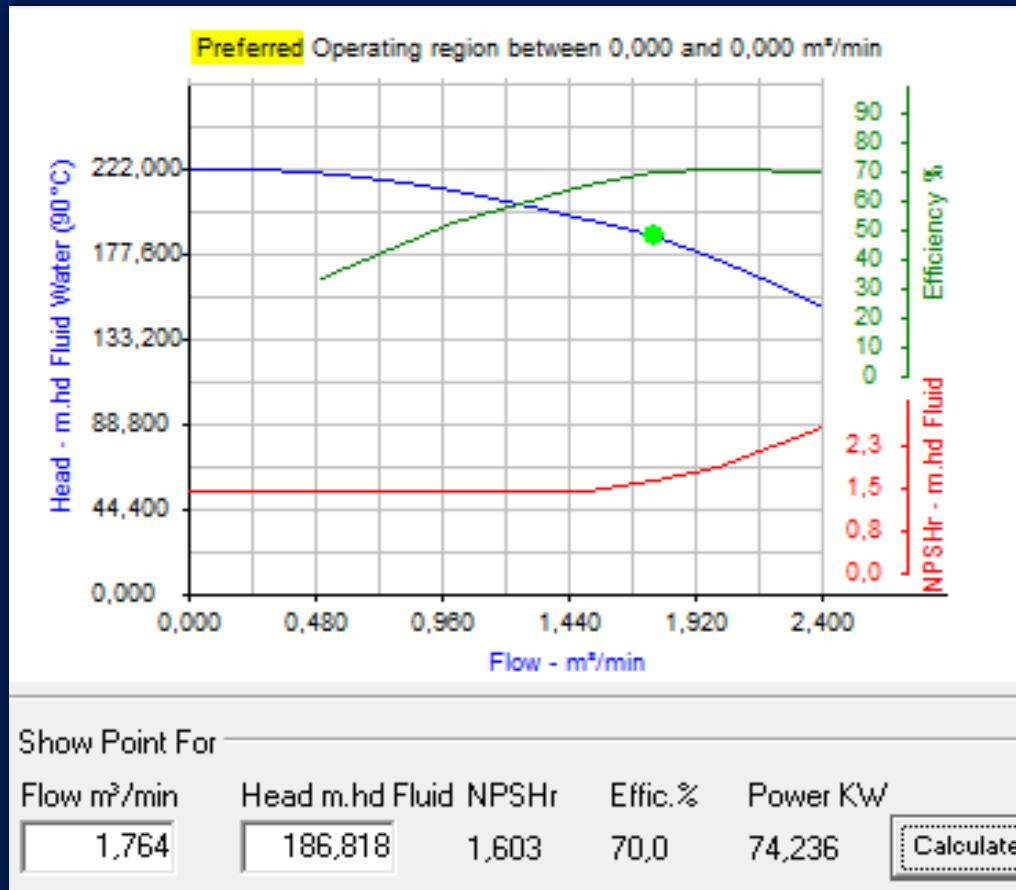
**Efisiensi = 70%**

**NPSHr = 1,6 m**

**Pshaft = 75 kW**

# FEED WATER HEATER DRAIN SYSTEM

## Karaktersistik Kerja Secara Numerik:



**Head Thrott = 186,818 m**

**Efisiensi = 70%**

**NPSHr = 1,603 m**

**Pshaft = 74,236 kW**

# FEED WATER HEATER DRAIN SYSTEM

Perbandingan Karaktersistik Kerja Secara  
Analitis & Karaktersistik Kerja Secara Numerik:

## Analitis



■  $H_{thrott} = 184,59 \text{ m}$

■  $NPSH_r = 1,6 \text{ m}$

■ Efisiensi = 70%

■  $P_{shaft} = 75 \text{ kW}$

## Numerik



■  $H_{thrott} = 186,818 \text{ m}$

■  $NPSH_r = 1,603 \text{ m}$

■ Efisiensi = 70%

■  $P_{shaft} = 74,236 \text{ kW}$

## Error

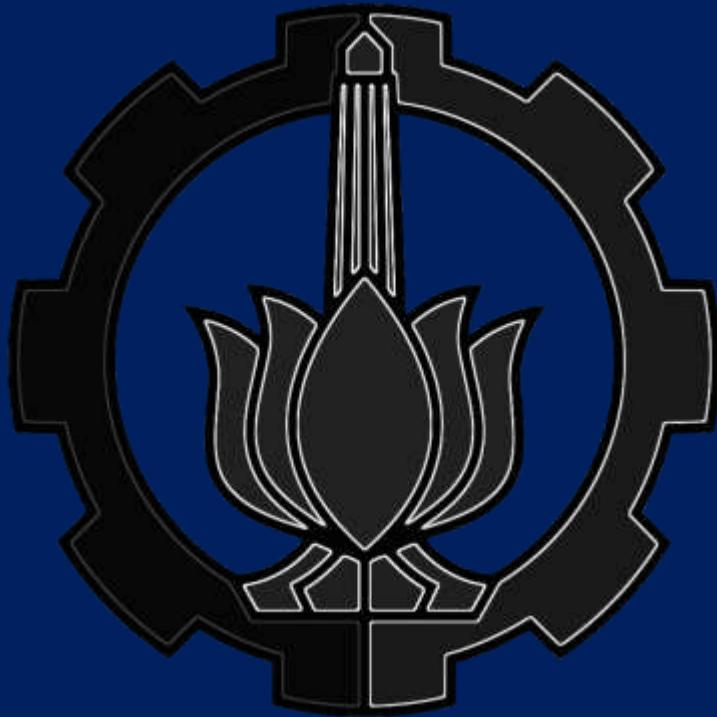


■ Error = 1,2%

■ Error = 0,19%

■ Error = 0%

■ Error = 1%



PENUTUP  
LITERASI

# KESIMPULAN

- ▶ Dari hasil perhitungan secara analitis didapatkan kapasitas pompa *Heater Drain Pump*  $105,84 \frac{m^3}{h}$ ,  $H_{eff} = 171,0353$  m,  $NPSH_A = 2,72$  m dan 7 stage.
- ▶ Pada perhitungan numerik dengan *software pipe flow expert v5.15* didapatkan nilai  $H_{eff\ PFE} = 171,543$  m. Jika dibandingkan dengan perhitungan secara analitis maka diketahui tingkat kesalahan perhitungan sebesar 0,3 %.
- ▶ Berdasarkan perhitungan diatas maka dipilih pompa sentrifugal multistage dengan kapasitas  $120 \frac{m^3}{h}$ ,  $H_{eff\ pompa} = 175$  m,  $NPSH_R = 2,1$  m dan 7 stage.
- ▶ Dari pemilihan pompa berdasarkan putaran spesifik, maka pemilihan pompa *Heater Drain Pump* dengan tipe TSM-7 pada PT. PJB UP Gresik PLTU Unit 3 sudah tepat.

# KESIMPULAN

- ▶ Pemilihan pompa sudah benar sehingga *backflow* terjadi karena rusaknya *swing check valve* dan terjadi kerusakan pada pompa.
- ▶ Perawatan yang dapat dilakukan untuk menjaga kehandalan kinerja pompa *Heater Drain Pump* ada 4 yaitu perawatan sebelum menjalankan pompa, perawatan selama pengoperasian, perawatan untuk penghentian pompa dan perawatan tahunan (*assembly* dan *diassembly*).

# SARAN

- ▶ Manajemen perawatan pada feed water heater drain system dilakukan secara teratur dan terjadwal mulai dari *Preventive Maintenance, Predictive Maintenance, Corrective Maintenance, dan Breakdown Maintenance* agar peralatan pada sistem instalasi mempunyai umur kerja yang panjang dengan performa yang maksimal.
- ▶ Perlu dijaga temperatur fluida kerja *heater drain pump* agar tidak melebihi 89,2 °C karena akan menyebabkan terjadinya keausan yang lebih cepat kepada pompa.