



SIDANG TUGAS AKHIR

DESAIN KONTROL KECEPATAN MOTOR BRUSHLESS DC BERBASIS *POWER FACTOR CORRECTION* (PFC) MENGUNAKAN *SINGLE ENDED PRIMARY INDUCTANCE CONVERTER* (SEPIC)

Dosen Pembimbing:

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1

**Latar
Belakang**

2

Tujuan

3

**Batasan
Masalah**

4

**Desain Kontrol
Kecepatan
dan PFC**

5

**Hasil dan
Pembahasan**

6

Kesimpulan

sample text

Outline



P. Yedamale (2003)

Lifetime tinggi

Respon dinamik baik

Efisiensi tinggi

Tidak ada percikan

Range kecepatan tinggi

Pengaplikasian

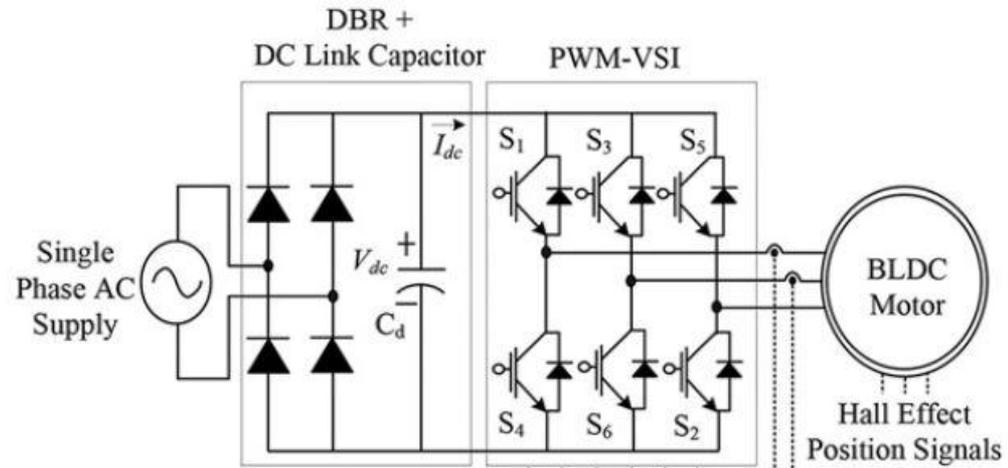
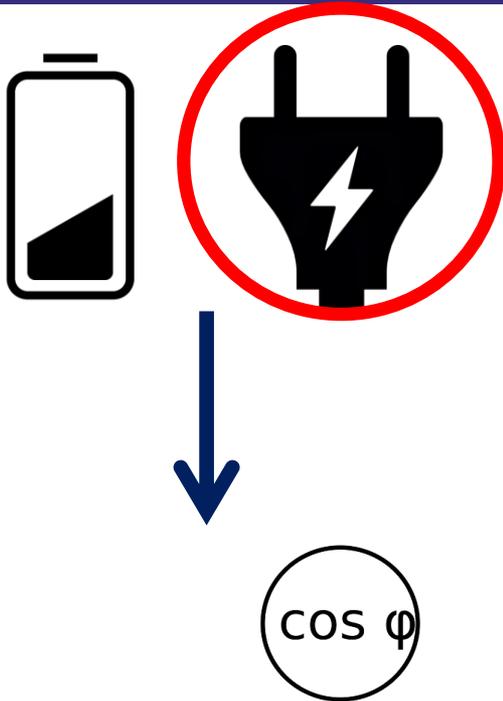
Pompa

Blower

Peralatan Medis



Latar Belakang



Rendahnya Faktor Daya



Tingginya Nilai THD Arus

PF

0.732

**THD
i**

74.39%



Tujuan

5 dari 30



1

Motor dapat dioperasikan pada tingkat kecepatan bervariasi

2

Motor dapat beroperasi pada tingkat pembebanan yang bervariasi

3

Memiliki PF dan THD yang memenuhi standar



1

Sumber yang digunakan merupakan sumber AC 220 rms

2

Motor brushless DC yang digunakan adalah motor brushless DC tiga fasa pabrikan Moog

3

Penelitian ini membahas tentang desain dan analisis simulasi, tidak membahas tentang implementasi secara langsung

4

Nilai *Gain* (K_p) dan *Time constant* (K_i) didapatkan dengan metode *trial and error*

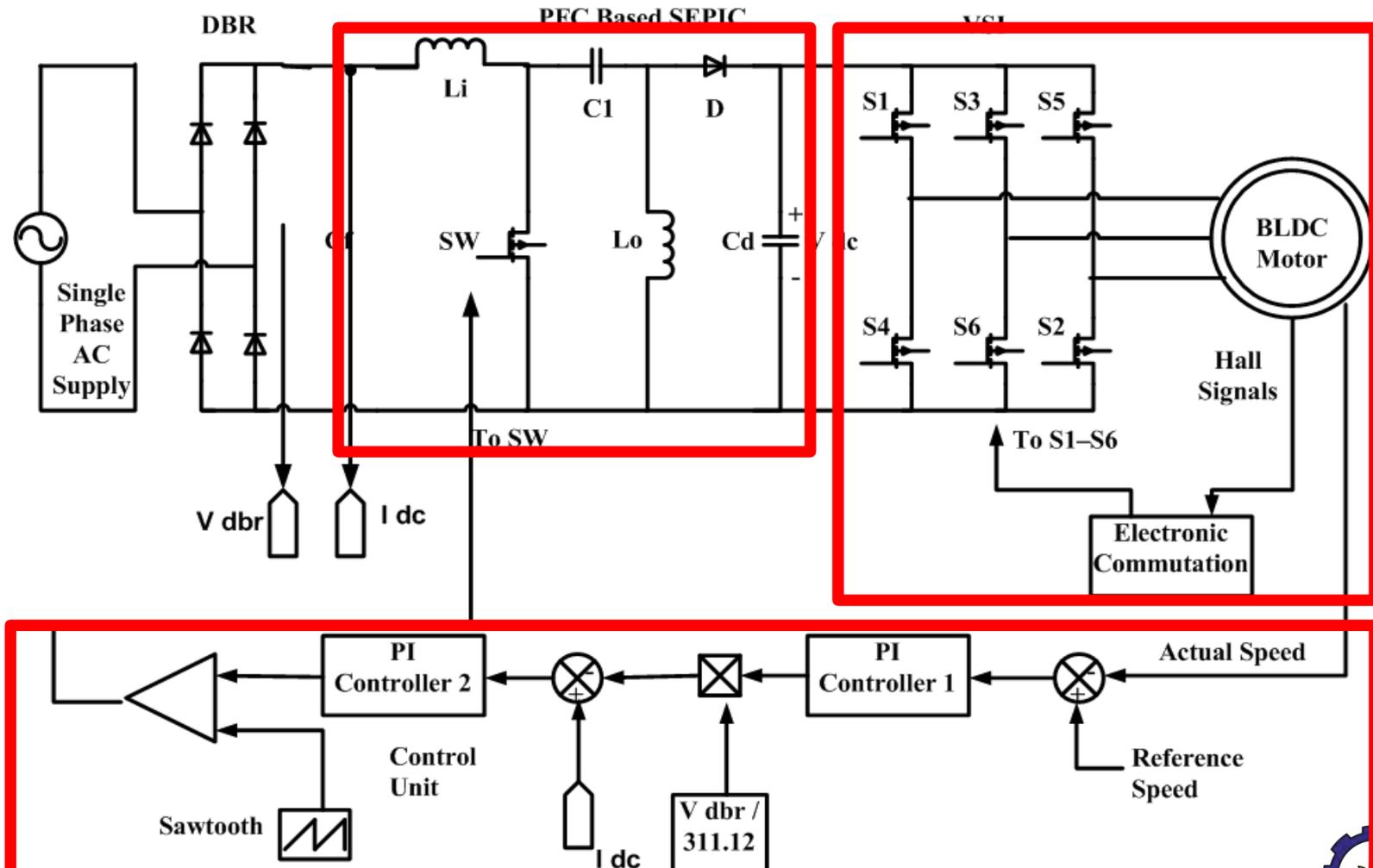


Datasheet Motor

Parameter	Nilai
Panjang	134.6 millimeter
Tegangan Terminal	100 Volt
Torsi Maksimal	18.0744 Nm
Kecepatan Rating	2500 Rpm
Torsi Rating	2.9588 Nm
Arus Rating	10.2 Ampere
Daya Rating	874 Watt
Sensitivitas Torsi	0.3269 Nm/Ampere
Back EMF	34.2 Volts/krpm
Resistansi	0.408 Ohm
Induktansi	1.71 mH
Inersia Rotor	4939.9 gr-cm ²
Berat	5168.8 gr
Timing	120 Derajat
Mech. Time Constant	1.9 ms
Electrical Time Constan	4.19 ms

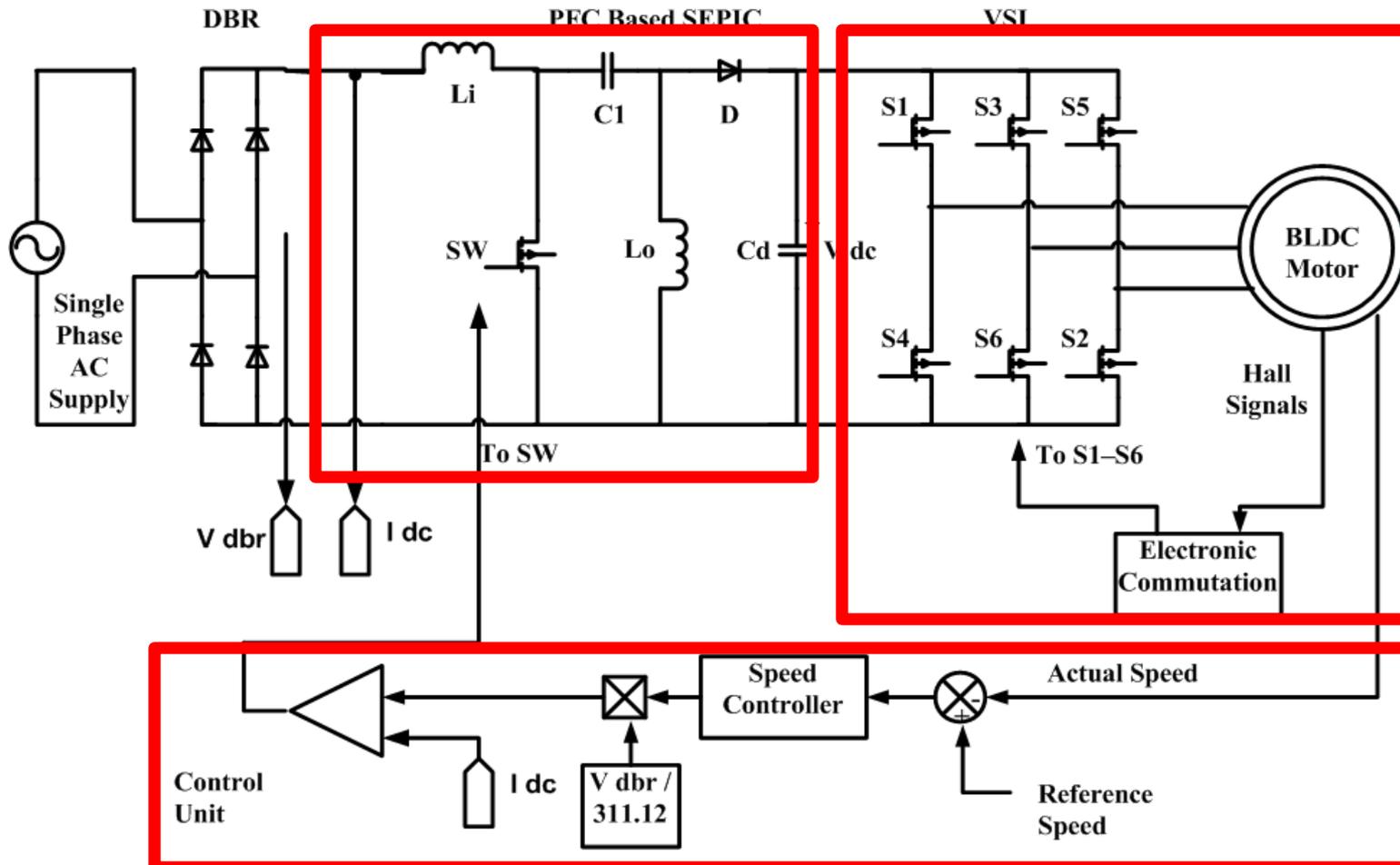


Average Current Control



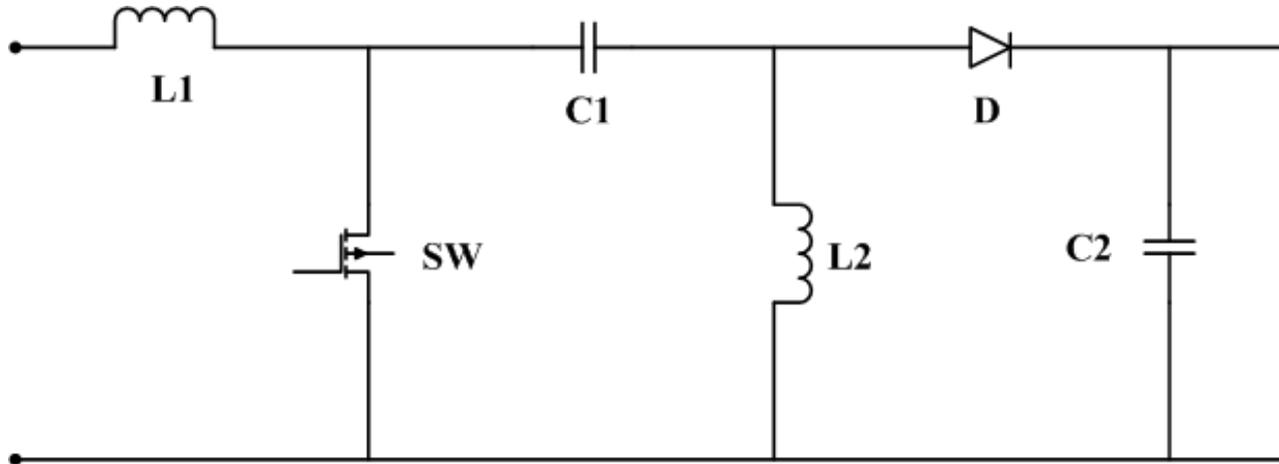


Hysteresis Current Control





Konverter SEPIC



V_s

220 V

Speed
max

2500 rpm

P_{max}

874 W

V_o

100 V

Speed
min

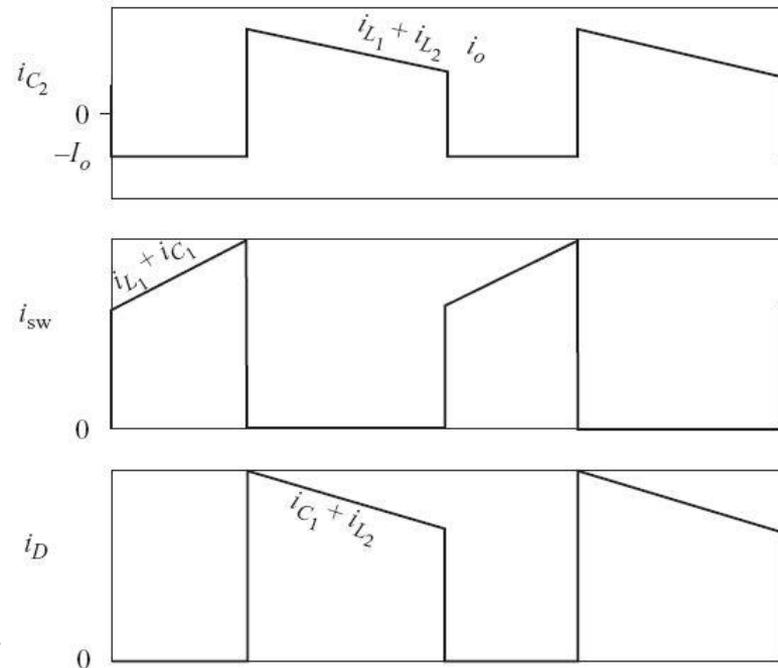
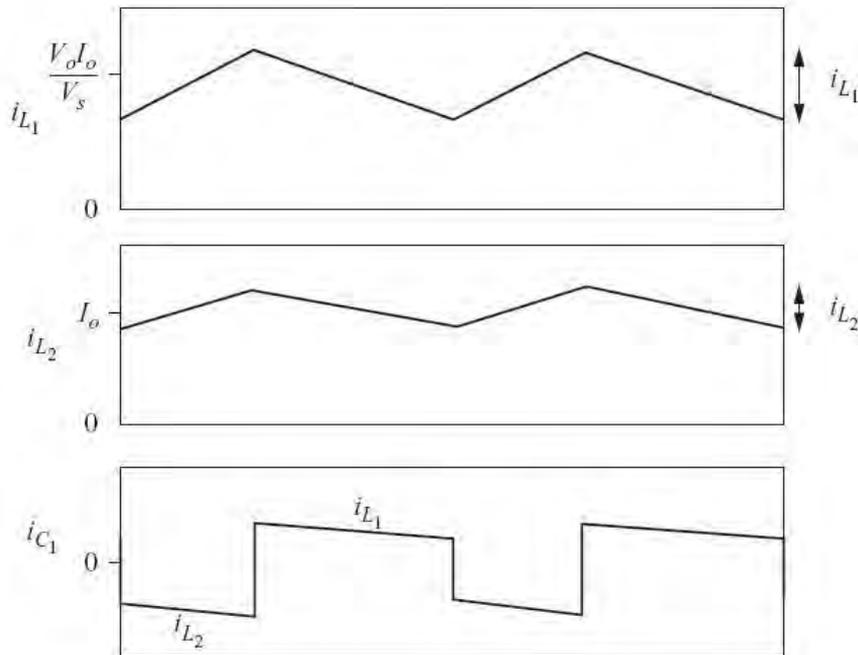
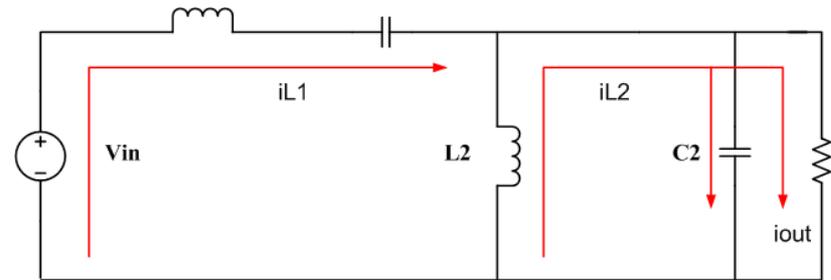
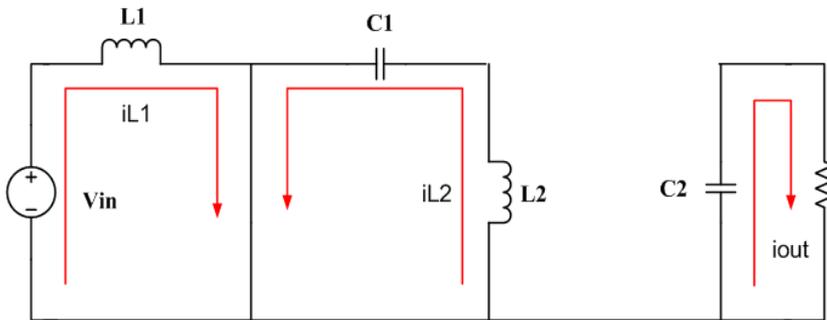
700 rpm

P_{min}

262 W



Mekanisme SEPIC





Nilai Induktor Input

$$L_1 = \frac{V_{in} \times D}{\Delta I_{L1} \times f}$$

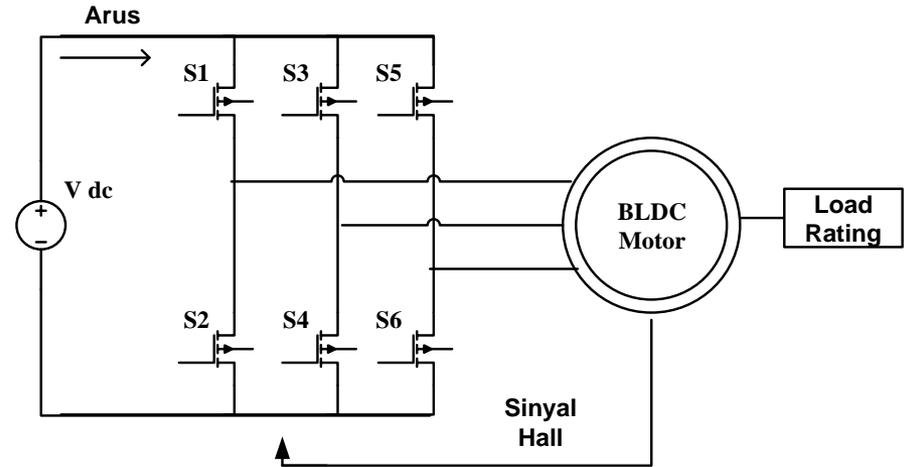


$$V_{in} = \frac{2\sqrt{2} V_s}{\pi} = \frac{2\sqrt{2} \times 220}{\pi} = 198 \text{ Volt}$$

$$D_n = \frac{V_{dc_link}}{V_{dc_link} + V_{rec}} = \frac{100}{100 + 198} = 0.3355$$

$$I_{L1} = \frac{100 \times 8.95}{198} = 4.52 \text{ Ampere}$$

$$\Delta I_{L1} \text{ (ripple 10\%)} = \frac{10}{100} \times I_{L1}$$



$$I_{L1} = \frac{V_o \times I_o}{V_{in}}$$

$$\Delta I_{L1} \text{ (ripple 10\%)} = \frac{10}{100} \times 4.52 = 0.452 \text{ Ampere}$$

$$L_1 = \frac{V_s \times D}{\Delta I_{L1} \times f} = \frac{198 \times 0.3355}{0.452 \times 20000} = 7.35 \text{ mH}$$



Nilai Induktor Output (CCM)

$$L_2 = \frac{V_{in} \times D}{\Delta I_{L2} \times f}$$

$$\Delta I_{L2} \text{ (ripple 10\%)} = \frac{10}{100} \times I_{out}$$

$$\Delta I_{L2} \text{ (ripple 10\%)} = \frac{10}{100} \times 8.95 = 0.895 \text{ Ampere}$$

$$L_2 = \frac{V_{in} \times D}{\Delta I_{L2} \times f} = \frac{198 \times 0.3355}{0.895 \times 20000} = \mathbf{3.71 \text{ mH}}$$

Nilai Induktor Output (DCM)

$$L_c = \frac{V_{in}^2}{P_{min}} \times \frac{V_{dc_min}}{2\sqrt{2}V_{inf}} \times \frac{V_{dc_min}}{\sqrt{2}V_{in} + V_{dc_min}}$$

$$L_c = \frac{220^2}{262} \times \frac{30}{2\sqrt{2} \times 220 \times 20000} \times \frac{30}{\sqrt{2} \times 220 + 30}$$

$$P_{min} = \frac{V_{dc_min}}{V_{dc_rating}} P_{rating}$$

$$P_{min} = \frac{30}{100} \times 874 = 262 \text{ Watt}$$

$$L_c = 0.039 \text{ mH}$$

$$L_c = \frac{0.039 \text{ mH}}{3}$$

$$L_c = \mathbf{0.013 \text{ mH}}$$





Nilai Kapasitor Intermediat

$$C_1 = \frac{P_{max}}{K \times f_s \times (\sqrt{2} V_{in} + V_{dc_link})^2}$$

$$C_1 = \frac{874}{0.25 \times 20000 \times (\sqrt{2} \times 220 + 100)^2}$$

$$C_1 = \mathbf{1.03 \mu F}$$

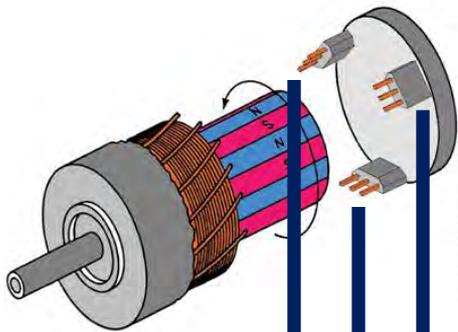
Nilai Kapasitor Output

$$C_2 = \frac{P_{rating}}{2 \times \omega \times \%ripple \times V_{dc_rating}^2}$$

$$C_2 = \frac{874}{2 \times 314 \times 0.03 \times 100^2} = \mathbf{4.63 mF}$$



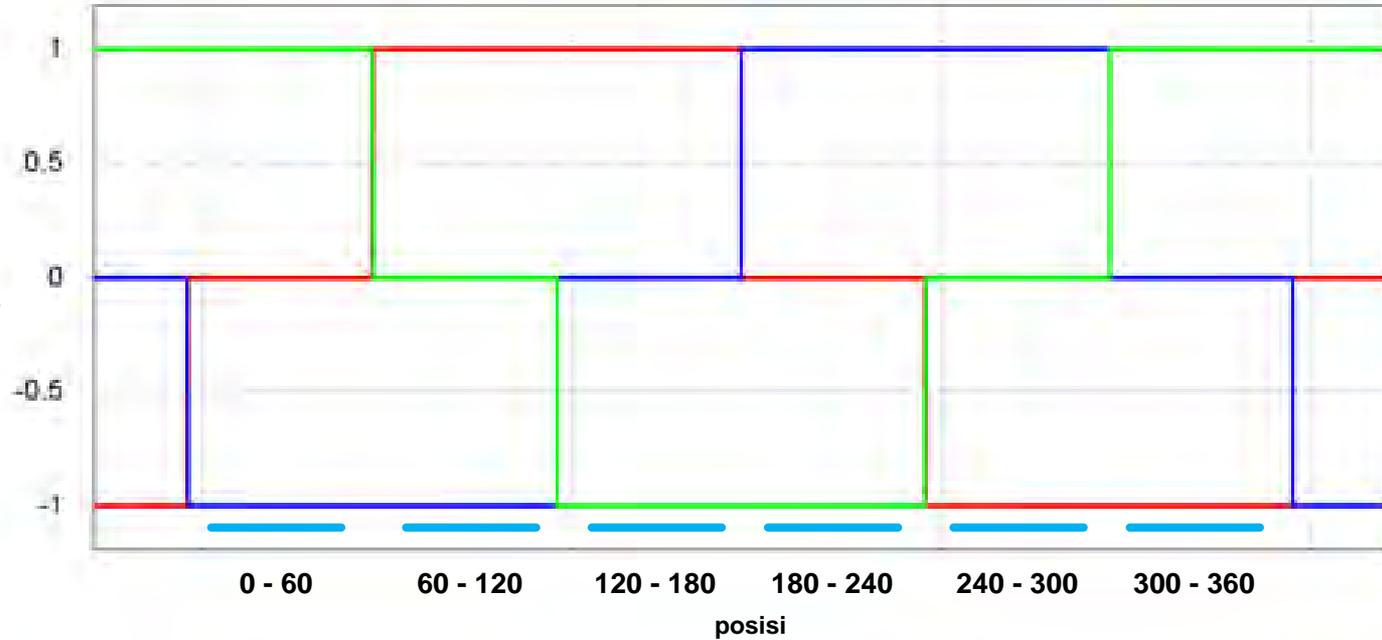
VSI - BLDC



Hall 1

Hall 2

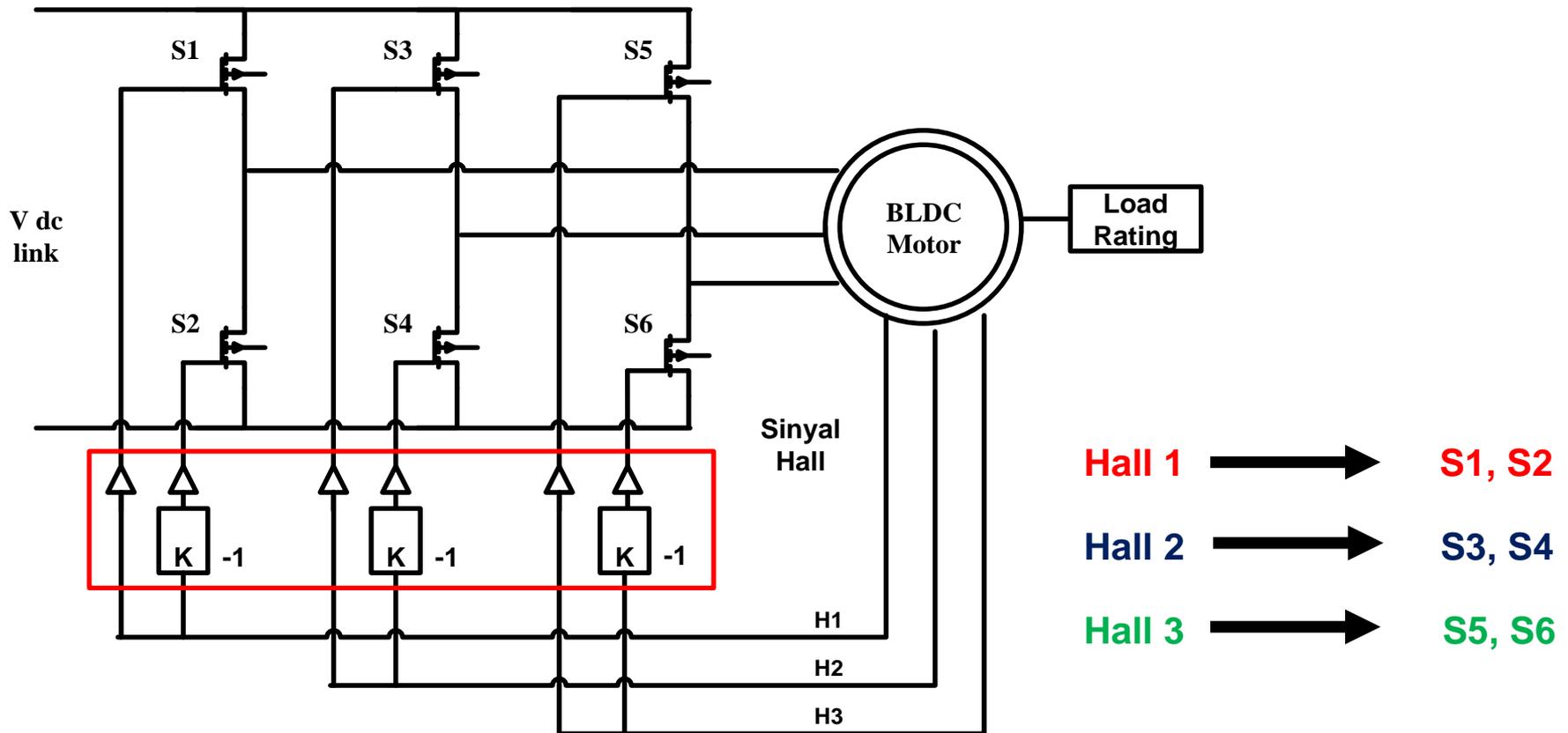
Hall 3



— Hall 1
— Hall 2
— Hall 3



VSI - BLDC

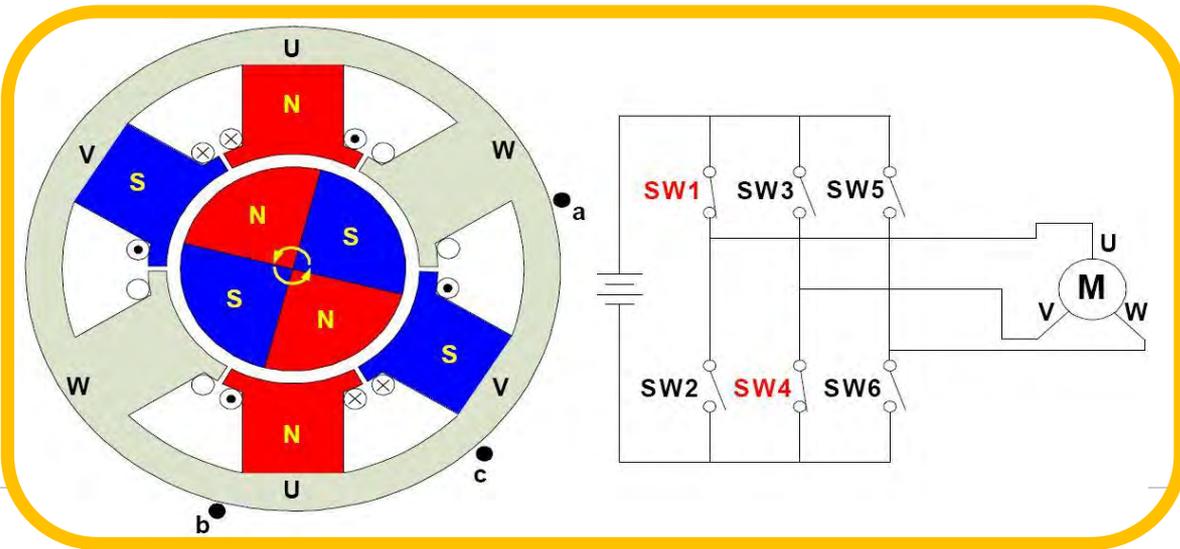
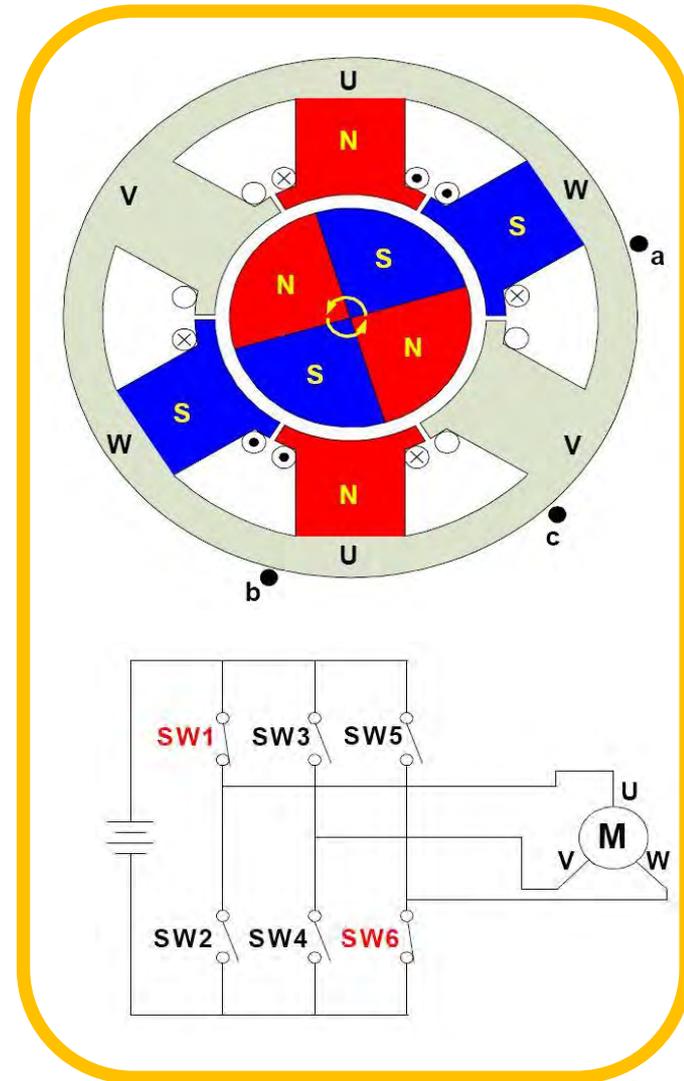




Desain Sistem Kontrol

VSI - BLDC

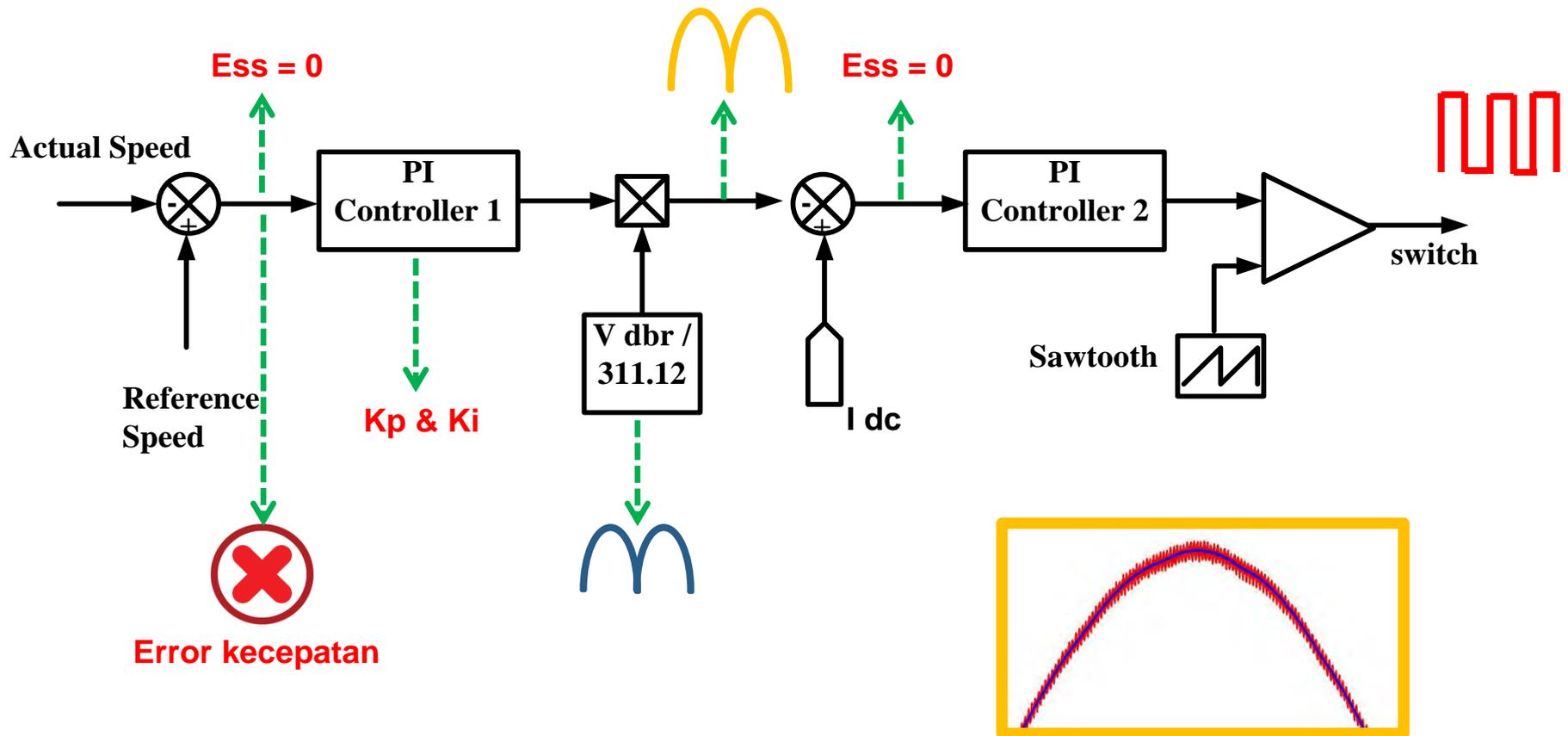
Interval switching	Sensor Hall			Switch ON	
	H1	H2	H3		
$0^{\circ}-60^{\circ}$	0	-1	1	S1	S4
$60^{\circ}-120^{\circ}$	1	-1	0	S1	S6
$120^{\circ}-180^{\circ}$	1	0	-1	S3	S6
$180^{\circ}-240^{\circ}$	0	1	-1	S3	S2
$240^{\circ}-300^{\circ}$	-1	1	0	S5	S2
$300^{\circ}-360^{\circ}$	-1	0	1	S5	S4





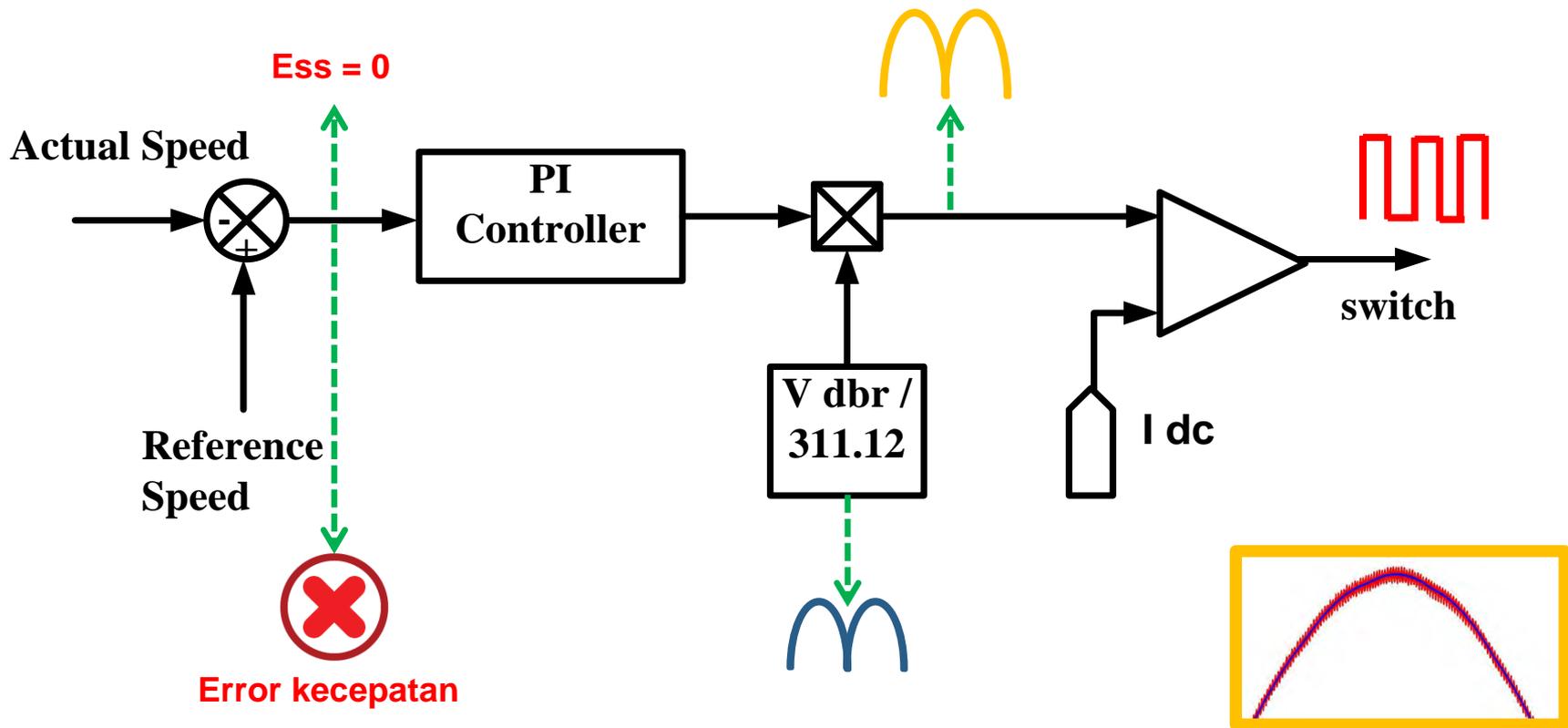
Desain Sistem Kontrol

Average Current Control





Hysteresis Current Control





1

CCM Hysteresis

2

CCM Average

3

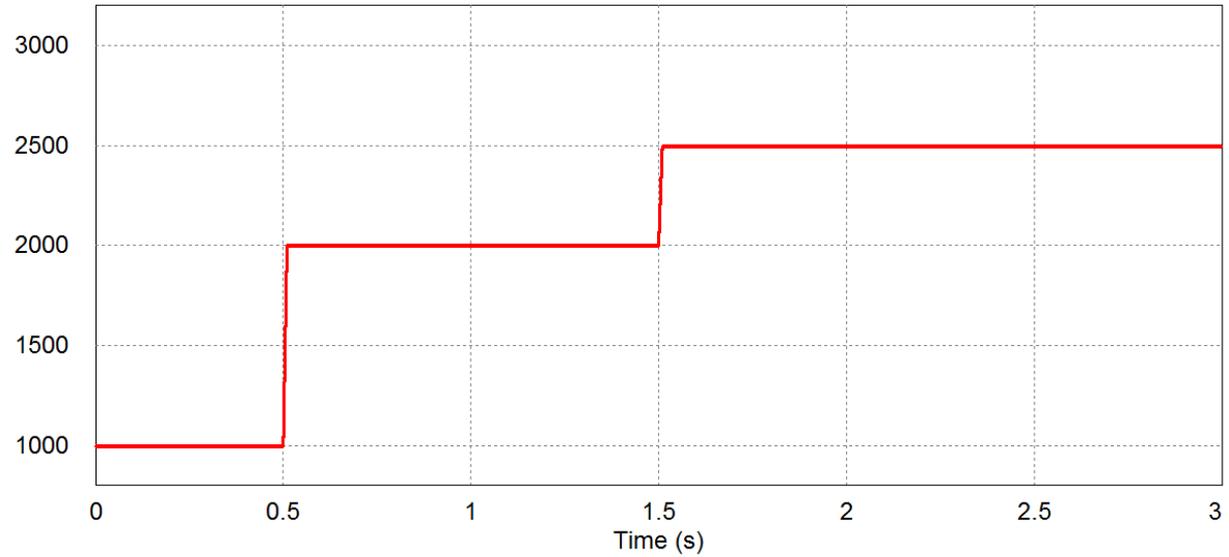
DCM Hysteresis

4

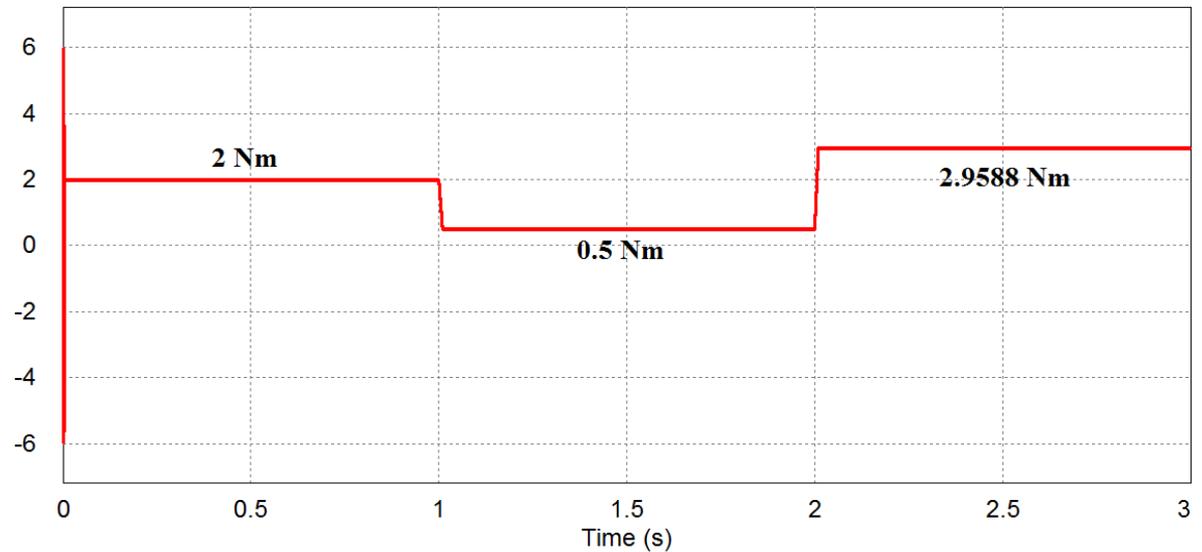
DCM Average



Skenario Kecepatan

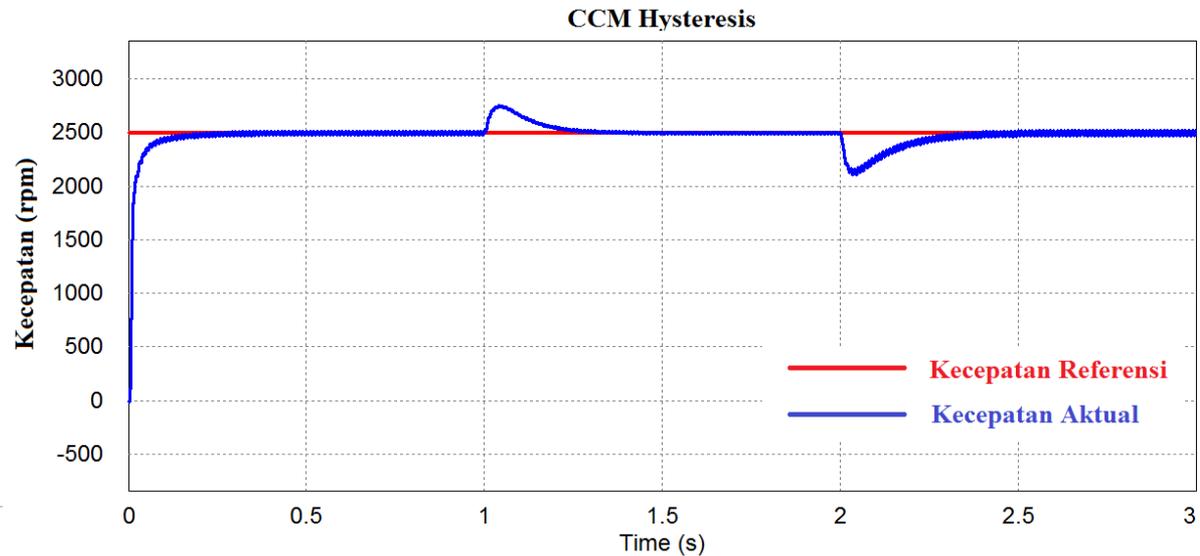
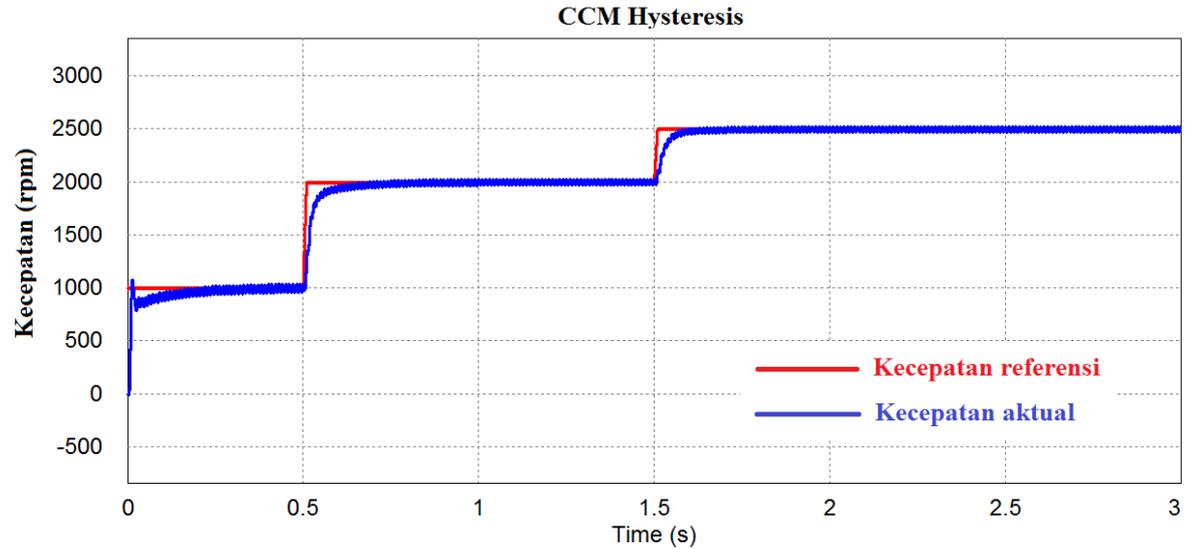


Skenario Pembebanan



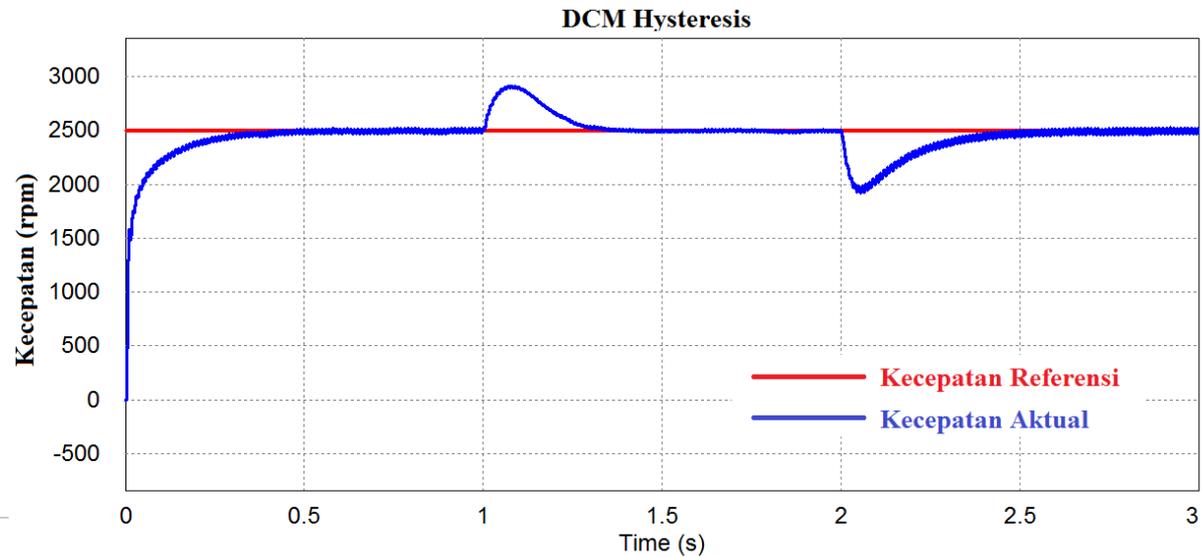
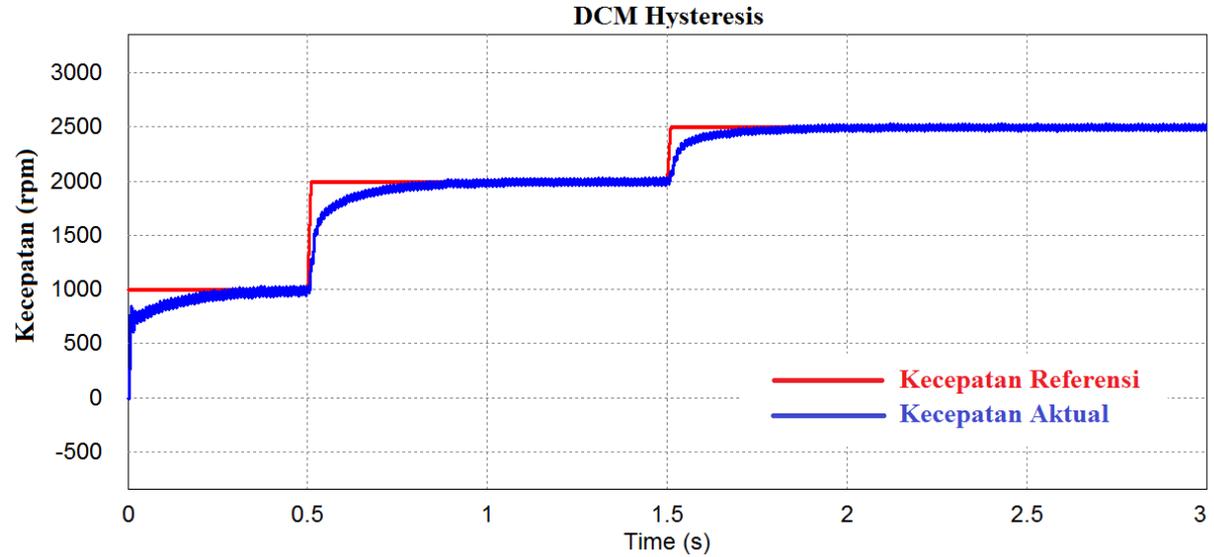


CCM Hysteresis





DCM Hysteresis

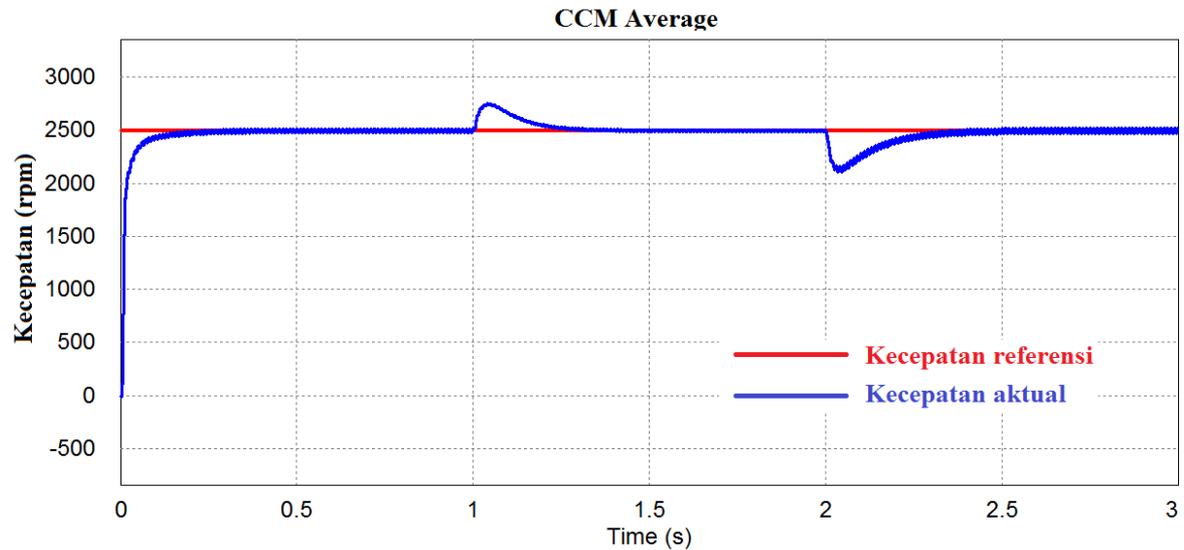
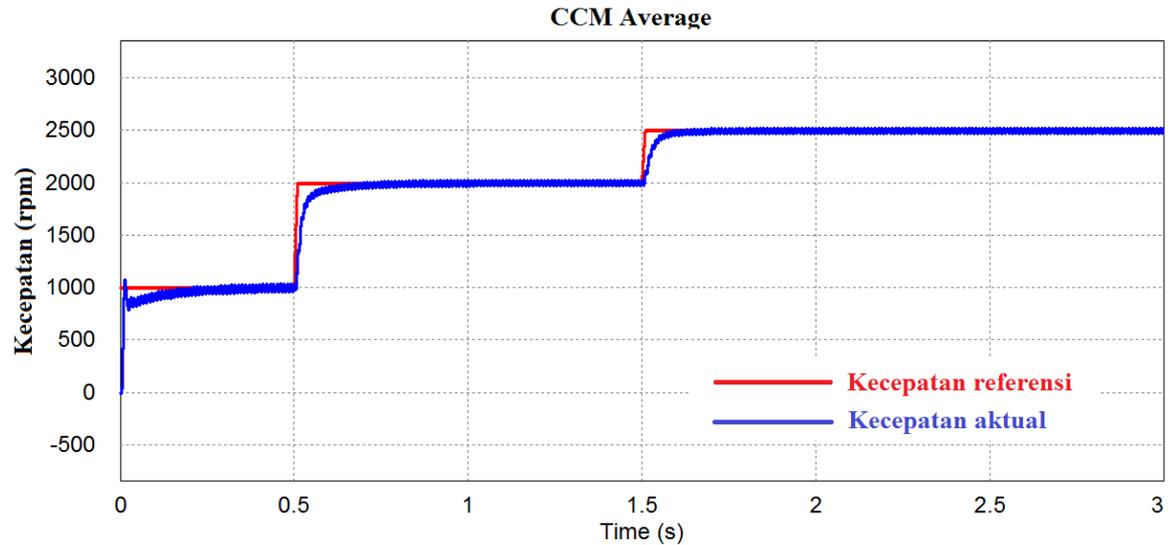




Hasil dan Pembahasan

24 dari 30

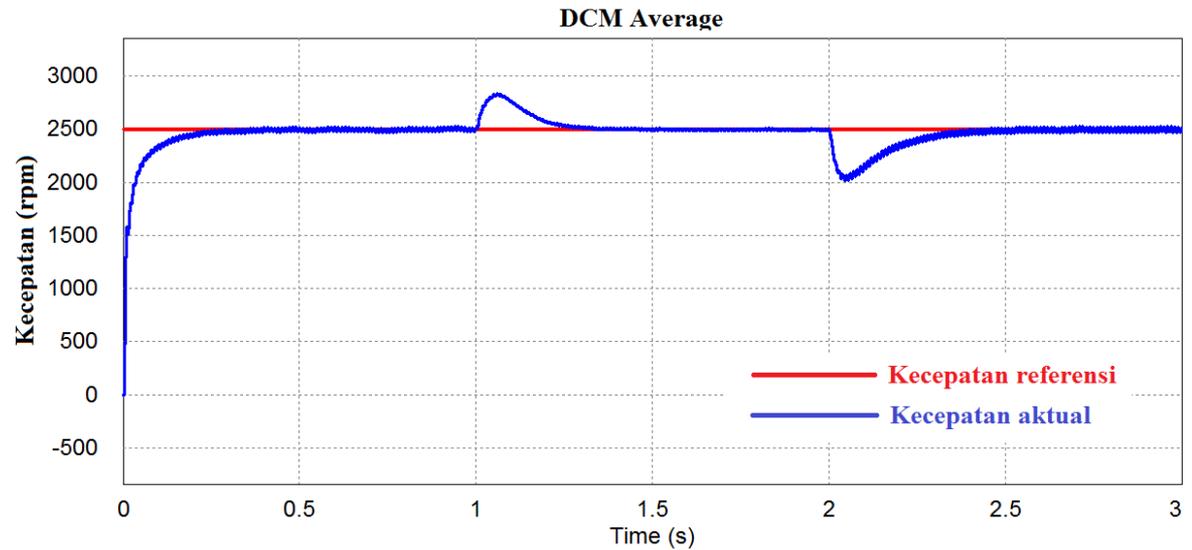
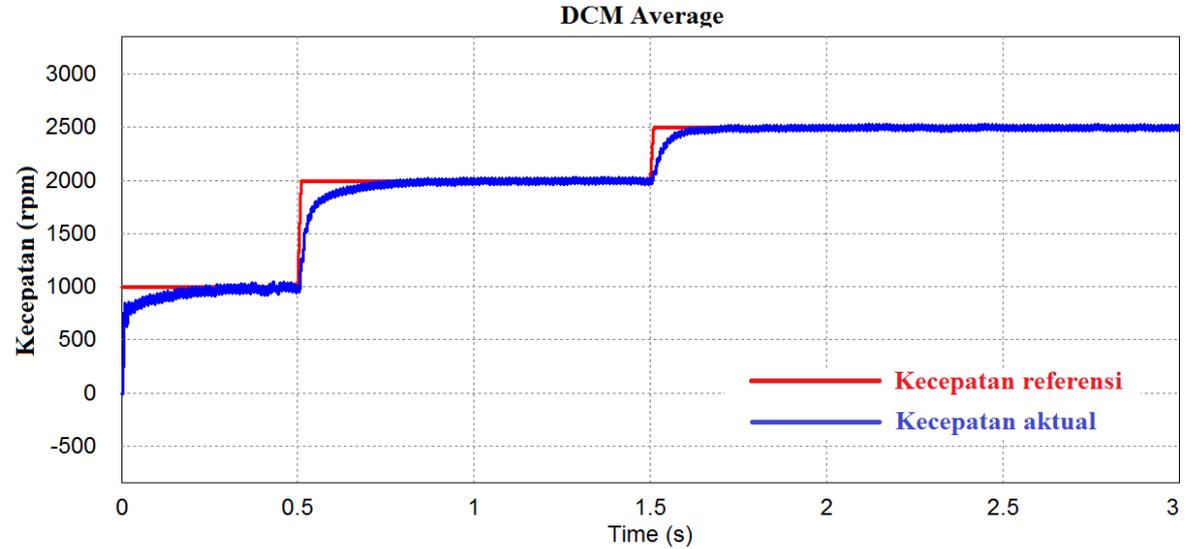
CCM Average





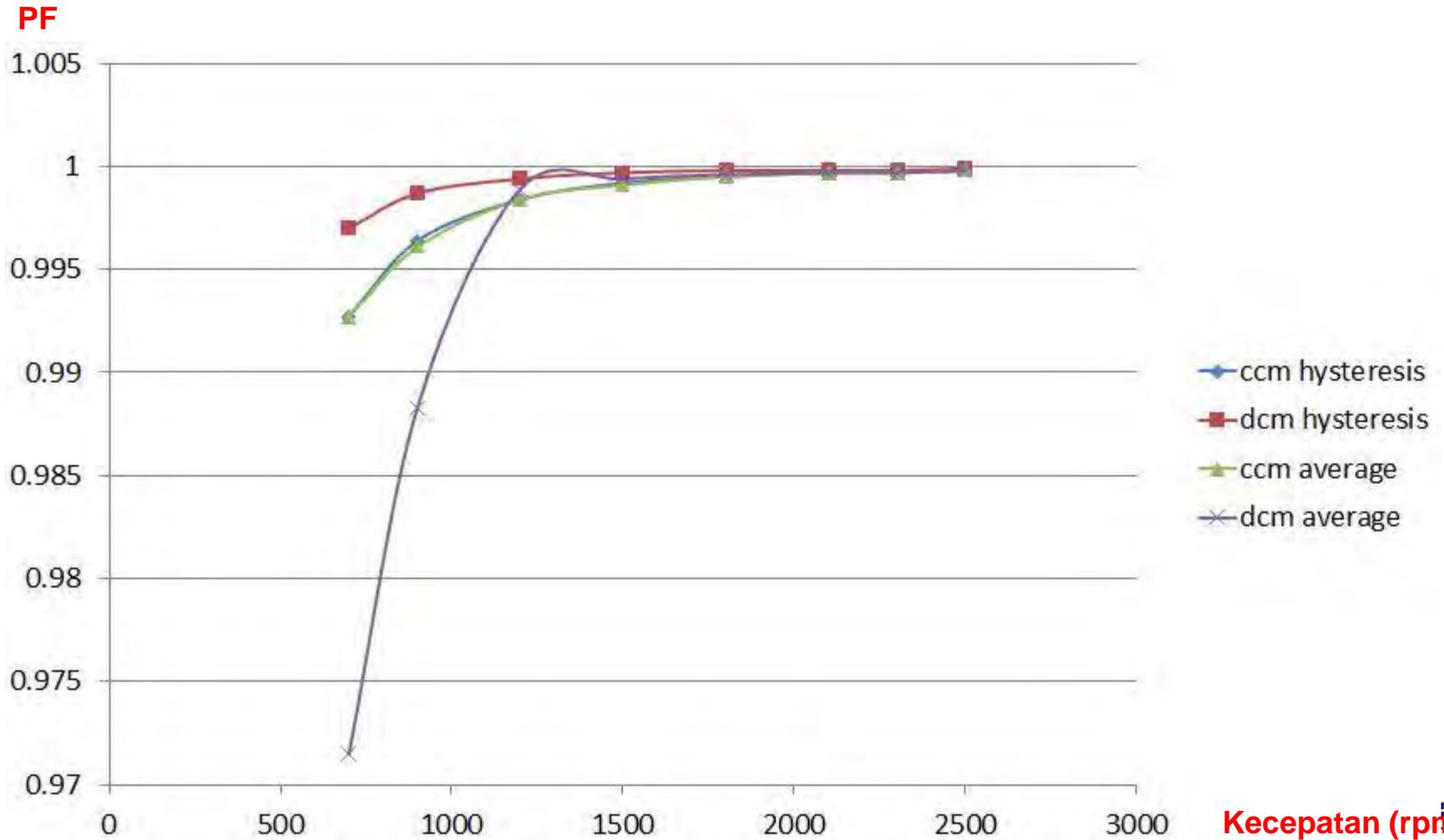
Hasil dan Pembahasan

DCM Average





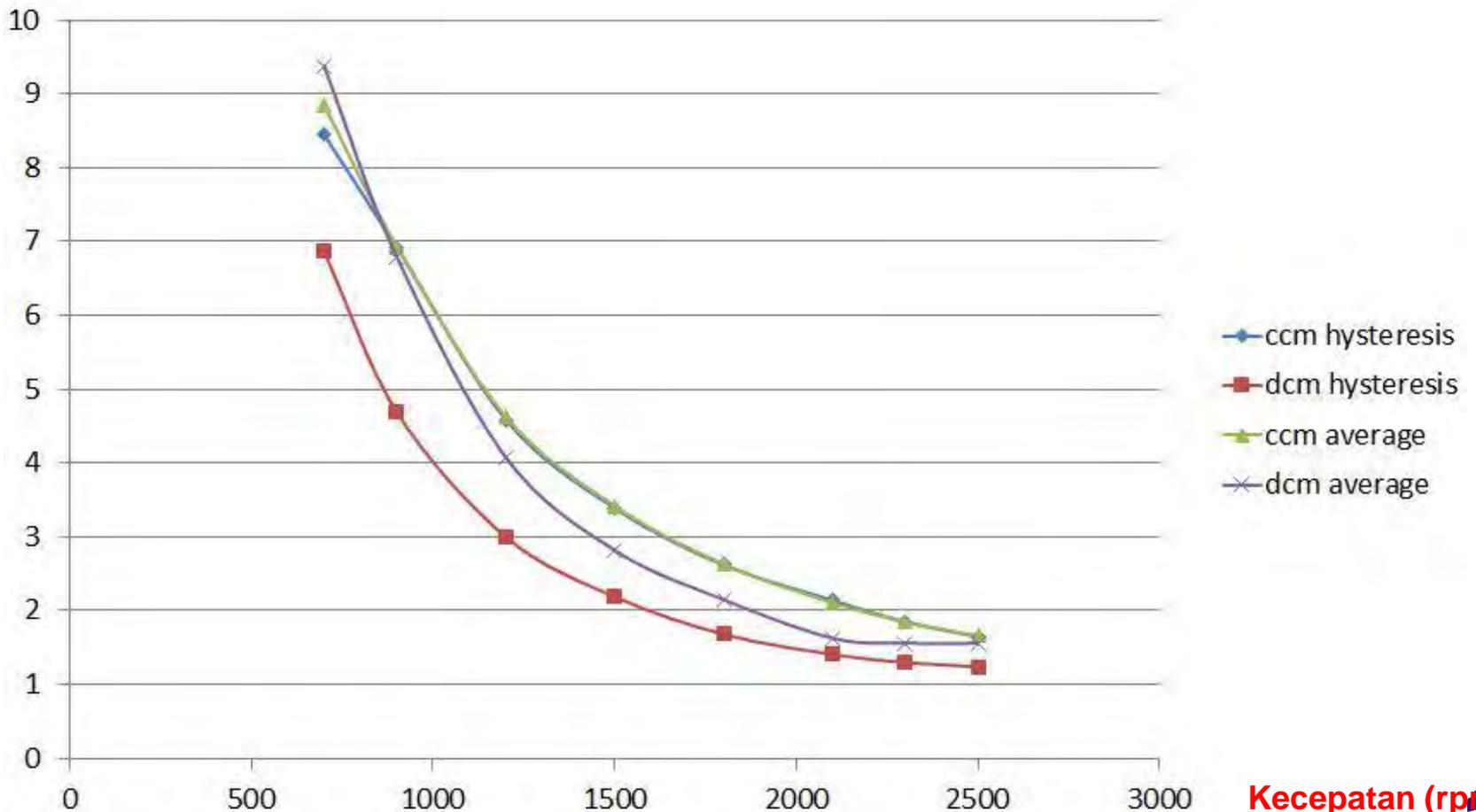
Nilai Faktor Daya





Nilai THD Arus

THD Arus



Kecepatan (rpm)





1

Pada pengujian kecepatan, sistem kontrol yang didesain bisa membuat kecepatan motor brushless DC mengikuti kecepatan referensi yang diberikan

2

Pada pengujian pembebanan yang diberikan, motor brushless DC bisa mempertahankan kecepatannya sekalipun adanya lonjakan kecepatan maupun penurunan kecepatan sesaat

3

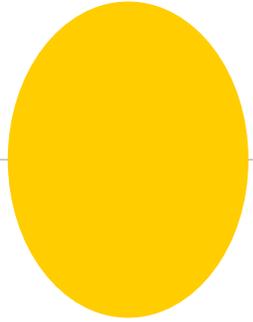
Konverter SEPIC berbasis *power factor correction* dapat memperbaiki faktor daya pada sistem dari 0.73 menjadi 0.999 pada kecepatan dan beban rating

4

Konverter SEPIC berbasis *power factor correction* dapat menurunkan nilai THD arus dari 74.39% menjadi 1.24%



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Terimakasih