



TUGAS AKHIR – MO141326

**ANALISA KEANDALAN STRUKTUR *SEAFASTENING* PADA
TRANSPORTASI *JACKET PLATFORM* BANUWATI KE *SOUTH EAST
SUMATERA BLOCK***

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**RELIABILITY ANALYSIS OF SEAFASTENING STRUCTURE IN
TRANSPORTATION BANUWATI JACKET PLATFORM TO SOUTH EAST
SUMATERA BLOCK**

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**Analisa Keandalan Stuktur Seafastening pada Transportasi Jacket Platform Banuwati
ke South East Sumatera Block**

TUGAS AKHIR

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ABSTRAK

KEANDALAN STRUKTUR *SEAFASTENING* PADA TRANSPORTASI *JACKET PLATFORM BANUWATI KE SOUTH EAST SUMATERA BLOCK*

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Abstrak - Struktur bangunan lepas pantai dibangun disebuah fabrikasi di darat dan kemudian dipindahkan ke laut di mana bangunan tersebut akan beroperasi. Transportasi bangunan lepas pantai membutuhkan pengikatan yang kuat supaya dalam proses transportasi, struktur tetap aman dan terjamin. Tugas akhir ini membahas tentang keandalan struktur *seafastening* pada transportasi *jacket platform* ke *South East Sumatera Block*. Struktur yang dianalisis adalah *jacket platform* Banuwati dengan menggunakan *barge* EOS-281. Pemodelan *jacket* dan *barge* menggunakan bantuan perangkat lunak komputer. Untuk melihat gerakan *barge* selama transportasi dilakukan analisa stabilitas dan juga RAO keadaan *lightship*, *half load*, dan *full load*. Hasil perhitungan RAO untuk gerakan *heave*, *roll* dan *pitch* berturut – turut adalah sebesar 0,99 m/s, 4,92 deg/m dan 0,989 deg/s. Tegangan aksial maksimum terdapat pada *member* 0003 – 0100 sebesar 14,02 ksi dan *member* 0005 – 0083 sebesar 13,93 ksi. Keandalan struktur *seafastening* dengan memperhatikan 2 member dengan tegangan aksial terbesar masing-masing 99,63% dan 99,85%.

Kata Kunci : Keandalan, Axial Compression Stress, Seafastening, Transportasi, Monte Carlo

ABSTRACT

REALIBILITY ANALYSIS OF SEAFASTENING STRUCTURE IN TRANSPORTATION BANUWATI JACKET PLATFORM TO SOUTH EAST SUMATERA BLOCK

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Abstrak - The structure of offshore building is constructed in a fabrication on land and then transferred to the ocean where the building is going to operate. Offshore building transportation requires a strong binding, so that in the transport process, the structure remains safe and secure. This paper discuss about reliability analysis of seafastening structure in transportation Banuwati Jacket Platform to South East Sumatera Block. The structure that analyzed is the banuwati platform jacket with using barge EOS-281. Modelling jacket and barge are using computer software. To see the movement of the barge during transportation performed stability analysis and also RAO lightship, half load and full load. The results of calculations for the movement RAO heave, roll and pitch are respectively of 0.99 m / s, 4.92 deg / m and 0.989 deg / s. The maximum axial stress contained in the member 0003 – 0100 amounted to 14,02 ksi and member 0005 – 0083 amounted to 13.93 ksi. Reliability structure seafastening by observing two maximum axial stress members respectively 99,63% and 99.85%.

Keywords : *Reliability, Axial Compression Stress, Seafastening, Transportation, Monte Carlo*

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Tugas akhir ini berjudul “Analisa Keandalan Struktur *Seafastening* pada Transportasi *Jacket Platform* Banuwati ke *South East Sumatera Block*”. Tugas akhir ini disusun guna memenuhi persyaratan dalam menyelesaikan Studi Kesarjanaan (S-1) di Jurusan Teknik Kelautan, Fakultas Teknologi Kelautan, Institut Teknologi Sepuluh Nopember Surabaya. Tugas akhir ini membahas tentang keandalan struktur *seafastening* selama proses transportasi dengan pertimbangan pengaruh beban *jacket* itu sendiri dan beban lingkungan.

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DAFTAR SIMBOL

| | | |
|-----------------------------|---|--|
| KG | = | Center of Gravity (m) |
| KB | = | Center of Bouyance (m) |
| KM | = | Metacenter (m) |
| T _A | = | Perubahan Tinggi Sarat Air pada Buritan (m) |
| T _F | = | Perubahan Tinggi Sarat Air pada Haluan (m) |
| l | = | Lengan Momen Penegak (m) |
| GZ | = | Righting Arm (m) |
| MG | = | Jarak Metacenter ke Titik Berat (m) |
| Δ | = | Displacement Kapal (ton) |
| A | = | Wind Surface Area (m ²) |
| V | = | Kecepatan Angin (knot) |
| X _p (ω) | = | Amplitudo Struktur (m) |
| H (ω) | = | Amplitudo Gelombang (m) |
| S (ω) | = | Spektrum Gelombang |
| γ | = | Parameter Puncak (<i>peakedness parameter</i>) |
| τ | = | Parameter Bentuk (<i>shape parameter</i>) |
| T _p | = | Periode Puncak Spektra (detik) |
| H _s | = | Tinggi Gelombang Signifikan (m) |
| S _R (ω) | = | Spektrum Respon (m ² -sec) |
| ω | = | Frekuensi Gelombang (rad/sec) |
| σ | = | Gaya Aksial (kN) |
| P | = | Gaya Tarik (N) |
| A | = | Luas Penampang Lintang (m ²) |
| F _t | = | Tegangan Tarik (MPa) |
| F _y | = | Tegangan Yield (MPa) |
| F _a | = | Tegangan Tekan (MPa) |
| E | = | Modulus Elastisitas (MPa) |
| k | = | Faktor Panjang Efektif |
| L | = | Panjang Tanpa <i>Bracing</i> (m) |
| r | = | Jari-jari Girasi (m) |

| | |
|----------|---|
| C | = Koefisien Tegangan Kritis <i>Buckling</i> |
| D | = Diameter Luar (m) |
| t | = Ketebalan Pipa (m) |
| F_{xc} | = <i>Local Buckling In-elastic</i> |
| LOA | = <i>Length Overall</i> (m) |
| B | = <i>Breadth</i> (m) |
| H | = <i>Height</i> (m) |
| GRT | = <i>Gross Tonnage</i> (ton) |
| NT | = <i>Nett Tonnage</i> (ton) |
| Hs | = Tinggi Gelombang Signifikan (m) |
| T | = Periode Gelombang (s) |
| LCB | = <i>Longitudinal Centre of Bouyance</i> (m) |
| LCF | = <i>Longitudinal Centre of Flotation</i> (m) |
| KMt | = <i>Transversal Keel to Metacentre</i> (m) |
| KML | = <i>Longitudinal Keel to Metacentre</i> (m) |
| ϕ_a | = Percepatan Tangensial (m/s^2) |
| F | = Inertia Force (kN) |

DAFTAR ISTILAH

| | |
|------------------------|---|
| <i>Surge</i> | = Gerakan translasi pada bangunan apung dengan arah gerakan pada sb. X. |
| <i>Sway</i> | = Gerakan translasi pada bangunan apung dengan arah gerakan pada sb. Y. |
| <i>Heave</i> | = Gerakan translasi pada bangunan apung dengan arah gerakan pada sb. Z. |
| <i>Roll</i> | = Gerakan osilasi rotasional pada bangunan apung dengan arah gerakan pada sb. X. |
| <i>Pitch</i> | = Gerakan osilasi rotasional pada bangunan apung dengan arah gerakan pada sb. Y. |
| <i>Yaw</i> | = Gerakan osilasi rotasional pada bangunan apung dengan arah gerakan pada sb. Z. |
| RAO | = <i>Respon Amplitude Operator</i> merupakan fungsi respon gerakan dinamis struktur yang terjadi akibat gelombang dalam rentang frekuensi tertentu. |
| Respon Spektra | = Respon densiti pada struktur akibat gelombang berupa <i>energy density spectrum</i> . |
| <i>Trim</i> | = Perbedaan sarat air antara haluan dan buritan pada kapal. |
| <i>Trim by Stren</i> | = Perbedaan sarat air ketika buritan lebih tinggi daripada haluan. |
| <i>Trim by Bow</i> | = Perbedaan sarat air ketika haluan lebih tinggi daripada buritan. |
| <i>Even Keel</i> | = Posisi kapal pada saat tidak ada perbedaan sarat pada haluan dan buritan. |
| <i>Righting Moment</i> | = Momen yang mengakibatkan kapal kembali ke posisi <i>even keel</i> . |
| <i>Righting Arm</i> | = Panjang lengan penegak. |
| <i>Heeling Arm</i> | = Panjang lengan momen pemutar. |
| <i>Lightship</i> | = Kondisi kapal ketika tidak ada muatan. |
| <i>Weight Check</i> | = Validasi berat struktur antara data dengan model pada <i>software</i> . |
| <i>Unity Check</i> | = Perbandingan antara tegangan aktual dengan tegangan ijin. |
| <i>Draft</i> | = Tinggi sarat air pada kapal. |
| <i>Deadwight</i> | = Berat maksimal muatan pada kapal. |

BAB 1

PENDAHULUAN

1.1. Latar Belakang Masalah

Bangunan lepas pantai dibangun di sebuah fabrikasi yang ada di darat. Setelah semua bagian struktur tersebut selesai maka akan dipindahkan dari fabrikasi menuju tempat instalasi dimana *platform* tersebut akan beroperasi. Dalam proses pemindahan ini biasanya digunakan 2 cara, yaitu sistem *load out* dan sistem *tow out*. Sistem *load out* biasanya digunakan untuk struktur *jacket* dan *top structure*. Pada proses *load* ini digunakan *barge* sebagai alat transportasi struktur bangunan lepas pantai. Sedangkan *sistem tow out* digunakan untuk struktur yang memiliki struktur terapung (*bouyancy tanks*). Struktur ini ditarik menuju tempat instalasi menggunakan *tug boat*.

Selama proses transportasi menggunakan *barge*, kondisi lingkungan yang dilalui akan memberikan beban berupa gelombang, angin dan arus. Kondisi pembebanan ini akan mempengaruhi stabilitas pada *barge*. Sehingga struktur yang ditempatkan pada *barge* memerlukan suatu sistem pengikatan tertentu agar tetap stabil di atas *barge*. Sistem pengikatan ini disebut *seafastening*. Pengikatan struktur dilakukan dengan cara pengelasan antara kaki struktur dengan deck dari tongkang (Soegiono, 2004). Pada umumnya *seafastening* terbuat dari pipa besi yang satu ujungnya dilas pada bagian struktur ujung yang lain dilas pada *barge*.

Menurut Soegiono (2004) fungsi *seafastening* ada tiga yaitu :

1. Untuk menghindarkan modul terbalik atau bergeser keluar dari *barge* akibat gerakan *barge*.
2. Untuk mendistribusikan gaya reaksi modul diatas titik-titik yang kuat di deck.
3. Untuk secara *lateral* mendukung modul menghindarkan tegangan yang berlebihan (*excessive stress*) dari *transverse frame modul*.

Pengikatan yang cukup kuat harus didesain dan diaplikasikan pada struktur dan semua komponennya untuk mencegah struktur bergerak saat transportasi. Muatan yang diangkut, *grillage*, dan *seafastening* harus mempunyai kekuatan untuk

menahan beban lingkungan selama proses transportasi (Nobel Denton No : 0030/ND,2009).

Pada saat posisi *barge* di atas permukaan air tenang maka tegangan-tegangan yang terjadi pada pipa *seafastening* berasal dari struktur itu sendiri (Murman,2002). Namun pada kondisi nyata di lautan, *barge* akan menerima gaya gelombang sehingga akan mengalami gerakan. Secara umum, struktur terapung diasumsikan *rigid* dan bergerak dengan enam derajat kebebasan (*six degree of freedom*), tiga gerakan *translational* dan tiga gerakan *rotational* (Chakrabakti,1987). Tiga gerakan *translational* yaitu *surge* (sepanjang sumbu x), *sway* (sepanjang sumbu y), dan *heave* (sepanjang sumbu z). Tiga gerakan *rotational* yaitu *roll* (dengan poros sumbu x), *pitch* (dengan poros sumbu y), dan *yaw* (dengan poros sumbu z). Gerakan-gerakan ini menimbulkan percepatan pada *barge* yang berakibat timbulnya gaya tambahan pada struktur di atasnya, dan hal ini kan mempengaruhi tegangan pada *seafastening*. Sehingga *seafastening* diharapkan mampu menerima tegangan total, yang diberikan oleh struktur dan beban lingkungan. *Seafastening* diharapkan mampu menerima tegangan total, yang diberikan oleh struktur dan beban lingkungan, sehingga tidak gagal saat transportasi. Oleh karena itu diperlukan analisis yang dalam mengenai *seafastening*.

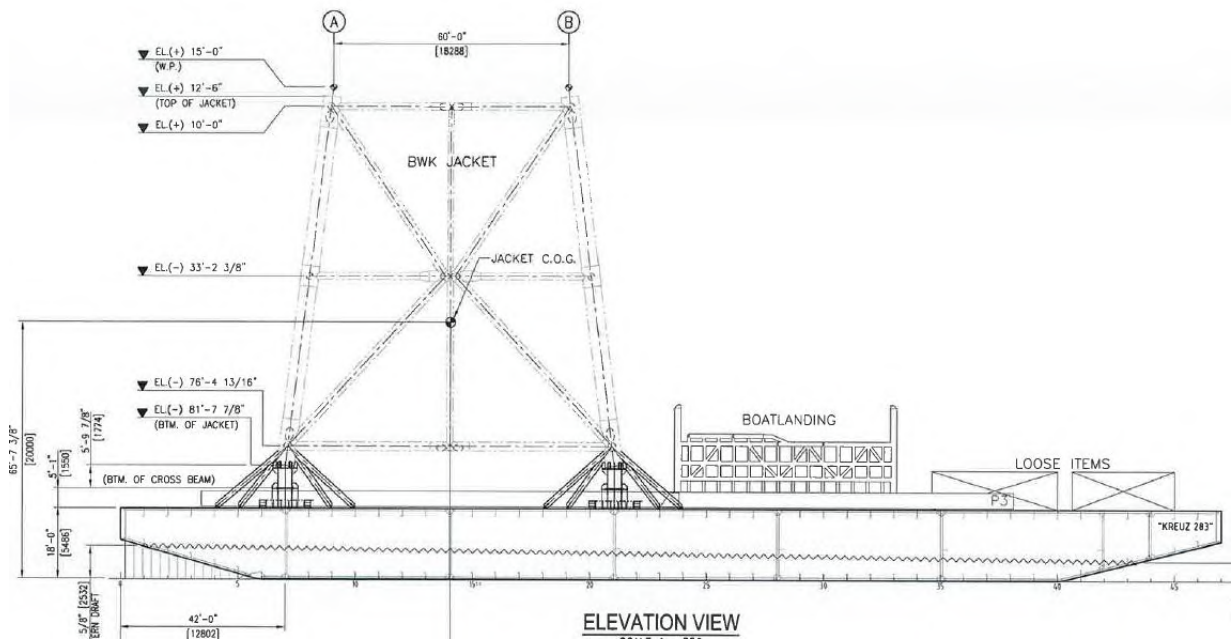
Dalam tugas akhir ini, objek studi yang digunakan adalah *Jacket Platform* Banuwati yang diangkat dengan *barge* ke *South East Sumatera Block*. *Platform* ini dikerjakan oleh PT.PAL Indonesia dan dioperasikan oleh CNOOC SES Ltd yang terletak di lepas pantai Laut Jawa, + 90 km sebelah Utara Teluk Jakarta. *Barge* yang digunakan untuk *seafastening* dan transportasi *jacket platform* Banuwati adalah “*EOS 281*” yang memiliki ukuran seperti berikut :

Tabel 1.1 *Principal Dimension Barge*

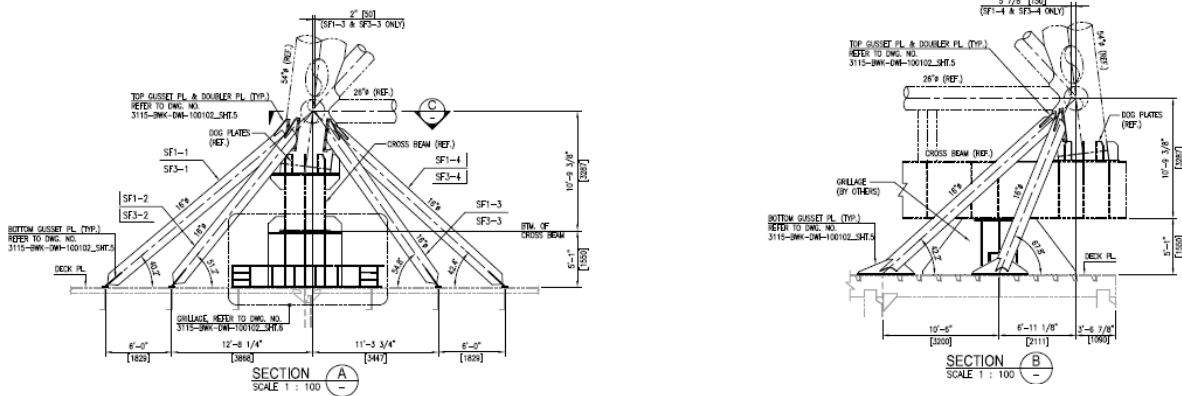
| | |
|-----------------|---------|
| LOA | 85.34 m |
| Breadth (B) | 27.43 m |
| Height (H) | 5.48 m |
| Extreme Draught | 4.3 m |



Gambar 1.1 Lokasi *Platform Banuwati*



Gambar 1.2 Side view BS 2101
(sumber: PT.PAL Indonesia)



Gambar 1.3 Jenis Seafastening yang akan Digunakan
(sumber: PT.PAL Indonesia)

1.2 Perumusan Masalah

Permasalahan yang akan dibahas pada studi ini adalah :

1. Bagaimana gerakan *barge* selama transportasi ?
2. Berapa besar tegangan *axial* pada struktur *seafastening* selama transportasi ?
3. Berapakah keandalan struktur *seafastening* selama proses transportasi dengan moda kegagalan *axial compression stress* ?

1.3 Tujuan

Tujuan dari tugas akhir ini antara lain :

1. Mengetahui gerakan *barge* selama transportasi.
2. Mengetahui besar tegangan *axial* pada struktur *seafastening* selama transportasi.
3. Mengetahui keandalan struktur *seafastening* selama proses transportasi dengan moda kegagalan *axial compression stress* ?

1.4 Manfaat

Manfaat yang didapat dari penelitian tugas akhir ini adalah :

1. Memberikan pemahaman tentang besarnya pengaruh beban lingkungan terhadap gerakan *barge* saat beroperasi.
2. Memberikan pemahaman untuk menganalisa kekuatan struktur *seafastening*.
3. Memberikan pemahaman dalam analisa keandalan.

1.5 Batasan Masalah

1. Gerakan *barge* selama transportasi (*heave*, *roll*, dan *pitch*).
2. *Deck barge* dianggap kuat.
3. Arah pembebanan lingkungan pada *heading* 0, 45, 90, 135, 180.
4. Analisa keandalan menggunakan metode Simulasi *Monte Carlo*.

1.6 Sistematika Laporan

Sistematika laporan yang digunakan didalam penyusunan tugas akhir ini adalah Pada bab pertama pendahuluan ini akan dijelaskan latar belakang dilakukannya penelitian tentang struktur *seafastening*. Selain itu juga dibahas mengenai perumusan masalah yang akan diselesaikan serta tujuan dan manfaat diadakannya penelitian ini. Agar pembahasan masalahnya tidak terlalu luas, maka akan dibahas mengenai batasan masalah yang digunakan. Agar laporan dari penelitian ini bisa lebih mudah mudah dipahami, maka akan dijelaskan pula sistematika dari penyusunan laporan.

Pada bab kedua dijelaskan dasar teori dan tinjauan pustaka yang digunakan dalam menyelesaikan permasalahan yang ada. Bagian ini berisi dasar teori yang digunakan sebagai landasan penyelesaian tugas akhir ini dan juga berisikan rumus-rumus serta referensi yang digunakan.

Pada bab ketiga menjelaskan tentang langkah-langkah secara terperinci dalam menyelesaikan tugas akhir ini. Selain itu juga dijelaskan permodelan yang akan dipakai dalam proses pengerjaan tugas akhir ini.

Pada bab keempat menjelaskan tentang semua hasil analisa dari penelitian ini. Pada bab ini juga dibahas tentang hasil pengolahan data yang nantinya akan menjawab tujuan dilakukannya penelitian ini.

Pada bab kelima berisi semua jawaban dari permasalahan yang ada dan menjawab tujuan dilakukannya penelitian ini. Selain itu, pada bab ini juga berisi saran-saran untuk penelitian selanjutnya.

BAB II

TINJAUAN PUSTAKA DAN DASAR TEORI

2.1 Tinjauan Pustaka

Seafastening dipasang dan didisain untuk mencegah pergeseran selama proses transportasi seluruh komponen *platform* di atas *barge*. *Seafastening* harus didisain untuk mampu menahan gaya defleksi yang diprediksikan terjadi pada *barge* akibat kondisi lingkungan. Beberapa desain kriteria perancangan *seafastening* (API RP 2A WSD 21st Edition, 2000) yang pertama harus terpasang sebagai *fixed structure* agar mampu mencegah pergeseran *jacket platform*, kedua peletakan *seafastening* harus dirancang dengan rinci dan harus sesuai dengan rencana desain.

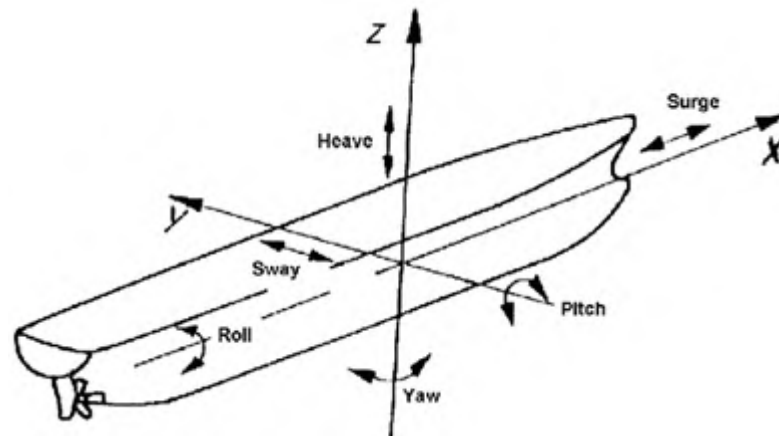
Pada *seafastening* banyak gaya yang terjadi seperti gaya *transversal*, *vertical*, *longitudinal* yang berkaitan dengan intergritas struktur yang diangkut. Selain itu *seafastening* sendiri dirancang agar memudahkan proses pemindahan *platform* ke lokasi instalasi di mana *platform* akan beroperasi. *Seafastening* merupakan suatu pengikat antara struktur dan *barge*. Selama proses transportasi ada beberapa gaya yang memengaruhi stabilitas struktur maupun *barge* seperti, kondisi lingkungan yang akan dilalui berupa beban gelombang dan angin.

Suatu sistem *seafastening* yang berhasil harus meliputi adanya data teknik dari *barge* yang akan mengangkut struktur ke lokasi instalasi dan data struktur yang akan ditransportasikan (Ward & Gebra, 2006).

2.2 Dasar Teori

2.2.1 Gerakan Bangunan Apung

Setiap struktur terapung yang bergerak di atas permukaan laut selalu mengalami gerakan osilasi. Gerakan osilasi ini terdiri dari 6 macam gerakan, yaitu 3 macam gerakan translasi dan 3 macam gerakan rotasional dalam 3 arah sumbu gerakan. Macam gerakan ini meliputi : *surging*, *heaving*, *sway*, *yawing*, *pitching*, dan *rolling*.



Gambar.2.1 6 (enam) derajat kebebasan struktur terapung

Keterangan :

1. *Surge* (x) = Translasi longitudinal
2. *Sway* (y) = Translasi lateral
3. *Heave* (z) = Translasi vertikal
4. *Roll* (Φ) = Rotasi terhadap sumbu $-x$ yang melalui titik pusat
5. *Pitch* (θ) = Rotasi terhadap sumbu $-y$ yang melalui titik pusat
6. *Yaw* (ψ) = Rotasi terhadap sumbu $-z$ yang melalui titik pusat

Pada *barge* yang berada di laut akan terpengaruh oleh gaya yang cenderung mengakibatkan *barge* tersebut bergerak dari posisi semula. Gerakan yang terjadi tergantung dari geometri struktur dan gaya yang mengenai *barge*, dimana gaya yang bekerja pada *barge* tersebut disebabkan oleh perilaku *irregular* dari lautan. Perilaku tersebut dibedakan menjadi dua bagian yaitu, gaya osilasi orde pertama dengan frekuensi gelombang relatif rendah dan gaya osilasi orde kedua dimana gaya perlahan yang bervariasi dengan frekuensi lebih rendah dari frekuensi gelombang (Chakrabarti, 1978).

Pada umumnya transportasi dirancang untuk menghadapi kemungkinan badai satu tahunan (*one year storm*) pada waktu ditunda ke lokasi. Konsep dasar *seafastening* (pengikatan) harus dibuat untuk mengakomodasikan gaya-gaya transversal, vertikal, dan longitudinal, berkaitan dengan integritas struktur yang diangkut. Setelah konsep dibuat dalam kaitan dengan *barge* yang dipilih, *seafastening and deck integrity*, maka harus dibuat spectra barge motions analysis agar *barge* dapat bertahan selama ditunda.

2.2.2 Gerakan Surge Murni

Surge adalah gerakan osilasi translasi pada kapal yang bekerja pada sumbu x sebagai pusat gerak. Persamaan untuk gerak *surge* adalah :

$$a\ddot{x} + b\dot{x} + cx = F_0 \cos \omega_e t \dots \dots \dots (2.1)$$

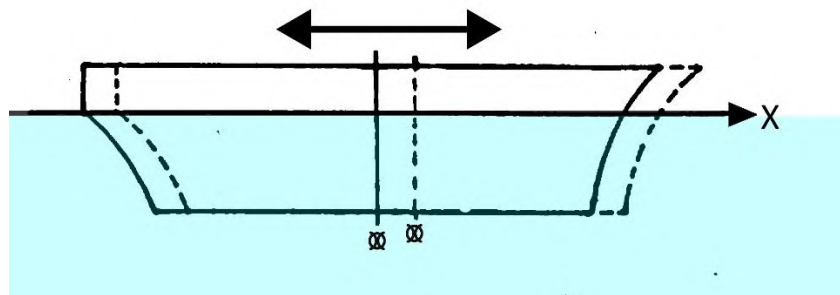
Dimana :

$a\ddot{x}$: *Inertial force* (N)

$b\dot{x}$: *Damping force* (N)

cx : *Restoring force* (N)

F_{0x} : *Exciting force* (N)



Gambar 2.2 Ilustrasi Gerakan *Surge*

2.2.3 Gerakan Sway Murni

Sway adalah gerakan osilasi translasi pada kapal yang bekerja pada sumbu y (melintang) sebagai pusat gerak. Persamaan untuk gerak *sway* dijelaskan pada persamaan 2.2.

$$a\ddot{y} + b\dot{y} + cy = F_o \cos \omega_e t \dots\dots\dots (2.2)$$

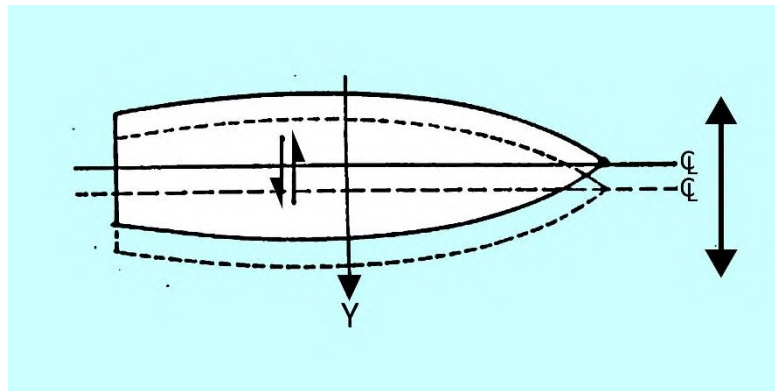
Dimana :

$a\ddot{y}$: *Inertial force* (N)

$b\dot{y}$: *Damping force* (N)

cy : *Restoring force* (N)

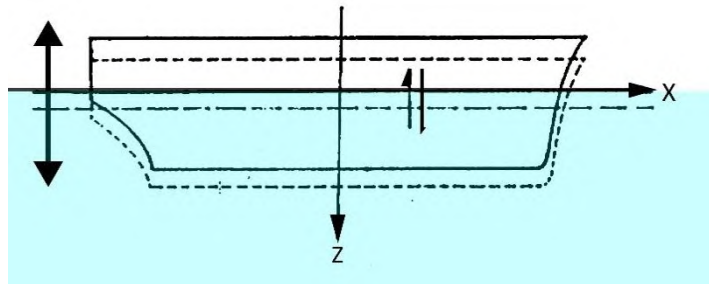
F_{oy} : *Exciting force* (N)



Gambar 2.3 Ilustrasi Gerakan *Sway*

2.2.4 Gerakan *Heave* Murni

Pada *Heaving* gaya kebawah akibat dari berat kapal membuat kapal tercelup ke air lebih dalam dan kembali ke awal hingga diperoleh kesetimbangan kapal. Ketika gaya *buoyancy* lebih besar akibat kapal tercelup, kapal akan bergerak secara vertikal ke atas, ketika posisi kapal telah setimbang lantas tidak berhenti akan tetapi tetap naik dikarenakan ada pangeruh momentum. Selanjutnya kejadiannya akan berulang. Ilustrasi gerakan *heave* dapat dilihat pada Gambar 2.4.



Gambar 2.4 Ilustrasi Gerakan *Heave*

Kejadian tersebut terjadi berulang-ulang. Maka, dapat dituliskan persamaan umum pada kapal kondisi *heave* adalah:

$$a\ddot{z} + b\dot{z} + cz = F_0 \cos \omega_e t \dots \dots \dots (2.3)$$

Keterangan :

- $a\ddot{z}$: *Inertial force* (N)
- $b\dot{z}$: *Damping force* (N)
- cz : *Restoring force* (N)
- F_{0z} : *Amplitude heave exciting force* (N)

Pada persamaan tersebut, terdapat empat elemen utama dalam gerakan *heave*, antara lain:

- *Inertial Force* ($F_a = a\ddot{z}$)

Inertial Force merupakan percepatan gerakan secara kontinu dari fluida yang memiliki gaya lebih besar dari massa percepatan waktu kapal. (Bhatacarya, 1972)

$$a \frac{d^2z}{dt^2} = M \frac{d^2z}{dt^2} + a_z \frac{d^2z}{dt^2} \dots \dots \dots (2.4)$$

Dengan :

- M : massa tambah kapal
- a_z : massa tambah akibat gerakan *heave*

- *Damping Force* ($F_b = b\dot{z}$)

Damping Force akan selalu bergerak berlawanan arah dari gerakan kapal sehingga menyebabkan redaman yang berangsur-angsur pada amplitudo gerakan.

$$F_b = b \frac{dz}{dt} \dots\dots\dots (2.5)$$

Pada persamaan diatas b merupakan koefisien pada gaya damping pada kondisi *heave*. Koefisien redaman tersebut akan bergantung pada faktor-faktor sebagai berikut:

- a. Tipe dari gerakan osilasi
- b. Frekuensi *encountering*
- c. Bentuk struktur terapung

- *Restoring Force* ($F_c = cz$)

Restoring Force pada gerakan *heave* diberikan sebagai tambahan pada gaya angkat kapal ketika dibawah permukaan air. Oleh karena itu, gaya pengembali diberikan sebagai jumlah displacement air, atau berat tamabahn spesifik pada volume tercelup.

$$C_z = \rho g A_{wp} Z = \rho g L B C_{wp} Z \dots\dots\dots (2.6)$$

Dengan :

- A_{wp} : Luas bidang garis air (m^2)
- Z : Simpangan gerak *heave*
- C_{wp} : Koefisien luad bidang garis air
- P : Massa jenis air laut ($1.025 \text{ ton}/m^3$)
- g : Kecepatan gravitasi (m/s^2)

- *Exciting Force* ($F = F_o \cos \omega_e t$)

Exciting Force pada gerak *heave* adalah pengintegrasian dari penambahan gaya angkat dikarenakan gelombang yang melewati sepanjang kapal. Sehingga dapat dituli persamaan sebagai berikut:

$$F = F_o \cos \omega_e t \dots \dots \dots (2.7)$$

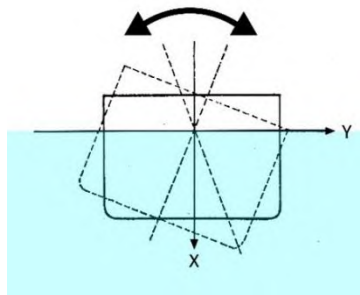
Dimana :

F_o : Amplitudo gaya eksitasi

ω_e : Frekuensi gelombang *encountering* (hz)

2.2.5 Gerakan *Roll* Murni

Roll adalah gerakan osilasi rotasional pada kapal yang bekerja dengan sumbu x sebagai pusat gerakannya. Ilustrasi gerakan *roll* dapat dilihat pada Gambar 2.5.



Gambar 2.5 Ilustrasi Gerakan *Roll*

Rumus umum dari persamaan gerak akibat *rolling* ialah:

$$a\ddot{\phi} + b\dot{\phi} + c\phi = M_o \cos \omega_e t \dots \dots \dots (2.8)$$

Dimana :

M_o : Amplitudo momen eksitasi (m)

ω_e : Frekuensi gelombang *encountering* (rad/sec)

$a\ddot{\phi}$: *Inertial Moment* (N/m)

$b\dot{\phi}$: *Damping Moment* (N/m)

$c\phi$: *Restoring Moment* (N/m)

M_{ox} : *Exciting Moment* (N/m)

2.2.6 Gerakan *Pitch* Murni

Pitch adalah gerakan osilasi rotasional pada kapal yang bekerja dengan sumbu y sebagai pusat gerakannya. Berbeda dengan *heave*, gerakan yang ditimbulkan akibat

pitch adalah gerak rotational yang menimbulkan momen. Gerak *pitch* juga berpengaruh terhadap kesetimbangan posisi, oleh karena itu momen yang terjadi akibat *pitch* perlu diperhitungkan. Persamaan umum dari persamaan gerakan akibat *pitching* adalah:

$$a\ddot{\theta} + b\dot{\theta} + c\theta = M_o \cos \omega_e t \dots \dots \dots (2.9)$$

Dimana :

- M_o : Amplitudo momen eksitasi (m)
- ω_e : Frekuensi gelombang *encountering* (rad/sec)
- $a\ddot{\theta}$: *Inertial Moment* (N/m)
- $b\dot{\theta}$: *Damping Moment* (N/m)
- $c\theta$: *Restoring Moment* (N/m)
- M_{oy} : *Exciting Moment* (N/m)

Pada persamaan tersebut, terdapat empat elemen utama dalam gerakan *heave*, antara lain:

- *Inertial Moment* ($a \frac{d^2\theta}{dt^2}$)

Konstanta a adalah massa virtual dari momen inertia dan $d \frac{d^2\theta}{dt^2}$ merupakan percepatan sudut yang ditimbulkan dari gerakan *pitch*. Massa dari momen inertia kondisi *pitch* adalah momen inertia kapal ditambah dengan massa tambah momen inertia dari gerak *pitch*.

$$d = I_{yy} + \delta I_{yy}$$

$$d = \frac{\Delta}{g} K_{yy}^2 + \delta I_{yy} \dots \dots \dots (2.10)$$

Dimana :

- δI_{yy} : Massa tambah momen inertia dari kapal untuk gerak *pitch*
- K_{yy}^2 : Kuadrat dari jari-jari girasi pada kondisi gerak *pitch*
- I_{yy} : Momen inersia massa struktur

Diasumsikan bahwa distribusi massa secara longitudinal sama dengan distribusi displacement secara longitudinal. Sehingga distribusi vertikal tidak begitu berpengaruh. Titik CG (pusat gravitasi) dari kapal diasumsikan berada di tengah struktur yaitu pada midship (Bhattacharya, 1972). Secara pendekatan, jari-jari girasi gerakan *pitch* adalah:

$$K_{yy} = 0.24L \text{ to } 0.26 L \dots\dots\dots (2.11)$$

- *Damping Moment* ($b \frac{d\theta}{dt}$)

Koefisien redaman pada gerakan *pitch* dapat diitung dengan melakukan pendekatan *strip theory* yang ditentukan oleh setiap *station* dan diintegrasikan sebanyak *station* yang ada di sepanjang struktur.

- *Restoring Moment* ($c\theta$)

Perhitungan untuk *Restoring Moment* pada gerakan *pitch* dapat dihitung dengan perhitungan sebagai berikut:

$$\begin{aligned} h\theta &= \rho g \theta \int_{-L/2}^{L/2} x^2 y(x) dx \\ &= \rho g \theta I_y \dots\dots\dots (2.12) \end{aligned}$$

Dimana :

- h : Koefisien restoring moment
- I_y : Momen inersia dari beban water plan area
- ρ : Massa jenis air laut (1.025 ton/m³)
- g : Kecepatan gravitasi (m/s²)
- ∇ : *Volume displacement*
- Δ : *Displacement*
- \overline{MB}_1 : Jari-jari metacenter memanjang
- \overline{MG}_1 : Tinggi metacenter memanjang

Dikarenakan

$$\overline{MB}_1 \cong \frac{I_y}{\nabla}$$

$$\Delta = \rho g \nabla$$

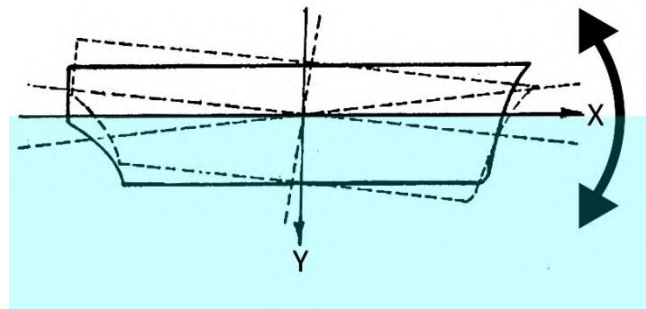
Sehingga,

$$\begin{aligned} h\theta &= \rho g \overline{MB}_1 \nabla \theta \\ &= \rho g \overline{MG}_1 \nabla \theta \\ &= \Delta \overline{MG}_1 \theta \dots\dots\dots (2.13) \end{aligned}$$

- *Exciting Force* ($F = M_o \cos \omega_e t$)

Exciting Force pada gerak *pitch* diakibatkan oleh tidak seimbangnya momen akibat gelombang dari sudut melintang kapal. Sehingga, momen dalam gerak *pitch* dapat dirumuskan sebagai berikut:

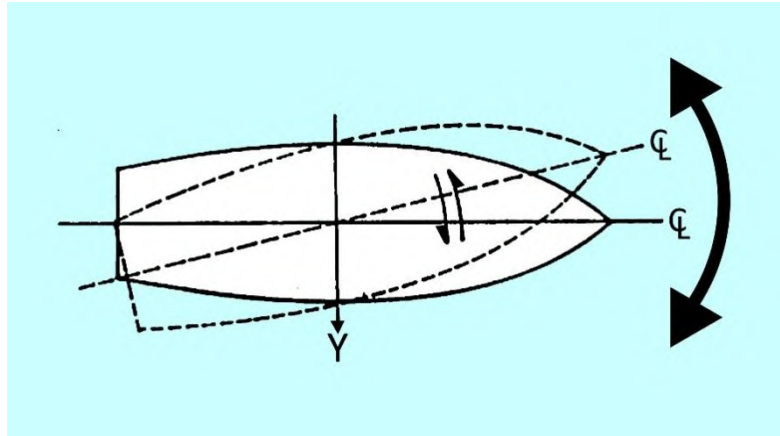
$$M_\theta = M_o \cos \omega_e t \dots\dots\dots (2.14)$$



Gambar 2.6 Ilustrasi Gerakan *Pitch*

2.2.7 Gerakan *Yaw* Murni

Gerak *yaw* adalah gerakan osilasi rotational pada kapal yang bekerja pada sumbu z sebagai pusat gerak. Gerak *yaw* juga berpengaruh pada kesetimbangan posisi kapal seperti gerak gerak lainnya.



Gambar 2.7 Ilustrasi Gerakan *Yaw*

Persamaan gerak kapal untuk *yaw* adalah:

$$a\ddot{\phi} + b\dot{\phi} + c\phi = M_o \cos \omega_e t \dots\dots\dots (2.15)$$

Dimana :

- M_o : Amplitudo momen eksitasi (m)
- ω_e : Frekuensi gelombang encountering (rad/sec)
- $a\ddot{\phi}$: *Inertial Moment* (N/m)
- $b\dot{\phi}$: *Damping Moment* (N/m)
- $c\phi$: *Restoring Moment* (N/m)
- M_{oz} : *Exciting Moment* (N/m)

2.2.8 *Seafastening*

Transportasi platform dari lapangan ke lokasi tergantung pada kapasitas angkut *cargo barge* yang tersedia dan biaya yang diperlukan untuk transportasi dan instalasi. Selama proses transportasi menggunakan *barge*, beberapa elemen struktur mengalami kondisi pembebanan yang mendominasi. Untuk itu *jacket, deck, piles, pipelines, boat landing*, dll yang telah diletakan di atas tongkang harus di *tie-down (seafastening)* yaitu diikat dengan konstruksi penyangga agar tetap aman pada waktu *barge* oleng dalam perjalanan ke lokasi. Dari awal harus diperhitungkan bahwa unit *barge* dan muatan yang diangkut akan mendapatkan gaya yang signifikan selama perjalanan ke lokasi instalasi.



Gambar.2.8 *Seafastening jacket pada barge*

Pengikatan struktur dilakukan dengan cara pengelasan antara kaki struktur dengan dek dari tongkang (Soegiono, 2004). Menurut Soegiono (2004) fungsi *seafastening* ada tiga yaitu :

1. Untuk menghindarkan modul terbalik atau bergeser keluar dari *barge* akibat gerakan *barge*
2. Untuk mendistribusikan gaya reaksi modul di atas titik-titik yang kuat di dek.
3. Untuk secara lateral mendukung modul menghindarkan tegangan yang berlebihan (*excessive stress*) dari *transverse frame modul*

Ward dan Gebra (2006) menyebutkan bahwa suatu sistem *tie down* yang sukses harus meliputi adanya data teknik dari *barge* yang akan mengangkut *offshore structure* ke lokasi dan data *offshore structure* yang ditransportasikan. Data *barge* meliputi karakteristik gerakan *barge*, akselerasi dek dan kecepatan. Sedangkan data dari *offshore structure* meliputi kondisi pembebanan angin struktur dan massa.

2.2.9 Beban lingkungan

2.2.9.1 Beban Gelombang

Syarat pemilihan teori untuk perhitungan gaya gelombang didasarkan pada perbandingan antara diameter struktur (D) dengan panjang gelombang (λ) sebagai berikut:

$\frac{D}{\lambda} > 1$: gelombang mendekati pemantulan murni

$\frac{D}{\lambda} > 0.2$: difraksi gelombang diperhitungkan

$\frac{D}{\lambda} < 0.2$: persamaan morisson

Berikut adalah teori yang digunakan pada perhitungan gaya gelombang, yaitu (Indiyono, 2003):

1. Teori morison.

Persamaan morison mengasumsikan bahwa gelombang terdiri dari komponen gaya inersia dan *drag* (hambatan) yang dijumlahkan secara linier. Persamaan morisson lebih tepat diterapkan pada kasus struktur dimana gaya *drag* merupakan komponen yang dominan. Hal ini biasanya dijumpai pada struktur yang ukurannya (D) relatif kecil dibandingkan dengan panjang gelombangnya (λ).

2. Teori froude-krylov.

Froude-Krylov digunakan bilamana gaya hambatan relatif kecil dan gaya inersia dianggap lebih berpengaruh, dimana struktur dianggap kecil. Teori ini mengadopsi metode tekanan gelombang *incident* dan bidang tekanan pada permukaan struktur. Keuntungan dari teori ini adalah untuk struktur yang simetris, perhitungan gaya dapat dilakukan dengan persamaan terangkai (*closed-form*) dan koefisien-koefisien gayanya mudah ditentukan.

3. Teori difraksi.

Bilamana suatu struktur mempunyai ukuran yang relatif besar, yakni memiliki ukuran yang kurang lebih sama dengan panjang gelombang, maka keberadaan struktur ini akan mempengaruhi timbulnya perubahan arah pada medan gelombang disekitarnya. Dalam hal ini difraksi gelombang dari permukaan struktur harus diperhitungkan dalam evaluasi gaya gelombang.

2.2.9.2 Spektra Gelombang

Analisis spektrum gelombang dapat menggunakan beberapa teori spektrum gelombang yang telah ada, antara lain model spektrum JONSWAP, Pierson Moskowitz, ISSC ataupun ITTC. Pemilihan spektrum gelombang didasarkan pada kondisi nyata laut yang ditinjau. Bila tidak ada maka dapat digunakan model spektrum yang dikeluarkan oleh berbagai institusi dengan mempertimbangkan kesamaan fisik lingkungan. Dari spektrum gelombang dapat diketahui parameter-parameter gelombang sebagaimana dalam tabel berikut

Tabel 2.1 Parameter gelombang

| Profil Gelombang | Amplitudo | Tinggi |
|--------------------------------------|-------------------|--------------------|
| Gelombangrata-rata | $1,25(m_0)^{1/2}$ | $2,50 (m_0)^{1/2}$ |
| Gelombangsignifikan | $2,00(m_0)^{1/2}$ | $4,00(m_0)^{1/2}$ |
| Rata-rata 1/10 gelombang tertinggi | $2,55(m_0)^{1/2}$ | $5,00(m_0)^{1/2}$ |
| Rata-rata 1/1000 gelombang tertinggi | $3,44(m_0)^{1/2}$ | $6,67(m_0)^{1/2}$ |

m_0 = luasan di bawah kurva spectrum (zero moment).

Dalam tugas akhir ini akan digunakan spektrum JONSWAP (*Joint North Sea Wave Project*).Berikut ini adalah persamaan spektrum JONSWAP dalam perhitungan gelombang.

$$S(\omega) = \alpha g^2 \omega^{-5} \exp \left[\left\{ -1.25 \left(\frac{\omega}{\omega_0} \right)^{-4} \right\} \gamma \cdot \exp \left(\frac{(\omega - \omega_0)^2}{2\tau^2 \omega_0^2} \right) \right] \dots \dots \dots (2.16)$$

Dengan:

- S (w) : Spektrum gelombang
- γ : Parameter puncak (peakedness parameter)
- τ : Parameter bentuk (shape parameter)

untuk $\omega \leq \omega_0$: 0,07 dan $\omega \geq \omega_0 = 0,09$

α : $0,0076 (X_0)^{-0,22}$, untuk X_0 tidak diketahui $\alpha = 0,0081$

Formulasi spectra JONSWAP akhir-akhir ini banyak dipakai dalam perancangan dan analisa bangunan lepas pantai yang dioperasikan di Indonesia. Hal ini cukup

dapat dimengerti karena perairan Indonesia dimana kebanyakan bangunan lepas pantai untuk kegiatan migas yang dioperasikan adalah di perairan kepulauan atau tertutup. Namun dari sejumlah kajian, untuk perairan Indonesia disarankan memakai parameter γ yang lebih kecil, sekitar 2.0 sampai 2.5. Hal ini pada intinya adalah untuk mengurangi dominasi energi yang dikontribusikan oleh frekuensi gelombang tertentu saja (Djarmiko, 2012)

2.2.9.3 Respon Struktur

Response amplitude operator (RAO) atau sering disebut sebagai *transfer function* adalah fungsi respon yang terjadi akibat gelombang dalam rentang frekuensi yang mengenai *offshore structure*. RAO disebut sebagai *transfer function* karena merupakan alat untuk mentransfer beban luar (gelombang) dalam bentuk respon pada suatu struktur. Bentuk umum dari persamaan RAO dalam fungsi frekuensi adalah sebagai berikut (Chakrabarti, 1987) :

$$RAO(\omega) = \frac{X_p(\omega)}{\eta(\omega)} \dots\dots\dots (2.17)$$

Dimana :

(ω) : amplitud struktur

$\eta(\omega)$: amplitud gelombang

Menurut Djarmiko (2012), respon gerakan RAO terbagi menjadi dua yaitu Respon gerakan RAO untuk gerakan translasi yaitu *surge*, *sway*, dan *heave* ($k=1, 2, 3$ atau x, y, z), merupakan perbandingan langsung antara 17 amplitud gerakannya dibanding dengan 17 amplitud gelombang (dalam satuan panjang).

2.2.9.4 Beban Angin

Beban angin merupakan beban dinamis, tapi beberapa struktur akan meresponnya pada model statis yang paling mendekati. Dalam perancangan bangunan lepas pantai pada umumnya perhitungan beban angin disyaratkan untuk didasarkan pada besarnya kecepatan ekstrim dengan periode ulang 50 atau 100 tahun.

Semakin lama periode ulang yang digunakan, maka resiko kegagalan semakin besar. Sedangkan formula untuk gaya angin *time series* dapat dibangkitkan dari spektrum gelombang menurut (API RP 2A WSD) adalah memakai rumus sebagai berikut :

$$F_{WD}(t) = \frac{1}{2} \rho_u C_S A x_a |V_c - x| (V_c - x) \dots \dots \dots (2.18)$$

Dimana :

- F_W : gaya angin (N)
- C_S : koefisien bentuk
- ρ_u : massa jenis udara (kg/m³)
- x : kecepatan dari *platform* (m/s)
- x_a : *aerodynamic amittance*
- A : luas area vertikal yang terkena angin (m²)
- V_c : kecepatan partikel air (m/s)

Sedangkan kecepatan angin dirumuskan sebagai berikut :

$$V_W = V_{10} \left(\frac{y}{10} \right) \dots \dots \dots (2.19)$$

Dimana :

- V_W : kecepatan angin, knots (m/s)
- V_{10} : kecepatan angin pada ketinggian 10 m, knots (m/s)
- y : ketinggian dimana kecepatan angin dihitung, (m)
- x : faktor eksponen

Bila informasi yang akurat tidak tersedia, maka harga eksponensial x sebesar 1/7 dapat diambil sebagai pendekatan. Harga ini cukup sesuai untuk ketinggian sampai dengan sekitar 200 m. Untuk semua sudut dari pendekatan beban angin pada struktur, gaya pada permukaan datar diasumsikan sebagai gaya normal pada permukaan dan gaya pada tanki silinder vertikal, pipa, dan silinder lain diasumsikan searah dengan arah angin, sedangkan yang tidak vertikal dapat dihitung

menggunakan formula yang diambil dari perhitungan arah angin berhubungan dengan gerak objek.

2.2.9.5 Beban Arus

Arus akibat pasang surut memiliki kecepatan yang semakin berkurang seiring dengan bertambahnya kedalaman sesuai fungsi *non-linier*. Sedangkan arus yang disebabkan oleh angin memiliki karakter yang sama, tetapi dalam fungsi linier. Kecepatan arus tersebut dirumuskan dalam formulasi matematis berikut :

$$U_T = U_{or} \left(\frac{y}{h}\right)^{1/7} \dots\dots\dots (2.20)$$

$$U_W = U_{ow} (y/h)^{1/7} \dots\dots\dots (2.21)$$

Dimana

U_T : kecepatan arus pasang surut (m/detik)

U_{or} : kecepatan arus pasang surut (m/detik)

U_W : kecepatan arus akibat angin (m/detik)

U_{ow} : kecepatan arus akibat angin di permukaan (m/detik)

y : jarak dari dasar laut (meter)

h : kedalaman laut (meter)

Gaya arus yang bekerja pada struktur dapat dirumuskan sebagai berikut :

$$F_{cx} = C_{cx} S V^2 c \dots\dots\dots (2.22)$$

$$F_{cy} = C_{cy} S V^2 c \dots\dots\dots (2.23)$$

Dimana :

F_{cx} : gaya arus pada *bow*

F_{cy} : gaya arus pada *beam*

C_{cx} : koefisien gaya arus pada *bow* (0.016 lb/ft²)

C_{cy} : koefisien gaya arus pada *bow* (0.4 lb/ft²)

S : luas penampang pada lambung kapal (m²)

V_c : kecepatan arus desain (m/s)

2.2.10 Kondisi Pembebanan dan Penentuan Beban Kombinasi

Platform harus didesain untuk kondisi pembebanan yang sesuai dimana akan menghasilkan efek yang paling buruk terhadap struktur. Kondisi pembebanan harus meliputi kondisi lingkungan yang dikombinasikan dengan beban hidup dan beban mati yang sesuai melalui cara-cara berikut :

1. Kondisi lingkungan saat operasi dikombinasikan dengan beban mati dan beban hidup maksimum sesuai dengan kondisi operasi normal pada *platform*.
2. Kondisi lingkungan saat operasi dikombinasikan dengan beban mati dan beban hidup minimum sesuai dengan kondisi operasi normal pada *platform*.
3. Kondisi lingkungan saat badai dikombinasikan dengan beban mati dan beban hidup maksimum sesuai kondisi ekstrem pada *platform*.
4. Kondisi lingkungan saat badai dikombinasikan dengan beban mati dan beban hidup minimum sesuai kondisi ekstrem pada *platform*.

2.2.11 Konsep Tegangan

2.2.11.1 Tegangan Aksial/Normal

Tegangan normal dapat diakibatkan karena dua hal yaitu disebabkan oleh gaya aksial dan lenturan.

1. Disebabkan oleh gaya aksial

$$\sigma = \frac{P}{A} \dots\dots\dots (2.24)$$

Dimana:

A : Luas penampang lintang (m²)

P : Gaya Tarik (N)

2. Disebabkan oleh lenturan, ada dua kondisi lenturan yaitu:

- a. Pada batang lurus

$$\sigma = \frac{My}{I} \dots\dots\dots (2.25)$$

b. Pada lengkung simetris

$$\sigma = \frac{My}{Ae(R-y)} \dots\dots\dots (2.26)$$

2.2.11.2 Kriteria Tegangan Ijin

Bagian struktur yang menerima beban kompresi dan beban tekuk harus memenuhi kriteria kekuatan dan kriteria stabilitas. Apabila tegangan pada setiap bagian konstruksi melebihi tegangan ijin maka keruntuhan akan terjadi. Tegangan ijin untuk member silinder (API RP 2A-WSD)

1. Tegangan tarik ijin Ft, dirumuskan:

$$F_t = 0.6F_y \dots\dots\dots (2.27)$$

Dimana:

Fy = Tegangan *yield*; ksi (MPa)

2. Tegangan Tekan

Tegangan tekan yang diijinkan adalah Fa.

Untuk D/t ≤ 60, maka:

$$F_a = \frac{\left[1 - \frac{\left(\frac{Kl}{r}\right)^2}{2Cc^2}\right]}{\frac{5}{3} + \frac{3\left(\frac{Kl}{r}\right)}{8Cc} - \frac{\left(\frac{Kl}{r}\right)^3}{8Cc^3}} \text{ for } \frac{Kl}{r} < Cc \dots\dots\dots (2.28)$$

$$F_a = \frac{12\pi^2 E}{23\left(\frac{Kl}{r}\right)^2} \text{ for } \frac{Kl}{r} \geq Cc$$

Dimana:

$$Cc = \left[\frac{22\pi^2 E}{F_y}\right]^{\frac{1}{2}}$$

- E : *Modulus Elastisitas*; ksi (MPa)
- k : Faktor panjang efektif
- L : Panjang tanpa bracing
- r : Jari-jari girasi

Untuk $D/t > 60$ dengan menggunakan local buckling

a. *Local buckling elastic*

$$F_{xe} = \frac{2C_{et}}{D}$$

Dimana:

- C : Koefisien tegangan kritis buckling
- D : Diameter luar
- t : Ketebalan pipa

b. *Local buckling inelastic*

$$F_{xc} = F_y \left[1.64 - 0.23 \left(\frac{D}{t} \right)^{\frac{1}{4}} \right] \leq F_{xe} \dots\dots\dots (2.29)$$

$$F_{xc} = F_y \text{ untuk } \frac{D}{t} \leq 60$$

2.2.12 Konsep Analisa Keandalan

2.2.12.1 Konsep Analisa Keandalan dalam Perancangan

Keandalan sebuah komponen atau sistem adalah peluang komponen atau sistem tersebut untuk mengetahui tugas yang telah ditetapkan tanpa mengalami kegagalan selama kurun waktu tertentu apabila dioperasikan dengan benar dalam lingkungan tertentu (Rosyid, 2007). Pemakaian konsep analisa keandalan yang didasari oleh metode probabilitik telah berkembang dan semakin penting untuk memecahkan masalah-masalah dalam perancangan struktur. Kecenderungan ini karena adanya kerusakan pada sistem rekayasa yang disebabkan terjadinya interaksi oleh beban statis maupun dinamis.

Dalam konsep ini akan dijelaskan bagaimana perancangan dapat menggambarkan suatu sistem dengan segala hal yang akan mempengaruhi kerusakan pada sistem tersebut misalnya kondisi pembebanan, ketahanan struktur, kondisi lingkungan

yang melibatkan aspek ketidakpastian dalam analisa ini. Dalam ketidakpastian yang diterima oleh struktur dapat dikelompokkan menjadi 3 yaitu:

1. Variabilitas fisik

Adalah ketidakpastian yang bersifat acak atau bervariasi seperti beban lingkungan, sifat material dan ukuran material. Keragaman fisik ini biasanya dinyatakan dalam data sampel atas pertimbangan praktis dan ekonomis.

2. Ketidakpastian statik

Adalah ketidakpastian yang berhubungan dengan nilai suatu parameter. Data yang dibuat untuk membuat model diambil dari berbagai macam keragaman fisik diatas.

3. Ketidakpastian model

Adalah ketidakpastian yang diambil dari asumsi dari jenis struktur yang akan dimodelkan.

2.2.12.2 Jenis Metode Analisa Keandalan

1. Metode Analisa Keandalan Level-0

Metode ini pada dasarnya bukan merupakan metode analisa keandalan, tetapi metode untuk perancangan atau pemeriksaan keamanan stuktur. Dalam metode ini struktur dinyatakan berdasarkan pada stuktur elemen dasar dengan menggunakan faktor keamana parsial atau koefisien parsial yang berhubungan dengan karateristik awal dari perubahan beban dan struktur utama.

2. Metode Analisa Keandalan Level-2

Metode ini dilakukan dengan cara pendekatan iterasi untuk memperkirakan probabilitas kegagalan suatu struktur atau sub-struktur. Metode ini memiliki titik tunggal sebagai pengecekan pada bidang kegagalan (*failure surface*) yaitu $X = X_1, X_2, \dots, X_n$ yang dinyatakan dalam perubahan dasar (n), dimensi ω (*n – dimensional basic variavel space ω*).

Bidang kegagalan dibagi menjadi 2 daerah yaitu sebuah daerah kegagalan (*failure region ω_t*) dan sebuah daerah aman (*safe region ω_s*). Bidang kegaglan secara matematis dapat dinyatakan dengan persamaan berbentuk sebagai berikut:

$$f(x) = f(x_1, x_2, \dots, x_n = 0 \dots\dots\dots (2.30)$$

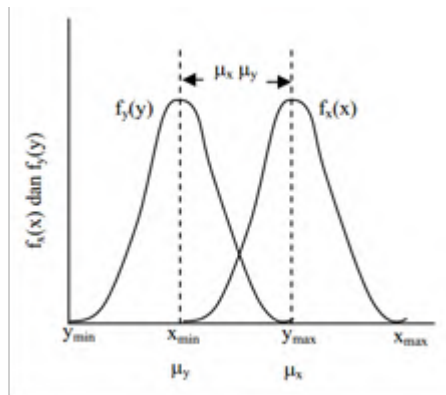
Harga positif dari persamaan diatas menunjukkan adanya daerah aman (*safe region*) dan harga negatif menunjukkan adanya daerah tidak aman (*failure region*).

2.2.12.3 Keandalan Pada Sistem Rekayasa

Pada dasarnya sistem keandalan dapat ditunjukkan sebagai problem dalam *demand* (tuntutan atau beban), *capacity* dan didasarkan atas *safety factor* (angka keamanan). Ukuran untuk konvensional angka keamanan adalah perbandingan antara asumsi nilai nominal kapasitas, X^* dan beban Y^* yang dirumuskan sebagai berikut:

$$Z^* = \frac{X^*}{Y^*} \dots\dots\dots (2.31)$$

Mengingat nilai nominal dari kapasitas, X^* dan beban, Y^* tidak dapat ditentukan dengan pasti, fungsi-fungsi kapasitas dan beban perlu dinyatakan sebagai peluang sebagaimana ditunjukkan pada Gambar 3.6. Dengan demikian, angka keamanan dinyatakan dengan perbandingan $Z = X/Y$ dari dua variabel acak X dan Y.



Gambar 2.9 Fungsi Kerapatan Peluang (fkp) dari kapasitas X dan tuntutan Y
(Rosyid, 2007)

2.2.12.4 Moda Kegagalan

Langkah pertama sebelum menentukan moda kegagalan adalah menentukan kegagalan yang akan dialami oleh struktur (Rosyid,2008). Moda Kegagalan terdiri dari dua parameter penting yaitu kekuatan dan beban.

MK = Kekuatan – Beban

MK = Tegangan izin-tegangan aktual

2.2.12.5 Simulasi Monte Carlo

Simulasi Monte Carlo adalah salah satu teknik asesmen risiko kuantitatif yang dapat digunakan oleh berbagai organisasi dalam proses manajemen risiko, terutama dalam tahapan analisis risiko dan/atau evaluasi risiko yang memiliki fenomena variabel acak (*random variable*). Analisis dan evaluasi risiko dengan fenomena variabel acak tidak hanya terjadi untuk peristiwa-peristiwa risiko pasar (*market risk*), risiko kredit (*credit risk*), dan risiko operasional (*operational risk*) dalam dunia perbankan, tetapi juga untuk risiko operasional di berbagai industri lain misalnya industri minyak dan gas (*oil and gas*) dan pertambangan (*mining*). Unsur pokok yang diperlukan didalam simulasi Monte Carlo adalah sebuah *random number generator* (RNG). Hal ini karena, secara teknis, prinsip dasar metode simultan Monte Carlo sebenarnya adalah sampling numerik dengan bantuan RNG, dimana simulasi dilakukan dengan mengambil beberapa sampel dari perubah acak berdasarkan distribusi peluang perubah acak tersebut. Ini berarti, Simulasi Monte Carlo mensyaratkan bahwa distribusi peluang dari perubah acak yang terlibat di dalam sistem yang sedang dipelajari telah diketahui atau dapat diasumsikan. Sampel yang telah diambil tersebut dipakai sebagai masukan ke dalam persamaan fungsi kinerja $FK(x)$, dan harga $FK(x)$ kemudian dihitung. Untuk suatu fungsi kinerja tertentu, misalnya, setiap kali $FK(x) < 0$, maka sistem/komponen yang ditinjau dianggap gagal. Jika jumlah sampel tersebut adalah N (atau replikasi sejumlah N), maka dapat dicatat kejadian $FK(x) < 0$ sejumlah n kali. Dengan demikian, peluang kegagalan sistem/komponen yang sedang ditinjau adalah rasio antara jumlah kejadian gagal dengan sampel atau replikasi, $P_g = n/N$.

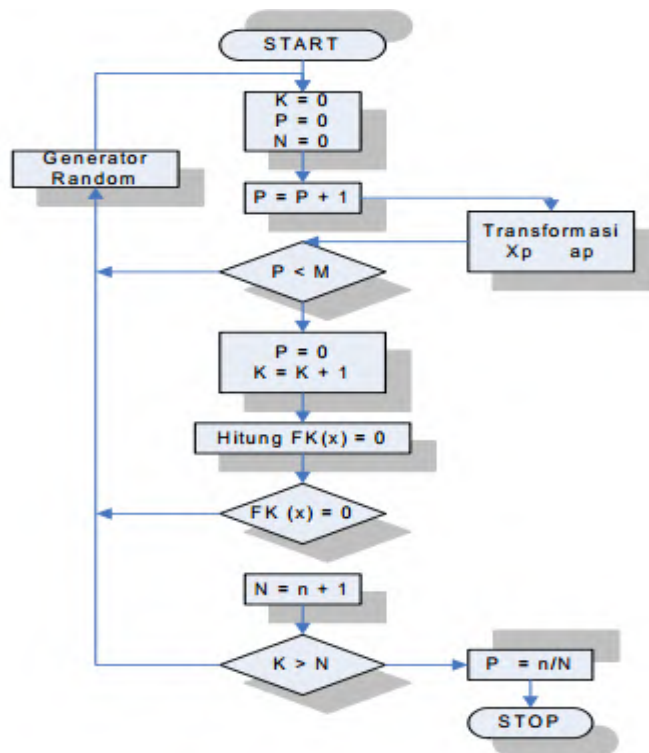
Persoalan utama di dalam simulasi Monte Carlo adalah bagaimana mentransformasikan angka acak yang dikeluarkan oleh *random number generator* (RNG) menjadi besaran fisis yang sesuai dengan fungsi kerapatan peluang (f_{kp})nya. Ini disebabkan karena angka acak yang dikeluarkan oleh RNG memiliki f_{kp} uniform, sedangkan perubah dasar dalam $FK(x)$ seringkali tidak demikian (misal terdistribusi secara normal, lognormal, dan sebagainya). RNG biasanya ada dalam CPU komputer sebagai built-in computer program dalam bagian ROM-nya. RNG yang disediakan ini hampir selalu berbentuk linear congruential generator yang

mengeluarkan suatu deretan bilangan cacah (integer) I_1, I_2, I_3, \dots , masing - masing antara 0 dan $m-1$ (mesebuah bilangan yang besar sekali) dengan menggunakan sebuah relasi rekurens berikut:

$$I_{j+1} = aI_j + C \pmod{m} \dots\dots\dots (2.32)$$

Dengan m disebut modulus, dan a adalah bilangan cacah (*integer*) yang berturut-turut disebut sebagai pengganda dan inkremen. Relasi rekuens di atas akan berulang dengan periode yang lebih kecil dari m . Jika m, a, c , dipilih secara seksama, maka periode ulang yang terjadi akan memiliki panjang maksimum. Dalam hal itu, semua bilangan cacah (*integer*) antara 0 dan $m-1$ akan muncul, sehingga setiap pilihan akan menghasilkan deret yang secara statistik sama baiknya.

Semua angka acak $a_p, P = 1, 2 \dots M$, dengan $f_k p$ uniform akan dikeluarkan oleh RNG untuk kemudian ditransformasikan menjadi $XP, P = 1, 2, \dots, M$. Transformasi a_P (bilangan acak) menjadi nilai XP (perubah acak ke P) dapat dilakukan dengan menggunakan persamaan distribusi kumulatif dari masing-masing perubah acak. Ini berarti bahwa pada loop paling atas pada gambar tersebut terdapat prosedur transformasi ini, dan untuk setiap perubah acak dihitung sendiri-sendiri sesuai dengan distribusi peluangnya (f_{kp}). Jika bilangan acak telah ditransformasikan menjadi nilai dari perubah acak, $FK(x)$ kemudian dihitung, ini adalah kondisi sukses (tidak gagal) dan eksperimen dilanjutkan; sedang apabila $FK(x) \geq 0$, maka ini adalah kondisi sukses (tidak gagal) dan eksperimen dilanjutkan; sedang apabila $FK(x) < 0$, maka ini dicatat dan simpan dalam n . Eksperimen ke k dilanjutkan sampai $K = N$, sesudah itu peluang kegagalan sistem/komponen dihitung sebagai n/N .



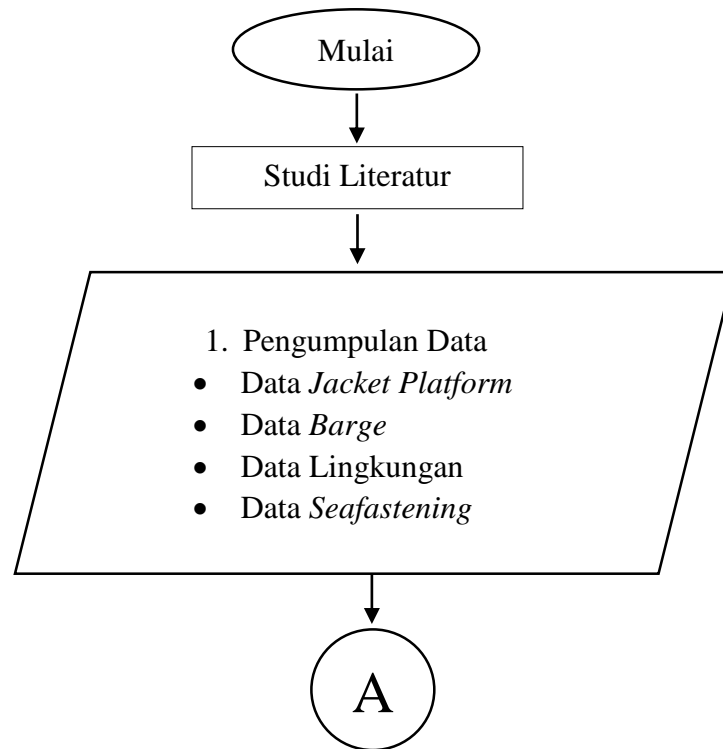
Gambar 2.10 Algoritma Untuk Simulasi Monte Carlo (Rosyid, 2007)

(halaman ini sengaja dikosongkan)

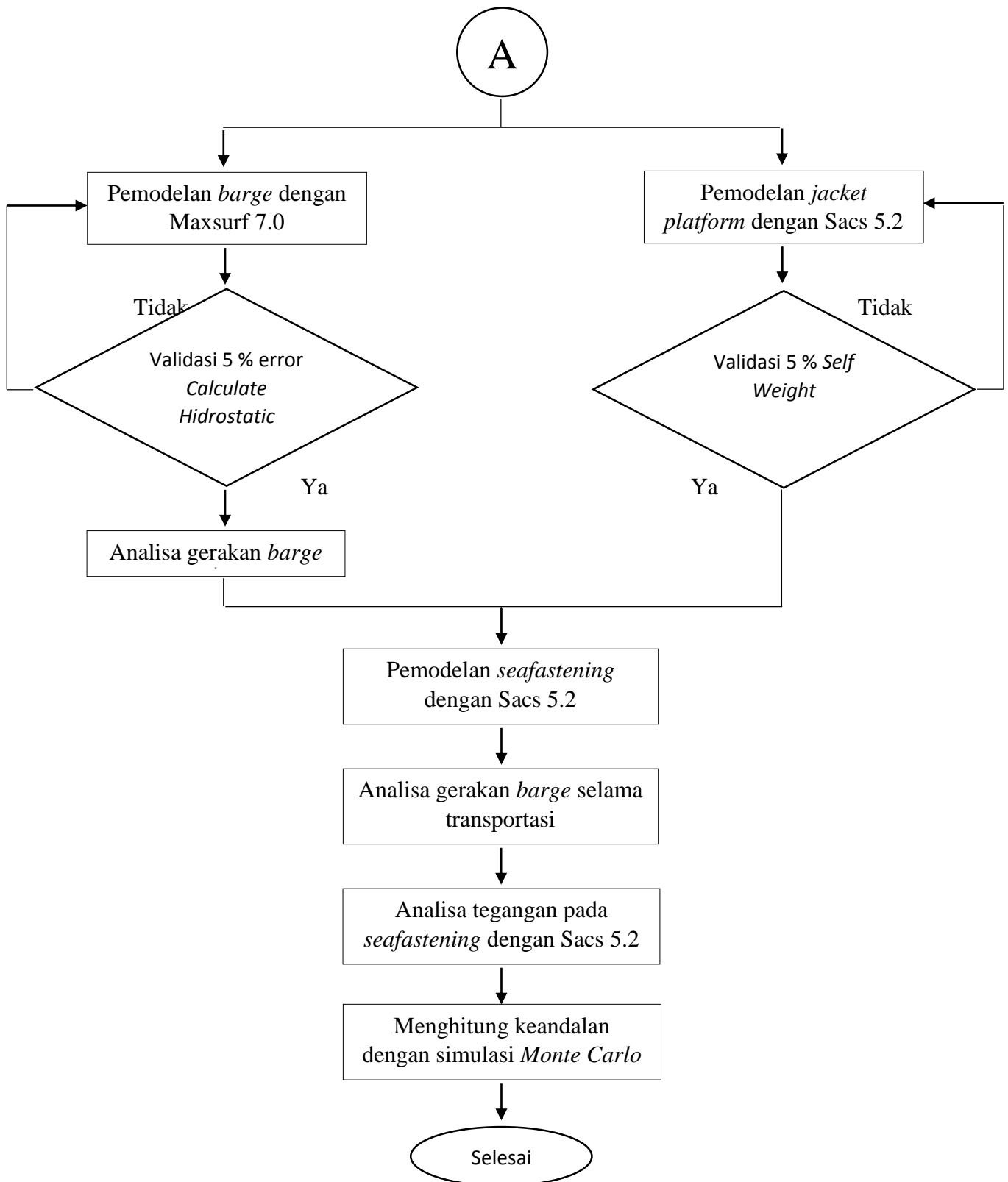
BAB III METODOLOGI PENELITIAN

3.1 Diagram Alir Umum

Berikut ini adalah alur penelitian yang digunakan dalam pengerjaan tugas akhir.

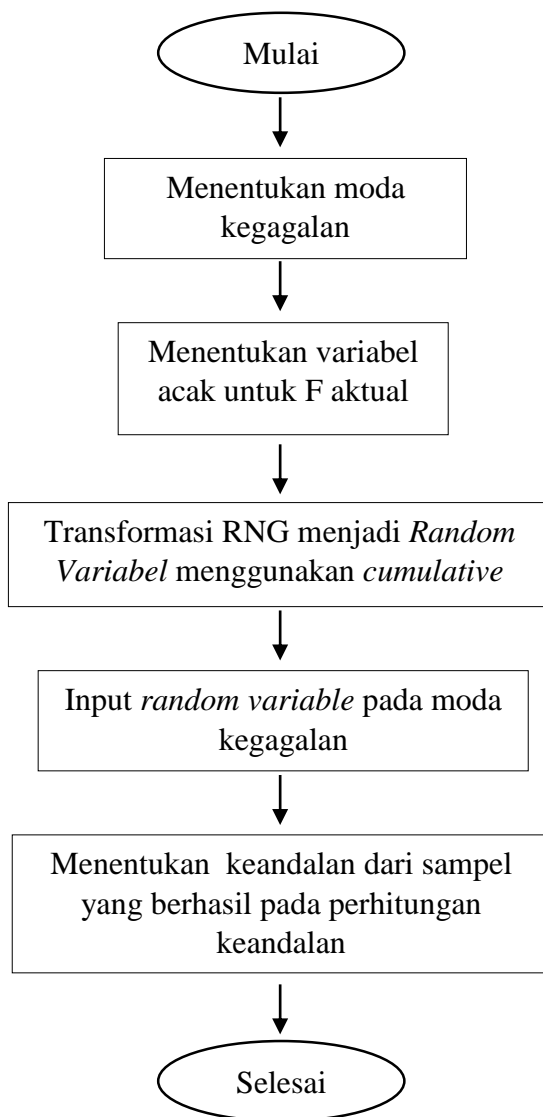


Gambar 3.1 Gambar Diagram Pengerjaan Tugas Akhir



Gambar 3.2 Gambar Diagram Pengerjaan Tugas Akhir (lanjutan)

Diagram Alir Keandalan



Gambar 3.3 Gambar Diagram Pengerjaan Tugas Akhir (Simulasi *Monte Carlo*)

3.2 Penjelasan Diagram Alir

1. Studi Literatur

Langkah pertama dalam prosedur pengerjaan tugas akhir ini adalah mempelajari buku, jurnal, penelitian, diktat dan tugas akhir.

2. Pengumpulan Data

Selanjutnya data yang relevan akan dijadikan referensi dalam mengerjakan tugas akhir. Selain itu juga dilakukan pencarian data-data berupa data struktur, *seafastening*, *barge*, lingkungan.

1. Pemodelan Struktur

a) Pemodelan *Barge*

Setelah mendapatkan data *barge*, maka dilakukan pemodelan *barge* dengan menggunakan *Software Moses 7.0*. Hasil parameter hidrostatis akan dijadikan sebagai parameter validasi. Setelah dimodelkan, akan dilakukan validasi *calculate hidrostatic* dengan tingkat error $< 5\%$. Jika tidak valid, maka akan dilakukan pemodelan ulang. Sedangkan jika valid maka akan dilanjutkan dengan analisa *motion barge* dengan keadaan free tanpa *load case jacket platform*.

b) Pemodelan *Jacket Platform*

Struktur jacket platform dimodelkan dengan menggunakan software *Sacs 5.2*. Setelah semua properti struktur dimasukkan dalam pemodelan, data berat struktur dijadikan parameter validasi dengan berat struktur dari PT.PAL Indonesia. Akan diberlakukan sistem yang sama dengan permodelan *barge*, akan dilakukan validasi sebesar 5 %.

4. Pemodelan Struktur *Seafastening*

Struktur *seafastening* akan dimodelkan dengan menggunakan software *Sacs 5.2* dan desain struktur ini yang akan diintegriti dengan pemodelan *barge* dan *jacket platform* yang berguna untuk memperhitungkan analisa gerak selama transportasi dan kekuatan struktur *seafastening* selama transportasi.

5. Analisa Gerak *Barge*

Langkah selanjutnya adalah menghitung respons *barge* akibat pengaruh beban lingkungan (gelombang, angin, dan arus). *Output* yang didapatkan adalah parameter gerak *barge* berupa *surge*, *sway*, *heave*, *roll*, *pitch*, *yaw*. Dengan menggunakan *software* didapatkan akselerasi maksimum dari setiap gerakan.

6. Analisis Tegangan Pada *Seafastening*

Dari data yang didapat, kemudian dilakukan perhitungan untuk mendapatkan UC terbesar pada struktur *seafastening*. Setelah perhitungan, UC terbesar akan dijadikan sebagai acuan dalam analisa keandalan struktur.

7. Analisa Keandalan Struktur dengan Metode *Monte Carlo*

Dengan menggunakan codes API RP 2A WSD, *axial compression stress* dijadikan sebagai moda kegagalan yang digunakan.

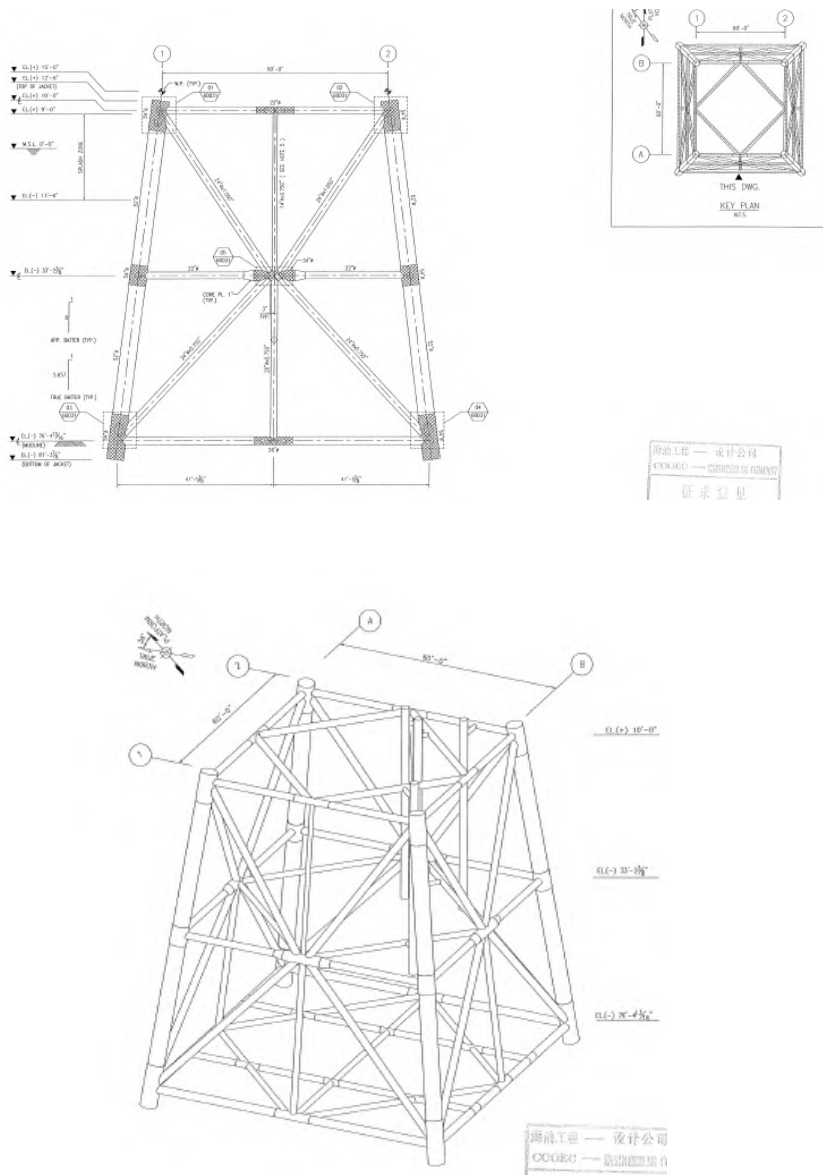
3.3 Pengumpulan Data

3.3.1 Data *Jacket* Struktur

Dalam tugas akhir ini struktur *Jacket* K-GAS Banuwati yang digunakan sebagai obyek penelitian. Struktur ini berjenis kompressor *platform* yang diangkut dari fabrikasi PT.PAL ke Utara Jakarta di Block Banuwati. *Jacket* K-GAS Banuwati menopang 1 struktur *main deck* pada EL (+) 17.67 m dari MSL, *cellar deck* pada EL (+) 10.6 m dari MSL dan sebuah *sub cellar deck* dengan EL (+) 7.015 m dari MSL. *Jacket leg* mempunyai OD 52". Berikut ini adalah data *jacket* struktur yang telah diproduksi PT.PAL

Tabel 3.1 Data *Jacket* Struktur

| Karakteristik | Deskripsi |
|---------------------------------|---------------|
| Jenis struktur | Kompresor gas |
| Jumlah kaki | 4 |
| Batter | 5.657 |
| Panjang kaki (m) | 23.28 |
| Jumlah elevasi horizontal frame | 3 |
| Jarak antar leg (m) | 18.288 |
| OD jacket leg (m) | 1.32 |



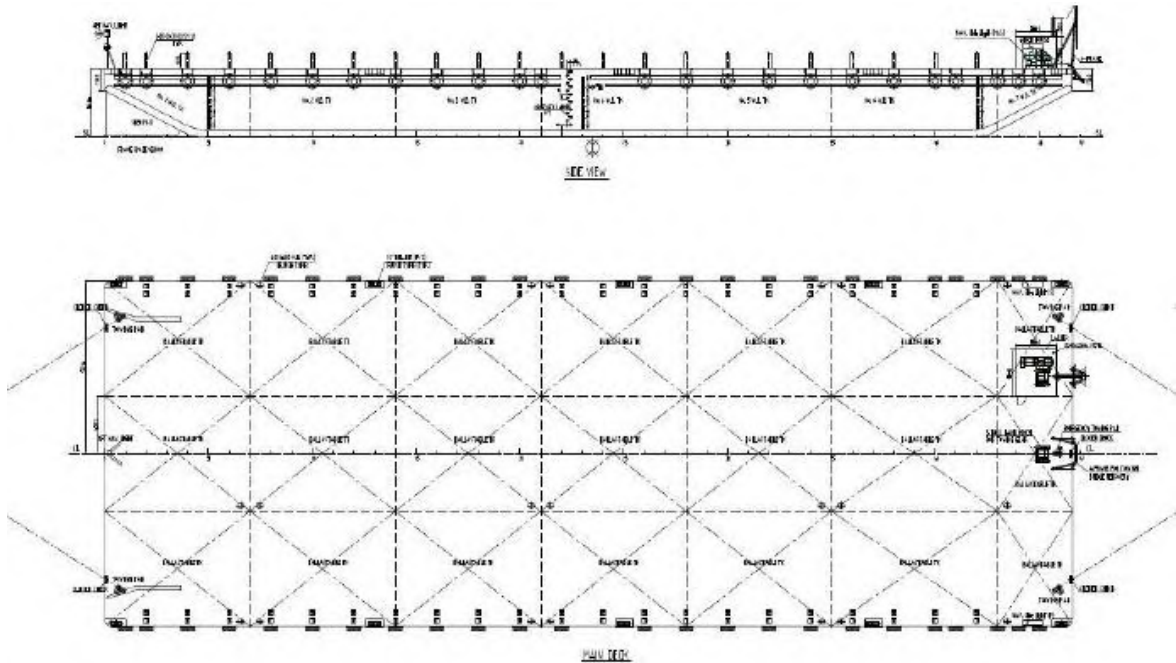
Gambar 3.4 General Arrangement *Jacket* Platform

3.3.2 Data Barge

Barge yang digunakan untuk *seafastening* dan transportasi K-GAS Platform Banuwati adalah “EOS 281”. Dimensinya adalah 280 x 90 x 18 ft dengan ukuran utamanya sebagai berikut :

Tabel 3.2 Data Barge

| | |
|-----------------|---------|
| LOA | 85.34 m |
| Breadth | 27.43 m |
| Height | 5.48 m |
| Extreme Draught | 4.3 m |



Gambar 3.5 General Arrangement EOS 281

3.3.3 Data Lingkungan

Data kondisi lingkungan dimana proses transportasi akan dilakukan adalah :

Tabel 3.3 Data Lingkungan

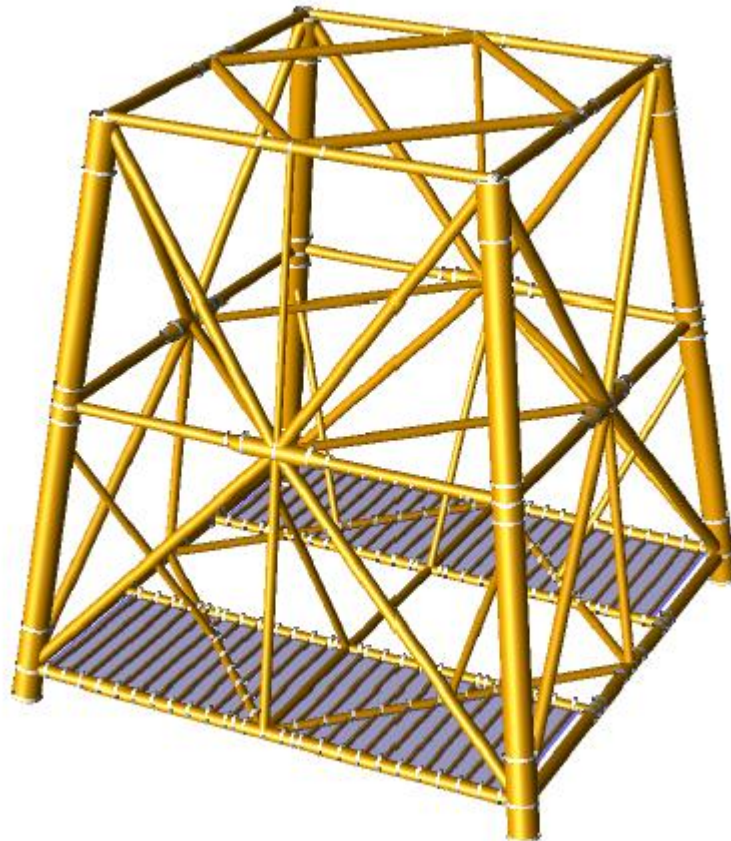
| Parameter | Value | |
|---------------------|--------|---------|
| | 1 year | 25 year |
| Hs (m) | 1,8 | 4,4 |
| Ts (Sec) | 4,98 | 7,14 |
| Wind Speed (m/s) | 15 | 27,5 |
| Current Speed (m/s) | 0,65 | 0,88 |

Data pada tabel di atas didapatkan dari PT.PAL Indonesia yang digunakan saat transportasi *Jacket Platform* Banuwati ke *South East Sumatera Block*. Data yang didapat merupakan data untuk arah pembebanan *omnidirectional* yang berarti nilainya sama untuk semua arah pembebanan. Data yang digunakan dalam penelitian tugas akhir ini adalah data lingkungan 1 tahunan.

BAB IV ANALISIS DATA DAN PEMBAHASAN

4.1 Pemodelan Struktur *Jacket*

Dari data struktur yang telah didapatkan maka dibuat model struktur *jacket* dengan perangkat lunak SACS.5.2. Setelah semua property struktur dimasukkan dalam model, data berat struktur dijadikan parameter validasi dengan data berat struktur dari PT.PAL.



Gambar 4.1 Model Struktur *Jacket* dengan SACS 5.2

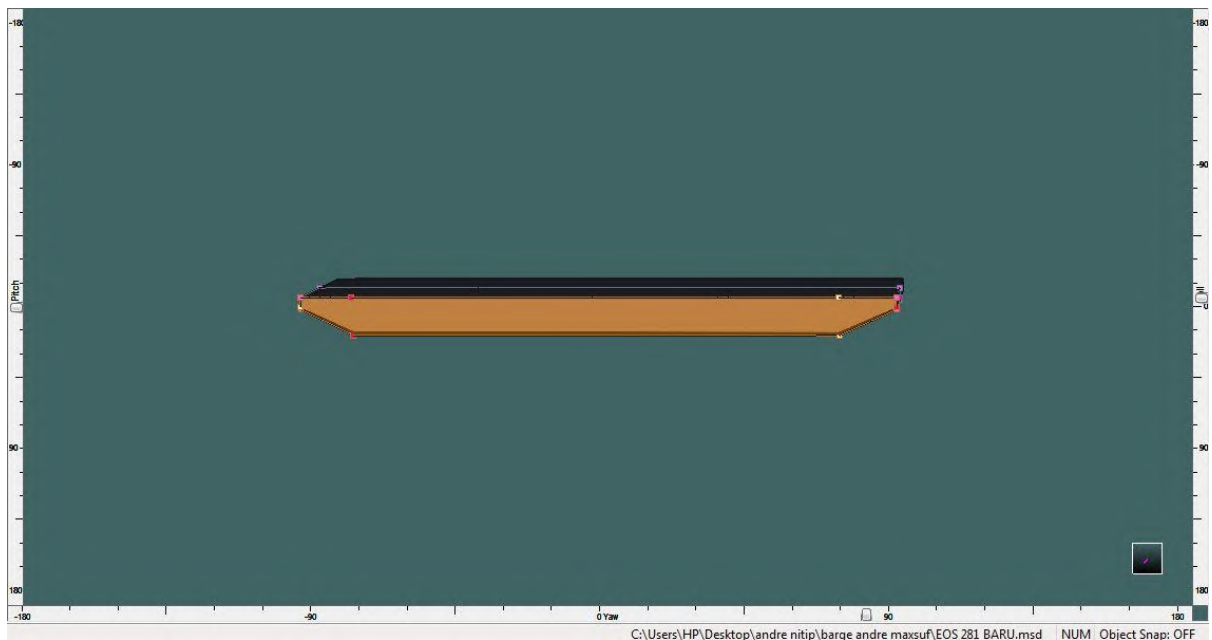
Tabel 4.1 Validasi *Jacket*

| Kondisi Self Weight | | | |
|---------------------|----------|---------|-------------|
| Parameter | Data | Sacs | Correction |
| Wight (kips) | 1198,435 | 1194,66 | 0,315989487 |
| Wight (tons) | 535,01 | 533,33 | 0,315001969 |

| Kondisi Self Weight + Support Weight | | | |
|--------------------------------------|---------|-----------|-------------|
| Parameter | Data | Sacs | Correction |
| Wight (kips) | 1621,22 | 1617,5372 | 0,227679462 |
| Wight (tons) | 723,250 | 722,114 | 0,157315881 |

4.2 Pemodelan *Barge*

Pembuatan model *barge* dengan menggunakan perangkat lunak MAXSURF dan hasil parameter hidrostatis digunakan sebagai parameter validasi. Pembebanan yang dilakukan pada pemodelan dengan MAXSURF yakni berupa *payload* yang diwakili dengan sarat air (*draught*) *barge*.



Gambar 4.2. Model *Barge* dengan Menggunakan MAXSURF

4.3 Hidrostatik

Setelah permodelan barge EOS 281 selesai dimodelkan dengan *software* Maxsurf maka dilakukan validasi *barge* dengan menggunakan data hasil luaran software dengan data hidrostatik yang didapatkan dari *stability booklet*. Untuk validasi *barge* akan dilakukan dengan perbandingan antara 2 *draft* yaitu *draft* dalam kondisi *lightship* dan *loaded* yang masing – masing 0,85 m dan 4,3 m.

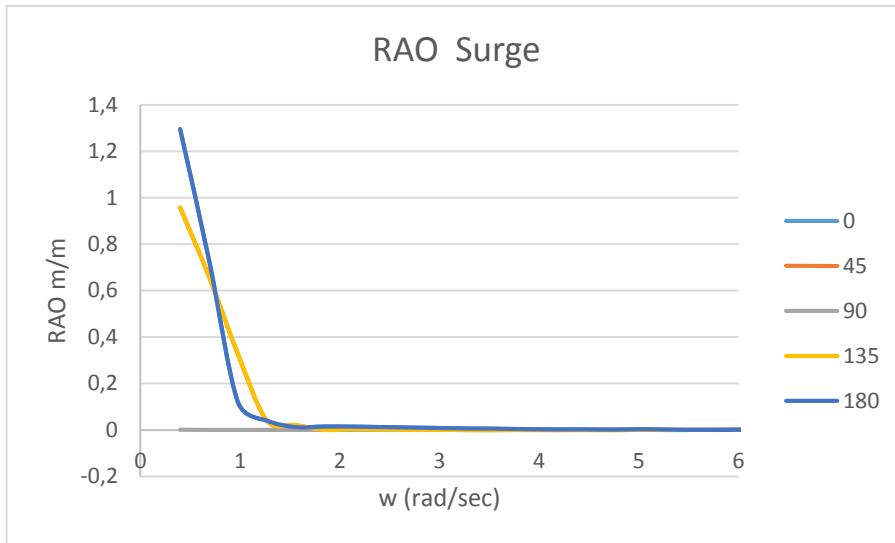
Tabel 4.2 Validasi *Barge*

| Draft 0,85 | Maxsurf | Data | Correction |
|--------------------|---------|----------|--------------|
| Displacement | 1676 | 1702,853 | -1,576941756 |
| Volume (displaced) | 1635 | 1636,034 | -0,063201621 |
| LCB length | 42 | 42,583 | -0,371040086 |
| LCF length | 42,433 | 42,562 | -0,303087261 |
| KB | 0,432 | 0,427 | 1,170960187 |
| KMt | 77,326 | 76,737 | 0,76755672 |
| KML | 549 | 547,802 | 0,218692155 |

| Draft 4,3 | Maxsurf | Data | Correction |
|--------------------|---------|----------|--------------|
| Displacement | 9466 | 9510,225 | -0,465025801 |
| Volume (displaced) | 9235 | 9242,149 | -0,07735214 |
| LCB length | 43 | 42,636 | -0,204052913 |
| LCF length | 42,67 | 42,67 | 0 |
| KB | 2,235 | 2,229 | 0,269179004 |
| KMt | 18,1 | 18,084 | 0,088476001 |
| KML | 156 | 155,416 | 0,375765687 |

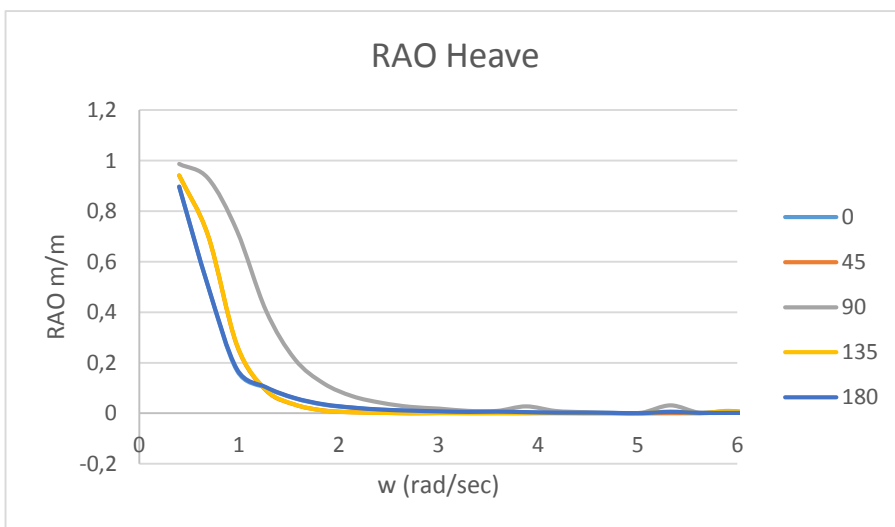
4.4 *Response Amplitude Operator (RAO) Lightship*

Pada tahap ini perilaku gerak *barge* pada saat kondisi *lightship* dianalisis menggunakan *software* Maxsurf dengan metode *strip theory*. Hasil yang diperoleh dari analisis tersebut adalah grafik RAO dengan arah 0° , 45° , 90° , 135° , 180° . RAO ini menunjukkan perilaku gerakan *barge* di gelombang reguler. Grafik fungsi transfer (RAO) untuk masing-masing arah pembebanan (*heading*) dan masing-masing derajat kebebasan dapat dilihat pada Gambar 4.3-4.8.



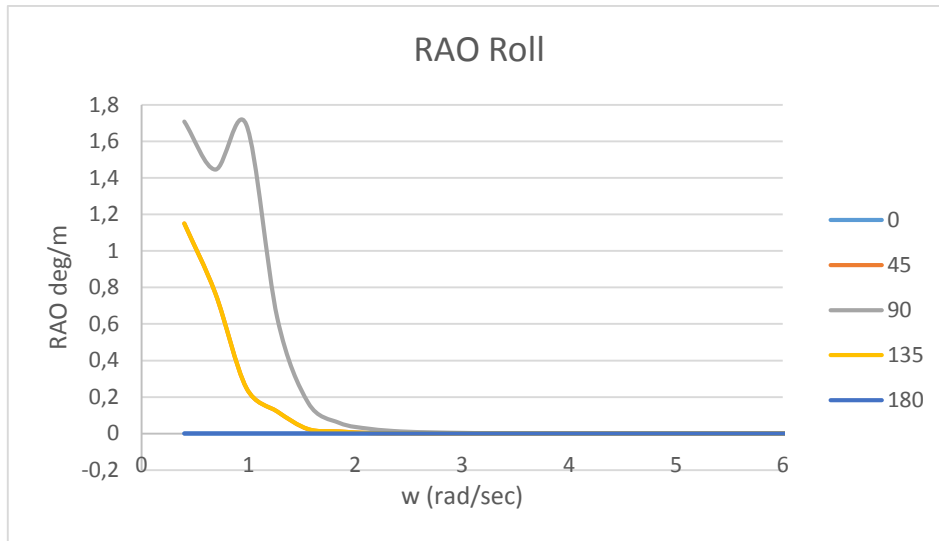
Gambar 4.3 Grafik RAO Gerakan *Surge*

Pada gambar 4.3 diatas menunjukkan grafik RAO *Surge* kondisi *lightship* dengan variasi *heading* 0 °, 45 °, 90 °, 135 °, 180 ° . Gerakan *surge* dominan pada saat gelombang 180 ° sebesar 1,296 m/m dan frekuensi gelombang datang 0,4 rad/s.



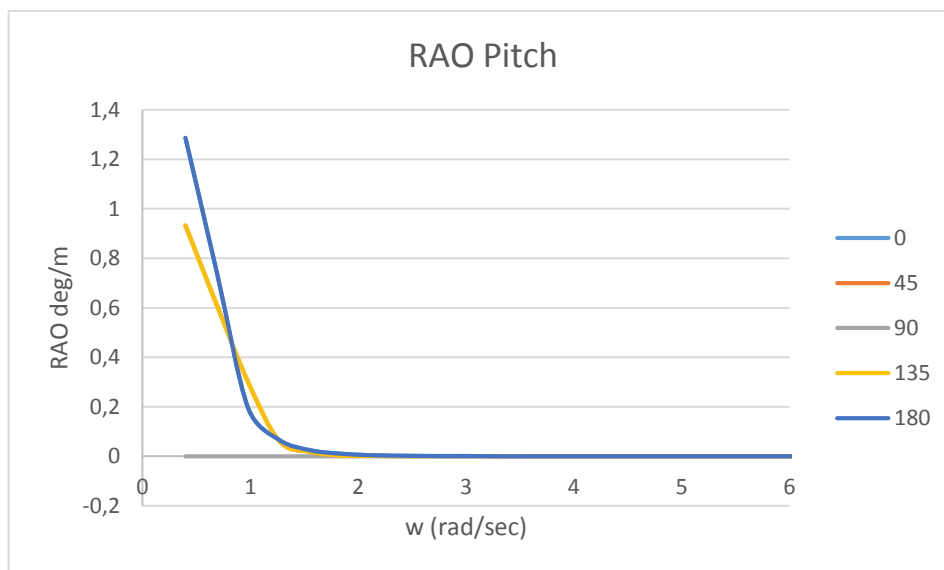
Gambar 4.4 Grafik RAO Gerakan *Heave*

Pada gambar 4.4 diatas menunjukkan grafik RAO *Heave* kondisi *lightship* dengan variasi *heading* 0 °, 45 °, 90 °, 135 °, 180 ° . Gerakan *Heave* dominan pada saat gelombang 90 ° sebesar 0,987 m/m dan frekuensi gelombang datang 0,4 rad/s.



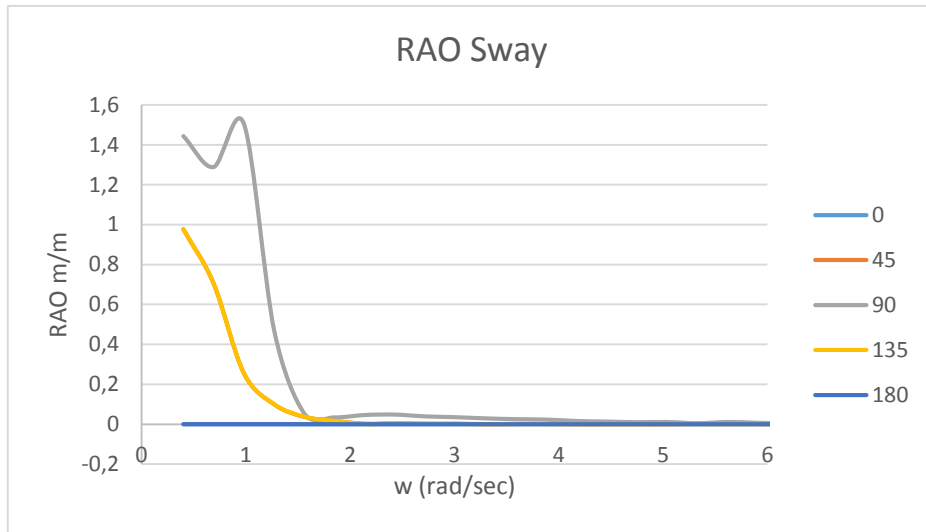
Gambar 4.5 Grafik RAO Gerakan *Roll*

Pada gambar 4.5 diatas menunjukkan grafik RAO *Roll* kondisi *lightship* dengan variasi *heading* 0 °, 45 °, 90 °, 135 °, 180 ° . Gerakan *Roll* dominan pada saat gelombang 90 ° sebesar 1,709 deg/m dan frekuensi gelombang datang 0,4 rad/s.



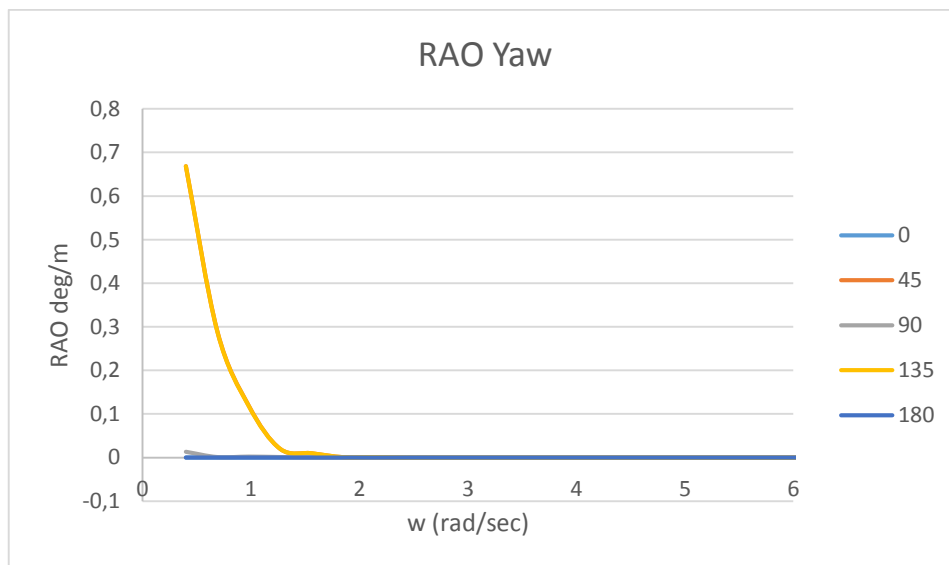
Gambar 4.6 Grafik RAO Gerakan *Pitch*

Pada gambar 4.6 diatas menunjukkan grafik RAO *Picth* kondisi *lightship* dengan variasi *heading* 0 °, 45 °, 90 °, 135 °, 180 ° . Gerakan *Pitch* dominan pada saat gelombang 180 ° sebesar 1,287 deg/m dan frekuensi gelombang datang 0,4 rad/s.



Gambar 4.7 Grafik RAO Gerakan Sway

Pada gambar 4.7 diatas menunjukkan grafik RAO Sway kondisi *lightship* dengan variasi heading 0°, 45°, 90°, 135°, 180°. Gerakan Sway dominan pada saat gelombang 90° sebesar 1,443 m/m dan frekuensi gelombang datang 0,4 rad/s.



Gambar 4.8 Grafik RAO Gerakan Yaw

Pada gambar 4.8 diatas menunjukkan grafik RAO Yaw kondisi *lightship* dengan variasi heading 0°, 45°, 90°, 135°, 180°. Gerakan Yaw dominan pada saat gelombang 135° sebesar 0,668 deg/m dan frekuensi gelombang datang 0,4 rad/s.

4.5 Analisa Stabilitas *Barge*

Stabilitas adalah kemampuan dari suatu benda yang melayang, yang miring untuk kembali berkedudukan tegak lagi atau kembali pada posisi semula. Sebagai persyaratan yang wajib, tentunya stabilitas *barge* harus mengacu pada standar yang telah ditetapkan oleh Biro Klasifikasi atau *Marine Authority* seperti *International Maritime Organisation (IMO) Code A.749(18) Ch 3 - design criteria applicable to all ships*.

Tabel 4.3 Tabel Hidrostatik

| Full load | |
|-------------------------------|---------|
| Draft Amidships m | 4,318 |
| Displacement t | 9509 |
| Heel deg | 0 |
| Trim (+ve by stern) m | 0 |
| Trim angle (+ve by stern) deg | 0 |
| KG fluid m | 5,608 |
| BMt m | 15,822 |
| MTc tonne.m | 166,889 |

| Half Load | |
|-------------------------------|---------|
| Draft Amidships m | 2,286 |
| Displacement t | 4754 |
| Heel deg | 0 |
| Trim (+ve by stern) m | 0 |
| Trim angle (+ve by stern) deg | -0,0001 |
| KG fluid m | 8,923 |
| BMt m | 29,37 |
| MTc tonne.m | 132,617 |

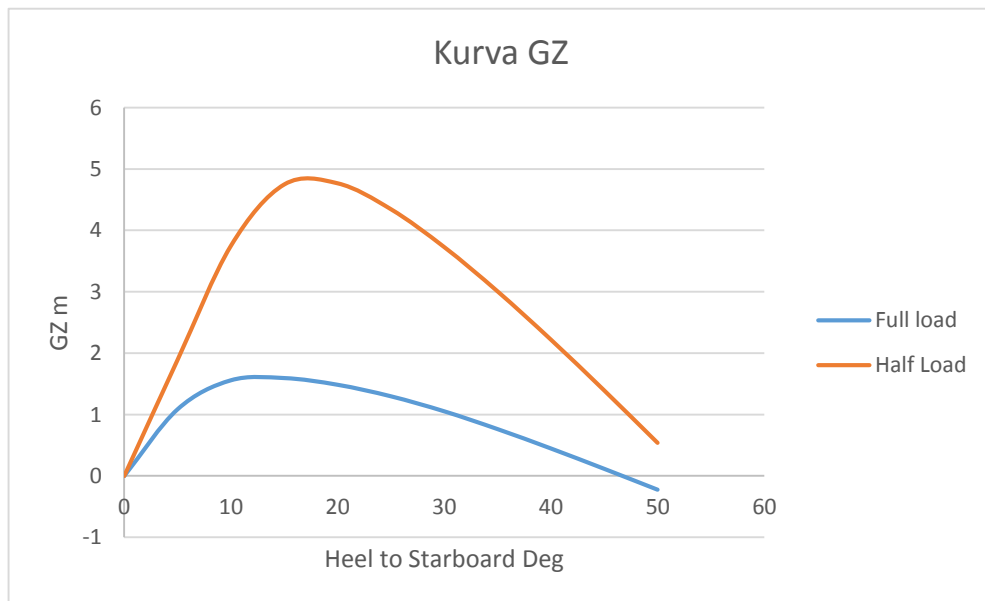
Berikut data hidrostatik dari kondisi *full load* dan *half load*. Tabel 4.3 diatas menjelaskan bahwa kondisi *barge* ketika mengangkut *jacket platform* dari setiap kondisi adalah *even keel*.

Menurut *IMO A.749 chapter 4.7* kriteria stabilitas untuk *pontoon* adalah sebagai berikut:

1. *Area under GZ* sampai dengan sudut maksimum tidak boleh kurang dari 0,08 m.rad.
2. *Minimum range stability* $LOA \leq 100$ m adalah 20° .

Tabel 4.4 Tabel Lengan *Righting Momen* dari Setiap Kondisi *Barge*

| Heel to starboard deg | GZ m | |
|-----------------------|-----------|-----------|
| | FULL LOAD | HALF LOAD |
| 0 | 0 | 0 |
| 5 | 1,087 | 1,891 |
| 10 | 1,56 | 3,748 |
| 15 | 1,596 | 4,747 |
| 20 | 1,487 | 4,766 |
| 25 | 1,299 | 4,344 |
| 30 | 1,054 | 3,727 |
| 35 | 0,764 | 3,006 |
| 40 | 0,448 | 2,22 |
| 45 | 0,116 | 1,392 |
| 50 | -0,224 | 0,539 |

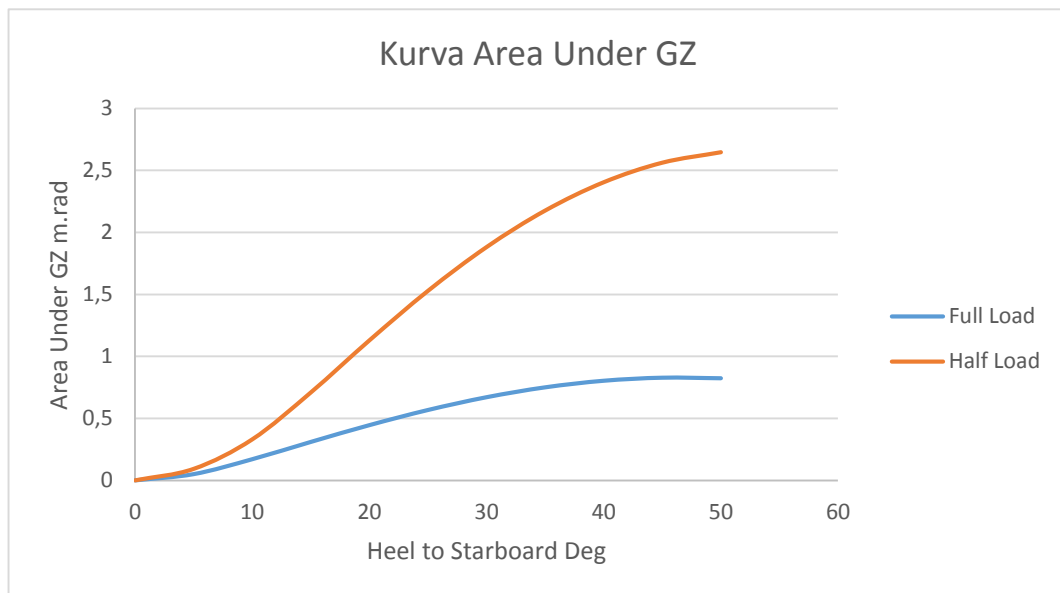


Gambar 4.9 Kurva Lengan *Righting Moment* dari Setiap Kondisi

Dari tabel dan kurva diatas menunjukkan besar lengan *righting moment* di beberapa sudut *heel* yaitu 0° , 10° , 20° , 30° , 40° dan 50° dari setiap kondisi *barge*.

Tabel 4.5 Tabel *Righting Momen* dari Setiap Kondisi *Barge*

| Area Under GZ | |
|---------------|-----------|
| FULL LOAD | HALF LOAD |
| 0 | 0 |
| 0,0504 | 0,0927 |
| 0,1704 | 0,3308 |
| 0,3099 | 0,7094 |
| 0,4451 | 1,1297 |
| 0,5671 | 1,5291 |
| 0,6701 | 1,8822 |
| 0,7497 | 2,1766 |
| 0,8027 | 2,405 |
| 0,8274 | 2,5628 |
| 0,8228 | 2,6472 |

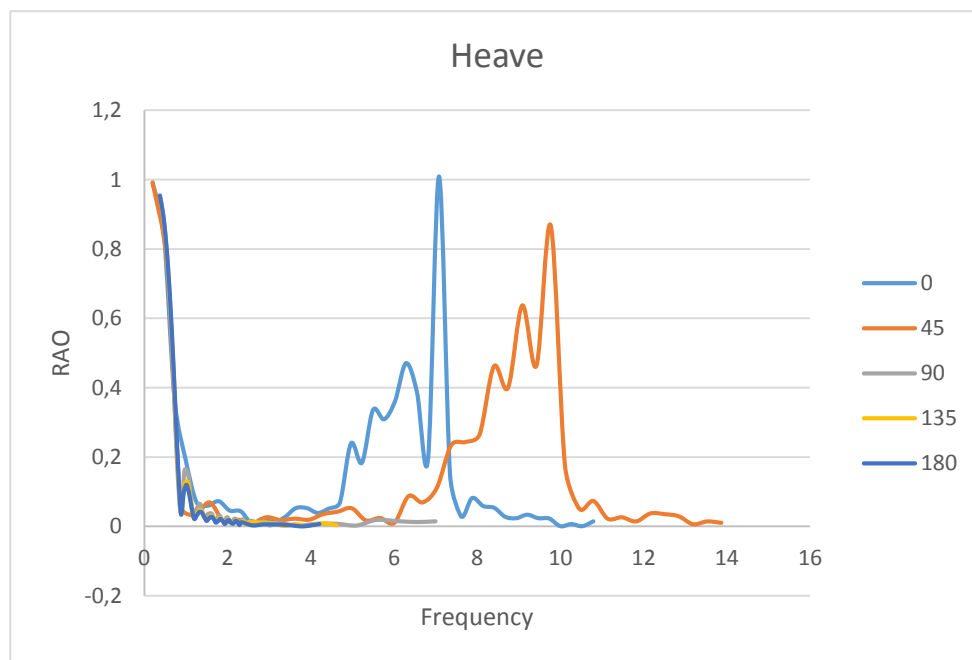


Gambar 4.10 Kurva *Righting Moment* dari Setiap Kondisi *Barge*

Tabel dan kurva diatas menunjukkan besar *righting moment* di beberapa sudut *heel* yaitu 0° , 10° , 20° , 30° , 40° dan 50° dari setiap kondisi *barge*. Hasil dari analisis stabilitas dilihat dari kurva GZ m dan *area under GZ* dengan mengacu pada IMO, kondisi *barge* terstabil adalah ketika kondisi *half load* dikarenakan panjang lengan *righting moment* pada kondisi tersebut sebesar 0,539 pada *heel* 50° dan *righting moment* pada kondisi tersebut sebesar 2,6472 pada *heel* 50° .

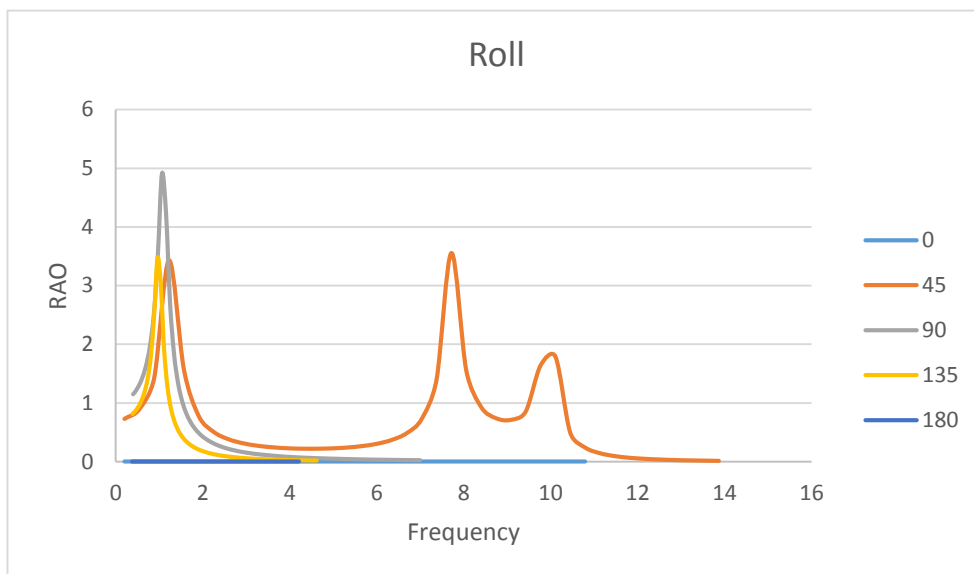
4.6 Analisis Gerak *Barge* pada Kondisi *Half Load*

Dari hasil analisis stabilitas sebelumnya, didapatkan kondisi *barge* yang paling stabil adalah pada kondisi *half load*. Dalam kondisi *loaded* untuk proses transportasi EOS 281 dilakukan analisis gerak *barge* dengan menggunakan *software* MAXSURF dan metode *strip theory*. Dilakukan analisis dengan kondisi lingkungan transportasi laut utara jawa dengan kecepatan 3 knots serta variasi *heading* 0° , 45° , 90° , 135° , 180° . *Response Amplitude Operator* dalam keadaan *loaded* yang ditinjau dari 3 gerakan yaitu *Heave*, *Roll*, *Pitch*.



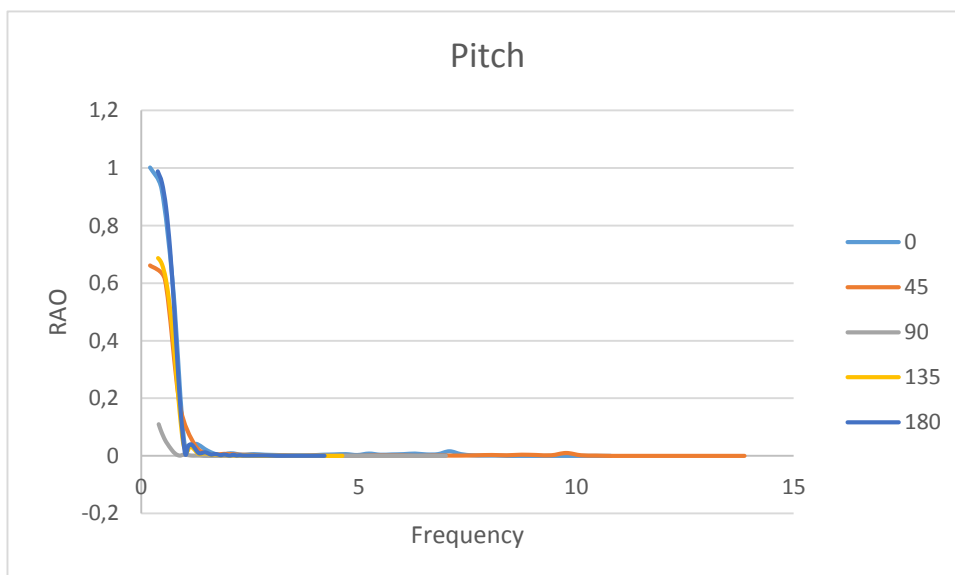
Gambar 4.11 Grafik RAO Gerakan *Heave*

Pada gambar 4.11 diatas menunjukkan grafik RAO *Heave* kondisi transportasi dengan variasi *heading* 0° , 45° , 90° , 135° , 180° . Gerakan *heave* dominan pada saat gelombang 0° sebesar 0,99 m/m.



Gambar 4.12 Grafik RAO Gerakan *Roll*

Pada gambar 4.12 diatas menunjukkan grafik RAO *Roll* kondisi transportasi dengan variasi heading 0 °, 45 °, 90 °, 135 °, 180 ° . Gerakan *roll* dominan pada saat gelombang 90 ° sebesar 4,92 deg/m.

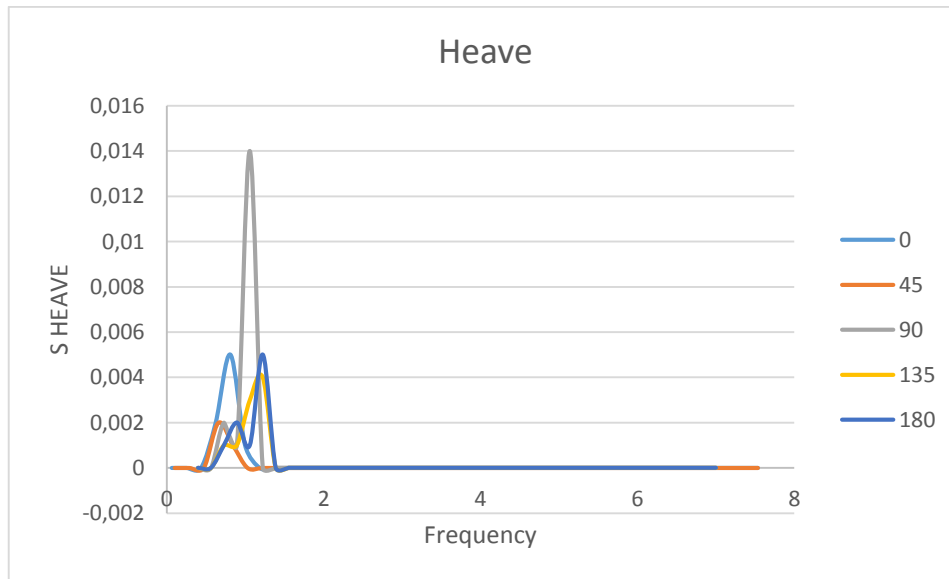


Gambar 4.13 Grafik RAO Gerakan *Pitch*

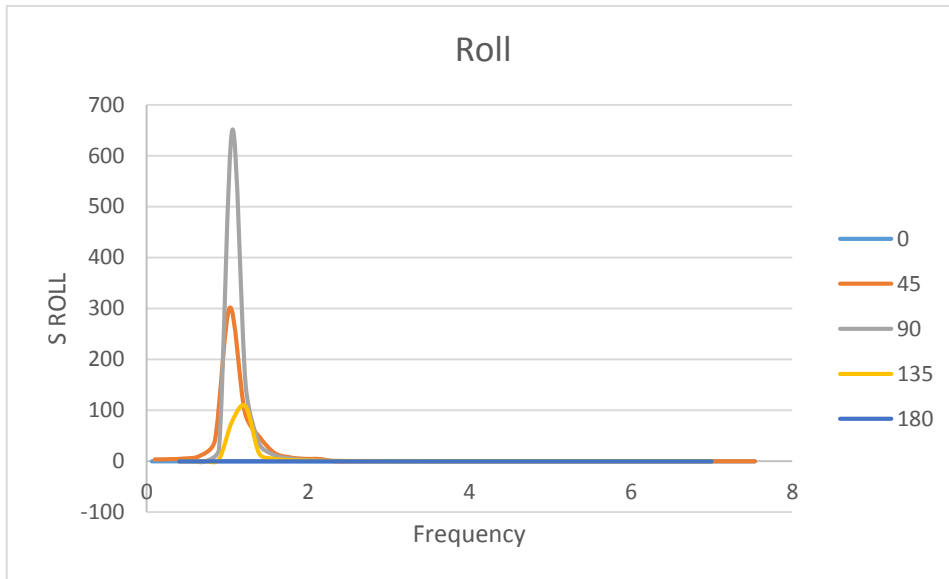
Pada gambar 4.13 diatas menunjukkan grafik RAO *Pitch* kondisi transportasi dengan variasi heading 0 °, 45 °, 90 °, 135 °, 180 ° . Gerakan *pitch* dominan pada saat gelombang 0 ° sebesar 0,989 deg/m.

4.7 Spektra Respon EOS 281 Selama Transportasi

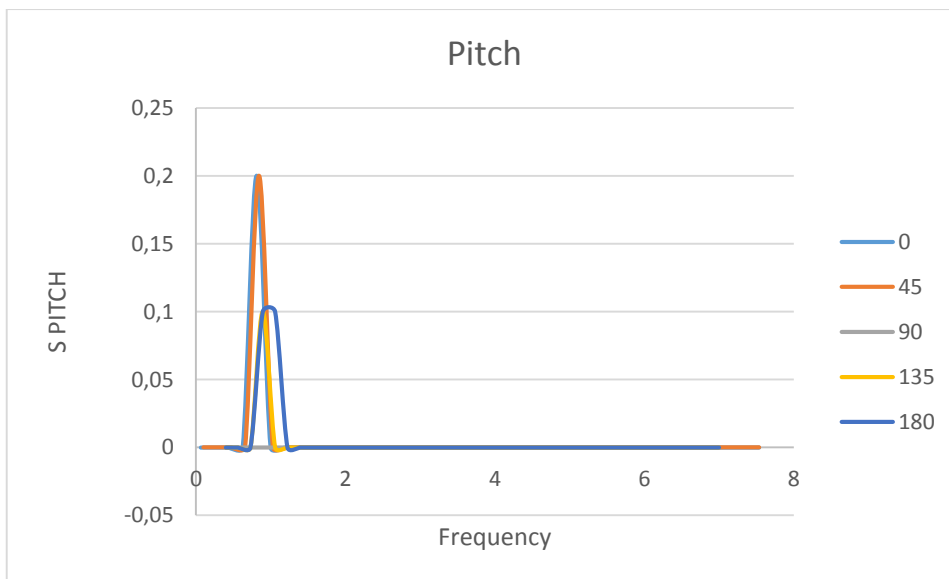
Perhitungan respon spektra dilakukan dalam beberapa *heading* yaitu arah 0° , 45° , 90° , 135° , 180° . Perhitungan ini dilakukan pada saat *loaded*, saat transportasi *Jacket* Banuwati K-Gas ditransportasikan dari PT. PAL ke *East Banuwati Block* di Utara Jakarta. Jalur transportasi menggunakan spektrum gelombang Jonswap dengan $H_s = 1,88$ m dan $T_s = 4,98$ s. Berikut adalah beberapa grafik respon spektra pada *barge*.



Gambar 4.14 Grafik Respon Spektra *Heave* EOS 281



Gambar 4.15 Grafik Respon Spektra *Roll* EOS 281



Gambar 4.16 Grafik Respon Spektra *Pitch* EOS 281

4.8 Analisa Respon Struktur Jacket Platform

Dalam mencari respon struktur *jacket platform* akibat terkena gaya gerakan *barge* dibantu dengan menggunakan software SACS. Berikut tabel percepatan *barge* yang didapat menggunakan *software* Maxsurf :

Tabel 4.6 Percepatan Setiap Gerakan pada Setiap *Heading*

| Heading | Modal Period (s) | Heave (m/s ²) | Percepatan | | | |
|---------|------------------|---------------------------|--------------|------------------------|--------------|------------------------|
| | | | Roll | | Pitch | |
| | | | motion (deg) | acceleration (rad/s/s) | motion (deg) | acceleration (rad/s/s) |
| 180 | 5,942 | 0,111 | 0,0 | 0,0 | 0,36 | 0,00788 |
| 135 | 5,942 | 0,11 | 12,06 | 0,36267 | 0,27 | 0,0054 |
| 90 | 5,942 | 0,105 | 22,25 | 0,59587 | 0,013 | 0,00023 |
| 45 | 5,942 | 0,039 | 17,56 | 0,44959 | 0,41 | 0,00580 |
| 0 | 5,942 | 0,074 | 0,00 | 0,00 | 0,43 | 0,00490 |

Dalam proses *input* besar percepatan dari *barge* digunakan fasilitas *tow* pada *software* SACS dengan menggunakan *load combination* dari heave, roll dan pitch.

Tabel 4.7 *Matriks Combination*

| Load Combination |
|------------------|
| +R + H |
| +R - H |
| -R + H |
| -R - H |
| +H +P |
| -H +P |
| +H - P |
| -H - P |

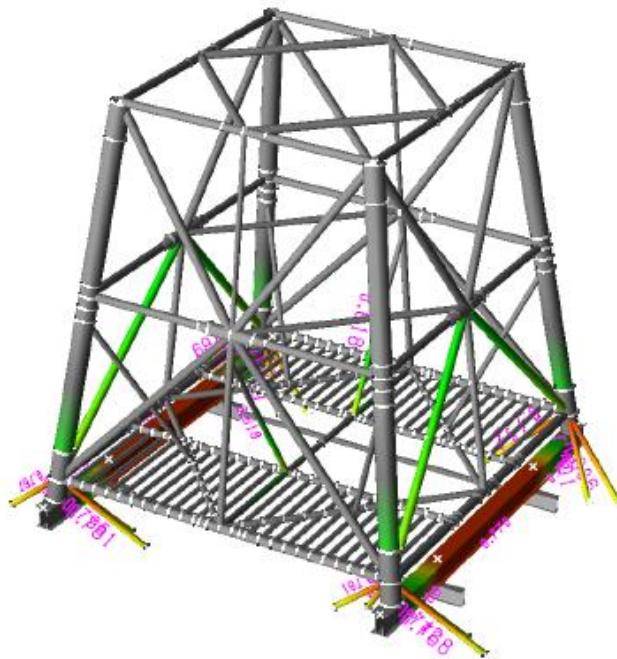
Load combination dalam proses *input* ke *software* SACS dapat dilihat pada tabel di atas. *Load combination* tersebut sesuai dengan yang terdapat pada buku El-Reedy, Mohamed A., 2015, *Marine Structural Design Calculation*

| General | |
|-----------------------------|-----------|
| Acceleration Input | |
| Load Case Name | +R+H |
| Translational Accelerations | |
| X | (G) |
| Y | (G) |
| Z | 0.001 (G) |
| Rotational Accelerations | |
| X (RAD/Sec**2) | 0.59587 |
| Y (RAD/Sec**2) | |
| Z (RAD/Sec**2) | |
| Rotational Velocities | |
| X (RAD/Sec) | |
| Y (RAD/Sec) | |
| Z (RAD/Sec) | |
| Exclude Structural Weight | No |
| Center ID | |

X (RAD/Sec)
Enter the Rotational Velocity components about the global axes in RAD/SEC

Gambar 4.17 Contoh *input* percepatan *barge* di SACS

Setelah proses mengombinasikan gerakan *barge* maka selanjutnya adalah *input* beban angin yang diterima jacket platform. Data angin yang digunakan adalah data angin yang didapat dari PT PAL dengan besar 15 m/s. Setelah semua *load input* sudah dimasukkan, selanjutnya adalah melakukan *running analysis* dengan menggunakan *software* SACS untuk melihat respon struktur *seafastening* akibat gerakan murni dari *barge*. Berikut adalah hasil *running analysis* respon struktur *seafastening jacket platform* :



Gambar 4.18 Output Kondisi Struktur *seafastening jacket platform* Akibat Gerakan Murni *Barge*

Dari gambar diatas dapat dilihat kondisi struktur *seafastening* kuat untuk menahan gaya dari gerakan murni *barge*. Adapun UC yang didapatkan untuk tiap struktur *seafastening* adalah sebagai berikut :

Tabel 4.8 UC Seafastening

| Member | Group | Max Unity Check | Critical Condition | Load Case No | Dist From End | Applied Stress | | | | |
|-----------|-------|-----------------|--------------------|--------------|---------------|----------------|---------|-----------|-----------|---------|
| | | | | | | Axial | Bending | | Shear | |
| | | | | | | | (Ksi) | Y-Y (Ksi) | Z-Z (Ksi) | Y (Ksi) |
| 0002-0091 | SF | 0.781 | C>.15A + | R+H | 0.00 | -12.87 | 4.19 | 5.51 | 0.11 | 0.00 |
| 0002-0092 | SF | 0.795 | C>.15A | -R+H | 0.00 | -12.94 | -6.47 | -5.08 | 0.20 | 0.00 |
| 0002-0093 | SF | 0.741 | C>.15A | -R+H | 0.00 | -11.81 | -5.56 | 5.63 | 0.19 | 0.00 |
| 0002-0094 | SF | 0.767 | C>.15A | +R+H | 0.00 | -13.36 | 1.80 | -5.06 | 0.13 | 0.00 |
| 0003-0100 | SF | 0.806 | C>.15A | -R+H | 0.00 | -14.02 | 2.37 | -5.49 | 0.13 | 0.00 |
| 0003-0101 | SF | 0.801 | C>.15A | +R+H | 0.00 | -12.91 | -6.20 | 5.75 | 0.21 | 0.00 |
| 0003-0103 | SF | 0.742 | C>.15A | +R+H | 0.00 | -11.94 | -5.87 | -5.03 | 0.19 | 0.00 |
| 0003-0104 | SF | 0.737 | C>.15A | -R+H | 0.00 | -12.17 | 3.58 | 5.14 | 0.11 | 0.00 |
| 0004-0095 | SF | 0.768 | C>.15A | +R+H | 0.00 | -13.37 | 1.81 | 5.07 | 0.13 | 0.00 |
| 0004-0096 | SF | 0.742 | C>.15A | -R+H | 0.00 | -11.82 | -5.57 | -5.64 | 0.19 | 0.00 |
| 0004-0097 | SF | 0.796 | C>.15A | -R+H | 0.00 | -12.95 | -6.47 | 5.08 | 0.20 | 0.00 |
| 0004-0098 | SF | 0.781 | C>.15A | +R+H | 0.00 | -12.87 | 4.20 | -5.50 | 0.11 | 0.00 |
| 0005-0083 | SF | 0.769 | C>.15A | -R+H | 0.00 | -13.39 | 1.80 | 5.05 | 0.13 | 0.00 |
| 0005-0084 | SF | 0.741 | C>.15A | +R+H | 0.00 | -11.79 | -5.57 | -5.66 | 0.19 | 0.00 |
| 0005-0085 | SF | 0.799 | C>.15A | +R+H | 0.00 | -13.00 | -6.48 | 5.08 | 0.20 | 0.00 |
| 0005-0086 | SF | 0.776 | C>.15A | -R+H | 0.00 | -12.78 | 4.18 | -5.48 | 0.11 | 0.00 |

Dari tabel diatas terlihat bahwa UC terbesar terjadi pada *member* 0003-0100 sebesar 0,806. UC pada *member* lain relatif lebih kecil sehingga struktur *seafastening* dinyatakan aman dan kuat dalam proses transportasi setelah mendapat gaya murni gerakan *barge*.

4.9 Analisa Keandalan Struktur *Seafastening*

4.9.1 Moda Kegagalan

Dalam proses menentukan keandalan suatu struktur, dibutuhkan moda kegagalan yang menjadi parameter dalam penentuan kesuksesan ataupun kegagalan dari suatu struktur. Moda kegagalan yang digunakan adalah *axial compression stress* sebagaimana yang telah diisyaratkan oleh API RP 2A WSD.

Berikut adalah persamaan moda kegagalan yang digunakan :

$$MK = F_{cr} - F_a$$

$$F_{cr} = \frac{\left[1 - \frac{\left(\frac{Kl}{r}\right)^2}{2Cc^2} \right]}{\frac{5}{3} + \frac{3\left(\frac{Kl}{r}\right)}{8Cc} - \frac{\left(\frac{Kl}{r}\right)^3}{8Cc^3}} \text{ for } \frac{Kl}{r} < Cc$$

Dimana:

$$Cc = \left[\frac{22\pi^2 E}{F_y} \right]^{\frac{1}{2}}$$

E : *Modulus Elastisitas*; ksi (MPa)

k : Faktor panjang efektif

L : Panjang tanpa *bracing*

r : Jari-jari girasi

Dalam tugas akhir ini, objek yang utama adalah member *seafastening* yang mendapatkan *axial compress stress* terbesar. Sebagai perbandingan maka 2 tegangan aksial terbesar yang akan dijadikan perhitungan dalam analisa keandalan struktur *seafastening* dalam proses transportasi *jacket platform* Banuwati.

4.9.2 Perhitungan Keandalan

Dalam perhitungan keandalan, suatu permasalahan akan akan didefinisikan sebagai hubungan permintaan dan hubungan penyedia, dengan kata lain masing-masing memiliki vairabel acak. Dalam tugas akhir ini permintaan dimaksudkan sebagai beban yang bekerja pada sistem dan penyedia sebagai kekuatan atau ketahanan dari sistem tersebut. Variabel acak dalam perhitungan keandalan struktur *seafastening* tugas akhir ini adalah tegangan *yield* (F_y) dan *modulus elastisitas* (E).

Tegangan *yield* (F_y) didapatkan dari *journal international elsevier Structural integrity assessment of offshore tubular joints based on reliability analysis* oleh J. Rajasankar dengan cov 0,1 dan distribusi untuk tegangan *yield* adalah distribusi *lognormal*. Sedangkan variabel acak *modulus elastisitas* (E) didapatkan dari *journal uncertainties in material strength, geometric, and load variables* oleh Paul E. Hess dengan cov 0,01 dan menggunakan distribusi normal. Nilai *mean* didapatkan dari hasil perhitungan *software* dan nilai standard deviasi didapatkan dari hasil perkalian antara cov dan *mean*.

Tabel 4.9 Parameter Variabel Acak 1

| Variabel | Data | | | | Distribusi | |
|---------------|-------|------------------|------|------------|------------|------------------|
| | Mean | Standart Deviasi | COV | Distribusi | Mean | Standart Deviasi |
| F_y (Ksi) | 36 | 3,6 | 0,1 | Lognormal | 3,57854377 | 0,099751345 |
| E (Ksi) | 29000 | 290 | 0,01 | Normal | | |
| F_a (Ksi) | 14,02 | 1,402 | 0,1 | Lognormal | 2,63550972 | 0,099751345 |

Tabel 4.10 Parameter Variabel Acak 2

| Variabel | Data | | | | Distribusi | |
|---------------|-------|------------------|------|------------|------------|------------------|
| | Mean | Standart Deviasi | COV | Distribusi | Mean | Standart Deviasi |
| F_y (Ksi) | 36 | 3,6 | 0,1 | Lognormal | 3,57854377 | 0,099751345 |
| E (Ksi) | 29000 | 290 | 0,01 | Normal | | |
| F_a (Ksi) | 13,39 | 1,339 | 0,1 | Lognormal | 2,58953299 | 0,099751345 |

Dengan menggunakan simulasi *monte carlo* maka dilakukan iterasi sebanyak 100000 kali percobaan. Diambil 2 nilai axial compression stress terbesar, rincian percobaan sebanyak 100000 kali akan dilampirkan. Berikut perhitungan keandalan *struktur seafastening*

Tabel 4.11 Perhitungan keandalan dengan Fa 14,02 ksi

| Jumlah simulasi | Simulasi berhasil | Simulasi gagal | Probabilitas kegagalan | Keandalan | Keandalan % |
|-----------------|-------------------|----------------|------------------------|-----------|-------------|
| 100000 | 99637 | 363 | 0,00363 | 0,9964 | 99,6370% |

Tabel 4.12 Perhitungan keandalan dengan Fa 13,39 ksi

| Jumlah simulasi | Simulasi berhasil | Simulasi gagal | Probabilitas kegagalan | Keandalan | Keandalan % |
|-----------------|-------------------|----------------|------------------------|-----------|-------------|
| 100000 | 99853 | 147 | 0,00147 | 0,9985 | 99,8530% |

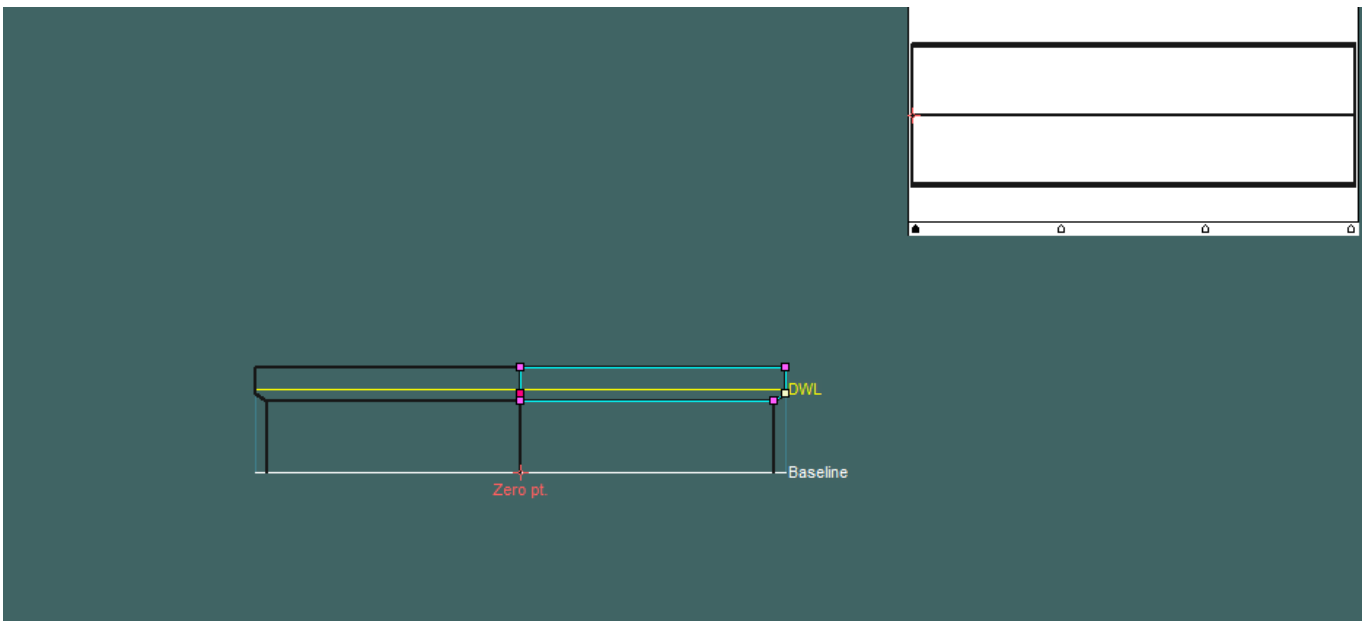
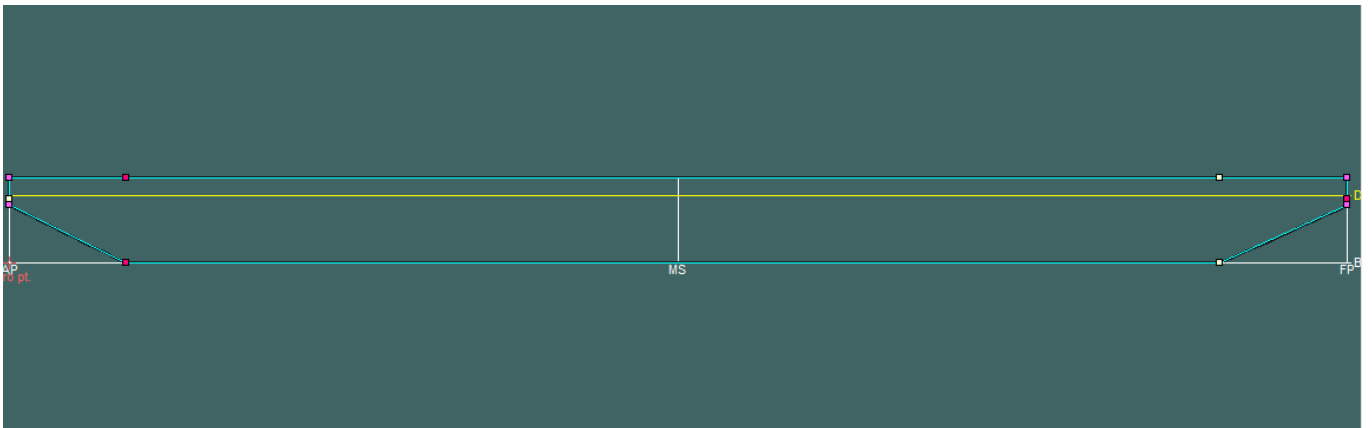
Dari percobaan diatas didapatkan masing-masing 2 nilai keandalan dengan perbandingan 2 nilai tegangan aksial terbesar. Untuk Fa 14,02 ksi didapatkan nilai keandalannya adalah 99,63 % sedangkan untuk Fa 13,39 nilai keandalannya adalah 99,85 %. Dengan hasil tersebut maka struktur *seafastening* dinyatakan andal dalam proses transportasi *jacket platform* Banuwati ke *East Sumatera Block*.

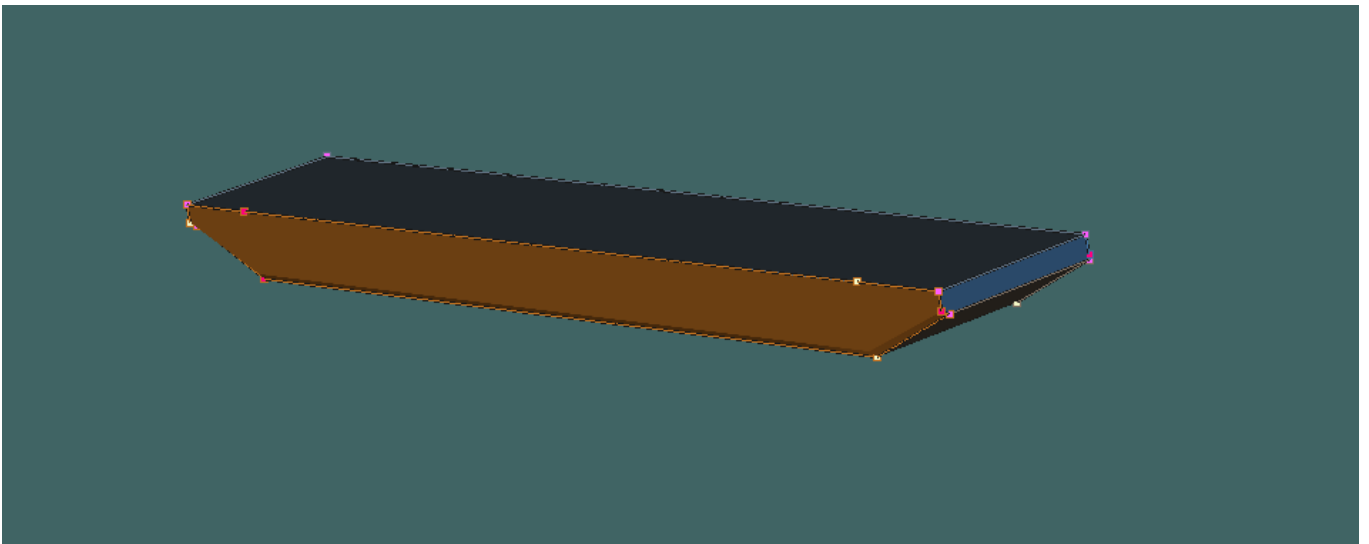
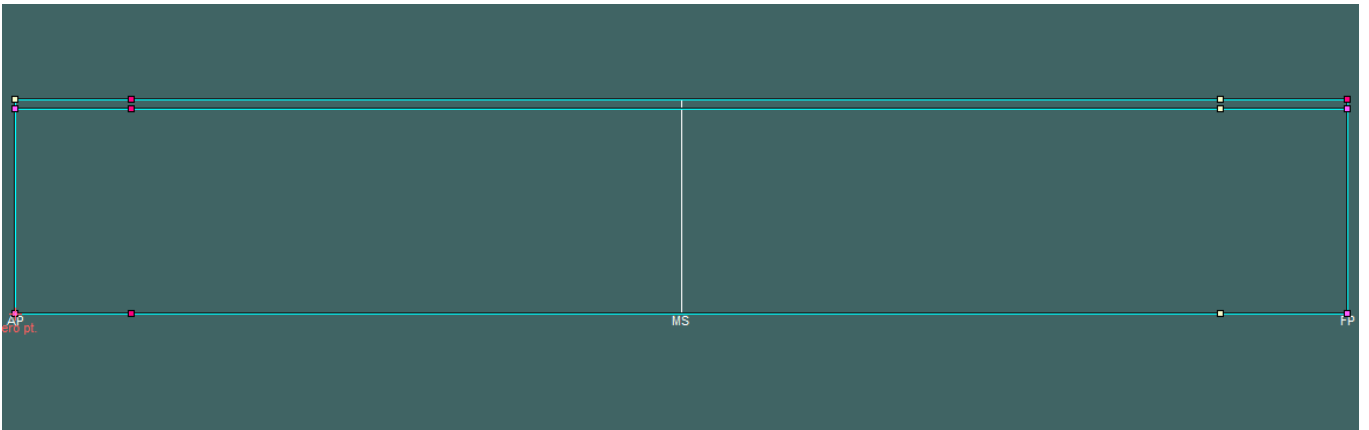
(halaman ini sengaja dikosongkan)

LAMPIRAN A

MAXSURF

Maxsurf Modeler





Maxsurf Stability Full Load and Half Load

| Full load | | | | | | | | | | | |
|--|----------|----------|----------|----------|----------|----------|----------|----------|----------|---------|----------|
| | 0,0 | 5,0 | 10,0 | 15,0 | 20,0 | 25,0 | 30 | 35 | 40 | 45 | 50 |
| Heel to starboard deg | 0,0 | 5,0 | 10,0 | 15,0 | 20,0 | 25,0 | 30 | 35 | 40 | 45 | 50 |
| GZ m | 0 | 1,087 | 1,56 | 1,596 | 1,487 | 1,299 | 1,054 | 0,764 | 0,448 | 0,116 | -0,224 |
| Area under GZ curve from zero heel m.rad | 0 | 0,0504 | 0,1704 | 0,3099 | 0,4451 | 0,5671 | 0,6701 | 0,7497 | 0,8027 | 0,8274 | 0,8228 |
| Displacement t | 9509 | 9509 | 9508 | 9508 | 9508 | 9508 | 9509 | 9509 | 9509 | 9509 | 9509 |
| Draft at FP m | 4,318 | 4,317 | 4,53 | 4,989 | 5,59 | 6,316 | 7,134 | 8,052 | 9,074 | 10,274 | 11,703 |
| Draft at AP m | 4,318 | 4,317 | 4,538 | 4,997 | 5,612 | 6,339 | 7,178 | 8,097 | 9,151 | 10,357 | 11,795 |
| WL Length m | 85,34 | 85,34 | 85,34 | 85,34 | 85,34 | 85,34 | 85,34 | 85,34 | 85,34 | 85,34 | 85,34 |
| Beam max extents on WL m | 27,43 | 27,111 | 19,392 | 16,095 | 14,267 | 13,776 | 12,91 | 11,934 | 11,111 | 10,358 | 9,651 |
| Wetted Area m ² | 2993,406 | 3022,757 | 3607,932 | 3841,432 | 3967,63 | 4043,571 | 4067,916 | 4073,426 | 4077,724 | 4080,82 | 4083,381 |
| Waterpl. Area m ² | 2340,876 | 2304,223 | 1621,526 | 1324,597 | 1154,778 | 1013,631 | 876,975 | 764,479 | 682,165 | 620,115 | 572,405 |
| Prismatic coeff. (Cp) | 0,921 | 0,921 | 0,922 | 0,924 | 0,925 | 0,927 | 0,929 | 0,93 | 0,931 | 0,932 | 0,932 |
| Block coeff. (Cb) | 0,918 | 0,737 | 0,831 | 0,822 | 0,781 | 0,699 | 0,659 | 0,644 | 0,634 | 0,633 | 0,637 |
| LCB from zero pt. (+ve fwd) m | 42,55 | 42,55 | 42,543 | 42,549 | 42,543 | 42,548 | 42,543 | 42,548 | 42,541 | 42,545 | 42,548 |
| LCF from zero pt. (+ve fwd) m | 42,67 | 42,664 | 42,652 | 42,625 | 42,614 | 42,586 | 42,576 | 42,576 | 42,577 | 42,577 | 42,577 |
| Max deck inclination deg | 0 | 5 | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 |
| Trim angle (+ve by stern) deg | 0 | 0 | 0,0052 | 0,0053 | 0,0146 | 0,0151 | 0,0289 | 0,0305 | 0,0515 | 0,0558 | 0,0614 |

| Half load | | | | | | | | | | | |
|--|----------|----------|----------|----------|----------|---------|----------|----------|----------|----------|----------|
| | 0,0 | 5,0 | 10,0 | 15,0 | 20,0 | 25,0 | 30 | 35 | 40 | 45 | 50 |
| Heel to starboard deg | 0,0 | 5,0 | 10,0 | 15,0 | 20,0 | 25,0 | 30 | 35 | 40 | 45 | 50 |
| GZ m | 0 | 1,891 | 3,748 | 4,747 | 4,766 | 4,344 | 3,727 | 3,006 | 2,22 | 1,392 | 0,539 |
| Area under GZ curve from zero heel m.rad | 0 | 0,0927 | 0,3308 | 0,7094 | 1,1297 | 1,5291 | 1,8822 | 2,1766 | 2,405 | 2,5628 | 2,6472 |
| Displacement t | 4754 | 4754 | 4754 | 4754 | 4754 | 4754 | 4754 | 4754 | 4754 | 4754 | 4754 |
| Draft at FP m | 2,286 | 2,272 | 2,219 | 1,996 | 1,689 | 1,361 | 1,005 | 0,611 | 0,165 | -0,352 | -0,968 |
| Draft at AP m | 2,285 | 2,272 | 2,231 | 2,021 | 1,732 | 1,425 | 1,091 | 0,723 | 0,307 | -0,175 | -0,749 |
| WL Length m | 79,357 | 84,138 | 85,34 | 85,34 | 85,34 | 85,34 | 85,34 | 85,34 | 85,34 | 85,34 | 85,34 |
| Beam max extents on WL m | 27,43 | 27,535 | 26,765 | 21,173 | 16,022 | 12,967 | 10,96 | 9,554 | 8,525 | 7,75 | 7,154 |
| Wetted Area m ² | 2460,653 | 2462,02 | 2423,846 | 2189,101 | 2207,149 | 2218,2 | 2225,686 | 2231,185 | 2235,474 | 2238,954 | 2241,852 |
| Waterpl. Area m ² | 2175,302 | 2180,825 | 2113,771 | 1694,185 | 1282,051 | 1037,55 | 876,975 | 764,48 | 682,166 | 620,115 | 572,405 |
| Prismatic coeff. (Cp) | 0,938 | 0,89 | 0,89 | 0,902 | 0,91 | 0,914 | 0,917 | 0,92 | 0,921 | 0,923 | 0,924 |
| Block coeff. (Cb) | 0,932 | 0,588 | 0,454 | 0,48 | 0,555 | 0,614 | 0,662 | 0,702 | 0,737 | 0,767 | 0,789 |
| LCB from zero pt. (+ve fwd) m | 42,47 | 42,478 | 42,472 | 42,471 | 42,469 | 42,467 | 42,465 | 42,463 | 42,46 | 42,458 | 42,456 |
| LCF from zero pt. (+ve fwd) m | 42,554 | 42,557 | 42,538 | 42,576 | 42,576 | 42,576 | 42,576 | 42,576 | 42,575 | 42,575 | 42,574 |
| Max deck inclination deg | 0,0001 | 5 | 10 | 15 | 20 | 25 | 30 | 35 | 40,0001 | 45,0001 | 50,0001 |
| Trim angle (+ve by stern) deg | -0,0001 | -0,0001 | 0,0079 | 0,017 | 0,0292 | 0,0427 | 0,0578 | 0,0751 | 0,0951 | 0,1186 | 0,147 |

Summary Maxsurf Motion (Half Load)

| Item | m0 | units | RMS | units | significant amp | units | modal peak | mean | mean | period units |
|--|--------------------|-------------|----------|---------|-----------------|---------|--------------|--------------|--------------|--------------|
| Modal period | 5,942 | s | -- | | -- | | -- | -- | -- | |
| Characteristic wave height | 1,88 | m | -- | | -- | | -- | -- | -- | |
| Spectrum type | JONSWAP | | -- | | -- | | -- | -- | -- | |
| Wave heading | 90 | deg | -- | | -- | | -- | -- | -- | |
| Vessel Speed | 3 | kn | -- | | -- | | -- | -- | -- | |
| Vessel displacement | 4618,257 | m^3 | Monohull | | -- | | -- | -- | -- | |
| Vessel GMt | 21,271 | m | -- | | -- | | -- | -- | -- | |
| Vessel trim | 0 | deg | -- | | -- | | -- | -- | -- | |
| Vessel heel | 0 | deg | -- | | -- | | -- | -- | -- | |
| Transom method | Transom terms | | -- | | -- | | -- | -- | -- | |
| Wave force method | seas approximation | | -- | | -- | | -- | -- | -- | |
| Added res. method | Salvesen | | -- | | -- | | -- | -- | -- | |
| Pitch gyradius | 23,042 | m | -- | | -- | | -- | -- | -- | |
| Roll gyradius | 11,521 | m | -- | | -- | | -- | -- | -- | |
| Wave spectrum | 0,222 | m^2 | 0,471 | m | 0,941 | m | 5,944 (1,06) | 4,976 (1,26) | 4,684 (1,34) | s (rad/s) |
| Encountered wave spectrum | 0,222 | m^2 | 0,471 | m | 0,941 | m | 5,942 (1,06) | 4,976 (1,26) | 4,683 (1,34) | s (rad/s) |
| Added resistance | 169,983 | kN | -- | | -- | | 5,904 (1,06) | 5,097 (1,23) | 4,833 (1,30) | s (rad/s) |
| Heave motion | 0,002 | m^2 | 0,048 | m | 0,096 | m | 6,010 (1,05) | 6,218 (1,01) | 6,157 (1,02) | s (rad/s) |
| Roll motion | 123,76 | deg^2 | 11,12 | deg | 22,25 | deg | 5,904 (1,06) | 5,496 (1,14) | 5,413 (1,16) | s (rad/s) |
| Pitch motion | 0,00004 | deg^2 | 0,0064 | deg | 0,013 | deg | 6,057 (1,04) | 6,317 (0,99) | 6,268 (1,00) | s (rad/s) |
| Heave velocity | 0,002 | m^2/s^2 | 0,049 | m/s | 0,098 | m/s | 5,964 (1,05) | 5,961 (1,05) | 5,859 (1,07) | s (rad/s) |
| Roll velocity | 0,05079 | (rad/s)^2 | 0,22536 | rad/s | 0,45073 | rad/s | 5,904 (1,06) | 5,040 (1,25) | 4,752 (1,32) | s (rad/s) |
| Pitch velocity | 0 | (rad/s)^2 | 0,00011 | rad/s | 0,00022 | rad/s | 6,011 (1,05) | 6,131 (1,02) | 6,088 (1,03) | s (rad/s) |
| Heave acceleration | 0,003 | m^2/s^4 | 0,053 | m/s^2 | 0,105 | m/s^2 | 5,908 (1,06) | 5,324 (1,18) | 4,775 (1,32) | s (rad/s) |
| Roll acceleration | 0,08877 | (rad/s/s)^2 | 0,29794 | rad/s/s | 0,59587 | rad/s/s | 5,904 (1,06) | 3,532 (1,78) | 2,946 (2,13) | s (rad/s) |
| Pitch acceleration | 0 | (rad/s/s)^2 | 0,00012 | rad/s/s | 0,00023 | rad/s/s | 5,969 (1,05) | 5,947 (1,06) | 5,873 (1,07) | s (rad/s) |
| Remote location1: Abs. vert. motion | 0,003 | m^2 | 0,052 | m | 0,104 | m | 6,017 (1,04) | 6,238 (1,01) | 6,178 (1,02) | s (rad/s) |
| Remote location1: Rel. vert. motion | 0,248 | m^2 | 0,498 | m | 0,995 | m | 5,955 (1,06) | 5,070 (1,24) | 4,785 (1,31) | s (rad/s) |
| Remote location1: Abs. vert. velocity | 0,003 | m^2/s^2 | 0,053 | m/s | 0,106 | m/s | 5,971 (1,05) | 5,988 (1,05) | 5,891 (1,07) | s (rad/s) |
| Remote location1: Rel. vert. velocity | 0,427 | m^2/s^2 | 0,653 | m/s | 1,306 | m/s | 5,904 (1,06) | 3,739 (1,68) | 3,267 (1,92) | s (rad/s) |
| Remote location1: Abs. vert. accel | 0,003 | m^2/s^4 | 0,056 | m/s^2 | 0,113 | m/s^2 | 5,918 (1,06) | 5,393 (1,17) | 4,871 (1,29) | s (rad/s) |
| Remote location1: Rel. vert. accel | 1,577 | m^2/s^4 | 1,256 | m/s^2 | 2,512 | m/s^2 | 5,870 (1,07) | 2,128 (2,95) | 1,890 (3,32) | s (rad/s) |
| Remote location1: Long. (due to pitch) motion | 0 | m^2 | 0,001 | m | 0,002 | m | 6,042 (1,04) | 6,310 (1,00) | 6,262 (1,00) | s (rad/s) |
| Remote location1: Long. (due to pitch) velocity | 0 | m^2/s^2 | 0,001 | m/s | 0,002 | m/s | 5,992 (1,05) | 6,130 (1,03) | 6,087 (1,03) | s (rad/s) |
| Remote location1: Long. (due to pitch) accel | 0 | m^2/s^4 | 0,001 | m/s^2 | 0,002 | m/s^2 | 5,945 (1,06) | 5,947 (1,06) | 5,873 (1,07) | s (rad/s) |
| Remote location1: Lat. (due to roll) motion | 3,001 | m^2 | 1,732 | m | 3,465 | m | 5,904 (1,06) | 5,503 (1,14) | 5,420 (1,16) | s (rad/s) |
| Remote location1: Lat. (due to roll) velocity | 4,032 | m^2/s^2 | 2,008 | m/s | 4,016 | m/s | 5,904 (1,06) | 5,047 (1,24) | 4,759 (1,32) | s (rad/s) |
| Remote location1: Lat. (due to roll) accel | 7,028 | m^2/s^4 | 2,651 | m/s^2 | 5,302 | m/s^2 | 5,904 (1,06) | 3,537 (1,78) | 2,951 (2,13) | s (rad/s) |
| Remote location1: MII slide; tip f/a; tip s/s | 0 | MI/h | 30,162 | MI/h | 12,096 | MI/h | -- | -- | -- | |
| Remote location1: SM; MSI 120 min.; MSI 120 min. | 0,103 | SM | 0,007 | % | 0,001 | % | -- | -- | -- | |

LAMPIRAN B

INPUT SACS

| | | | |
|--------------------|--------------------------------|-----------------------------|--|
| LDOPT | NF+Z64.20000490.0000 | GLOBEN | MEMBER 01900195 16B |
| OPTIONS | EN | 1 1 | MEMBER 01910197 16B |
| SECT | | | MEMBER 01920196 16B |
| SECT 22C | CON | 34.0001.75022.000 | MEMBER 01930194 16B |
| SECT CB | PGD | 47.2441.68161.4171.681 23.6 | MEMBER 00190184 20B |
| SECT CB1 | BOX | 51.1811.43123.6221.431 | MEMBER 00200186 20B |
| SECT MG | WF | 10.4000.77010.1300.470 | MEMBER 01350223 20B |
| SECT SS | PGD | 23.6221.43144.0941.431 11.8 | MEMBER 01370251 20B |
| GRUP | | | MEMBER 01400263 20B |
| GRUP 16B 490.00 | 16.000 0.750 29.0011.2036.00 1 | 1.001.00 0.500 | MEMBER 01420235 20B |
| GRUP 20B 490.00 | 20.000 1.250 29.0011.2036.00 1 | 1.001.00 0.500 | MEMBER 01830019 20B MEMBER 01850020 20B |
| GRUP 22B 490.00 | 22.000 0.750 29.0011.2036.00 1 | 1.001.00 0.500 | MEMBER 02230302 20B |
| GRUP 22C 22C | 29.0011.2036.00 1 | 1.001.00 0.500 490.00 | MEMBER 02240136 20B |
| GRUP 22D 490.00 | 22.000 1.750 29.0011.2036.00 1 | 1.001.00 0.500 | MEMBER 02350301 20B MEMBER 02360141 20B |
| GRUP 24A 490.00 | 24.000 1.075 29.0011.2036.00 1 | 1.001.00 0.500 | MEMBER 02510303 20B |
| GRUP 24B 490.00 | 24.000 1.250 29.0011.2036.00 1 | 1.001.00 0.500 | MEMBER 02520138 20B MEMBER 02630300 20B |
| GRUP 26B 490.00 | 26.000 1.500 29.0011.2036.00 1 | 1.001.00 0.500 | MEMBER 02640139 20B |
| GRUP 34B 490.00 | 34.000 1.750 29.0011.2036.00 1 | 1.001.00 0.500 | MEMBER 03000264 20B MEMBER 03010236 20B |
| GRUP B14 490.00 | 14.000 1.000 29.0011.2036.00 1 | 1.001.00 0.500 | MEMBER 03020224 20B |
| GRUP B16 490.00 | 16.000 2.200 29.0011.2036.00 1 | 1.001.00 0.500 | MEMBER 03030252 20B |
| GRUP B18 490.00 | 18.000 0.870 29.0011.2036.00 1 | 1.001.00 0.500 | MEMBER 00270028 22B MEMBER 00280030 22B |
| GRUP B20 490.00 | 20.000 1.000 29.0011.2036.00 1 | 1.001.00 0.500 | MEMBER 00290027 22B MEMBER 00300029 22B |
| GRUP B22 490.00 | 22.000 1.650 29.0011.2036.00 1 | 1.001.00 0.500 | MEMBER 00310134 22B |
| GRUP B26 490.00 | 26.000 1.000 29.0011.2036.00 1 | 1.001.00 0.500 | MEMBER 00320132 22B MEMBER 00330130 22B |
| GRUP C52 490.00 | 52.000 1.500 29.0011.2036.00 1 | 1.001.00 0.500 | MEMBER 00340127 22B |
| GRUP C54 490.00 | 54.000 2.500 29.0011.2036.00 1 | 1.001.00 0.500 | MEMBER 01280031 22B MEMBER 01290034 22B |
| GRUP CB CB | 29.0011.2036.00 1 | 1.001.00 490.00 | MEMBER 01310033 22B |
| GRUP CB1 CB1 | 29.0011.2036.00 1 | 1.001.00 490.00 | MEMBER 01330032 22B |
| GRUP MG MG | 29.0011.2045.00 1 | 1.001.00 490.00 | MEMBER 00560127 22C |
| GRUP PSS 490.00 | 16.000 1.750 29.0011.2036.00 1 | 1.001.00 0.500 | MEMBER 00570129 22C |
| GRUP SF 490.00 | 16.000 1.950 29.0011.2036.00 1 | 1.001.00 0.500 | MEMBER 00600130 22C MEMBER 00640131 22C |
| GRUP SS SS | 29.0011.2036.00 1 | 1.001.00 490.00 | MEMBER 00650132 22C |
| MEMBER | | | MEMBER 00660133 22C |

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| MEMBER 01250134 22C | MEMBER 01800012 26B |
| MEMBER 01260128 22C | MEMBER 01820013 26B |
| MEMBER 00150029 22D | MEMBER 00350126 34B |
| MEMBER 00180027 22D | MEMBER 00360066 34B |
| MEMBER 00270017 22D | MEMBER 00370057 34B |
| MEMBER 00280053 22D | MEMBER 00380064 34B |
| MEMBER 00290016 22D | MEMBER 00560035 34B |
| MEMBER 00300055 22D | MEMBER 00600037 34B |
| MEMBER 00520028 22D | MEMBER 00650038 34B |
| MEMBER 00540030 22D | MEMBER 01250036 34B |
| MEMBER 00020035 24A | MEMBER 00360028 B14 |
| MEMBER 00020036 24A | MEMBER 00370029 B14 |
| MEMBER 00030037 24A | MEMBER 01870020 B16 |
| MEMBER 00030038 24A | MEMBER 01890019 B16 |
| MEMBER 00040036 24A | MEMBER 00010020 B18 |
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| MEMBER 00050035 24A | MEMBER 00070303 B18 |
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| MEMBER 01780010 26B | MEMBER 02810194 B18 |

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| MEMBER 02820283 B18 | MEMBER 02320233 B20 |
| MEMBER 02830302 B18 | MEMBER 02330234 B20 |
| MEMBER 02840285 B18 | MEMBER 02340142 B20 |
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| MEMBER 03010284 B18 | MEMBER 02550011 B20 |
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| MEMBER 00130232 B20 | MEMBER 02650266 B20 |
| MEMBER 01360225 B20 | MEMBER 02660267 B20 |
| MEMBER 01380253 B20 | MEMBER 02670010 B20 |
| MEMBER 01390265 B20 | MEMBER 00160025 B22 |
| MEMBER 01410237 B20 | MEMBER 00170026 B22 |
| MEMBER 01840244 B20 | MEMBER 00230018 B22 |
| MEMBER 01860256 B20 | MEMBER 00230052 B22 |
| MEMBER 02200221 B20 | MEMBER 00240054 B22 |
| MEMBER 02210222 B20 | MEMBER 00260015 B22 |
| MEMBER 02220135 B20 | MEMBER 00530024 B22 |
| MEMBER 02250226 B20 | MEMBER 00550025 B22 |
| MEMBER 02260227 B20 | MEMBER 00020148 B26 |
| MEMBER 02270228 B20 | MEMBER 00020182 B26 |
| MEMBER 02280229 B20 | MEMBER 00040178 B26 |
| MEMBER 02290230 B20 | MEMBER 00050088 B26 |
| MEMBER 02300231 B20 | MEMBER 00880089 B26 |
| MEMBER 02310183 B20 | MEMBER 00890090 B26 |

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| MEMBER 00900099 B26 | MEMBER 01710004 B26 | | |
| MEMBER 00990102 B26 | MEMBER 01730180 B26 | | |
| MEMBER 01020105 B26 | MEMBER 01750003 B26 | | |
| MEMBER 01050106 B26 | MEMBER 01770172 B26 | | |
| MEMBER 01060107 B26 | MEMBER 01790005 B26 | | |
| MEMBER 01070108 B26 | MEMBER 01810174 B26 | | |
| MEMBER 01080109 B26 | MEMBER 00310205 C52 | | |
| MEMBER 01090110 B26 | MEMBER 00320199 C52 | | |
| MEMBER 01100143 B26 | MEMBER 00330201 C52 | | |
| MEMBER 01130114 B26 | MEMBER 00340203 C52 | | |
| MEMBER 01140115 B26 | MEMBER 00410204 C52 | | |
| MEMBER 01150116 B26 | MEMBER 00420202 C52 | | |
| MEMBER 01160117 B26 | MEMBER 00480200 C52 | | |
| MEMBER 01170118 B26 | MEMBER 00510198 C52 | | |
| MEMBER 01180119 B26 | MEMBER 01900049 C52 | | |
| MEMBER 01190120 B26 | MEMBER 01910047 C52 | | |
| MEMBER 01200121 B26 | MEMBER 01920046 C52 | | |
| MEMBER 01210122 B26 | MEMBER 01930050 C52 | | |
| MEMBER 01220123 B26 | MEMBER 01980032 C52 | | |
| MEMBER 01230003 B26 | MEMBER 01990191 C52 | | |
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| MEMBER 01460161 B26 | MEMBER 02010190 C52 | | |
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| MEMBER 01510152 B26 | MEMBER 00020039 C54 | | |
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| MEMBER 01530154 B26 | MEMBER 00040043 C54 | | |
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| MEMBER 01550156 B26 | MEMBER 00230041 C54 | | |
| MEMBER 01560157 B26 | MEMBER 00240051 C54 | | |
| MEMBER 01570158 B26 | MEMBER 00250048 C54 | | |
| MEMBER 01580145 B26 | MEMBER 00260042 C54 | | |
| MEMBER 01610162 B26 | MEMBER 00460002 C54 | | |
| MEMBER 01620163 B26 | MEMBER 00470004 C54 | | |
| MEMBER 01630164 B26 | MEMBER 00490003 C54 | | |
| MEMBER 01640165 B26 | MEMBER 00500005 C54 | | |
| MEMBER 01650166 B26 | MEMBER100390059 CB | | |
| MEMBER 01660167 B26 | MEMBER OFFSETS | -30.71 | -30.71 |
| MEMBER 01670168 B26 | MEMBER100400068 CB | | |
| MEMBER 01680169 B26 | MEMBER OFFSETS | -30.71 | -30.71 |
| MEMBER 01690170 B26 | MEMBER100430063 CB | | |
| MEMBER 01700171 B26 | MEMBER OFFSETS | -30.71 | -30.71 |

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|---------------------|--------|--------|--------------------|
| MEMBER100440061 CB | | | MEMBER 01220254 MG |
| MEMBER OFFSETS | -30.71 | -30.71 | MEMBER 01230255 MG |
| MEMBER100580040 CB | | | MEMBER 02320148 MG |
| MEMBER OFFSETS | -30.71 | -30.71 | MEMBER 02330149 MG |
| MEMBER100620043 CB | | | MEMBER 02340150 MG |
| MEMBER OFFSETS | -30.71 | -30.71 | MEMBER 02350151 MG |
| MEMBER100630067 CB | | | MEMBER 02360284 MG |
| MEMBER OFFSETS | -30.71 | -30.71 | MEMBER 02370285 MG |
| MEMBER100670044 CB | | | MEMBER 02380286 MG |
| MEMBER OFFSETS | -30.71 | -30.71 | MEMBER 02390287 MG |
| MEMBER100680069 CB | | | MEMBER 02400288 MG |
| MEMBER OFFSETS | -30.71 | -30.71 | MEMBER 02410289 MG |
| MEMBER100690039 CB | | | MEMBER 02420290 MG |
| MEMBER OFFSETS | -30.71 | -30.71 | MEMBER 02430291 MG |
| MEMBER100630070 CB1 | | | MEMBER 02560292 MG |
| MEMBER OFFSETS | -77.17 | | MEMBER 02570293 MG |
| MEMBER100670071 CB1 | | | MEMBER 02580294 MG |
| MEMBER OFFSETS | -77.17 | | MEMBER 02590295 MG |
| MEMBER100680072 CB1 | | | MEMBER 02600296 MG |
| MEMBER OFFSETS | -77.17 | | MEMBER 02610297 MG |
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| MEMBER 00890221 MG | | | MEMBER 02650169 MG |
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| MEMBER 00990223 MG | | | MEMBER 02670171 MG |
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| MEMBER 01180269 MG | | | MEMBER 02820225 MG |
| MEMBER 01190268 MG | | | MEMBER 02830224 MG |
| MEMBER 01200252 MG | | | MEMBER 02840152 MG |
| MEMBER 01210253 MG | | | MEMBER 02850153 MG |

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|---------------------|--------|--------|--------------------|--------|------------------------------|
| MEMBER 02860154 MG | | | MEMBER100770073 SS | | |
| MEMBER 02870155 MG | | | MEMBER OFFSETS | -77.17 | -77.17 |
| MEMBER 02880156 MG | | | MEMBER100790070 SS | | |
| MEMBER 02890157 MG | | | MEMBER OFFSETS | -77.17 | -77.17 |
| MEMBER 02900158 MG | | | MEMBER100800071 SS | | |
| MEMBER 02910159 MG | | | MEMBER OFFSETS | -77.17 | -77.17 |
| MEMBER 02920160 MG | | | JOINT | | |
| MEMBER 02930161 MG | | | JOINT 0001 | 0. | 0. |
| MEMBER 02940162 MG | | | JOINT 0002 | -41. | -41. 0. -5.088 -5.088 |
| MEMBER 02950163 MG | | | JOINT 0003 | 41. | 41. 0. 5.088 5.088 |
| MEMBER 02960164 MG | | | JOINT 0004 | 41. | -41. 0. 5.088 -5.088 |
| MEMBER 02970165 MG | | | JOINT 0005 | -41. | 41. 0. -5.088 5.088 |
| MEMBER 02980166 MG | | | JOINT 0006 | -41. | 0. 0. -5.088 |
| MEMBER 02990167 MG | | | JOINT 0007 | 41. | 0. 0. 5.088 |
| MEMBER100740080 PSS | | | JOINT 0008 | 0. | -41. 0. -5.088 |
| MEMBER OFFSETS | -77.17 | -77.17 | JOINT 0009 | 0. | 41. 0. 5.088 |
| MEMBER100770079 PSS | | | JOINT 0010 | 41. | -14. 0. 5.088 -5.088 |
| MEMBER OFFSETS | -77.17 | -77.17 | JOINT 0011 | 41. | 14. 0. 5.088 5.088 |
| MEMBER 00020091 SF | | | JOINT 0012 | -41. | 14. 0. -5.088 5.088 |
| MEMBER 00020092 SF | | | JOINT 0013 | -41. | -14. 0. -5.088 -5.088 |
| MEMBER 00020093 SF | | | JOINT 0015 | -5. | 30. 87. 0.875 |
| MEMBER 00020094 SF | | | JOINT 0016 | 5. | 30. 87. 0.875 |
| MEMBER 00030100 SF | | | JOINT 0017 | -30. | 5. 87. 0.875 |
| MEMBER 00030101 SF | | | JOINT 0018 | -30. | -5. 87. 0.875 |
| MEMBER 00030103 SF | | | JOINT 0019 | 0. | 14. 0. 5.088 |
| MEMBER 00030104 SF | | | JOINT 0020 | 0. | -14. 0. -5.088 |
| MEMBER 00040095 SF | | | JOINT 0023 | -30. | -30. 87. 0.875 |
| MEMBER 00040096 SF | | | JOINT 0024 | 30. | -30. 87. 0.875 |
| MEMBER 00040097 SF | | | JOINT 0025 | 30. | 30. 87. 0.875 |
| MEMBER 00040098 SF | | | JOINT 0026 | -30. | 30. 87. 0.875 |
| MEMBER 00050083 SF | | | JOINT 0027 | -30. | 0. 87. 0.875 |
| MEMBER 00050084 SF | | | JOINT 0028 | 0. | -30. 87. 0.875 |
| MEMBER 00050085 SF | | | JOINT 0029 | 0. | 30. 87. 0.875 |
| MEMBER 00050086 SF | | | JOINT 0030 | 30. | 0. 87. 0.875 |
| MEMBER100700078 SS | | | JOINT 0031 | -35. | -35. 43. -8.544 -8.544 6.437 |
| MEMBER OFFSETS | -77.17 | -77.17 | JOINT 0032 | 35. | -35. 43. 8.544 -8.544 6.437 |
| MEMBER100710081 SS | | | JOINT 0033 | 35. | 35. 43. 8.544 8.544 6.437 |
| MEMBER OFFSETS | -77.17 | -77.17 | JOINT 0034 | -35. | 35. 43. -8.544 8.544 6.437 |
| MEMBER100720075 SS | | | JOINT 0035 | -35. | 0. 43. -8.544 6.437 |
| MEMBER OFFSETS | -77.17 | -77.17 | JOINT 0036 | 0. | -35. 43. -8.544 6.437 |
| MEMBER100730076 SS | | | JOINT 0037 | 0. | 35. 43. 8.544 6.437 |
| MEMBER OFFSETS | -77.17 | -77.17 | JOINT 0038 | 35. | 0. 43. 8.544 6.437 |
| MEMBER100740072 SS | | | JOINT 0039 | -42. | -42. -5. -0.498 -0.498 |
| MEMBER OFFSETS | -77.17 | -77.17 | JOINT 0040 | -42. | 42. -5. -0.498 0.498 |

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|------------|------|------|-----|---------|--------|-------|------------|------|------|-----|---------|--------|--------|
| JOINT 0133 | 8. | -35. | 43. | 2.000 | -8.544 | 6.437 | JOINT 0177 | 41. | -12. | 0. | 5.088 | -6.088 | |
| JOINT 0134 | -8. | -35. | 43. | -2.000 | -8.544 | 6.437 | JOINT 0178 | 41. | -16. | 0. | 5.088 | -4.088 | |
| JOINT 0135 | -30. | 14. | 0. | -4.562 | 5.088 | | JOINT 0179 | -41. | 16. | 0. | -5.088 | 4.088 | |
| JOINT 0136 | -23. | 14. | 0. | -7.438 | 5.088 | | JOINT 0180 | -41. | 12. | 0. | -5.088 | 6.088 | |
| JOINT 0137 | 23. | 14. | 0. | 7.438 | 5.088 | | JOINT 0181 | -41. | -12. | 0. | -5.088 | -6.088 | |
| JOINT 0138 | 30. | 14. | 0. | 4.562 | 5.088 | | JOINT 0182 | -41. | -16. | 0. | -5.088 | -4.088 | |
| JOINT 0139 | 30. | -14. | 0. | 4.562 | -5.088 | | JOINT 0183 | -1. | 14. | 0. | -11.000 | 5.088 | |
| JOINT 0140 | 23. | -14. | 0. | 7.438 | -5.088 | | JOINT 0184 | 1. | 14. | 0. | 11.000 | 5.088 | |
| JOINT 0141 | -23. | -14. | 0. | -7.438 | -5.088 | | JOINT 0185 | -1. | -14. | 0. | -11.000 | -5.088 | |
| JOINT 0142 | -30. | -14. | 0. | -4.562 | -5.088 | | JOINT 0186 | 1. | -14. | 0. | 11.000 | -5.088 | |
| JOINT 0143 | -5. | 41. | 0. | 5.088 | | | JOINT 0187 | 0. | -36. | 37. | -6.051 | 5.973 | |
| JOINT 0144 | 5. | 41. | 0. | 5.088 | | | JOINT 0189 | 0. | 36. | 37. | 6.051 | 5.973 | |
| JOINT 0145 | -5. | -41. | 0. | -5.088 | | | JOINT 0190 | 36. | 36. | 37. | 5.399 | 5.399 | 10.944 |
| JOINT 0146 | 5. | -41. | 0. | -5.088 | | | JOINT 0191 | 36. | -36. | 37. | 5.399 | -5.399 | 10.944 |
| JOINT 0147 | 41. | 3. | 0. | 5.088 | 9.000 | | JOINT 0192 | -36. | -36. | 37. | -5.399 | -5.399 | 10.944 |
| JOINT 0148 | -38. | -41. | 0. | -2.850 | -5.088 | | JOINT 0193 | -36. | 36. | 37. | -5.399 | 5.399 | 10.944 |
| JOINT 0149 | -35. | -41. | 0. | -0.613 | -5.088 | | JOINT 0194 | -20. | 20. | 0. | -11.919 | 5.169 | |
| JOINT 0150 | -31. | -41. | 0. | -10.375 | -5.088 | | JOINT 0195 | 20. | 20. | 0. | 11.919 | 5.169 | |
| JOINT 0151 | -28. | -41. | 0. | -8.138 | -5.088 | | JOINT 0196 | -20. | -20. | 0. | -11.919 | -5.169 | |
| JOINT 0152 | -25. | -41. | 0. | -5.900 | -5.088 | | JOINT 0197 | 20. | -20. | 0. | 11.919 | -5.169 | |
| JOINT 0153 | -22. | -41. | 0. | -3.663 | -5.088 | | JOINT 0198 | 35. | -35. | 46. | 4.416 | -4.416 | 1.900 |
| JOINT 0154 | -19. | -41. | 0. | -1.425 | -5.088 | | JOINT 0199 | 36. | -36. | 40. | 0.672 | -0.672 | 10.974 |
| JOINT 0155 | -15. | -41. | 0. | -11.188 | -5.088 | | JOINT 0200 | 35. | 35. | 46. | 4.416 | 4.416 | 1.900 |
| JOINT 0156 | -12. | -41. | 0. | -8.950 | -5.088 | | JOINT 0201 | 36. | 36. | 40. | 0.672 | 0.672 | 10.974 |
| JOINT 0157 | -9. | -41. | 0. | -6.713 | -5.088 | | JOINT 0202 | -35. | 35. | 46. | -4.416 | 4.416 | 1.900 |
| JOINT 0158 | -6. | -41. | 0. | -4.475 | -5.088 | | JOINT 0203 | -36. | 36. | 40. | -0.672 | 0.672 | 10.974 |
| JOINT 0159 | -3. | -41. | 0. | -2.238 | -5.088 | | JOINT 0204 | -35. | -35. | 46. | -4.416 | -4.416 | 1.900 |
| JOINT 0160 | 3. | -41. | 0. | 2.238 | -5.088 | | JOINT 0205 | -36. | -36. | 40. | -0.672 | -0.672 | 10.974 |
| JOINT 0161 | 6. | -41. | 0. | 4.475 | -5.088 | | JOINT 0220 | -38. | 14. | 0. | -2.850 | 5.088 | |
| JOINT 0162 | 9. | -41. | 0. | 6.713 | -5.088 | | JOINT 0221 | -35. | 14. | 0. | -0.613 | 5.088 | |
| JOINT 0163 | 12. | -41. | 0. | 8.950 | -5.088 | | JOINT 0222 | -31. | 14. | 0. | -10.375 | 5.088 | |
| JOINT 0164 | 15. | -41. | 0. | 11.188 | -5.088 | | JOINT 0223 | -28. | 14. | 0. | -8.138 | 5.088 | |
| JOINT 0165 | 19. | -41. | 0. | 1.425 | -5.088 | | JOINT 0224 | -25. | 14. | 0. | -5.900 | 5.088 | |
| JOINT 0166 | 22. | -41. | 0. | 3.663 | -5.088 | | JOINT 0225 | -22. | 14. | 0. | -3.663 | 5.088 | |
| JOINT 0167 | 25. | -41. | 0. | 5.900 | -5.088 | | JOINT 0226 | -19. | 14. | 0. | -1.425 | 5.088 | |
| JOINT 0168 | 28. | -41. | 0. | 8.138 | -5.088 | | JOINT 0227 | -15. | 14. | 0. | -11.188 | 5.088 | |
| JOINT 0169 | 31. | -41. | 0. | 10.375 | -5.088 | | JOINT 0228 | -12. | 14. | 0. | -8.950 | 5.088 | |
| JOINT 0170 | 35. | -41. | 0. | 0.613 | -5.088 | | JOINT 0229 | -9. | 14. | 0. | -6.713 | 5.088 | |
| JOINT 0171 | 38. | -41. | 0. | 2.850 | -5.088 | | JOINT 0230 | -6. | 14. | 0. | -4.475 | 5.088 | |
| JOINT 0172 | 41. | -3. | 0. | 5.088 | -9.000 | | JOINT 0231 | -3. | 14. | 0. | -2.238 | 5.088 | |
| JOINT 0173 | -41. | 3. | 0. | -5.088 | 9.000 | | JOINT 0232 | -38. | -14. | 0. | -2.850 | -5.088 | |
| JOINT 0174 | -41. | -3. | 0. | -5.088 | -9.000 | | JOINT 0233 | -35. | -14. | 0. | -0.613 | -5.088 | |
| JOINT 0175 | 41. | 16. | 0. | 5.088 | 4.088 | | JOINT 0234 | -31. | -14. | 0. | -10.375 | -5.088 | |
| JOINT 0176 | 41. | 12. | 0. | 5.088 | 6.088 | | JOINT 0235 | -28. | -14. | 0. | -8.138 | -5.088 | |

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|-----------------|---------|---------|----|---------|---------|-----------|----|--|--|
| JOINT 0236 | -25. | -14. | 0. | -5.900 | -5.088 | | | | |
| JOINT 0237 | -22. | -14. | 0. | -3.663 | -5.088 | | | | |
| JOINT 0238 | -19. | -14. | 0. | -1.425 | -5.088 | | | | |
| JOINT 0239 | -15. | -14. | 0. | -11.188 | -5.088 | | | | |
| JOINT 0240 | -12. | -14. | 0. | -8.950 | -5.088 | | | | |
| JOINT 0241 | -9. | -14. | 0. | -6.713 | -5.088 | | | | |
| JOINT 0242 | -6. | -14. | 0. | -4.475 | -5.088 | | | | |
| JOINT 0243 | -3. | -14. | 0. | -2.238 | -5.088 | | | | |
| JOINT 0244 | 3. | 14. | 0. | 2.238 | 5.088 | | | | |
| JOINT 0245 | 6. | 14. | 0. | 4.475 | 5.088 | | | | |
| JOINT 0246 | 9. | 14. | 0. | 6.713 | 5.088 | | | | |
| JOINT 0247 | 12. | 14. | 0. | 8.950 | 5.088 | | | | |
| JOINT 0248 | 15. | 14. | 0. | 11.188 | 5.088 | | | | |
| JOINT 0249 | 19. | 14. | 0. | 1.425 | 5.088 | | | | |
| JOINT 0250 | 22. | 14. | 0. | 3.663 | 5.088 | | | | |
| JOINT 0251 | 25. | 14. | 0. | 5.900 | 5.088 | | | | |
| JOINT 0252 | 28. | 14. | 0. | 8.138 | 5.088 | | | | |
| JOINT 0253 | 31. | 14. | 0. | 10.375 | 5.088 | | | | |
| JOINT 0254 | 35. | 14. | 0. | 0.613 | 5.088 | | | | |
| JOINT 0255 | 38. | 14. | 0. | 2.850 | 5.088 | | | | |
| JOINT 0256 | 3. | -14. | 0. | 2.238 | -5.088 | | | | |
| JOINT 0257 | 6. | -14. | 0. | 4.475 | -5.088 | | | | |
| JOINT 0258 | 9. | -14. | 0. | 6.713 | -5.088 | | | | |
| JOINT 0259 | 12. | -14. | 0. | 8.950 | -5.088 | | | | |
| JOINT 0260 | 15. | -14. | 0. | 11.188 | -5.088 | | | | |
| JOINT 0261 | 19. | -14. | 0. | 1.425 | -5.088 | | | | |
| JOINT 0262 | 22. | -14. | 0. | 3.663 | -5.088 | | | | |
| JOINT 0263 | 25. | -14. | 0. | 5.900 | -5.088 | | | | |
| JOINT 0264 | 28. | -14. | 0. | 8.138 | -5.088 | | | | |
| JOINT 0265 | 31. | -14. | 0. | 10.375 | -5.088 | | | | |
| JOINT 0266 | 35. | -14. | 0. | 0.613 | -5.088 | | | | |
| JOINT 0267 | 38. | -14. | 0. | 2.850 | -5.088 | | | | |
| JOINT 0268 | 25. | 15. | 0. | 5.900 | 11.188 | | | | |
| JOINT 0269 | 22. | 19. | 0. | 3.663 | 1.425 | | | | |
| JOINT 0270 | 19. | 22. | 0. | 1.425 | 3.663 | | | | |
| JOINT 0271 | 15. | 25. | 0. | 11.188 | 5.900 | | | | |
| JOINT 0272 | 12. | 28. | 0. | 8.950 | 8.138 | | | | |
| JOINT 0273 | 9. | 31. | 0. | 6.713 | 10.375 | | | | |
| JOINT 0274 | 6. | 35. | 0. | 4.475 | 0.613 | | | | |
| JOINT 0275 | 3. | 38. | 0. | 2.238 | 2.850 | | | | |
| JOINT 0276 | -3. | 38. | 0. | -2.238 | 2.850 | | | | |
| JOINT 0277 | -6. | 35. | 0. | -4.475 | 0.613 | | | | |
| JOINT 0278 | -9. | 31. | 0. | -6.713 | 10.375 | | | | |
| JOINT 0279 | -12. | 28. | 0. | -8.950 | 8.138 | | | | |
| JOINT 0280 | -15. | 25. | 0. | -11.188 | 5.900 | | | | |
| JOINT 0281 | -19. | 22. | 0. | -1.425 | 3.663 | | | | |
| JOINT 0282 | -22. | 19. | 0. | -3.663 | 1.425 | | | | |
| JOINT 0283 | -25. | 15. | 0. | -5.900 | 11.188 | | | | |
| JOINT 0284 | -25. | -15. | 0. | -5.900 | -11.188 | | | | |
| JOINT 0285 | -22. | -19. | 0. | -3.663 | -1.425 | | | | |
| JOINT 0286 | -19. | -22. | 0. | -1.425 | -3.663 | | | | |
| JOINT 0287 | -15. | -25. | 0. | -11.188 | -5.900 | | | | |
| JOINT 0288 | -12. | -28. | 0. | -8.950 | -8.138 | | | | |
| JOINT 0289 | -9. | -31. | 0. | -6.713 | -10.375 | | | | |
| JOINT 0290 | -6. | -35. | 0. | -4.475 | -0.613 | | | | |
| JOINT 0291 | -3. | -38. | 0. | -2.238 | -2.850 | | | | |
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| JOINT 0293 | 6. | -35. | 0. | 4.475 | -0.613 | | | | |
| JOINT 0294 | 9. | -31. | 0. | 6.713 | -10.375 | | | | |
| JOINT 0295 | 12. | -28. | 0. | 8.950 | -8.138 | | | | |
| JOINT 0296 | 15. | -25. | 0. | 11.188 | -5.900 | | | | |
| JOINT 0297 | 19. | -22. | 0. | 1.425 | -3.663 | | | | |
| JOINT 0298 | 22. | -19. | 0. | 3.663 | -1.425 | | | | |
| JOINT 0299 | 25. | -15. | 0. | 5.900 | -11.188 | | | | |
| JOINT 0300 | 27. | -14. | 0. | -5.088 | | | | | |
| JOINT 0301 | -27. | -14. | 0. | -5.088 | | | | | |
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| JOINT 0303 | 27. | 14. | 0. | 5.088 | | | | | |
| LOAD | | | | | | | | | |
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| LOAD Z 00280030 | -0.1149 | -0.1149 | | | | GLOB UNIF | 01 | | |
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| LOAD Z 00020035 | -0.1864 | -0.1864 | | | | GLOB UNIF | 01 | | |
| LOAD Z 00020036 | -0.1864 | -0.1864 | | | | GLOB UNIF | 01 | | |
| LOAD Z 00030037 | -0.1864 | -0.1864 | | | | GLOB UNIF | 01 | | |
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| LOAD Z 00050037 | -0.1864 | -0.1864 | | | | GLOB UNIF | 01 | | |
| LOAD Z 00230035 | -0.2459 | -0.2459 | | | | GLOB UNIF | 01 | | |
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| LOAD Z 00240038 | -0.2459 | -0.2459 | | | | GLOB UNIF | 01 | | |
| LOAD Z 00250037 | -0.2459 | -0.2459 | | | | GLOB UNIF | 01 | | |
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| LOAD Z 00260035 | -0.2459 | -0.2459 | GLOB UNIF | 01 | LOAD Z 00740072 | -0.5253 | -0.5253 | GLOB UNIF | 01 |
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| LOAD Z 00190001 | -0.0935 | -0.0935 | GLOB UNIF | 01 | LOAD Z 01050106 | -0.2024 | -0.2024 | GLOB UNIF | 01 |
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| LOAD Z 00040043 | -1.1118 | -1.1118 | GLOB UNIF | 01 | LOAD Z 01090110 | -0.2024 | -0.2024 | GLOB UNIF | 01 |
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| LOAD Z 00630070 | -0.5822 | -0.5822 | GLOB UNIF | 01 | LOAD Z 01490150 | -0.2024 | -0.2024 | GLOB UNIF | 01 |
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| LOAD Z 00080160 | -0.2024 | -0.2024 | GLOB UNIF | 01 | LOAD Z 02610262 | -0.1042 | -0.1042 | GLOB UNIF | 01 |
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| LOAD Z 01640165 | -0.2024 | -0.2024 | GLOB UNIF | 01 | LOAD Z 02680269 | -0.0935 | -0.0935 | GLOB UNIF | 01 |
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| LOAD Z 01660167 | -0.2024 | -0.2024 | GLOB UNIF | 01 | LOAD Z 02710272 | -0.0935 | -0.0935 | GLOB UNIF | 01 |
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| LOAD Z 01700171 | -0.2024 | -0.2024 | GLOB UNIF | 01 | LOAD Z 02750009 | -0.0935 | -0.0935 | GLOB UNIF | 01 |
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| LOAD Z 01630164 | -0.2673 | -0.2673 | GLOB UNIF 01 | LOAD Z 00490003 | -1.3764 | -1.3764 | GLOB UNIF 01 |
| LOAD Z 01640165 | -0.2673 | -0.2673 | GLOB UNIF 01 | LOAD Z 00500005 | -1.3764 | -1.3764 | GLOB UNIF 01 |
| LOAD Z 01650166 | -0.2673 | -0.2673 | GLOB UNIF 01 | LOAD Z 00390059 | -1.2046 | -1.2046 | GLOB UNIF 01 |
| LOAD Z 01660167 | -0.2673 | -0.2673 | GLOB UNIF 01 | LOAD Z 00400068 | -1.2046 | -1.2046 | GLOB UNIF 01 |
| LOAD Z 01670168 | -0.2673 | -0.2673 | GLOB UNIF 01 | LOAD Z 00430063 | -1.2046 | -1.2046 | GLOB UNIF 01 |
| LOAD Z 01680169 | -0.2673 | -0.2673 | GLOB UNIF 01 | LOAD Z 00440061 | -1.2046 | -1.2046 | GLOB UNIF 01 |
| LOAD Z 01690170 | -0.2673 | -0.2673 | GLOB UNIF 01 | LOAD Z 00580040 | -1.2046 | -1.2046 | GLOB UNIF 01 |
| LOAD Z 01700171 | -0.2673 | -0.2673 | GLOB UNIF 01 | LOAD Z 00620043 | -1.2046 | -1.2046 | GLOB UNIF 01 |
| LOAD Z 01710004 | -0.2673 | -0.2673 | GLOB UNIF 01 | LOAD Z 00630067 | -1.2046 | -1.2046 | GLOB UNIF 01 |
| LOAD Z 01730180 | -0.2673 | -0.2673 | GLOB UNIF 01 | LOAD Z 00670044 | -1.2046 | -1.2046 | GLOB UNIF 01 |
| LOAD Z 01750003 | -0.2673 | -0.2673 | GLOB UNIF 01 | LOAD Z 00680069 | -1.2046 | -1.2046 | GLOB UNIF 01 |
| LOAD Z 01770172 | -0.2673 | -0.2673 | GLOB UNIF 01 | LOAD Z 00690039 | -1.2046 | -1.2046 | GLOB UNIF 01 |
| LOAD Z 01790005 | -0.2673 | -0.2673 | GLOB UNIF 01 | LOAD Z 00630070 | -0.7006 | -0.7006 | GLOB UNIF 01 |
| LOAD Z 01810174 | -0.2673 | -0.2673 | GLOB UNIF 01 | LOAD Z 00670071 | -0.7006 | -0.7006 | GLOB UNIF 01 |
| LOAD Z 00310205 | -0.8098 | -0.8098 | GLOB UNIF 01 | LOAD Z 00680072 | -0.7006 | -0.7006 | GLOB UNIF 01 |
| LOAD Z 00320199 | -0.8098 | -0.8098 | GLOB UNIF 01 | LOAD Z 00690073 | -0.7006 | -0.7006 | GLOB UNIF 01 |
| LOAD Z 00330201 | -0.8098 | -0.8098 | GLOB UNIF 01 | LOAD Z 00880220 | -0.0256 | -0.0256 | GLOB UNIF 01 |
| LOAD Z 00340203 | -0.8098 | -0.8098 | GLOB UNIF 01 | LOAD Z 00890221 | -0.0256 | -0.0256 | GLOB UNIF 01 |
| LOAD Z 00410204 | -0.8098 | -0.8098 | GLOB UNIF 01 | LOAD Z 00900222 | -0.0256 | -0.0256 | GLOB UNIF 01 |
| LOAD Z 00420202 | -0.8098 | -0.8098 | GLOB UNIF 01 | LOAD Z 00990223 | -0.0256 | -0.0256 | GLOB UNIF 01 |

| | | | | | | | |
|-----------------|---------|---------|-------------------|---|---------|------|-------------------|
| LOAD Z 00040097 | -0.1223 | -0.1223 | GLOBAL UNIF 01 | LOAD 0004 | -515.69 | | GLOBAL JOIN ROLL |
| LOAD Z 00040098 | -0.1223 | -0.1223 | GLOBAL UNIF 01 | LOADCN 2E | | | |
| LOAD Z 00050083 | -0.1223 | -0.1223 | GLOBAL UNIF 01 | LOAD 0004 | 0.30130 | | GLOBAL JOIN PITCH |
| LOAD Z 00050084 | -0.1223 | -0.1223 | GLOBAL UNIF 01 | LOADCN 2F | | | |
| LOAD Z 00050085 | -0.1223 | -0.1223 | GLOBAL UNIF 01 | LOAD 0004 | -0.3013 | | GLOBAL JOIN PITCH |
| LOAD Z 00050086 | -0.1223 | -0.1223 | GLOBAL UNIF 01 | LOADCN 3A | | | |
| LOAD Z 00700078 | -0.6316 | -0.6316 | GLOBAL UNIF 01 | LOAD 0003 | 4.26136 | | GLOBAL JOIN HEAVE |
| LOAD Z 00710081 | -0.6316 | -0.6316 | GLOBAL UNIF 01 | LOADCN 3B | | | |
| LOAD Z 00720075 | -0.6316 | -0.6316 | GLOBAL UNIF 01 | LOAD 0003 | -4.2614 | | GLOBAL JOIN HEAVE |
| LOAD Z 00730076 | -0.6316 | -0.6316 | GLOBAL UNIF 01 | LOADCN 3C | | | |
| LOAD Z 00740072 | -0.6316 | -0.6316 | GLOBAL UNIF 01 | LOAD 0003 | 515.691 | | GLOBAL JOIN ROLL |
| LOAD Z 00770073 | -0.6316 | -0.6316 | GLOBAL UNIF 01 | LOADCN 3D | | | |
| LOAD Z 00790070 | -0.6316 | -0.6316 | GLOBAL UNIF 01 | LOAD 0003 | -515.69 | | GLOBAL JOIN ROLL |
| LOAD Z 00800071 | -0.6316 | -0.6316 | GLOBAL UNIF 01 | LOADCN 3E | | | |
| LOAD 0003 | -5.7087 | | GLOBAL JOIN 01 | LOAD 0003 | 0.30130 | | GLOBAL JOIN PITCH |
| LOAD 0011 | -5.7087 | | GLOBAL JOIN 01 | LOADCN 3F | | | |
| LOAD 0005 | -5.7087 | | GLOBAL JOIN 01 | LOAD 0003 | -0.3013 | | GLOBAL JOIN PITCH |
| LOAD 0012 | -5.7087 | | GLOBAL JOIN 01 | LOADCN 4A | | | |
| LOAD 0002 | -5.7087 | | GLOBAL JOIN 01 | LOAD 0005 | 4.26136 | | GLOBAL JOIN HEAVE |
| LOAD 0013 | -5.7087 | | GLOBAL JOIN 01 | LOADCN 4B | | | |
| LOAD 0010 | -5.7087 | | GLOBAL JOIN 01 | LOAD 0005 | -4.2614 | | GLOBAL JOIN HEAVE |
| LOAD 0004 | -5.7087 | | GLOBAL JOIN 01 | LOADCN 4C | | | |
| LOADCN 0D | | | | LOAD 0005 | 515.691 | | GLOBAL JOIN ROLL |
| WIND | | | | LOADCN 4D | | | |
| WIND D F 51.020 | 0.00 | AP08 | | LOAD 0005 | -515.69 | | GLOBAL JOIN ROLL |
| LOADCN 1A | | | | LOADCN 4E | | | |
| LOAD 0002 | 4.26136 | | GLOBAL JOIN HEAVE | LOAD 0005 | 0.30130 | | GLOBAL JOIN PITCH |
| LOADCN 1B | | | | LOADCN 4F | | | |
| LOAD 0002 | -4.2614 | | GLOBAL JOIN HEAVE | LOAD 0005 | -0.3013 | | GLOBAL JOIN PITCH |
| LOADCN 1C | | | | LOADCN 90D | | | |
| LOAD 0002 | 515.691 | | GLOBAL JOIN ROLL | WIND | | | |
| LOADCN 1D | | | | WIND D F 51.020 | 90.00 | AP08 | |
| LOAD 0002 | -515.69 | | GLOBAL JOIN ROLL | LOADCN180D | | | |
| LOADCN 1E | | | | WIND | | | |
| LOAD 0002 | 0.30130 | | GLOBAL JOIN PITCH | WIND D F 51.020 | 180.00 | AP08 | |
| LOADCN 1F | | | | LOADCN270D | | | |
| LOAD 0002 | -0.3013 | | GLOBAL JOIN PITCH | WIND | | | |
| LOADCN 2A | | | | WIND D F 51.020 | 270.00 | AP08 | |
| LOAD 0004 | 4.26136 | | GLOBAL JOIN HEAVE | LCOMB | | | |
| LOADCN 2B | | | | LCOMB +R+H 1A 1.00001C 1.00002A 1.00002C 1.00003A 1.00003C 1.0000 | | | |
| LOAD 0004 | -4.2614 | | GLOBAL JOIN HEAVE | LCOMB +R+H 4A 1.00004C 1.0000 | | | |
| LOADCN 2C | | | | LCOMB 201 0D 1.0000+R+H1.0000 | | | |
| LOAD 0004 | 515.691 | | GLOBAL JOIN ROLL | LCOMB +R-H 1B 1.00001C 1.00002B 1.00002C 1.00003B 1.00003C 1.0000 | | | |
| LOADCN 2D | | | | | | | |

LCOMB +R-H 4B 1.00004C 1.0000
 LCOMB 202 0D 1.0000+R-H1.0000
 LCOMB -R+H 1A 1.00001D 1.00002A 1.00002D 1.00003A 1.00003D 1.0000
 LCOMB -R+H 4A 1.00004D 1.0000
 LCOMB 203 0D 1.0000-R+H1.0000
 LCOMB -R-H 1B 1.00001D 1.00002B 1.00002D 1.00003B 1.00003D 1.0000
 LCOMB -R-H 4B 1.00004D 1.0000
 LCOMB 204 0D 1.0000-R-H1.0000
 LCOMB +H+P 1A 1.00001E 1.00002A 1.00002E 1.00003A 1.00003E 1.0000
 LCOMB +H+P 4A 1.00004E 1.0000
 LCOMB 205 0D 1.0000+H+P1.0000
 LCOMB -H+P 1B 1.00001E 1.00002B 1.00002E 1.00003B 1.00003E 1.0000
 LCOMB -H+P 4B 1.00004E 1.0000
 LCOMB 206 0D 1.0000-H+P1.0000
 LCOMB +H-P 1A 1.00001F 1.00002A 1.00002F 1.00003A 1.00003F 1.0000
 LCOMB +H-P 4A 1.00004F 1.0000
 LCOMB 207 0D 1.0000+H-P1.0000
 LCOMB -H-P 1B 1.00001F 1.00002B 1.00002F 1.00003B 1.00003F 1.0000
 LCOMB -H-P 4B 1.00004F 1.0000
 LCOMB 208 0D 1.0000-H-P1.0000
 LCOMB 209 90D 1.0000+R+H1.0000
 LCOMB 210 90D 1.0000+R-H1.0000
 LCOMB 211 -R+H1.000090D 1.0000
 LCOMB 212 90D 1.0000-R-H1.0000
 LCOMB 213 +H+P1.000090D 1.0000
 LCOMB 214 -H+P1.000090D 1.0000
 LCOMB 215 90D 1.0000+H-P1.0000
 LCOMB 216 90D 1.0000-H-P1.0000
 LCOMB 217 +R+H1.0000180D1.0000
 LCOMB 218 +R-H1.0000180D1.0000
 LCOMB 219 -R+H1.0000180D1.0000
 LCOMB 220 -R-H1.0000180D1.0000
 LCOMB 221 180D1.0000+H+P1.0000
 LCOMB 222 -H+P1.0000180D1.0000
 LCOMB 223 180D1.0000+H-P1.0000
 LCOMB 224 180D1.0000-H-P1.0000
 LCOMB 225 +R+H1.0000270D1.0000
 LCOMB 226 270D1.0000+R-H1.0000
 LCOMB 227 270D1.0000-R+H1.0000
 LCOMB 228 270D1.0000-R-H1.0000
 LCOMB 229 +H+P1.0000270D1.0000
 LCOMB 230 270D1.0000-H+P1.0000
 LCOMB 231 270D1.0000+H-P1.0000
 LCOMB 232 -H-P1.0000270D1.0000
 END
 PHY1T0002-0004 THRO0002-0148 MEM0148-0149 MEM0149-0150 MEM0150-0151 MEM
 PHY1T0002-0004 THRO0151-0152 MEM0152-0153 MEM0153-0154 MEM0154-0155 MEM
 PHY1T0002-0004 THRO0155-0156 MEM0156-0157 MEM0157-0158 MEM0158-0145 MEM
 PHY1T0002-0004 THRO0145-0159 MEM0159-0008 MEM0008-0160 MEM0160-0146 MEM
 PHY1T0002-0004 THRO0146-0161 MEM0161-0162 MEM0162-0163 MEM0163-0164 MEM
 PHY1T0002-0004 THRO0164-0165 MEM0165-0166 MEM0166-0167 MEM0167-0168 MEM
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 PHY1T0002-0005 THRO0002-0182 MEM0182-0013 MEM0013-0181 MEM0181-0174 MEM
 PHY1T0002-0005 THRO0174-0006 MEM0006-0173 MEM0173-0180 MEM0180-0012 MEM
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 PHY1T0004-0003 THRO0004-0178 MEM0178-0010 MEM0010-0177 MEM0177-0172 MEM
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 PHY1T0004-0003 THRO0011-0175 MEM0175-0003 MEM
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 PHY1T0005-0003 THRO0099-0102 MEM0102-0105 MEM0105-0106 MEM0106-0107 MEM
 PHY1T0005-0003 THRO0107-0108 MEM0108-0109 MEM0109-0110 MEM0110-0143 MEM
 PHY1T0005-0003 THRO0143-0111 MEM0111-0009 MEM0009-0112 MEM0112-0144 MEM
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 PHY1T0005-0003 THRO0116-0117 MEM0117-0118 MEM0118-0119 MEM0119-0120 MEM
 PHY1T0005-0003 THRO0120-0121 MEM0121-0122 MEM0122-0123 MEM0123-0003 MEM
 PHY1T0006-0008 THRO0006-0301 MEM0301-0284 MEM0284-0285 MEM0285-0196 MEM
 PHY1T0006-0008 THRO0196-0286 MEM0286-0287 MEM0287-0288 MEM0288-0289 MEM
 PHY1T0006-0008 THRO0289-0290 MEM0290-0291 MEM0291-0008 MEM
 PHY1T0007-0009 THRO0007-0303 MEM0303-0268 MEM0268-0269 MEM0269-0195 MEM
 PHY1T0007-0009 THRO0195-0270 MEM0270-0271 MEM0271-0272 MEM0272-0273 MEM
 PHY1T0007-0009 THRO0273-0274 MEM0274-0275 MEM0275-0009 MEM
 PHY1T0008-0007 THRO0008-0292 MEM0292-0293 MEM0293-0294 MEM0294-0295 MEM

PHY1T0008-0007 THRO0295-0296 MEM0296-0297 MEM0297-0197 MEM0197-0298 MEM
 PHY1T0008-0007 THRO0298-0299 MEM0299-0300 MEM0300-0007 MEM
 PHY1T0009-0006 THRO0009-0276 MEM0276-0277 MEM0277-0278 MEM0278-0279 MEM
 PHY1T0009-0006 THRO0279-0280 MEM0280-0281 MEM0281-0194 MEM0194-0282 MEM
 PHY1T0009-0006 THRO0282-0283 MEM0283-0302 MEM0302-0006 MEM
 PHY1T0012-0019 THRO0012-0220 MEM0220-0221 MEM0221-0222 MEM0222-0135 MEM
 PHY1T0012-0019 THRO0135-0223 MEM0223-0302 MEM0302-0224 MEM0224-0136 MEM
 PHY1T0012-0019 THRO0136-0225 MEM0225-0226 MEM0226-0227 MEM0227-0228 MEM
 PHY1T0012-0019 THRO0228-0229 MEM0229-0230 MEM0230-0231 MEM0231-0183 MEM
 PHY1T0012-0019 THRO0183-0019 MEM
 PHY1T0013-0020 THRO0013-0232 MEM0232-0233 MEM0233-0234 MEM0234-0142 MEM
 PHY1T0013-0020 THRO0142-0235 MEM0235-0301 MEM0301-0236 MEM0236-0141 MEM
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 PHY1T0019-0011 THRO0019-0184 MEM0184-0244 MEM0244-0245 MEM0245-0246 MEM
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 PHY1T0023-0024 THRO0023-0052 MEM0052-0028 MEM0028-0053 MEM0053-0024 MEM
 PHY1T0023-0026 THRO0023-0018 MEM0018-0027 MEM0027-0017 MEM0017-0026 MEM
 PHY1T0024-0004 THRO0024-0051 MEM0051-0198 MEM0198-0032 MEM0032-0199 MEM
 PHY1T0024-0004 THRO0199-0191 MEM0191-0047 MEM0047-0004 MEM
 PHY1T0024-0025 THRO0024-0054 MEM0054-0030 MEM0030-0055 MEM0055-0025 MEM
 PHY1T0025-0003 THRO0025-0048 MEM0048-0200 MEM0200-0033 MEM0033-0201 MEM
 PHY1T0025-0003 THRO0201-0190 MEM0190-0049 MEM0049-0003 MEM
 PHY1T0026-0005 THRO0026-0042 MEM0042-0202 MEM0202-0034 MEM0034-0203 MEM
 PHY1T0026-0005 THRO0203-0193 MEM0193-0050 MEM0050-0005 MEM
 PHY1T0026-0025 THRO0026-0015 MEM0015-0029 MEM0029-0016 MEM0016-0025 MEM
 PHY1T0040-0039 THRO0040-0068 MEM0068-0069 MEM0069-0039 MEM
 PHY1T0043-0044 THRO0043-0063 MEM0063-0067 MEM0067-0044 MEM
 PHY1T0102-0224 THRO0102-0283 MEM0283-0224 MEM
 PHY1T0105-0225 THRO0105-0282 MEM0282-0225 MEM
 PHY1T0106-0226 THRO0106-0281 MEM0281-0226 MEM
 PHY1T0107-0227 THRO0107-0280 MEM0280-0227 MEM
 PHY1T0108-0228 THRO0108-0279 MEM0279-0228 MEM
 PHY1T0109-0229 THRO0109-0278 MEM0278-0229 MEM
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 PHY1T0112-0244 THRO0112-0275 MEM0275-0244 MEM
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 PHY1T0115-0247 THRO0115-0272 MEM0272-0247 MEM
 PHY1T0116-0248 THRO0116-0271 MEM0271-0248 MEM
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 PHY1T0118-0250 THRO0118-0269 MEM0269-0250 MEM
 PHY1T0119-0251 THRO0119-0268 MEM0268-0251 MEM
 PHY1T0236-0152 THRO0236-0284 MEM0284-0152 MEM
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 PHY1T0243-0159 THRO0243-0291 MEM0291-0159 MEM
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 PHY1T0258-0162 THRO0258-0294 MEM0294-0162 MEM
 PHY1T0259-0163 THRO0259-0295 MEM0295-0163 MEM
 PHY1T0260-0164 THRO0260-0296 MEM0296-0164 MEM
 PHY1T0261-0165 THRO0261-0297 MEM0297-0165 MEM
 PHY1T0262-0166 THRO0262-0298 MEM0298-0166 MEM
 PHY1T0263-0167 THRO0263-0299 MEM0299-0167 MEM

LAMPIRAN C
OUTPUT SACS

DATE 17-Jul-2016 TIME 15:33:50

MEMBER STRESS AT MAX UNITY CHECK REPORT

| MEMBER | GRP | MAXIMUM UNITY CHECK | CRITICAL COND. | LOAD COND NO. | DIST FROM END FT | ***** APPLIED STRESSES ***** | | | | | * CM VALUES * | | * NEXT TWO HIGHEST CASES * | | | |
|-----------|-----|---------------------------|-------------------|---------------------|---------------------------|------------------------------|-----------------------------|------------|---------------------------|----------|---------------|------|----------------------------|--------------|----------------|--------------|
| | | | | | | AXIAL ksi | ** BENDING ** Y-Y ksi | Z-Z ksi | *** SHEAR *** Y ksi | Z ksi | Y | Z | UNITY CHECK | LOAD COND | UNITY CHECK | LOAD COND |
| 0002-0091 | SF | 0.781 | C>.15A | +R+H | 0.00 | -12.87 | 4.19 | 5.51 | 0.11 | 0.00 | 0.85 | 0.85 | 0.78 | +R-H | 0.55 | -R-H |
| 0002-0092 | SF | 0.795 | C>.15A | -R+H | 0.00 | -12.94 | -6.47 | -5.08 | 0.20 | 0.00 | 0.85 | 0.85 | 0.80 | -R-H | 0.57 | +R-H |
| 0002-0093 | SF | 0.741 | C>.15A | -R+H | 0.00 | -11.81 | -5.56 | 5.63 | 0.19 | 0.00 | 0.85 | 0.85 | 0.74 | -R-H | 0.47 | +R-H |
| 0002-0094 | SF | 0.767 | C>.15A | +R+H | 0.00 | -13.36 | 1.80 | -5.06 | 0.13 | 0.00 | 0.85 | 0.85 | 0.77 | +R-H | 0.53 | -R-H |
| 0003-0100 | SF | 0.806 | C>.15A | -R+H | 0.00 | -14.02 | 2.37 | -5.49 | 0.13 | 0.00 | 0.85 | 0.85 | 0.81 | -R-H | 0.56 | +R-H |
| 0003-0101 | SF | 0.801 | C>.15A | +R+H | 0.00 | -12.91 | -6.20 | 5.75 | 0.21 | 0.00 | 0.85 | 0.85 | 0.80 | +R-H | 0.52 | -R-H |
| 0003-0103 | SF | 0.742 | C>.15A | +R+H | 0.00 | -11.94 | -5.87 | -5.03 | 0.19 | 0.00 | 0.85 | 0.85 | 0.74 | +R-H | 0.52 | -R-H |
| 0003-0104 | SF | 0.737 | C>.15A | -R+H | 0.00 | -12.17 | 3.58 | 5.14 | 0.11 | 0.00 | 0.85 | 0.85 | 0.74 | -R-H | 0.52 | +R-H |
| 0004-0095 | SF | 0.768 | C>.15A | +R+H | 0.00 | -13.37 | 1.81 | 5.07 | 0.13 | 0.00 | 0.85 | 0.85 | 0.77 | +R-H | 0.53 | -R-H |
| 0004-0096 | SF | 0.742 | C>.15A | -R+H | 0.00 | -11.82 | -5.57 | -5.64 | 0.19 | 0.00 | 0.85 | 0.85 | 0.74 | -R-H | 0.47 | +R-H |
| 0004-0097 | SF | 0.796 | C>.15A | -R+H | 0.00 | -12.95 | -6.47 | 5.08 | 0.20 | 0.00 | 0.85 | 0.85 | 0.80 | -R-H | 0.57 | +R-H |
| 0004-0098 | SF | 0.781 | C>.15A | +R+H | 0.00 | -12.87 | 4.20 | -5.50 | 0.11 | 0.00 | 0.85 | 0.85 | 0.78 | +R-H | 0.55 | -R-H |
| 0005-0083 | SF | 0.769 | C>.15A | -R+H | 0.00 | -13.39 | 1.80 | 5.05 | 0.13 | 0.00 | 0.85 | 0.85 | 0.77 | -R-H | 0.53 | +R-H |
| 0005-0084 | SF | 0.741 | C>.15A | +R+H | 0.00 | -11.79 | -5.57 | -5.66 | 0.19 | 0.00 | 0.85 | 0.85 | 0.74 | +R-H | 0.47 | -R-H |
| 0005-0085 | SF | 0.799 | C>.15A | +R+H | 0.00 | -13.00 | -6.48 | 5.08 | 0.20 | 0.00 | 0.85 | 0.85 | 0.80 | +R-H | 0.57 | -R-H |
| 0005-0086 | SF | 0.776 | C>.15A | -R+H | 0.00 | -12.78 | 4.18 | -5.48 | 0.11 | 0.00 | 0.85 | 0.85 | 0.78 | -R-H | 0.55 | +R-H |

LAMPIRAN D
KEANDALAN

Keandalan F Aktual 14,02 ksi

| Variabel | Data | | | | Distribusi | | ASTM 36 | General Structural Steel 29000 Ksi | ASTM 36 | | | | | | | | | | | |
|------------|----------|------------------|----------|-------------|------------|------------------|----------|---|---|----------|------------|-----|--|--|--|--|--|--|--|--|
| | Mean | Standart Deviasi | COV | Distribusi | Mean | Standart Deviasi | | | | | | | | | | | | | | |
| Fy (Ksi) | 36 | 3,6 | 0,1 | Lognormal | 3,57854377 | 0,099751345 | | | | | | | | | | | | | | |
| E (Ksi) | 29000 | 290 | 0,01 | Normal | | | | | | | | | | | | | | | | |
| Fa (Ksi) | 14,02 | 1,402 | 0,1 | Lognormal | 2,63550972 | 0,099751345 | | | | | | | | | | | | | | |
| no | a1 | Fy (Ksi) | a2 | E (Ksi) | a3 | Fa (Ksi) | Cc | $\frac{1}{\sigma} \ln \frac{F - \mu}{\sigma}$ | $\frac{1}{\sigma} \ln \frac{F - \mu}{\sigma}$ | Fcr | MK (Ksi) | Ket | | | | | | | | |
| 1 | 0,545215 | 36,23 | 0,152999 | 28703,1394 | 0,02480344 | 11,46918729 | 306,1638 | 35,52346 | 1,73973849 | 20,41885 | 8,949663 | 1 | | | | | | | | |
| 2 | 0,994372 | 46,13 | 0,16825 | 28721,28031 | 0,47575559 | 13,8660571 | 271,4244 | 44,98236 | 1,74879539 | 25,72191 | 11,85585 | 1 | | | | | | | | |
| 3 | 0,690204 | 37,64 | 0,764659 | 29209,19706 | 0,82309904 | 15,30230019 | 303,0094 | 36,89097 | 1,74047883 | 21,19588 | 5,893576 | 1 | | | | | | | | |
| 4 | 0,385993 | 34,80 | 0,436379 | 28953,55458 | 0,17426941 | 12,70505675 | 313,7452 | 34,1549 | 1,73801757 | 19,65164 | 6,946587 | 1 | | | | | | | | |
| 5 | 0,681613 | 37,55 | 0,162335 | 28714,37658 | 0,88616813 | 15,73440356 | 300,795 | 36,79093 | 1,74100747 | 21,13198 | 5,397573 | 1 | | | | | | | | |
| 6 | 0,47014 | 35,55 | 0,291458 | 28840,75191 | 0,03236866 | 11,60298303 | 309,7957 | 34,8779 | 1,73890397 | 20,05741 | 8,454422 | 1 | | | | | | | | |
| 7 | 0,89006 | 40,48 | 0,27252 | 28824,4892 | 0,50137961 | 13,95523455 | 290,239 | 39,60676 | 1,74363339 | 22,71508 | 8,759841 | 1 | | | | | | | | |
| 8 | 0,598326 | 36,72 | 0,217515 | 28773,6223 | 0,4525155 | 13,78537901 | 304,4758 | 35,99868 | 1,74013284 | 20,68732 | 6,901938 | 1 | | | | | | | | |
| 9 | 0,926702 | 41,40 | 0,466667 | 28975,74127 | 0,99189232 | 17,73101049 | 287,7548 | 40,48942 | 1,74427809 | 23,21271 | 5,481699 | 1 | | | | | | | | |
| 10 | 0,440459 | 35,29 | 0,905124 | 29380,28005 | 0,05363504 | 11,87994443 | 313,8501 | 34,63558 | 1,73799433 | 19,92847 | 8,04853 | 1 | | | | | | | | |
| 11 | 0,259071 | 33,59 | 0,724743 | 29173,1272 | 0,01372663 | 11,19600265 | 320,5813 | 32,98817 | 1,73653298 | 18,99657 | 7,800568 | 1 | | | | | | | | |
| 12 | 0,223495 | 33,20 | 0,928771 | 29425,34295 | 0,12876185 | 12,46051587 | 323,8038 | 32,62609 | 1,73585411 | 18,79541 | 6,334897 | 1 | | | | | | | | |
| 13 | 0,397345 | 34,90 | 0,610213 | 29081,16383 | 0,18615462 | 12,76256071 | 313,9727 | 34,25668 | 1,73796716 | 19,71078 | 6,948215 | 1 | | | | | | | | |
| 14 | 0,972265 | 43,36 | 0,053252 | 28531,90849 | 0,55786617 | 14,15445846 | 279,0169 | 42,34462 | 1,74663262 | 24,24358 | 10,08912 | 1 | | | | | | | | |
| 15 | 0,201755 | 32,96 | 0,453811 | 28966,34858 | 0,67982932 | 14,61598358 | 322,4712 | 32,37841 | 1,73613326 | 18,64973 | 4,033742 | 1 | | | | | | | | |
| 16 | 0,538557 | 36,17 | 0,078946 | 28590,46301 | 0,67754867 | 14,60670425 | 305,8181 | 35,46245 | 1,7398189 | 20,38284 | 5,776134 | 1 | | | | | | | | |
| 17 | 0,134245 | 32,08 | 0,060334 | 28549,92667 | 0,17149622 | 12,69132377 | 324,5043 | 31,52134 | 1,73570825 | 18,16051 | 5,469184 | 1 | | | | | | | | |
| 18 | 0,044474 | 30,23 | 0,115664 | 28652,88579 | 0,50784835 | 13,97782634 | 334,8713 | 29,73859 | 1,73361858 | 17,15405 | 3,176227 | 1 | | | | | | | | |
| 19 | 0,97906 | 43,88 | 0,071398 | 28575,01747 | 0,49065992 | 13,91787427 | 277,5679 | 42,84177 | 1,74703671 | 24,52254 | 10,60466 | 1 | | | | | | | | |
| 20 | 0,704619 | 37,80 | 0,765364 | 29209,86238 | 0,81845577 | 15,27523896 | 302,3893 | 37,04019 | 1,74062611 | 21,27981 | 6,004569 | 1 | | | | | | | | |
| 21 | 0,656911 | 37,29 | 0,142487 | 28689,92901 | 0,17246256 | 12,69612338 | 301,6909 | 36,54608 | 1,7407927 | 20,99393 | 8,297804 | 1 | | | | | | | | |
| 22 | 0,969839 | 43,20 | 0,313569 | 28859,13021 | 0,45701099 | 13,80098377 | 281,1271 | 42,20486 | 1,74605125 | 24,1716 | 10,37062 | 1 | | | | | | | | |
| 23 | 0,298156 | 33,98 | 0,290923 | 28840,29946 | 0,83208964 | 15,3561489 | 316,9007 | 33,35965 | 1,73732464 | 19,20174 | 3,845589 | 1 | | | | | | | | |
| 24 | 0,047848 | 30,34 | 0,388238 | 28917,66519 | 0,1627025 | 12,64691241 | 335,8301 | 29,84508 | 1,73343161 | 17,21734 | 4,570428 | 1 | | | | | | | | |
| 25 | 0,856994 | 39,84 | 0,443672 | 28958,91728 | 0,36934726 | 13,49385505 | 293,2449 | 38,99752 | 1,74286724 | 22,3755 | 8,88164 | 1 | | | | | | | | |
| 26 | 0,698793 | 37,73 | 0,184769 | 28739,77197 | 0,04934486 | 11,8318657 | 300,1976 | 36,96712 | 1,74115134 | 21,23142 | 9,399558 | 1 | | | | | | | | |
| 27 | 0,517551 | 35,98 | 0,148962 | 28698,13969 | 0,21003562 | 12,87233505 | 307,2012 | 35,28251 | 1,73949817 | 20,28315 | 7,41082 | 1 | | | | | | | | |
| 28 | 0,730869 | 38,09 | 0,875458 | 29334,24772 | 0,29159713 | 13,20735235 | 301,8602 | 37,32577 | 1,74075224 | 21,44232 | 8,234967 | 1 | | | | | | | | |
| 29 | 0,650769 | 37,23 | 0,377634 | 28909,60665 | 0,2875028 | 13,19159196 | 303,0953 | 36,49234 | 1,74045849 | 20,96708 | 7,77549 | 1 | | | | | | | | |
| 30 | 0,662992 | 37,36 | 0,189262 | 28744,62065 | 0,19256943 | 12,79275491 | 301,7284 | 36,60681 | 1,74078372 | 21,02892 | 8,236168 | 1 | | | | | | | | |
| 31 | 0,119843 | 31,86 | 0,651653 | 29113,03835 | 0,18715219 | 12,76729318 | 328,8223 | 31,31884 | 1,73482243 | 18,05305 | 5,28576 | 1 | | | | | | | | |
| 32 | 0,330604 | 34,29 | 0,371063 | 28904,57867 | 0,58143616 | 14,23943873 | 315,8097 | 33,66109 | 1,73756272 | 19,37259 | 5,133153 | 1 | | | | | | | | |
| 33 | 0,805443 | 39,03 | 0,764001 | 29208,57693 | 0,86783626 | 15,59350186 | 297,543 | 38,22932 | 1,74179743 | 21,9482 | 6,354702 | 1 | | | | | | | | |
| 34 | 0,905154 | 40,83 | 0,72836 | 29176,27981 | 0,94975133 | 16,43389614 | 290,7746 | 39,94584 | 1,74349575 | 22,91135 | 6,477452 | 1 | | | | | | | | |
| 35 | 0,607975 | 36,81 | 0,835196 | 29282,7222 | 0,16866711 | 12,67718532 | 306,7744 | 36,09949 | 1,73959686 | 20,75164 | 8,074456 | 1 | | | | | | | | |
| 36 | 0,766097 | 38,51 | 0,923709 | 29414,83698 | 0,18973624 | 12,77948798 | 300,6116 | 37,73345 | 1,74105157 | 21,67279 | 8,893303 | 1 | | | | | | | | |
| 37 | 0,505472 | 35,87 | 0,341689 | 28881,72153 | 0,73143622 | 14,83623507 | 308,6482 | 35,18256 | 1,73916586 | 20,22956 | 5,393325 | 1 | | | | | | | | |
| 38 | 0,684176 | 37,58 | 0,352247 | 28890,01451 | 0,15588448 | 12,61150529 | 301,6053 | 36,82141 | 1,74081317 | 21,15184 | 8,54034 | 1 | | | | | | | | |
| 39 | 0,381093 | 34,76 | 0,660518 | 29120,02477 | 0,69308433 | 14,67059936 | 314,8473 | 34,11572 | 1,73777403 | 19,63185 | 4,961249 | 1 | | | | | | | | |
| 40 | 0,657211 | 37,30 | 0,709743 | 29160,26398 | 0,65796065 | 14,52830636 | 304,1414 | 36,56106 | 1,74021147 | 21,00955 | 6,481245 | 1 | | | | | | | | |
| 41 | 0,278441 | 33,78 | 0,523502 | 29017,09428 | 0,48426795 | 13,89563915 | 318,7877 | 33,17522 | 1,73691657 | 19,10007 | 5,204428 | 1 | | | | | | | | |
| 42 | 0,336112 | 34,34 | 0,834013 | 29281,34258 | 0,98890429 | 17,52535278 | 317,6212 | 33,71915 | 1,73716828 | 19,41041 | 1,885058 | 1 | | | | | | | | |
| 43 | 0,94741 | 42,10 | 0,343685 | 28883,29631 | 0,80381079 | 15,19290043 | 284,89 | 41,15727 | 1,74503489 | 23,58536 | 8,392458 | 1 | | | | | | | | |
| 44 | 0,240149 | 33,39 | 0,743182 | 29189,42447 | 0,24010351 | 13,0018063 | 321,6257 | 32,79644 | 1,73631152 | 18,88857 | 5,886761 | 1 | | | | | | | | |
| 45 | 0,924426 | 41,34 | 0,433176 | 28951,19485 | 0,9961879 | 18,20458863 | 287,865 | 40,42485 | 1,74424926 | 23,17607 | 4,971844 | 1 | | | | | | | | |
| 46 | 0,706446 | 37,82 | 0,663321 | 29122,24766 | 0,16113499 | 12,63885055 | 301,8557 | 37,05711 | 1,74075333 | 21,28797 | 8,649121 | 1 | | | | | | | | |
| 47 | 0,696026 | 37,70 | 0,136663 | 28682,3235 | 0,61455886 | 14,36161952 | 300,016 | 36,93698 | 1,74119519 | 21,21358 | 8,851959 | 1 | | | | | | | | |
| 48 | 0,954699 | 42,41 | 0,82234 | 29269,23628 | 0,39885737 | 13,59827395 | 285,7592 | 41,45967 | 1,74480374 | 23,7618 | 10,16352 | 1 | | | | | | | | |
| 49 | 0,12185 | 31,89 | 0,684566 | 29139,34621 | 0,68439124 | 14,63464624 | 328,807 | 31,35 | 1,73482552 | 18,07098 | 3,436337 | 1 | | | | | | | | |
| 50 | 0,635129 | 37,08 | 0,006159 | 28274,16168 | 0,50373525 | 13,96345681 | 300,3732 | 36,3266 | 1,741109 | 20,86406 | 6,900604 | 1 | | | | | | | | |
| 51 | 0,007248 | 28,07 | 0,942161 | 29456,22036 | 0,33348804 | 13,36429404 | 352,365 | 27,65636 | 1,73036228 | 15,98299 | 2,618694 | 1 | | | | | | | | |
| 52 | 0,221018 | 33,18 | 0,35918 | 28895,41098 | 0,68274444 | 14,62789343 | 321,0079 | 32,58893 | 1,73644236 | 18,76764 | 4,139747 | 1 | | | | | | | | |
| 53 | 0,601057 | 36,75 | 0,194165 | 28749,83139 | 0,4823428 | 13,8894605 | 304,2426 | 36,02296 | 1,74018764 | 20,70062 | 6,81167 | 1 | | | | | | | | |
| 54 | 0,952064 | 42,29 | 0,462204 | 28972,48391 | 0,2846976 | 13,18074355 | 284,6903 | 41,34095 | 1,74508818 | 23,68989 | 10,50915 | 1 | | | | | | | | |
| 55 | 0,92944 | 41,49 | 0,111197 | 28646,14618 | 0,29088992 | 13,20463618 | 285,8286 | 40,5578 | 1,74478533 | 23,24515 | 10,04052 | 1 | | | | | | | | |
| 56 | 0,085706 | 31,25 | 0,091424 | 28613,70867 | 0,83534999 | 15,37618102 | 329,1254 | 30,72597 | 1,73476108 | 17,71193 | 2,335754 | 1 | | | | | | | | |
| 57 | 0,321515 | 34,20 | 0,203894 | 28759,93988 | 0,74940239 | 14,91852162 | 315,415 | 33,57495 | 1,73764923 | 19,32205 | 4,403529 | 1 | | | | | | | | |
| 58 | 0,62553 | 36,98 | 0,812192 | 29256,94059 | 0,7888752 | 15,11311057 | 305,9367 | 36,26156 | 1,73979129 | 20,84247 | 5,729364 | 1 | | | | | | | | |
| 59 | 0,399856 | 34,93 | 0,673967 | 29130,75917 | 0,44482341 | 13,7586691 | 314,1384 | 34,27959 | 1,73793049 | 19,72438 | 5,965707 | 1 | | | | | | | | |
| 60 | 0,299137 | 33,99 | 0,75768 | 29202,66923 | 0,55385305 | 14,14012167 | 318,8404 | 33,37656 | 1,73690525 | 19,21611 | 5,075989 | 1 | | | | | | | | |
| 61 | 0,998971 | 48,71 | 0,040646 | 28494,46167 | 0,69811255 | 14,69164022 | 263,0729 | 47,42766 | 1,75131079 | 27,08123 | 12,38959 | 1 | | | | | | | | |
| 62 | 0,531239 | 36,10 | 0,128066 | 28670,6819 | 0,86439349 | 15,56871527 | 306,5282 | 35,40064 | 1,73965389 | 20,34924 | 4,780525 | 1 | | | | | | | | |
| 63 | 0,714645 | 37,91 | 0,26476 | 28817,66611 | 0,86160189 | 15,54895992 | 299,9142 | 37,13596 | 1,74121981 | 21,32756 | 5,778595 | 1 | | | | | | | | |
| 64 | 0,155927 | 32,38 | 0,341501 | 28881,57293 | 0,18153871 | 12,74047836 | 324,8375 | 31,82328 | 1,7356391 | 18,33519 | 5,594716 | 1 | | | | | | | | |
| 65 | 0,418578 | 35,09 | 0,695557 | 29148,38286 | 0,37583828 | 13,5169635 | 313,4791 | 34,44203 | 1,73807662 | 19,81618 | 6,292123 | 1 | | | | | | | | |
| 66 | 0,200439 | 32,94 | 0,821465 | 29267,07901 | 0,4658588 | 13,83169392 | 324,2166 | 32,36949 | 1,73576808 | 18,64851 | 4,816819 | 1 | | | | | | | | |
| 67 | 0,020449 | 29,21 | 0,912109 | 29392,61799 | 0,3836875 | 13,54479371 | 345,0287 | 28,76421 | 1,73168893 | 16,61049 | 3,0657 | 1 | | | | | | | | |
| 68 | 0,442215 | 35,31 | 0,108035 | 28641,25704 | 0,61383384 | 14,3589052 | 309,8089 | 34,63376 | 1,73890098 | 19,91704 | 5,558133 | 1 | | | | | | | | |
| 69 | 0,959724 | 42,64 | 0,600085 | 29073,53446 | 0,07414369 | 12,0706793 | 284,0183 | | | | | | | | | | | | | |

| | | | | | | | | | | | | |
|-------|----------|-------|----------|-------------|------------|-------------|----------|------------|------------|----------|----------|---|
| 99925 | 0,502493 | 35,84 | 0,713202 | 29163,2017 | 0,7309551 | 14,834077 | 310,2642 | 35,16349 | 1,7387977 | 20,22288 | 5,388801 | 1 |
| 99926 | 0,620853 | 36,94 | 0,078343 | 28589,27058 | 0,93932101 | 16,28157988 | 302,6115 | 36,2011 | 1,74057328 | 20,79838 | 4,5168 | 1 |
| 99927 | 0,68293 | 37,56 | 0,683945 | 29138,84051 | 0,09192322 | 12,21835975 | 302,9542 | 36,81526 | 1,74049193 | 21,15222 | 8,933858 | 1 |
| 99928 | 0,388855 | 34,83 | 0,366682 | 28901,21012 | 0,18814508 | 12,7719897 | 313,3447 | 34,17872 | 1,73810649 | 19,66434 | 6,892352 | 1 |
| 99929 | 0,97555 | 43,60 | 0,59716 | 29071,34101 | 0,91563304 | 16,00331414 | 280,8807 | 42,58804 | 1,74611869 | 24,39012 | 8,386806 | 1 |
| 99930 | 0,301173 | 34,01 | 0,004539 | 28243,35763 | 0,88014249 | 15,68629362 | 313,4682 | 33,37493 | 1,73807905 | 19,20219 | 3,515899 | 1 |
| 99931 | 0,522781 | 36,03 | 0,341604 | 28881,65386 | 0,94957745 | 16,43114744 | 307,9802 | 35,33226 | 1,73931876 | 20,31385 | 3,882704 | 1 |
| 99932 | 0,139185 | 32,15 | 0,721976 | 29170,72906 | 0,2230514 | 12,92943303 | 327,6446 | 31,60298 | 1,73506179 | 18,21433 | 5,284895 | 1 |
| 99933 | 0,484473 | 35,68 | 0,637652 | 29102,13527 | 0,74696246 | 14,90714346 | 310,6383 | 35,00701 | 1,73871305 | 20,13387 | 5,226722 | 1 |
| 99934 | 0,612606 | 36,86 | 0,572834 | 29053,24245 | 0,7478931 | 14,91147548 | 305,386 | 36,13647 | 1,73991967 | 20,76905 | 5,857572 | 1 |
| 99935 | 0,268235 | 33,68 | 0,572347 | 29052,88224 | 0,44940351 | 13,77457479 | 319,4727 | 33,07644 | 1,73676958 | 19,04481 | 5,270233 | 1 |
| 99936 | 0,897581 | 40,65 | 0,654004 | 29114,8846 | 0,7442125 | 14,89439883 | 291,1009 | 39,77444 | 1,74341215 | 22,81413 | 7,919736 | 1 |
| 99937 | 0,310411 | 34,10 | 0,88041 | 29341,34073 | 0,56757262 | 14,18930372 | 319,0837 | 33,48487 | 1,73685299 | 19,27905 | 5,089741 | 1 |
| 99938 | 0,473126 | 35,58 | 0,401167 | 28927,40502 | 0,73095254 | 14,83406549 | 310,1447 | 34,90554 | 1,73882478 | 20,07422 | 5,24015 | 1 |
| 99939 | 0,769305 | 38,55 | 0,101114 | 28630,18276 | 0,3090498 | 13,27362696 | 296,4197 | 37,75082 | 1,74207417 | 21,67004 | 8,396415 | 1 |
| 99940 | 0,831359 | 39,42 | 0,794879 | 29238,80535 | 0,07754628 | 12,10581669 | 296,2406 | 38,59895 | 1,74211845 | 22,15633 | 10,05051 | 1 |
| 99941 | 0,139031 | 32,15 | 0,323465 | 28867,17112 | 0,45704761 | 13,80111087 | 325,9466 | 31,59508 | 1,73540984 | 18,20612 | 4,40501 | 1 |
| 99942 | 0,557854 | 36,35 | 0,666104 | 29124,46256 | 0,15550833 | 12,60952546 | 307,9116 | 35,64487 | 1,73933454 | 20,4934 | 7,883872 | 1 |
| 99943 | 0,94384 | 41,97 | 0,831384 | 29278,29815 | 0,84481979 | 15,43602507 | 287,2951 | 41,04026 | 1,74439855 | 23,52689 | 8,09086 | 1 |
| 99944 | 0,775173 | 38,63 | 0,121568 | 28661,51718 | 0,84803969 | 15,45697398 | 296,2945 | 37,82339 | 1,74210512 | 21,71131 | 6,254337 | 1 |
| 99945 | 0,145767 | 32,24 | 0,466806 | 28975,84287 | 0,09234812 | 12,2214942 | 326,0726 | 31,68995 | 1,73538389 | 18,26106 | 6,039566 | 1 |
| 99946 | 0,598809 | 36,73 | 0,305759 | 28852,70685 | 0,63466116 | 14,43775344 | 304,8749 | 36,00506 | 1,74003921 | 20,69209 | 6,254341 | 1 |
| 99947 | 0,513616 | 35,94 | 0,609247 | 29080,43348 | 0,30876509 | 13,27255682 | 309,3929 | 35,2576 | 1,73899559 | 20,27469 | 7,002137 | 1 |
| 99948 | 0,026102 | 29,51 | 0,367435 | 28901,78997 | 0,66198485 | 14,54423115 | 340,3808 | 29,04914 | 1,73255809 | 16,76662 | 2,222385 | 1 |
| 99949 | 0,854849 | 39,81 | 0,423269 | 28943,87426 | 0,43543406 | 13,72603711 | 293,307 | 38,96111 | 1,74285156 | 22,35481 | 8,628772 | 1 |
| 99950 | 0,689057 | 37,63 | 0,13867 | 28684,9684 | 0,78298043 | 15,08264959 | 300,3267 | 36,86558 | 1,74112021 | 21,17348 | 6,090835 | 1 |
| 99951 | 0,591896 | 36,66 | 0,699181 | 29151,39377 | 0,63750769 | 14,44867512 | 306,7217 | 35,94969 | 1,73960905 | 20,66538 | 6,216708 | 1 |
| 99952 | 0,710461 | 37,86 | 0,122812 | 28663,2977 | 0,06543885 | 11,99896466 | 299,293 | 37,08732 | 1,74137028 | 21,29778 | 9,298817 | 1 |
| 99953 | 0,503133 | 35,85 | 0,752877 | 29198,23606 | 0,08327422 | 12,15226683 | 310,4256 | 35,16983 | 1,73876115 | 20,22695 | 8,074683 | 1 |
| 99954 | 0,575887 | 36,51 | 0,009298 | 28317,47282 | 0,64821644 | 14,49010595 | 302,9222 | 35,78491 | 1,7404995 | 20,56014 | 6,070031 | 1 |
| 99955 | 0,533042 | 36,12 | 0,177452 | 28731,71561 | 0,19715872 | 12,8140233 | 306,785 | 35,41782 | 1,73959441 | 20,35981 | 7,545799 | 1 |
| 99956 | 0,404895 | 30,11 | 0,555129 | 29040,20324 | 0,8474038 | 15,45281147 | 337,7905 | 29,63032 | 1,73305251 | 17,09718 | 1,644371 | 1 |
| 99957 | 0,520332 | 36,00 | 0,472789 | 28980,2042 | 0,36252189 | 13,46945566 | 308,5998 | 35,31338 | 1,73917667 | 20,30466 | 6,835199 | 1 |
| 99958 | 0,413837 | 35,05 | 0,257537 | 28811,22214 | 0,69976548 | 14,69859781 | 311,8498 | 34,39348 | 1,73844028 | 19,7841 | 5,085503 | 1 |
| 99959 | 0,46975 | 35,55 | 0,462283 | 28972,54134 | 0,67955256 | 14,61485576 | 310,5179 | 34,87764 | 1,73874027 | 20,05914 | 5,444286 | 1 |
| 99960 | 0,611501 | 36,85 | 0,011486 | 28340,56803 | 0,32018044 | 13,31520291 | 301,6606 | 36,10814 | 1,74079993 | 20,74227 | 7,427065 | 1 |
| 99961 | 0,439499 | 35,28 | 0,905725 | 29381,31511 | 0,79785463 | 15,1606099 | 313,8937 | 34,62734 | 1,73798466 | 19,92385 | 4,763238 | 1 |
| 99962 | 0,106305 | 31,63 | 0,663173 | 29122,13048 | 0,6555659 | 14,51887177 | 330,0345 | 31,10282 | 1,73457775 | 17,93106 | 3,412189 | 1 |
| 99963 | 0,784694 | 38,75 | 0,071863 | 28576,00481 | 0,42321372 | 13,68349007 | 295,3781 | 37,99989 | 1,74233255 | 21,77534 | 8,091851 | 1 |
| 99964 | 0,334051 | 34,32 | 0,109803 | 28644,00237 | 0,82396451 | 15,30739893 | 314,2341 | 33,68666 | 1,73790933 | 19,38344 | 4,076042 | 1 |
| 99965 | 0,531772 | 36,11 | 0,842231 | 29291,06387 | 0,9841153 | 17,2826965 | 309,8061 | 35,42014 | 1,73890161 | 20,36926 | 3,086566 | 1 |
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| 99970 | 0,554781 | 36,32 | 0,343417 | 28883,08488 | 0,50265638 | 13,95969044 | 306,752 | 35,61192 | 1,73960205 | 20,4713 | 6,511611 | 1 |
| 99971 | 0,713375 | 37,89 | 0,187404 | 28742,62454 | 0,69849717 | 14,69325733 | 299,5792 | 37,12041 | 1,74130087 | 21,31763 | 6,24372 | 1 |
| 99972 | 0,457621 | 35,44 | 0,581391 | 29059,58162 | 0,4740242 | 13,86004365 | 311,4579 | 34,77563 | 1,73852829 | 20,00291 | 6,142867 | 1 |
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| 99974 | 0,762172 | 38,46 | 0,992813 | 29709,80609 | 0,26911087 | 13,11966614 | 302,3075 | 37,6942 | 1,74064559 | 21,6553 | 8,535634 | 1 |
| 99975 | 0,783595 | 38,74 | 0,086575 | 28604,97531 | 0,63269686 | 14,43023818 | 295,5831 | 37,92681 | 1,74228155 | 21,76847 | 7,338236 | 1 |
| 99976 | 0,295927 | 33,96 | 0,290787 | 28840,18463 | 0,81370685 | 15,24805474 | 317,0018 | 33,33862 | 1,73730265 | 19,18968 | 3,94123 | 1 |
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| 99986 | 0,342695 | 34,40 | 0,572048 | 29052,6613 | 0,90075432 | 15,85961823 | 316,0949 | 33,77365 | 1,73750032 | 19,43807 | 3,578448 | 1 |
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| 99997 | 0,430502 | 35,20 | 0,801314 | 29245,43366 | 0,19009954 | 12,78119519 | 313,5242 | 34,54695</ | | | | |

| | | | | | | | | | | | | |
|-------|----------|-------|----------|-------------|------------|-------------|----------|----------|------------|----------|----------|---|
| 99925 | 0,438452 | 35,27 | 0,61 | 29081,00229 | 0,52913067 | 13,42103563 | 312,3268 | 34,61159 | 1,73833344 | 19,91079 | 6,489756 | 1 |
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| 99927 | 0,304355 | 34,04 | 0,362156 | 28897,71621 | 0,93034092 | 15,44057661 | 316,9346 | 33,41905 | 1,73731728 | 19,23601 | 3,795434 | 1 |
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| 99929 | 0,647756 | 37,20 | 0,503651 | 29002,65403 | 0,98649027 | 16,61169243 | 303,7057 | 36,46573 | 1,74031413 | 20,95353 | 4,341841 | 1 |
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| 99935 | 0,107283 | 31,65 | 0,666825 | 29125,03709 | 0,04354928 | 11,23313475 | 329,9635 | 31,11909 | 1,73459204 | 17,94029 | 6,707157 | 1 |
| 99936 | 0,761657 | 38,46 | 0,107707 | 28640,74396 | 0,24246704 | 12,42695336 | 296,843 | 37,65939 | 1,74196964 | 21,61885 | 9,1919 | 1 |
| 99937 | 0,080019 | 31,14 | 0,394119 | 28922,10609 | 0,60489351 | 13,68185155 | 331,5098 | 30,61951 | 1,73428232 | 17,65543 | 3,973582 | 1 |
| 99938 | 0,084324 | 31,23 | 0,457713 | 28969,20274 | 0,70382963 | 14,05452716 | 331,3104 | 30,70568 | 1,73432211 | 17,70472 | 3,65019 | 1 |
| 99939 | 0,512446 | 35,93 | 0,685568 | 29140,1645 | 0,52088624 | 13,39334269 | 309,7558 | 35,24889 | 1,73891304 | 20,27065 | 6,877305 | 1 |
| 99940 | 0,806895 | 39,06 | 0,692353 | 29145,73438 | 0,09613437 | 11,6985807 | 297,1445 | 38,24731 | 1,74189538 | 21,9573 | 10,25871 | 1 |
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| 99946 | 0,928633 | 41,46 | 0,684792 | 29139,53088 | 0,23552149 | 12,39922425 | 288,3652 | 40,54997 | 1,7441187 | 23,24955 | 10,85032 | 1 |
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| 99948 | 0,53908 | 36,17 | 0,990859 | 29684,3577 | 0,37471315 | 12,90574837 | 311,5932 | 35,49305 | 1,73849788 | 20,41593 | 7,510182 | 1 |
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| 99956 | 0,934437 | 41,64 | 0,473329 | 28980,59781 | 0,15176474 | 12,02393725 | 286,9474 | 40,71925 | 1,74448993 | 23,34164 | 11,3177 | 1 |
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| 99958 | 0,784653 | 38,75 | 0,328901 | 28871,54429 | 0,40888908 | 13,02082404 | 296,9037 | 37,94767 | 1,74195468 | 21,78454 | 8,763712 | 1 |
| 99959 | 0,934949 | 41,66 | 0,952985 | 29485,60802 | 0,85356938 | 14,7974963 | 289,3787 | 40,75105 | 1,74385546 | 23,36837 | 8,57087 | 1 |
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| 99961 | 0,268951 | 33,69 | 0,001351 | 28130,10223 | 0,3480707 | 12,81449126 | 314,3242 | 33,06369 | 1,73788943 | 19,0252 | 6,210709 | 1 |
| 99962 | 0,580639 | 36,56 | 0,08382 | 28599,8508 | 0,77441948 | 14,36354956 | 304,2445 | 35,83461 | 1,74018721 | 20,59239 | 6,228837 | 1 |
| 99963 | 0,43734 | 35,26 | 0,498372 | 28998,81648 | 0,96269728 | 15,91684402 | 311,929 | 34,60017 | 1,73842251 | 19,9032 | 3,986358 | 1 |
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| 99966 | 0,075316 | 31,04 | 0,048972 | 28520,07718 | 0,57600382 | 13,58075067 | 329,7294 | 30,51525 | 1,73463917 | 17,5917 | 4,010947 | 1 |
| 99967 | 0,902946 | 40,78 | 0,127741 | 28670,23139 | 0,956711 | 15,80742943 | 288,4284 | 39,8798 | 1,74410222 | 22,86552 | 7,058088 | 1 |
| 99968 | 0,961001 | 42,66 | 0,239586 | 28794,78624 | 0,70488094 | 14,05879525 | 282,5918 | 41,68554 | 1,74565256 | 23,85963 | 9,820837 | 1 |
| 99969 | 0,168537 | 32,55 | 0,72549 | 29173,77611 | 0,09160291 | 11,66705487 | 325,6411 | 31,98956 | 1,73547285 | 18,43276 | 6,76571 | 1 |
| 99970 | 0,903571 | 40,79 | 0,5869 | 29063,6776 | 0,85243939 | 14,79024693 | 290,3479 | 39,90614 | 1,74360537 | 22,88714 | 8,096892 | 1 |
| 99971 | 0,916908 | 41,13 | 0,45098 | 28964,27629 | 0,73758485 | 14,19609042 | 288,6622 | 40,22505 | 1,74404138 | 23,06428 | 8,868186 | 1 |
| 99972 | 0,494138 | 35,77 | 0,292541 | 28841,667 | 0,28035969 | 12,57235459 | 308,8715 | 35,08397 | 1,73911454 | 20,17347 | 7,601115 | 1 |
| 99973 | 0,227701 | 33,25 | 0,962166 | 29515,15445 | 0,3065021 | 12,66800825 | 324,0711 | 32,67266 | 1,73579837 | 18,82284 | 6,154834 | 1 |
| 99974 | 0,531602 | 36,11 | 0,110769 | 28645,48947 | 0,93356334 | 15,47840776 | 306,3796 | 35,40317 | 1,73968836 | 20,3503 | 4,871888 | 1 |
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| 99980 | 0,289582 | 33,89 | 0,838531 | 29286,64752 | 0,89881323 | 15,13027704 | 319,7403 | 33,28781 | 1,73671233 | 19,16714 | 4,036865 | 1 |
| 99981 | 0,241483 | 33,40 | 0,166607 | 28719,37848 | 0,79855332 | 14,48294141 | 318,9575 | 32,80054 | 1,73688009 | 18,88475 | 4,401805 | 1 |
| 99982 | 0,733444 | 38,12 | 0,311016 | 28857,03806 | 0,34724039 | 12,81161909 | 299,2781 | 37,34165 | 1,7413739 | 21,44378 | 8,632165 | 1 |
| 99983 | 0,965314 | 42,94 | 0,431876 | 28950,23626 | 0,65771261 | 13,87453054 | 282,4488 | 41,95206 | 1,74569133 | 24,03177 | 10,15724 | 1 |
| 99984 | 0,542843 | 36,21 | 0,202303 | 28758,30739 | 0,34836621 | 12,81551301 | 306,5493 | 35,50404 | 1,739649 | 20,40874 | 7,593225 | 1 |
| 99985 | 0,850327 | 39,73 | 0,627688 | 29094,46324 | 0,58266469 | 13,60384685 | 294,3569 | 38,89093 | 1,74258758 | 22,31792 | 8,714076 | 1 |
| 99986 | 0,094088 | 31,41 | 0,457435 | 28968,99973 | 0,57063538 | 13,56221935 | 330,3099 | 30,88858 | 1,73452242 | 17,80812 | 4,245901 | 1 |
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| 99988 | 0,374489 | 34,70 | 0,371999 | 28905,29665 | 0,03974356 | 11,18531863 | 313,9563 | 34,053 | 1,73797079 | 19,59354 | 8,408222 | 1 |
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| 99992 | 0,398197 | 34,91 | 0,393479 | 28921,62409 | 0,43958498 | 13,12302923 | 313,0758 | 34,26051 | 1,73816629 | 19,71072 | 6,587691 | 1 |
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| 99995 | 0,490498 | 35,74 | 0,73023 | 29177,91715 | 0,82514801 | 14,62623486 | 310,8082 | 35,06055 | 1,73867467 | 20,1651 | 5,538868 | 1 |
| 99996 | 0,657797 | 37,30 | 0,554508 | 29039,74697 | 0,09418688 | 11,68515878 | 303,4881 | 36,5637 | 1,74036554 | 21,00921 | 9,32405 | 1 |
| 99997 | 0,945823 | 42,04 | 0,834479 | 29281,88474 | 0,42585577 | 13,0774055 | 287,0579 | 41,11161 | | | | |

BAB V

KESIMPULAN DAN SARAN

5.1 Kesimpulan

Berdasarkan analisis dan pembahasan yang dilakukan diperoleh beberapa kesimpulan sebagai berikut:

1. Nilai RAO maksimum gerakan *heave*, *roll* dan *pitch* berturut – turut adalah sebesar 0,99 m/s, 4,92 deg/m dan 0,989 deg/s.
2. Tegangan aksial maksimum adalah terdapat pada *member* 0003 – 0100 sebesar 14,02 ksi dan *member* 0005 – 0083 sebesar 13,39 ksi.
3. Keandalan yang diperoleh dengan memperhatikan 2 *member seafastening* dengan tegangan aksial terbesar adalah masing-masing 99,63% dan 99,85%. Dapat disimpulkan bahwa struktur *seafastening jacket platform* Banuwati andal dalam proses transportasi ke *South East Sumatera Block*.

5.2 Saran

Beberapa hal yang dapat dijadikan saran yang sifatnya membangun penelitian selanjutnya adalah sebagai berikut:

1. Menghitung kekuatan *deck strenght barge* yang digunakan.
2. Menggunakan persamaan moda kegagalan lainnya.
3. Menggunakan metode simulasi keandalan lainnya.
4. Menggunakan *codes*, referensi serta jenis distribusi yang lain dalam proses perhitungan keandalan struktur *seafastening*.

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BIODATA PENULIS



Andre Themas Miko lahir di Bukittinggi Sumatera Barat pada tanggal 20 September 1993, merupakan anak kedua dari tiga bersaudara. Pendidikan formal penulis dimulai dengan jenjang Pendidikan Dasar di SDN 002 Batu Besar Batam, lalu penulis pindah ke daerah Payakumbuh Sumatera Barat di SDN 06 Palokoto dan akhirnya menyelesaikan pendidikan dasar di SDN 02 Percontohan Bukittinggi pada tahun 2006. Kemudian melanjutkan pendidikan sekolah di SMP Negeri 1 Bukittinggi pada tahun 2006-2009 dan SMA N 1 Bukittinggi pada tahun 2009-2012. Setelah lulus SMA pada tahun 2012, penulis mengikuti program Seleksi Mandiri Institut Teknologi Sepuluh Nopember (ITS) dan diterima untuk melanjutkan ke jenjang Pendidikan Tinggi Strata 1 di Jurusan Teknik Kelautan, Fakultas Teknologi Kelautan. Selama menempuh masa perkuliahan, penulis aktif dalam kegiatan *Extra-Campuss* diantaranya Himpunan Mahasiswa Teknik Kelautan dalam Departemen PSDM dan tim SC Kaderisasi 2013, menjadi Ketua Pelaksana ITS EXPO 2015 dengan persiapan 1 tahun dengan menaungi 550 anggota panitia dan berhasil membawa event terbesar ITS ini sebagai salah satu program PEMPROV Jawa Timur. Pada tahun 2015 penulis berkesempatan melaksanakan kerja praktek di PT. Java Energy Semesta di Jakarta. Awal tahun 2016 penulis melaksanakan kembali kerja praktek di PT. SIEMENS OIL and GAS Batam sebagai *Structural Engineer* selama 1 bulan.

Pada semester 8, dengan bimbingan Prof. Ir. Daniel M. Rosyid, Ph.D., MRINA dan Yoyok Setyo Hadiwidodo, S.T., M.T., Ph.D, mengambil Tugas Akhir dengan judul “Keandalan Struktur *Seafastening* pada Transportasi *Jacket Platform* Banuwati ke *East Sumatera Block*.”

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