

TUGAS AKHIR (MO184804)

**PERBANDINGAN UMUR KELELAHAN STRUKTUR *JACKET*
3 KAKI MODIFIKASI DAN KONVENSIONAL**

MUHAMMAD NABIL GIFFARY

04311640000073

Dosen Pembimbing

Ir. Murdjito, M.Sc.Eng.

Dr.Eng. Rudi Walujo Prastianto, S.T., M.T.

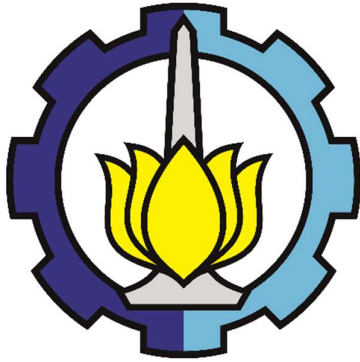
DEPARTEMEN TEKNIK KELAUTAN

FAKULTAS TEKNOLOGI KELAUTAN

INSTITUT TEKNOLOGI SEPULUH NOPEMBER

SURABAYA

2020



TUGAS AKHIR (MO184804)

**PERBANDINGAN UMUR KELELAHAN STRUKTUR *JACKET*
3 KAKI MODIFIKASI DAN KONVENSIONAL**

MUHAMMAD NABIL GIFFARY

04311640000073

Dosen Pembimbing

Ir. Murdjito, M.Sc.Eng.

Dr.Eng. Rudi Walujo Prastianto, S.T., M.T.

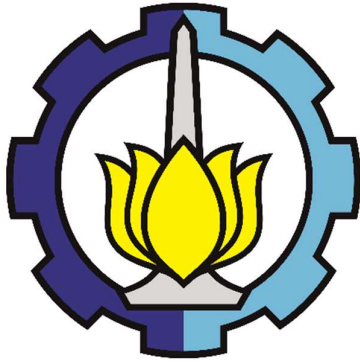
DEPARTEMEN TEKNIK KELAUTAN

FAKULTAS TEKNOLOGI KELAUTAN

INSTITUT TEKNOLOGI SEPULUH NOPEMBER

SURABAYA

2020



FINAL PROJECT (MO184804)

**FATIGUE LIFE COMPARISON OF MODIFIED AND
CONVENTIONAL 3 LEGGED JACKET STRUCTURE**

MUHAMMAD NABIL GIFFARY

04311640000073

SUPERVISORS

Ir. Murdjito, M.Sc.Eng.

Dr.Eng. Rudi Walujo Prastianto, S.T., M.T.

DEPARTMENT OF OCEAN ENGINEERING

FACULTY OF MARINE TECHNOLOGY

INSTITUT TEKNOLOGI SEPULUH NOPEMBER

SURABAYA

2020

LEMBAR PENGESAHAN
PERBANDINGAN UMUR KELELAHAN STRUKTUR *JACKET* 3 KAKI
MODIFIKASI DAN KONVENSIONAL
TUGAS AKHIR

Diajukan untuk memenuhi salah satu syarat memperoleh gelar Sarjana Teknik
pada Program Studi S-1 Departemen Teknik Kelautan

Fakultas Teknologi Kelautan
Institut Teknologi Sepuluh Nopember

Oleh:

Muhammad Nabil Giffary

NRP. 04311640000073

Disetujui oleh:

1. Ir. Murdjito, M.Sc.Eng. (Pembimbing 1)

.....
2. Dr.Eng. Rudi Walujo Prastianto, S.T., M.T. (Pembimbing 2)

.....
3. Prof. Ir. Eko Budi Djatmiko, M.Sc., Ph.D (Penguji 1)

.....
4. Ir. Wisnu Wardhana, S.E., M.Sc., Ph.D. (Penguji 2)

.....
Surabaya, Agustus 2020

PERBANDINGAN UMUR KELELAHAN STRUKTUR *JACKET* 3 KAKI MODIFIKASI DAN KONVENSIONAL

Nama : Muhammad Nabil Giffary

NRP : 04311640000073

Departemen : Teknik Kelautan FTK-ITS

Dosen Pembimbing : Ir. Murdjito, M.Sc.Eng

Dr.Eng. Rudi Walujo Prastianto, S.T., M.T

ABSTRAK

Dalam perkembangannya, struktur lepas pantai mengalami banyak perubahan demi menunjang faktor-faktor tertentu yang umumnya untuk mendapatkan hasil yang sebaik mungkin tak terkecuali untuk struktur *jacket*. Untuk menunjang faktor ekonomi, struktur *jacket* harus disesuaikan dengan kondisi lapangan produksinya. Sebagai contoh, untuk lapangan marginal yang memiliki umur produksi pendek maka desain struktur *jacket* akan dibuat seminimal mungkin untuk mencapai biaya yang serendah mungkin. Dari ide tersebut, maka muncul konsep tentang platform modular untuk fasilitas minimal yang rendah biaya. Namun dengan minimalnya, perbedaan desain akan berpengaruh pada performa dari *jacket* itu sendiri, dengan kata lain sebuah *jacket* modular dapat menumpu beban yang sama dengan model *jacket* konvensional namun memiliki performa struktur yang berbeda. Dengan demikian, penelitian ini membahas tentang perbandingan performa yang meliputi umur kelelahan dan periode natural dari struktur *jacket* konvensional dan modular yang dalam penelitian ini disebut sebagai *jacket* modifikasi. *Jacket* konvensional sebagai struktur pembanding mengambil basis desain dari struktur modifikasi meliputi properties material, jumlah elevasi, bangunan atas, dan beban lingkungan yang sama. Pada penelitian ini kedua *jacket* hanya akan dimodelkan bagian *jacket* dan bangunan atas akan dimodelkan sebagai beban *joint* pada ketiga ujung atas kaki *jacket*. Analisa umur kelelahan pada penelitian ini menggunakan metode *full spectral analysis*. Dengan menggunakan *software* SACS, maka didapatkan periode natural *jacket* modifikasi adalah 1,756 s dan *jacket* konvensional sebesar 1,472 s. Sementara umur kelelahan terendah pada *jacket* modifikasi adalah 44,98 tahun dan *jacket* konvensional sebesar 9125,79 tahun.

Kata kunci : *Jacket* konvensional, *jacket* modifikasi, periode natural, umur kelelahan

FATIGUE LIFE COMPARISON OF MODIFIED AND CONVENTIONAL 3 LEGGED JACKET STRUCTURE

Name : Muhammad Nabil Giffary
NRP : 04311640000073
Department : Ocean Engineering FTK-ITS
Supervisors : Ir. Murdjito, M.Sc.Eng
Dr.Eng. Rudi Walujo Prastianto, S.T., M.T

ABSTRACT

In its development, offshore structures undergo many changes in order to support certain factors which are generally to get the best results possible without exception for jacket structures. To support economic factors, the jacket structure must adjust the production field, for example, for marginal fields that have a small production life, the jacket structure design will be made as minimum as possible to achieve the lowest possible cost, from this idea, the idea of a low cost modular platform for minimal facilities emerged. But with its minimum, design differences will affect the performance of the jacket itself, in other words a modular jacket can support the same load as conventional jacket models but have different structural performance. Thus, this study discusses the performance comparison which includes the fatigue life and natural period of conventional jacket structure and modular jacket which in this study is called modified jacket. Conventional jacket as a comparison structure takes the design basis of the modified structure including material properties, the same amount of elevation, upper building, and environmental loads. In this study the two jackets will only be modeled as the leg section and the upper structure will be modeled as joint loads at the three upper ends of the jacket legs. Fatigue life analysis in this study uses the full spectral analysis method. Using SACS software, the natural period of modified jacket results 1,756 s and the conventional jacket with 1,472 s, while the lowest fatigue life on the modified jacket was 44,98 years and the conventional jacket with 9125,79 years.

Keywords : Conventional jacket, modified jacket, natural period, fatigue life

KATA PENGANTAR

Segala puji bagi Allah Tuhan Semesta Alam, dengan rahmat dan ilmu-Nya lah penulis dapat menyelesaikan tugas akhir dengan sebaik yang dapat dilakukan.

Tugas akhir ini berjudul “Perbandingan Umur Kelelahan Struktur *Jacket* 3 Kaki Modifikasi dan Konvensional”. Penelitian dan penulisan tugas akhir ini dilakukan untuk menyelesaikan program studi S1 di Departemen Teknik Kelautan, Fakultas Teknologi Kelautan, Institut Teknologi Sepuluh Nopember Surabaya.

Pada tugas akhir ini dibahas tentang perbandingan umur kelelahan struktur *jacket* 3 kaki modifikasi dan konvensional. Perbandingan umur kelelahan ini menggunakan *jacket* modifikasi sebagai dasar desain struktur pembanding yang dalam tugas akhir ini disebut *jacket* konvensional dengan konfigurasi yang berbeda. Dalam tugas akhir ini kedua *jacket* hanya dimodelkan bagian *jacket* dan bagian *topside* dimodelkan sebagai beban *joint* pada ketiga ujung atas *jacket leg*. Dengan menggunakan beban lingkungan, beban *topside*, dan *properties* material yang sama serta konfigurasi struktur yang berbeda, penelitian dilakukan untuk mengetahui perbedaan umur kelelahan pada *joint-joint* di lokasi yang sama pada kedua model *jacket*.

Dalam pengerjaan dan penulisan tugas akhir ini, penulis menyadari banyaknya kekurangan. Oleh karena itu, penulis sangat terbuka dengan segala bentuk kritik maupun saran untuk meningkatkan pengetahuan dan pemahaman yang lebih baik lagi bagi penulis dan peneliti selanjutnya. Diharapkan dengan dilakukan penelitian ini penulis dapat sedikit memberikan sumbangan ilmu terhadap dunia teknologi kelautan dan dapat bermanfaat di kemudian hari.

Surabaya, Juli 2020

Penulis

UCAPAN TERIMAKASIH

Pada laporan tugas akhir ini, penulis ingin mengucapkan terimakasih kepada pihak-pihak yang telah memberi dukungan baik dalam bentuk moral dan material selama pelaksanaan penelitian hingga pengerjaan laporan di antaranya adalah :

1. Kedua orangtua, saudara, dan keluarga besar penulis yang selalu memberikan doa dan semangat, khususnya untuk Bu Umik selaku nenek penulis yang ingin melihat kelulusan penulis namun wafat mendahului kelulusan penulis.
2. Ir. Murdjito, M.Sc.Eng dan Dr.Eng. Rudi Walujo Prastianto, S.T., M.T selaku dosen pembimbing yang selalu sabar dalam memberikan bimbingan dan ilmu dalam pengerjaan tugas akhir dari awal hingga akhir pengerjaan.
3. Yoyok Setyo Hadiwidodo, S.T., M.T., Ph.D selaku dosen wali yang selalu membimbing penulis dalam hal perkuliahan.
4. Prof. Ir. Eko Budi Djatmiko, M.Sc., Ph.D, Ir. Wisnu Wardhana, S.E., M.Sc., Ph.D, dan Wimala Lalitya Dhanista, S.T., M.T selaku dosen penguji penulis selama periode sidang tugas akhir.
5. Ketua Departemen, Sekertaris Departemen, Seluruh Dosen, dan Staff Departemen Teknik Kelautan yang tidak bisa penulis sebutkan satu-persatu yang selalu membantu dalam urusan administrasi perkuliahan.
6. Teman-teman seperjuangan Bimbingan Tugas Akhir Pak Murdjito yang selalu solid dalam memberikan bantuan dan menjadi teman diskusi dalam pengerjaan tugas akhir penulis.
7. Teman-teman Teknik Kelautan 2016 ADHIWAMASTYA yang telah memberi banyak bantuan dan menjadi teman selama perkuliahan penulis.
8. Teman-teman Goes To, Apa Ya, Goldies, Smada Big Band, Divisi Rungkut, dan sobat rungkut yang selalu memberikan semangat dalam perkuliahan dan pengerjaan tugas akhir.
9. Seluruh pihak yang telah membantu dalam proses pengerjaan tugas akhir yang tidak dapat penulis sebutkan satu persatu.

Semoga seluruh bantuan yang telah diberikan mendapat balasan kebaikan dari Allah SWT dan menjadi tabungan kebaikan bagi masa depan pihak-pihak yang telah membantu penulis.

DAFTAR ISI

| | |
|--|-------------|
| LEMBAR PENGESAHAN | i |
| ABSTRAK | iii |
| ABSTRACT | v |
| KATA PENGANTAR..... | vii |
| UCAPAN TERIMAKASIH..... | ix |
| DAFTAR ISI..... | xi |
| DAFTAR GAMBAR..... | xiii |
| DAFTAR TABEL | xiv |
| BAB I..... | 1 |
| PENDAHULUAN..... | 1 |
| 1.1 Latar Belakang Masalah | 1 |
| 1.2 Rumusan Masalah | 1 |
| 1.3 Tujuan..... | 2 |
| 1.4 Manfaat..... | 2 |
| 1.5 Batasan Masalah..... | 2 |
| 1.6 Sistematika Penulisan..... | 2 |
| BAB II | 5 |
| TINJAUAN PUSTAKA DAN DASAR TEORI..... | 5 |
| 2.1 Tinjauan Pustaka | 5 |
| 2.2 Dasar Teori..... | 5 |
| 2.2.1 Struktur Jacket..... | 5 |
| 2.2.2 Pembebanan Pada Struktur Jacket | 6 |
| 2.2.3 Tubular Joint | 10 |
| 2.2.4 Periode dan Frekuensi Natural | 11 |
| 2.2.5 Analisa Kelelahan Metode Cumulative Damage | 12 |
| BAB III..... | 21 |
| METODOLOGI PENELITIAN | 21 |
| 3.1 Diagram Alir Penelitian..... | 21 |
| 3.2 Metodologi Penelitian | 22 |
| 3.2.1 Studi Literatur | 22 |
| 3.2.2 Pengumpulan Data | 22 |

| | | |
|------------------------------------|--|-----------|
| 3.2.3 | Pemodelan Struktur <i>Jacket</i> 3 Kaki Modifikasi..... | 28 |
| 3.2.4 | Pemodelan Struktur <i>Jacket</i> 3 Kaki Konvensional | 28 |
| 3.2.5 | Analisa <i>Inplace</i> Dengan <i>Software</i> SACS | 29 |
| 3.2.6 | Analisa <i>Fatigue</i> Dengan <i>Software</i> SACS..... | 29 |
| 3.2.7 | Kesimpulan dan Saran | 30 |
| 3.3 | Rencana Kegiatan Tugas Akhir | 31 |
| BAB IV | | 33 |
| ANALISA DAN PEMBAHASAN..... | | 33 |
| 4.1 | Pemodelan <i>Jacket</i> 3 Kaki Modifikasi dan Konvensional | 33 |
| 4.2 | Analisa <i>Inplace</i> Dengan <i>Software</i> SACS..... | 36 |
| 4.2.1 | Pengolahan Data Lingkungan..... | 36 |
| 4.2.2 | Kombinasi Beban | 39 |
| 4.2.3 | Hasil Analisa <i>Inplace</i> | 40 |
| 4.3 | Analisa <i>Fatigue</i> Dengan <i>Software</i> SACS | 41 |
| 4.3.1 | Periode dan Frekuensi Natural | 41 |
| 4.3.2 | Response Amplitude Operator (RAO) | 41 |
| 4.3.3 | <i>Dynamic Amplification Factor</i> (DAF) | 44 |
| 4.3.4 | Umur Kelelahan..... | 44 |
| BAB V..... | | 49 |
| KESIMPULAN DAN SARAN..... | | 49 |
| 5.1 | Kesimpulan | 49 |
| 5.2 | Saran | 49 |
| DAFTAR PUSTAKA | | |
| LAMPIRAN A | | |
| LAMPIRAN B | | |
| LAMPIRAN C | | |
| BIODATA PENULIS | | |

DAFTAR GAMBAR

| | |
|--|----|
| Gambar 2.1 Struktur <i>jacket</i> (sumber : drillingformulas.com)..... | 6 |
| Gambar 2.2 Profil kecepatan arus (sumber : Riyanto, 2015)..... | 8 |
| Gambar 2.3 Grafik <i>doppler shift due to steady current</i> (sumber : API, 2010) | 9 |
| Gambar 2.4 Grafik <i>regions of applicability</i> (sumber : API, 2010) | 10 |
| Gambar 2.5 Klasifikasi <i>tubular joints</i> (Sumber : Saini, 2016) | 10 |
| Gambar 2.6 Gaya dan beban pada tubular joint (Sumber : Saini, 2016) | 11 |
| Gambar 2.7 Skenario analisa spektral (Djatkiko, 2006) | 12 |
| Gambar 2.8 Tegangan yang dialami <i>member-joint</i> (sumber : API, 2000)..... | 13 |
| Gambar 2.9 Analisa beban gelombang untuk memperoleh RAO dan RAO Tegangan (Djatkiko, 2006) | 14 |
| Gambar 2.10 Perhitungan Spektra tegangan..... | 15 |
| Gambar 2.11 Perhitungan distribusi Rayleigh kurun waktu pendek (Djatkiko, 2006). | 16 |
| Gambar 2.12 Perhitungan distribusi Weibull kurun waktu panjang (Djatkiko, 2006) | 16 |
| Gambar 2.13 Parameter <i>tubular joint</i> (API, 2000) | 18 |
| Gambar 2.14 Kurva S-N <i>tubular joint</i> $T = 5/8$ in (sumber : API, 2010)..... | 19 |
| Gambar 3.1 Diagram alir pengerjaan | 21 |
| Gambar 3.2 Diagram alir pengerjaan (lanjutan) | 22 |
| Gambar 3.3 Platform MBH..... | 23 |
| Gambar 4.1 <i>Jacket</i> 3 kaki modifikasi dengan beban <i>topside</i> | 33 |
| Gambar 4.2 Ilustrasi penentuan <i>batter jacket</i> konvensional | 34 |
| Gambar 4.3 Ilustrasi penentuan <i>batter jacket</i> konvensional (lanjutan)..... | 34 |
| Gambar 4.4 <i>Jacket</i> 3 kaki konvensional dengan beban <i>topside</i> | 35 |
| Gambar 4.5 Pembagian elevasi..... | 35 |
| Gambar 4.6 Hasil analisa <i>inplace jacket</i> modifikasi..... | 40 |
| Gambar 4.7 Hasil analisa <i>inplace jacket</i> konvensional..... | 40 |
| Gambar 4.8 RAO <i>overturning moment jacket</i> modifikasi terhadap frekuensi | 42 |
| Gambar 4.9 RAO <i>base shear jacket</i> modifikasi terhadap frekuensi | 42 |
| Gambar 4.10 RAO <i>overturning moment jacket</i> konvensional terhadap frekuensi | 43 |
| Gambar 4.11 RAO <i>base shear jacket</i> konvensional terhadap frekuensi..... | 43 |
| Gambar 4.12 Lokasi <i>joint</i> yang ditinjau pada <i>bracing</i> | 44 |
| Gambar 4.13 Lokasi <i>joint</i> yang ditinjau pada <i>jacket</i> | 45 |
| Gambar 4.14 Lokasi <i>joint</i> dengan umur kelelahan terendah..... | 47 |
| Gambar 4.15 Posisi <i>joint</i> kritis dan <i>joint</i> yang sama pada struktur pembanding.. | 47 |

DAFTAR TABEL

| | |
|---|----|
| Tabel 2.1 <i>shape coefficient</i> (sumber : ISO 19902:2007)..... | 8 |
| Tabel 2.2 Parameter <i>tubular joint</i> | 18 |
| Tabel 2.3 Batas parameter Penentuan SCF Efthymiou (Almar-Næss, 1985) | 18 |
| Tabel 2.4 Teori penentuan SCF Efthymiou..... | 19 |
| Tabel 2.5 Nilai $\log(k_l)$ dan m (sumber : API 2010)..... | 20 |
| Tabel 3.1 Data kejadian gelombang arah N | 23 |
| Tabel 3.2 Data kejadian gelombang arah NNE | 24 |
| Tabel 3.3 Data kejadian gelombang arah NE | 24 |
| Tabel 3.4 Data kejadian gelombang arah ENE..... | 24 |
| Tabel 3.5 Data kejadian gelombang arah E | 24 |
| Tabel 3.6 Data kejadian gelombang arah ESE | 25 |
| Tabel 3.7 Data kejadian gelombang arah SE | 25 |
| Tabel 3.8 Data kejadian gelombang arah SSE | 25 |
| Tabel 3.9 Data kejadian gelombang arah S | 25 |
| Tabel 3.10 Data kejadian gelombang arah SSW | 26 |
| Tabel 3.11 Data kejadian gelombang arah SW | 26 |
| Tabel 3.12 Data kejadian gelombang arah WSW..... | 26 |
| Tabel 3.13 Data kejadian gelombang arah W..... | 26 |
| Tabel 3.14 Data kejadian gelombang arah WNW | 27 |
| Tabel 3.15 Data kejadian gelombang arah NW..... | 27 |
| Tabel 3.16 Data kejadian gelombang arah NNW | 27 |
| Tabel 3.17 Rangkuman Hs dan Tp setiap arah..... | 28 |
| Tabel 3.18 Data Arus..... | 28 |
| Tabel 3.19 Alur pengerjaan analisa <i>inplace</i> | 29 |
| Tabel 3.20 Alur pengerjaan analisa <i>fatigue</i> | 29 |
| Tabel 3.21 Rencana pengerjaan tugas akhir | 31 |
| Tabel 4.1 Perhitungan <i>apparent wave period</i> kondisi operasi | 36 |
| Tabel 4.2 Perhitungan <i>apparent wave period</i> kondisi badai | 37 |
| Tabel 4.3 Penentuan teori gelombang kondisi operasi | 37 |
| Tabel 4.4 Penentuan teori gelombang kondisi badai..... | 38 |
| Tabel 4.5 Kecepatan arus pada setiap kedalaman di setiap arah. | 38 |
| Tabel 4.6 Kombinasi beban operasi | 39 |
| Tabel 4.7 Kombinasi beban badai | 39 |
| Tabel 4.8 5 <i>mode shape</i> pertama <i>jacket</i> modifikasi | 41 |
| Tabel 4.9 5 <i>mode shape</i> pertama <i>jacket</i> konvensional | 41 |
| Tabel 4.10 Hasil perhitungan DAF..... | 44 |
| Tabel 4.11 Umur kelelahan setiap <i>joint</i> bagian <i>top</i> | 45 |
| Tabel 4.12 Umur kelelahan setiap <i>joint</i> bagian <i>middle</i> | 46 |
| Tabel 4.13 Umur kelelahan setiap <i>joint</i> bagian <i>bottom</i> | 46 |
| Tabel 4.14 Umur kelelahan terendah pada setiap setiap struktur | 46 |
| Tabel 4.15 Hasil SCF pada <i>joint</i> kritis dan <i>joint</i> di posisi yang sama pada struktur pembandingnya..... | 48 |

BAB I

PENDAHULUAN

1.1 Latar Belakang Masalah

Energi minyak dan gas merupakan salah satu sumber energi yang masih banyak digunakan hingga saat ini, khususnya di Indonesia. Tercatat kegiatan eksplorasi minyak dan gas di Indonesia sudah dilakukan sejak tahun 1971 hingga sekarang baik di laut dangkal maupun laut dalam. Klasifikasi kedalaman laut digunakan untuk menentukan jenis struktur lepas pantai yang digunakan di mana laut dalam akan menggunakan struktur terapung sedangkan laut dangkal akan menggunakan struktur terpancang.

Struktur terpancang yang umum digunakan di Indonesia adalah struktur *jacket*. Struktur ini sesuai dengan kondisi perairan di Indonesia yang rata-rata adalah laut dangkal. Struktur *jacket* secara keseluruhan terbagi menjadi dua bagian, yaitu *topside* dan *leg*. Desain dari struktur ini dapat divariasikan sesuai kebutuhan dan kondisi lingkungan tempat struktur di bangun, dalam arti dengan kebutuhan dan kondisi lingkungan yang sama dapat memiliki desain yang berbeda.

Perbedaan desain tentu memiliki kelebihan dan kekurangan masing-masing, suatu contoh jika struktur ramping maka gerakan struktur akan besar yang dapat diketahui dari periode natural struktur yang besar, periode natural struktur yang besar dengan kondisi lingkungan tertentu dapat menyebabkan umur kelelahan struktur mengecil akibat penambahan faktor amplifikasi dinamis yang besar. Sebaliknya jika struktur besar maka struktur akan cenderung stabil yang dapat diketahui dari periode natural yang kecil, periode natural yang kecil dengan kondisi lingkungan tertentu dapat meningkatkan umur kelelahan akibat faktor amplifikasi dinamis yang mendekati angka 1.

Pada penelitian ini akan dibahas mengenai perbandingan umur kelelahan antara struktur *jacket* 3 kaki konvensional dan 3 kaki modifikasi. Penelitian dilakukan untuk mengetahui pengaruh dari konfigurasi struktur *jacket* 3 kaki terhadap umur kelelahan dengan beban bangunan atas dan kondisi lingkungan yang sama. Penelitian dilakukan dengan bantuan *software* SACS meliputi pemodelan hingga simulasi pembebanan untuk didapatkan hasil yang dituju.

1.2 Rumusan Masalah

Adapun rumusan masalah yang akan dibahas pada tugas akhir ini adalah sebagai berikut :

1. Berapa periode natural struktur *jacket* 3 kaki konvensional dan 3 kaki modifikasi ?
2. Berapa umur kelelahan struktur *jacket* 3 kaki konvensional dan 3 kaki modifikasi menggunakan metode *full spectral analysis* ?

1.3 Tujuan

Dari rumusan masalah yang ada, adapun tujuan yang diharapkan menjadi hasil dari penelitian ini :

1. Mengetahui periode natural masing-masing struktur *jacket* 3 kaki dan 3 kaki modifikasi.
2. Mengetahui umur kelelahan masing-masing struktur *jacket* 3 kaki dan 3 kaki modifikasi dengan menggunakan metode *full spectral analysis*.

1.4 Manfaat

Adapun manfaat yang diharapkan bisa dihasilkan dari penelitian tugas akhir ini adalah memberi pengetahuan lebih lanjut kepada pembaca terkait pengaruh konfigurasi struktur *jacket* terhadap periode natural dan umur kelelahan struktur.

1.5 Batasan Masalah

Berikut merupakan batasan masalah yang digunakan pada pengerjaan tugas akhir ini :

1. Analisa kelelahan struktur dilakukan secara global menggunakan metode *spectral analysis*.
2. Objek yang digunakan pada analisa ini adalah struktur *jacket* 3 kaki jenis modular dengan bagian bawah berbentuk konvensional yang selanjutnya disebut dengan struktur *jacket* 3 kaki modifikasi dan *jacket* 3 kaki berbentuk konvensional.
3. Parameter desain pada struktur *jacket* 3 kaki konvensional meliputi jumlah elevasi dan *properties* material yang disamakan dengan *jacket* 3 kaki modifikasi dengan mengambil kemiringan kaki *jacket* konvensional yaitu gairs lurus dari ujung atas kaki *jacket* modifikasi hingga ujung bawah kaki *jacket* modifikasi yang terletak pada elevasi yang sama dengan *mudmat*.
4. Bangunan atas kedua struktur dianggap sama sehingga dimodelkan sebagai beban *joint*.
5. Spektrum gelombang yang digunakan adalah spektrum JONSWAP dengan $\gamma = 2,0$.
6. Teori penentuan *stress concentration factor* yang digunakan adalah Efthymiou dengan batas mengaplikasikan batas atas dengan nilai 10 dan batas bawah dengan nilai 1,5.
7. Analisa kelelahan dan pemodelan pada tugas akhir ini menggunakan *software* SACS.

1.6 Sistematika Penulisan

BAB I Pendahuluan

Bab ini berisi tentang penjelasan secara global apa saja yang akan dibahas dalam tugas akhir ini dari latar belakang masalah, rumusan masalah, tujuan,

manfaat, batasan masalah, dan sistematika penulisan. Dari bab ini diharapkan penulis dapat memberikan gambaran kepada pembaca tentang ide-ide bahasan yang akan dikerjakan pada tugas akhir ini.

BAB II Tinjauan Pustaka dan Dasar Teori

Bab kedua berisikan tentang dasar-dasar teori dan literatur yang digunakan penulis dalam membuat tugas akhir. Bab ini juga berisi penjelasan lebih terperinci setiap komponen dan peralatan yang digunakan dalam melakukan analisa. Diharapkan dalam bab ini bisa memberi wawasan tentang untuk pembaca

BAB III Metodologi Penelitian

Berisi tentang langkah-langkah penelitian yang dilakukan mulai dari pengumpulan data hingga hasil. Bab ini terdiri dari diagram alir yang menunjukkan langkah awal penelitian hingga perolehan hasil dan penjelasan tiap langkah penelitian.

BAB IV Analisa dan Pembahasan

Bab ke-empat merupakan inti dari penelitian yang berisi tentang hasil tiap langkah analisa yang sudah disebutkan dalam bab sebelumnya.

BAB V Kesimpulan dan Saran

Kesimpulan yang didasarkan hasil analisa dimasukkan ke dalam bab ini. Kekurangan dalam penelitian ini dicantumkan dalam bentuk saran di dalam bab ini.

BAB II

TINJAUAN PUSTAKA DAN DASAR TEORI

2.1 Tinjauan Pustaka

Seperti dunia *engineering* pada umumnya yang mengalami banyak inovasi dalam pengembangannya, struktur lepas pantai terpancang tidak lepas dari inovasi tersebut, salah satu dari inovasi yang ada merupakan konfigurasi yang dimodifikasi agar memiliki konfigurasi dengan kekuatan tertentu dengan pertimbangan harga yang lebih murah. Pertimbangan tersebut tentunya mempengaruhi konfigurasi dari sebuah struktur yang mana selanjutnya berpengaruh pada kinerja dari struktur tersebut.

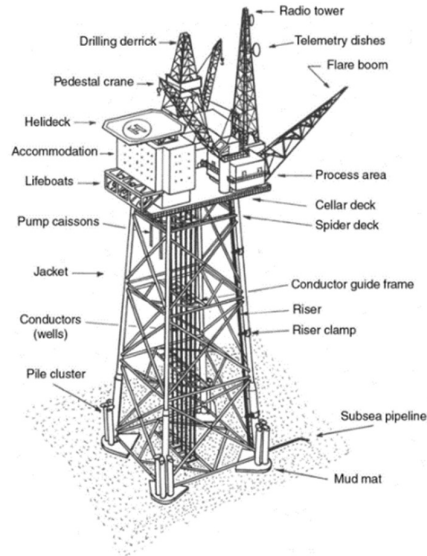
Seperti studi kasus yang digunakan pada tugas akhir ini, terdapat struktur *jacket* yang memiliki konfigurasi dengan bentuk kaki bagian atas modular dan bagian bawah yang konvensional yang dalam tugas akhir ini disebut sebagai struktur *jacket* 3 kaki modifikasi.

Dalam tugas akhir ini dilakukan analisa terkait perbandingan umur kelelahan struktur *jacket* 3 kaki konvensional dan 3 kaki modifikasi untuk mengetahui berapa kah periode natural dan umur kelelahan masing-masing *jacket* 3 kaki dengan beban bangunan atas dan kondisi lingkungan yang sama. Setyadi (2018) dalam tugas akhirnya menganalisa umur kelahan struktur *jacket* yang sama dan menyebutkan jika umur kelelahan paling rendah terletak pada *joint* tipe-Y dengan 121,25 tahun dengan metode spectral dan 1045,66 tahun dengan metode spectral. Maka dalam tugas akhir ini akan dilakukan analisa umur kelahan dengan menggunakan metode metode yang sama namun terdapat satu tambahan struktur sebanding sebagai pengembangan lebih lanjut.

2.2 Dasar Teori

2.2.1 Struktur Jacket

Jacket platform merupakan suatu struktur lepas pantai yang terdiri dari *topside*, *jacket*, dan pondasi. Struktur ini banyak digunakan pada kegiatan eksploitasi minyak dan gas lepas pantai karena fungsinya yang beragam mulai dari *drilling platform*, *wellhead platform*, *production platform*, *living quarter*, hingga 3 fungsi tersebut sekaligus (Riyanto, 2015). Bentuk umum struktur *jacket* dapat dilihat pada Gambar 2.1.



Gambar 2.1 Struktur *jacket* (sumber : drillingformulas.com)

Topside merupakan salah satu bagian dari platform *jacket* yang menjadi pusat semua operasi platform yang umumnya terdiri dari tiga *deck* yaitu *sub-cellar deck*, *cellar deck*, dan *main deck*. Peralatan yang terpasang pada *topside* disesuaikan dengan desain fungsi platform.

Jacket memegang peranan paling penting karena fungsinya sebagai penopang utama dari platform, bagian ini diperkuat dengan adanya *bracing* untuk menambah kekakuan dari *jacket* sendiri.

Pondasi berfungsi sebagai penambat dari platform ke tanah agar keseluruhan platform *jacket* tetap pada posisinya. Pondasi untuk platform *jacket* umumnya menggunakan *pile* yang ditempatkan di dalam *jacket leg* atau di pinggiran bagian ujung bawah *jacket leg* (*skirt pile*) yang kemudian dipancangkan hingga kedalaman tanah tertentu tergantung pada ukuran *pile* dan daya dukung tanah dalam desain.

2.2.2 Pembebanan Pada Struktur Jacket

2.2.2.1 Beban Mati

Beban mati adalah beban yang tidak berubah dalam satuan waktu, beban ini termasuk beban platform dan segala struktur yang berhubungan yang bersifat permanen dan tidak berubah dalam mode operasi (API, 2010). Beban ini didapat dari penjumlahan member dan beban yang dimodelkan pada *software* yang terasuk pada beban mati. Yang termasuk pada beban ini adalah :

1. Berat platform di udara termasuk *pile*, *grout*, dan *ballast*.
2. Berat peralatan dan segala yang berhubungan yang bersifat terpasang permanen pada platform.
3. Gaya hidrostatis di bawah air yang bekerja pada platform, termasuk tekanan eksternal dan *buoyancy*.

2.2.2.2 Beban Hidup

Beban hidup adalah beban yang mengenai platform selama masa penggunaannya dan dapat berubah dalam satuan waktu yang lama, beban ini juga didefinisikan sebagai beban yang dapat berubah dalam suatu mode operasi ataupun pada pergantian mode operasi (API, 2010). Beban ini termasuk :

1. Berat peralatan pengeboran dan produksi yang dapat ditambahkan dan dihilangkan dari platform.
2. Berat dari tempat tinggal, *helipad*, peralatan keselamatan, peralatan menyelam, dan peralatan lain yang dapat ditambahkan atau dihilangkan dari platform.
3. Berat dari barang yang dapat dikondumsi dan cairan yang terdapat pada tangki penyimpanan.
4. Gaya yang berkerja pada platform dari kegiatan operasi seperti pengeboran, *material handling*, penambatan kapal, dan beban helikopter.
5. Gaya yang terjadi dari kegiatan yang menggunakan *crane*.

2.2.2.3 Beban Lingkungan

Beban ini yterjadi akibat kejadian alami yang dihasilkan dari lingkungan lokasi platform termasuk angin, arus, gelombang, pasang surut, gempa, salju, es, dan pergerakan bumi (API, 2010). Beban ini juga termasuk variasi tekanan hidrostatis dan *buoyancy* pada member yang timbul akibat perubahan ketinggian gelombang dan pasang surut. Beban lingkungan harus ditinjau dari segala arah untuk mengantisipasi arah yang berdampak paling signifikan pada platform.

a. Beban Angin

Beban angin dalam perancangan struktur lepas pantai terpancang dihitung pada bagian struktur yang tidak tercelup air, terutama *topside*.

1. Menghtuing tinggi tiap *deck* dan titik tertinggi *topside* menggunakan titik acuan MSL.
2. Menghitung titik tangkap beban angin dengan menggunakan selisih ketinggian *deck* yang ditinjau dengan *deck* di atasnya.
3. Menghitung kecepatan angin pada elevasi 30 ft dengan menggunakan *the one-sevent power law* yang ditunjukkan pada persamaan 2.1.

$$V_z = V_{30} \cdot \left[\frac{z}{30} \right]^{\frac{1}{7}} \quad (2.1)$$

Keterangan :

- V_z = kecepatan angin pada elevasi yang ditinjau
 V_{30} = kecepatan angin pada elevasi 30 ft
 z = elevasi yang ditinjau (ft)
30 = elevasi refrensi (ft)

4. Setelah titik tangkap dan kecepatan angin didapat maka dapat menghitung beban angin menggunakan persamaan 2.2.

$$F_{wind} = C_s \cdot \frac{1}{2} \cdot \rho \cdot V_z \cdot A \quad (2.2)$$

Keterangan :

C_s = *shape coefficient*

ρ = massa jenis

V_z = kecepatan angin pada elevasi yang ditinjau

A = area yang tegak lurus terhadap arah datang angin

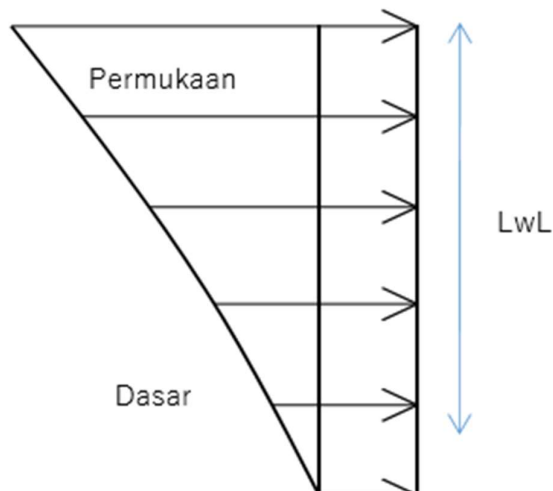
Nilai *shape coefficient* dapat ditentukan dari Tabel 2.1

Tabel 2.1 *shape coefficient* (sumber : ISO 19902:2007)

| Component | | shape coefficients C_s |
|--|---------------------------------|-----------------------------|
| Flat walls of buildings | | 1,50 |
| Overall projected area of structure | | 1,00 |
| Beams | | 1,50 |
| Cylinders | Smooth, $Re > 5 \times 10^5$ | 0,65 |
| | Smooth, $Re \leq 5 \times 10^5$ | 1,20 |
| | Rough, all Re | 1,05 |
| | Covered with ice, all Re | 1,20 |
| <small>Re Reynolds number</small> | | |

b. Beban Arus

Beban arus dalam perancangan struktur *jacket* berpengaruh signifikan pada *jacket*, dalam hal ini beban arus dihitung pada elevasi permukaan dan dasar laut. Profil kecepatan arus dapat dilihat pada Gambar 2.2.



Gambar 2.2 Profil kecepatan arus (sumber : Riyanto, 2015)

1. Beban arus dapat dihitung dengan persamaan 2.3.

$$F_{current} = \frac{1}{2} \cdot \rho \cdot C_D \cdot V^2 \cdot A \quad (2.3)$$

Keterangan :

- ρ = massa jenis air laut
- C_D = *drag coefficient*
- V = kecepatan arus
- A = area yang tegak lurus dengan arah datangnya arus

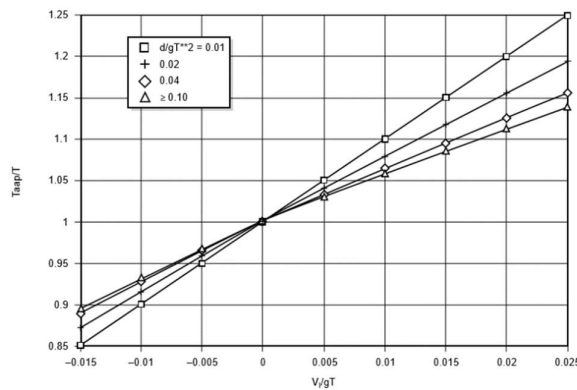
Drag coefficient dapat ditentukan menggunakan API (2010). Untuk kondisi *smooth* atau tidak memperhitungkan pengaruh *marine growth* $C_d = 0,65$ dan $C_m = 1,6$. Sementara untuk kondisi *rough* atau dengan memperhitungkan pengaruh *marine growth* maka $C_d = 1,05$ dan $C_m = 1,2$.

2. Setelah didapat beban arus di permukaan dan dasar laut maka perhitungan total beban arus dapat dilakukan dengan menjumlahkan beban arus di permukaan laut dan dasar laut.

c. Beban Gelombang

Dalam perancangan struktur lepas pantai terpancang, beban gelombang merupakan hal yang perlu untuk dipertimbangkan pada perhitungan beban lingkungan. Dengan bantuan *software* SACS maka hanya diperlukan untuk menentukan teori gelombang yang akan digunakan. Berikut merupakan langkah-langkah penentuan teori gelombang :

1. Menentukan teori gelombang dengan mencari nilai periode *apparent wave* terlebih dahulu menggunakan grafik *doppler shift due to steady current* pada Gambar 2.3.

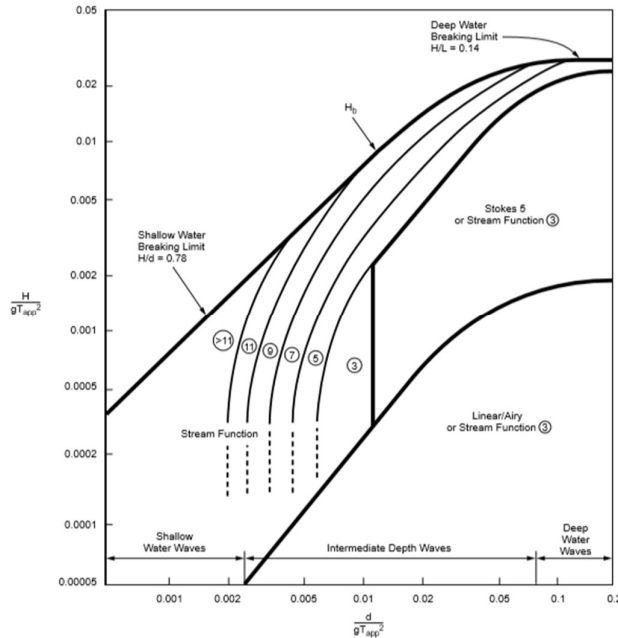


Gambar 2.3 Grafik *doppler shift due to steady current* (sumber : API, 2010)

Keterangan :

- T_{app} = periode *apparent wave*
- T = periode gelombang
- V_l = kecepatan arus
- g = percepatan gravitasi
- d = kedalaman laut rata-rata

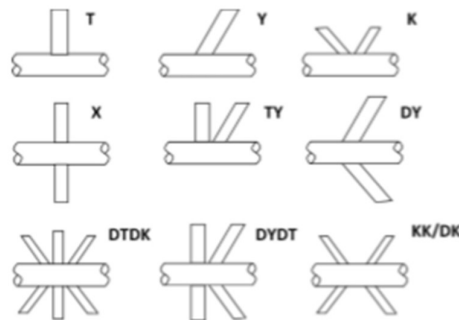
2. Setelah periode *apparent wave* diketahui, kemudian dilanjutkan dengan menentukan teori gelombang yang akan digunakan menggunakan grafik *regions of applicability* seperti pada Gambar 2.4. Penentuan teori gelombang yang akan digunakan dengan cara mencari perpotongan dari kedua sumbu x dan y.



Gambar 2.4 Grafik *regions of applicability* (sumber : API, 2010)

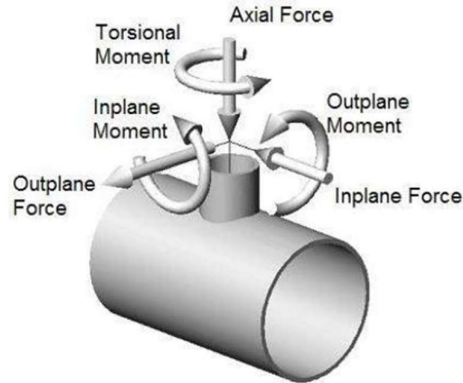
2.2.3 Tubular Joint

Dengan pembagian keseluruhan struktur *jacket* menjadi *topside*, *jacket*, dan pondasi, dua di antara 3 bagian tersebut merupakan *tubular joints*. *Tubular joints* merupakan sambungan antara dua atau lebih member dengan bentuk *tubular*, bentuk ini digunakan karena kemampuannya menerima beban dari segala arah tepat dengan kondisi yang dialami struktur *jacket* saat operasi. *Joint* diperlukan untuk mentransfer gaya yang diterima suatu member ke member lain pada *joint*, Saini (2016) dalam jurnalnya menyebutkan klasifikasi *tubular joints* seperti pada Gambar 2.5.



Gambar 2.5 Klasifikasi *tubular joints* (Sumber : Saini, 2016)

Tubular joint sebagai penopang utama pada platform *jacket* tentunya mengalami gaya yang dihasilkan dari segala arah baik dari gelombang maupun dari beban *topside* di atasnya, Saini (2016) dalam jurnalnya mengklasifikasikan jenis-jenis gaya yang bekerja pada suatu *tubular joint* seperti pada Gambar 2.6.



Gambar 2.6 Gaya dan beban pada tubular joint (Sumber : Saini, 2016)

2.2.4 Periode dan Frekuensi Natural

Periode natural merupakan waktu yang diperlukan oleh struktur untuk melakukan satu frekuensi gerakan, sementara frekuensi natural merupakan jumlah osilasi yang dilakukan struktur per detik. Dalam analisa kelelahan struktur lepas pantai, periode natural dari struktur perlu diketahui untuk mendapatkan faktor dinamis dari struktur yang nantinya juga berhubungan dengan *dynamic amplification factor* yang merupakan faktor pembesaran beban gelombang yang terjadi akibat resonansi periode natural struktur dengan periode gelombang. Persamaan frekuensi natural struktur menurut El-Reedy (2012) ditunjukkan pada persamaan 2.4.

$$\omega_n = \sqrt{\frac{k}{m}} \quad (2.4)$$

Keterangan :

ω_n = frekuensi natural (rad/s)

k = kekakuan struktur

m = massa struktur

Dengan mengaplikasikan persamaan periode natural seperti pada persamaan (2.5).

$$T_n = \frac{1}{\omega_n} \quad (2.5)$$

Maka dengan mensubstitusikan persamaan frekuensi natural sebelumnya didapatkan bahwa persamaan periode natural adalah seperti pada persamaan (2.6).

$$T_n = 2\pi \sqrt{\frac{m}{k}} \quad (2.6)$$

Keterangan :

T_n = periode natural

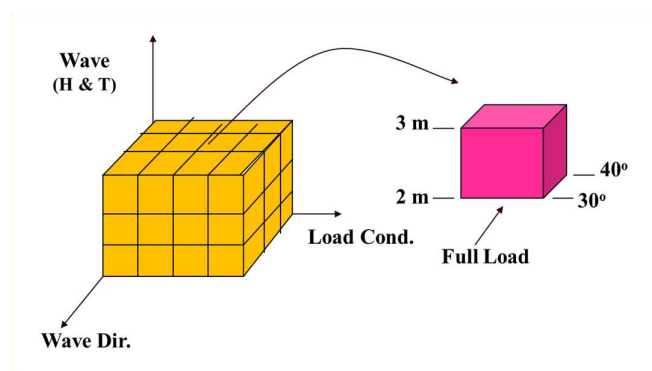
2.2.5 Analisa Kelelahan Metode Cummulative Damage

Analisa kelelahan platform lepas pantai mulai dikembangkan sejak tahun 1980 dari kecelakaan Platform *Semisubmersible* Alexander L. Kielland yang diduga mengalami kegagalan akibat kelelahan, sejak kecalakaan itu banyak penelitian yang membahas tentang kegagalan platform akibat kelelahan.

Kegagalan akibat kelelahan *cummmulative damage* merupakan salah satu metode analisa umur kelelahan dengan menggunakan beban lingkungan yang bersifat siklik sebagai penyebab kelelahannya, beban ini dapat meliputi beban suhu, gelombang, angin, dan arus. Terdapat dua metode analisa pada *cumulative damage*, yaitu *deterministic analysis* dan *spectral analysis*. API (2010) menyarankan jika analisa umur kelelahan dilakukan dalam metode *spectral analysis*, namun jika periode natural dari struktur < 3 detik maka analisa kelelahan dapat menggunakan metode *deterministic analysis*. Pada tugas akhir ini akan dilakukan perhitungan umur kelalahan hanya dengan menggunakan metode *spectral analysis*.

2.2.5.1 Spectral Analysis

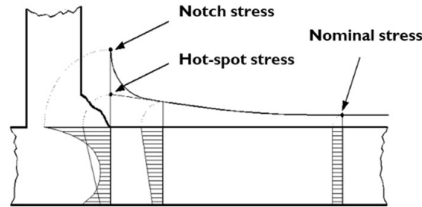
Pada perhiutngannya, metode ini menggunakan spektrum gelombang dan respon struktur akibat gelombang yang mengenainya. Dalam analisa spektral, respon acak dari struktur juga dapat diwakilkan dalam bentuk spektrum respon dengan mengkorelasikan respon struktur dalam gelombang regular dan spektrum gelombang. Liu (1989) menyarankan minimal penggunaan 8 arah RAO yang ditinjau yaitu 0°, 45°, 90°, 135°, 180°, 225°, 270°, dan 315°, namun pada tugas akhir ini akan digunakan 16 arah RAO yaitu 0°, 22,5°, 45°, 67,5°, 90°, 112,5°, 135°, 157,5°, 180°, 202,5°, 225°, 247,5°, 270°, 292,5°, 315°, dan 337,5°. Pada Gambar 2.7 dapat dilihat skenario perhitungan umur kelelahan menggunakan metode *full spectral analysis*.



Gambar 2.7 Skenario analisa spektral (Djutmiko, 2006)

a. Tegangan Member-Joint

Pada Gambar 2.8 dapat dilihat jenis-jenis tegangan yang dialami oleh *member* dan *joint* pada saat mengalami pembebanan.



Gambar 2.8 Tegangan yang dialami *member-joint* (sumber : API, 2000)

- **Tegangan Nominal**

Merupakan tegangan yang dialami oleh *member*. Dalam hal platform *jacket* yang memiliki banyak *member*, analisa tegangan yang dialami oleh *member* dapat menggunakan *finite element method* yang dibantu dengan *software* SACS untuk membantu perhitungan tegangan yang dialami setiap *member*. Berikut persamaan tegangan nominal ditunjukkan pada persamaan 2.7.

$$\sigma_{nom} = \frac{F}{A} + \frac{M}{I}y \quad (2.7)$$

- **Tegangan Notch**

Merupakan tegangan lokal yang meningkat pada suatu *notch*, yaitu pada kaki las-lasan atau didaerah tepi dari suatu potongan. Pendekatan *notch stress* memperhitungkan konsentrasi tegangan yang disebabkan oleh kualitas las-lasan. Persamaan tegangan *notch* dapat dilihat pada persamaan 2.8.

$$\sigma_{ln} = K_t \cdot \sigma_{nom} \quad (2.8)$$

- **Tegangan Hot Spot**

Merupakan tegangan pada daerah kritis yang dialami oleh *joint* dimana terjadi tegangan tarik/tekan maksimum. Secara umum diidentifikasi ada tiga tipe tegangan dasar yang menyebabkan munculnya hot spot (Becker et al., 1970):

1. Tipe A, disebabkan oleh gaya-gaya aksial dan momen-momen yang merupakan hasil dari kombinasi frame dan truss jacket.
2. Tipe B disebabkan detail-detail sambungan struktur seperti geometri sambungan yang kurang memadai, variasi kekakuan yang bervariasi disambungan dan lain-lain.
3. Tipe C, disebabkan oleh faktor metalurgis yang dihasilkan dan kesalahan pengelasan, seperti undercut, porosity, dan lain-lain.

Tegangan ini dapat digenreasi menggunakan *finite element method* yang dibantu dengan *software* SACS, namun secara teoritis tegangan *hot spot* memiliki persamaan seperti pada persamaan 2.9.

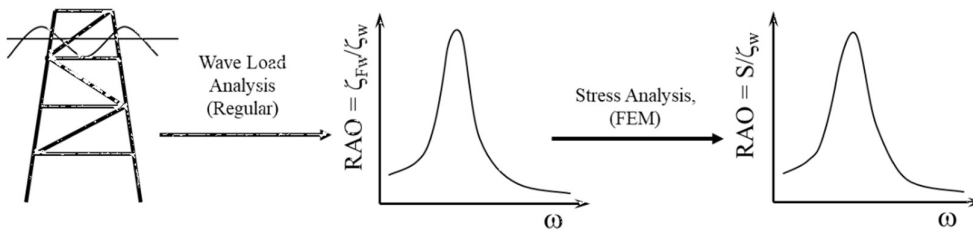
$$\sigma_{hs} = \sigma_{nom} \times SCF \quad (2.9)$$

Keterangan :

- σ_{hs} = tegangan *hot spot*
- σ_{nom} = tegangan nominal
- SCF = *stress concentration factor*

b. Response Amplitude Operator (RAO)

Dengan nama lain *transfer function*, RAO merupakan suatu grafik yang fungsi respon struktur akibat gelombang dalam rentang frekuensi maupun periode tertentu. Dalam hal ini RAO dari struktur *jacket* dapat digenerasi dengan bantuan *software* SACS dengan ilustrasi seperti pada Gambar 2.9.



Gambar 2.9 Analisa beban gelombang untuk memperoleh RAO dan RAO Tegangan (Djatkiko, 2006)

c. Dynamic Amplification Factor (DAF)

DAF merupakan faktor amplifikasi respon struktur terhadap suatu periode gelombang yang mengenai struktur tersebut, hal ini dikaitkan dengan periode natural struktur. Pada daerah periode natural struktur akan terjadi pembesaran respon struktur yang diakibatkan oleh periode gelombang dan periode natural struktur yang beresonansi, hal ini membuat DAF perlu dijadikan pertimbangan dalam analisa kelelahan struktur sehingga efek resonansi struktur terwakilkan. DAF dapat dihitung dengan menggunakan persamaan 2.10.

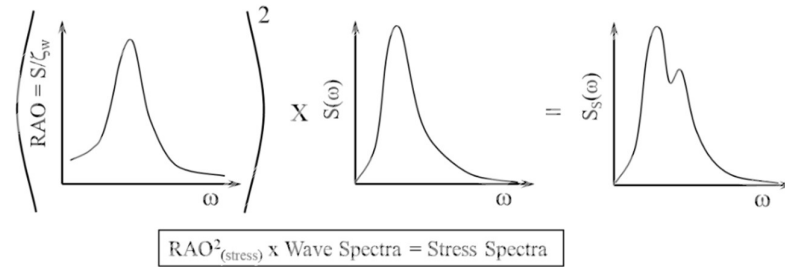
$$DAF = \frac{1}{\sqrt{\left\{1 - \left(\frac{T_n}{T}\right)^2\right\}^2 + \left(2\beta \frac{T_n}{T}\right)^2}} \quad (2.10)$$

Keterangan :

- T_n = periode natural struktur *jacket*
- T = periode gelombang
- β = *damping ratio* struktur dapat dianggap 0.02

d. Spektra Gelombang

Spektra gelombang merupakan hasil transformasi suatu rekaman gelombang acak dalam domain waktu menjadi domain frekuensi menggunakan matematika deret fourier yang disajikan dalam grafik dengan absis frekuensi gelombang (ω) dan ordinat berupa sepkra energi gelombang ($S_{\zeta}(\omega)$) itu sendiri (Djatkiko, 2012). Adapun penggunaan spektra gelombang pada tahap ini adalah untuk dikalikan dengan kuadrat dari RAO tegangan agar menjadi spektra tegangan seperti yang terlihat pada Gambar 2.10.



Gambar 2.10 Perhitungan Spektra tegangan

Adapun formulasi spektra gelombang yang digunakan pada analisa ini adalah spektra JONSWAP. Formulasi spektra ini banyak digunakan untuk mentransformasikan rekaman gelombang pada perairan yang berkepulauan, hal ini tentunya tepat digunakan pada perairan Indonesia yang mana merupakan perairan yang memiliki kondisi serupa dengan penggunaan formulasi spektra JONSWAP. Persamaan spektra JONSWAP dapat dilihat pada persamaan 2.11.

$$S_{\zeta}(\omega) = \alpha g^2 \omega^{-5} \exp \{-1.25(\omega/\omega_0)^{-4}\} \gamma \exp \left\{ -\frac{(\omega/\omega_0)^2}{2\tau\omega_0^2} \right\} \quad (2.11)$$

Keterangan :

$$\alpha = 0.076(X_0)^{-0.22}$$

$$X_0 = gX/U_w^2$$

X = panjang fetch

U_w = kecepatan angin

α = 0.0081 jika X tidak diketahui

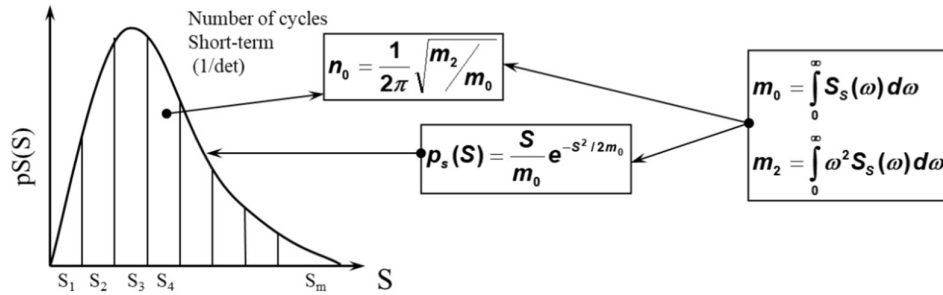
γ = parameter ketinggian atau peakedness parameter, yang harganya dapat bervariasi antara 1.0 sampai dengan 7.0.

$$\tau = 0.07 \text{ jika } \omega \leq \omega_0$$

$$\tau = 0.07 \text{ jika } \omega > \omega_0$$

$$\omega_0 = 2\pi \left(\frac{g}{U_w} \right) (X_0)^{-0.33}$$

e. Distribusi Rayleigh Untuk Distribusi Rentang Tegangan Jangka Pendek



Gambar 2.11 Perhitungan distribusi Rayleigh kurun waktu pendek (Djatkiko, 2006).

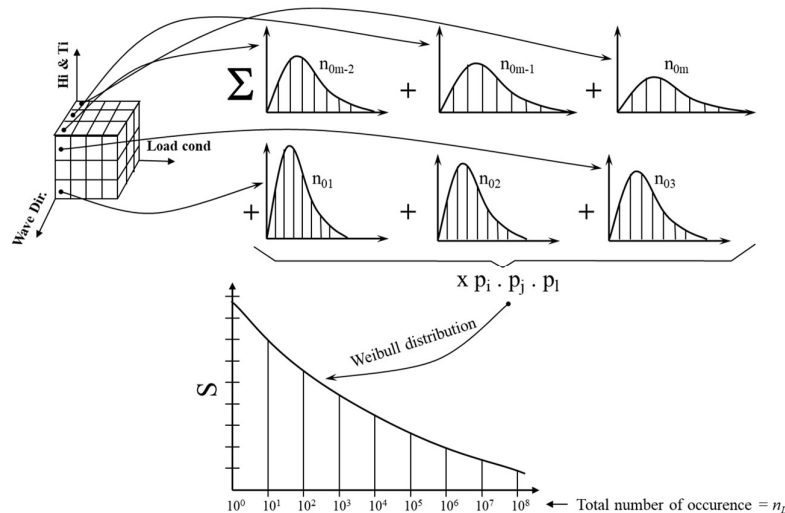
Distribusi Rayleigh digunakan untuk perhitungan rentang tegangan jangka pendek seperti pada Gambar 2.11. Dengan menggunakan persamaan 2.12.

$$n_0 = \frac{1}{2\pi} \sqrt{\frac{m_2}{m_0}} \quad (2.12)$$

Dimana m_0 dan m_2 masing-masing merupakan luasan dan momen luasan beidang dibawah kurva spektra tegangan yang diperoleh dari fungsi transfer dalam kurun waktu pendek. Sementara peluang rentang tegangan untuk jangka pendek dinyatakan dengan persamaan 2.13.

$$p_s(S) = \frac{S}{m_0} e^{-S^2/2m_0} \quad (2.13)$$

f. Distribusi Weibull Untuk Distribusi Rentang Tegangan Jangka Panjang



Gambar 2.12 Perhitungan distribusi Weibull kurun waktu panjang (Djatkiko, 2006)

Menghitung jumlah siklus gelombang dalam jangka panjang seperti pada Gambar 2.12 dengan persamaan 2.14.

$$n_L = \left(\sum_i \sum_j \sum_k n_0 \times p_i p_j p_k \right) \times T_L \quad (2.14)$$

Keterangan :

p_i = peluang sudut gelombang datang

p_j = peluang gabungan dari H_s dan T tertentu yang diperoleh dari data sebaran gelombang

p_k = peluang kejadian spektrum tertentu

n_0 = jumlah siklus tegangan per satuan waktu (1/detik) yang dapat diperoleh dari interval operasi untuk kurun waktu pendek yang dirumuskan pada persamaan sebelumnya.

Pada perhitungan fungsi kerapatan peluang untuk rentang tegangan S jangka Panjang dapat dihitung menggunakan persamaan 2.15.

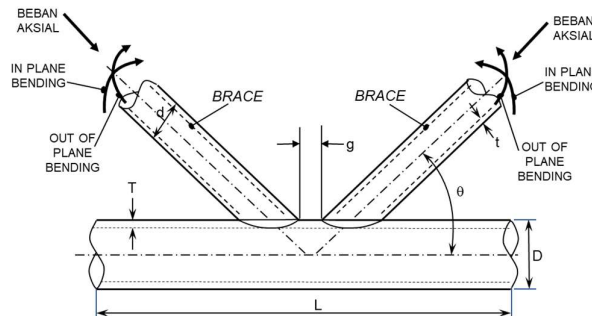
$$P_L(S) = \frac{\sum_i \sum_j \sum_k n_0 \times p_i p_j p_k \times p_s(S)}{\sum_i \sum_j \sum_k n_0 \times p_i p_j p_k} \quad (2.15)$$

g. Stress Concentration Factor (SCF)

Stress concentration factor merupakan suatu konstanta dari hasil pembagian rentang tegangan *hot spot* dengan rentang tegangan nominal pada *brace*, sementara seperti telah dijelaskan di bagian sebelumnya jika tegangan hotspot merupakan tegangan yang dialami suatu titik di *joint*. Menurut Gibstein (1985) persamaan SCF dapat dijabarkan seperti pada persamaan 2.16.

$$SCF = \frac{HSSR \text{ (Hot Spot Stress Range)}}{\text{Nominal brace stress range}} \quad (2.16)$$

Penentuan nilai SCF secara lebih detail dapat mempertimbangkan parameter gaya pada *tubular joint* yang ditunjukkan pada Gambar 2.13.



Gambar 2.13 Parameter *tubular joint* (API, 2000)

Selain parameter gaya pada *tubular joint*, penentuan nilai SCF juga mempertimbangkan parameter ukuran *tubular joint* yang ditunjukkan pada Tabel 2.2.

Tabel 2.2 Parameter *tubular joint*

| Parameter | Formula | Keterangan |
|-----------|---------|---|
| γ | $D/2T$ | Rasio kerampingan <i>chord</i> |
| β | d/D | Rasio diameter |
| τ | t/T | Rasio Ketebalan |
| θ | - | Sudut orientasi |
| ξ | g/D | Rasio <i>gap</i> dengan diameter <i>chord</i> |

Keterangan :

θ = sudut dalam antara *bracing* dan *chord*

g = jarak antar *bracing joint*

t = tebal dinding *bracing*

T = tebal dinding *chord*

d = diameter luar *bracing*

D = diameter luar *chord*

Dari sekian banyak teori penentuan SCF, dalam tugas akhir ini penentuan SCF menggunakan teori dari Efthymiou. Batas-batas parameter yang digunakan pada teori SCF Efthymiou dapat dilihat pada Tabel 2.3.

Tabel 2.3 Batas parameter Penentuan SCF Efthymiou (Almar-Næss, 1985)

| Batas Bawah | Parameter | Batas Atas |
|---------------------------|-----------|------------|
| 8 | γ | 32 |
| 0,2 | β | 1 |
| 0,2 | τ | 1 |
| 20° | θ | 90° |
| $-0,6 \beta / \sin\theta$ | ξ | 1 |

Sementara penentuan nilai SCF dengan teori Efthymiou dapat menggunakan persamaan pada Tabel 2.4.

Tabel 2.4 Teori penentuan SCF Efthymiou

| Klasifikasi Joint | Brace Load | | | |
|-------------------|--|---|------------------------------|--------------------------------------|
| | Axial Tension | Axial Compression | In-Plane Bending | Out-of-Plane Bending |
| K | $(16 + 1.2\gamma)\beta^{1.2}Q_g$ but $\leq 40\beta^{1.2}Q_g$ | | $(5 + 0.7\gamma)\beta^{1.2}$ | $2.5 + (4.5 + 0.2\gamma)\beta^{2.6}$ |
| T/Y | 30β | $2.8 + (20 + 0.8\gamma)\beta^{1.6}$ but $\leq 2.8 + 36\beta^{1.6}$ | | |
| X | $\frac{23\beta}{\text{for } \beta \leq 0.9}$ $\frac{20.7 + (\beta - 0.9)(17\gamma - 220)}{\text{for } \beta > 0.9}$ | $[2.8 + (12 + 0.1\gamma)\beta]Q_\beta$ | | |

Keterangan :

$$Q\beta = 0.3/\beta(1-0.833 \beta) \text{ for } \beta > 0.6$$

$$Q\beta = 1.0 \text{ for } \beta \leq 0.6$$

$$Q_g = 1 + 0.2 [1 - 2.8g/D]^3 \text{ for } g/D \geq 0.05 \text{ but } \geq 1.0$$

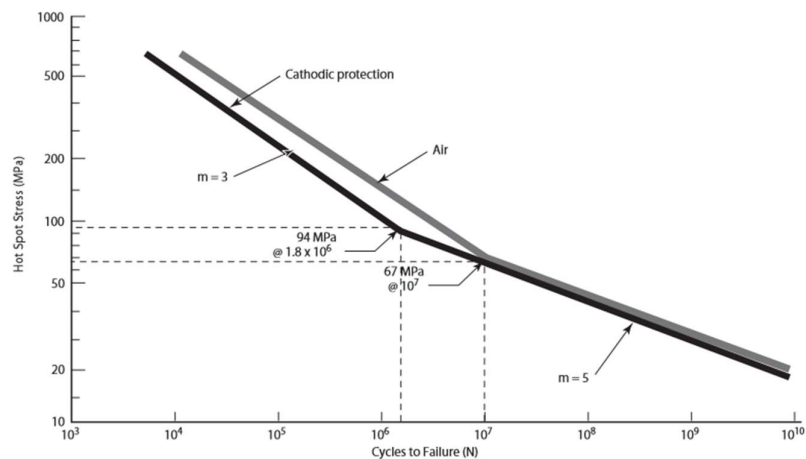
$$Q_g = 0.13 + 0.65\Phi\gamma^{0.5} \text{ for } g/D \leq -0.05 \text{ dimana, } \Phi = tF_{yb}/(TF_{yc})$$

F_{yb} = yield stress brace (atau 0.8 dari tensile strength jika kurang)

F_{yc} = yield stress chord

h. Kurva S-N

Merupakan plot dari rentang tegangan (S) dan jumlah siklus (N), kurva S-N dalam metode ini digunakan untuk mencari nilai N sebagai pembagi dalam persamaan akumulasi kerusakan Palmgren-Miner. Sementara penelitian ini menggunakan kurva S-N dengan koreksi ketebalan dari API Gambar 2.14.



Gambar 2.14 Kurva S-N tubular joint $T = 5/8$ in (sumber : API, 2010)

Secara teoritis dari kurva S-N dapat digenerasi persamaan 2.17 untuk mencari parameter N .

$$\log_{10}(N) = \log_{10}(k_1) - m \log_{10}(S) \quad (2.17)$$

Keterangan :

- N = jumlah siklus untuk gagal
 S = rentang tegangan *hot spot* (MPa)
 $\log(k_1)$ = *Tabel 2.5 Nilai $\log(k_1)$ dan m (sumber : API 2010)
 m = *Tabel 2.5 Nilai $\log(k_1)$ dan m (sumber : API 2010)

Tabel 2.5 Nilai $\log(k_1)$ dan m (sumber : API 2010)

| Curve | $\log_{10}(k_1)$ S in ksi | $\log_{10}(k_1)$ S in MPa | m |
|--------------------|--------------------------------|--------------------------------|------------------|
| Welded Joints (WJ) | 9.95 | 12.48 | 3 for $N < 10^7$ |
| | 11.92 | 16.13 | 5 for $N > 10^7$ |
| Cast Joints (CJ) | 11.80 | 15.17 | 4 for $N < 10^7$ |
| | 13.00 | 17.21 | 5 for $N > 10^7$ |

Pemilihan kurva S-N harus tepat berdasarkan tipe material dan dan ketebalan, maka dari itu terdapat efek ketebalan untuk digunakan dalam segala kurva S-N. Persamaan ini dapat dilihat pada persamaan 2.18.

$$S = S_o(t_{ref}/t)^{0,25} \quad (2.18)$$

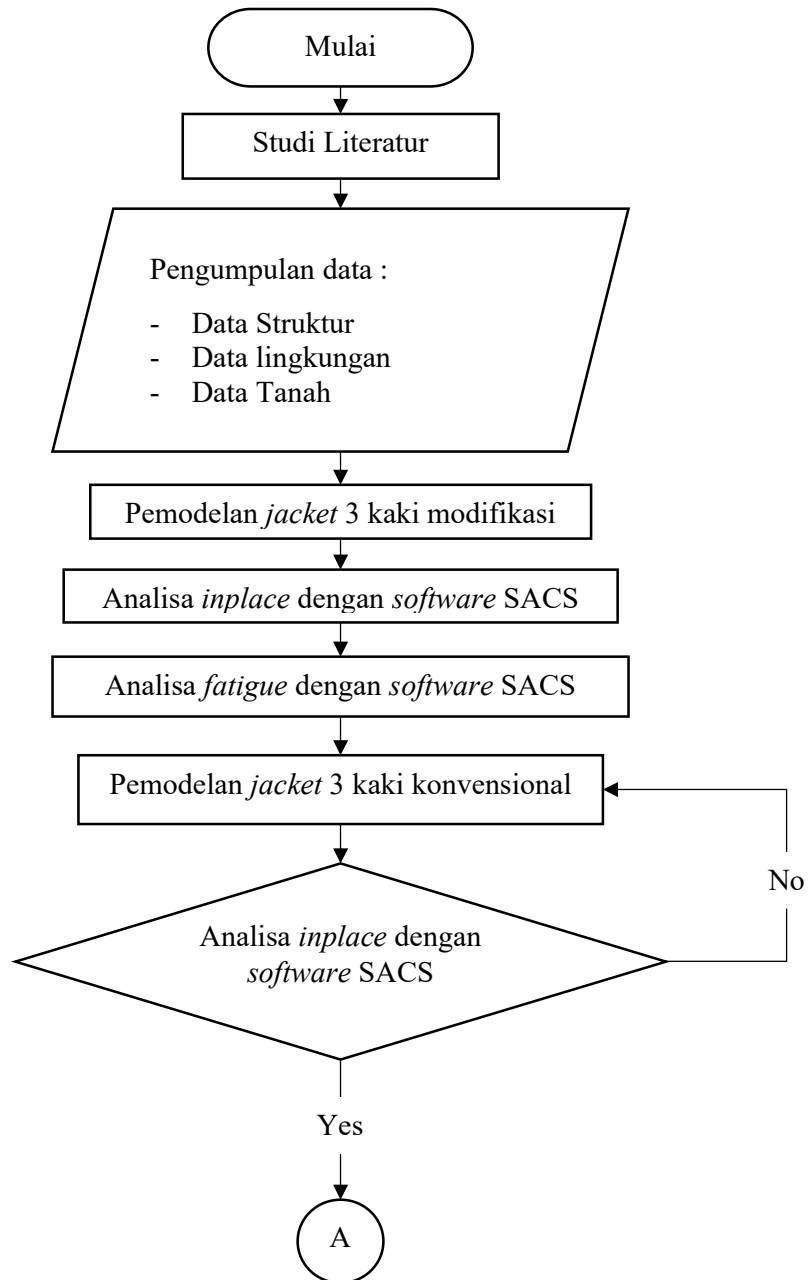
Keterangan :

- S = rentang tegangan
 S_o = rentang tegangan awal
 t_{ref} = ketebalan refrensi, 5/8 in (16 mm)
 t = ketebalan *joint* yang ditinjau

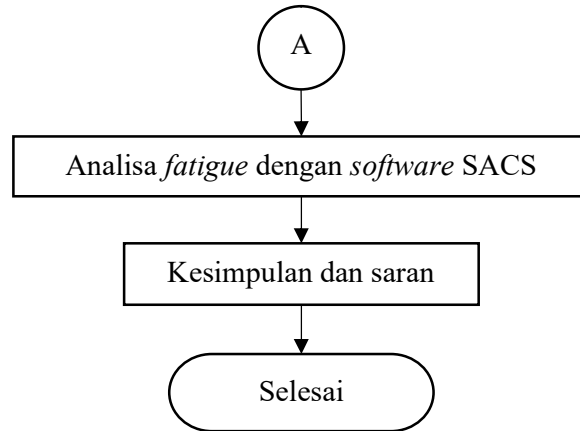
BAB III
METODOLOGI PENELITIAN

3.1 Diagram Alir Penelitian

Pada Gambar 3.1 hingga Gambar 3.2 dapat dilihat alur pengerjaan dari studi literatur hingga analisa kelelahan menggunakan metode *full spectral analysis*.



Gambar 3.1 Diagram alir pengerjaan



Gambar 3.2 Diagram alir pengerjaan (lanjutan)

3.2 Metodologi Penelitian

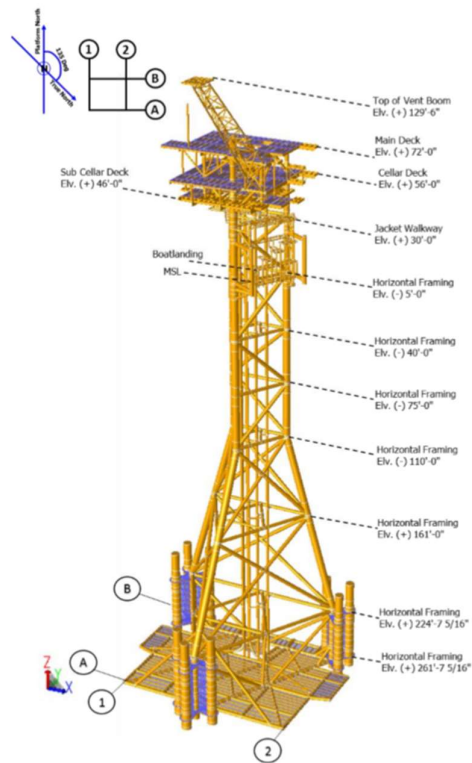
3.2.1 Studi Literatur

Pada tahap ini, studi literatur dilakukan dengan mencari jurnal, buku, tugas akhir lain dan informasi dari internet yang berkaitan dengan judul tugas akhir yang dikerjakan.

3.2.2 Pengumpulan Data

Untuk objek analisa, data struktur menggunakan struktur milik Husky-CNOOC Madura Limited (HCML) yang didapatkan dari dosen. Data struktur ini akan dijadikan objek analisa yang meliputi analisa kekuatan statis dan dinamis untuk umur kelelahan. Data struktur ini nantinya juga akan dijadikan refrensi untuk mendesain ulang *jacket leg* dari struktur sebagai pembanding umur kelelahan struktur *jacket* 3 kaki modifikasi. Model struktur yang digunakan dapat dilihat pada Gambar 3.3:

- Jenis Struktur : *Wellhead Platform*
- Lokasi Operasi : 114° 18' 21.63" E dan 7° 18' 45.70" S
- Jumlah Deck : 3 (tiga)
- Jumlah Kaki : 3 (tiga)
- Jumlah Pile : 9 buah tipe *skirt pile* OD 64 inch
- Jumlah Elevasi Kaki : 8 (delapan)
- Orientasi Platform : (-) 135°



Gambar 3.3 Platform MBH.

Sementara beban lingkungan yang digunakan pada analisa kelelahan dan *inplace* untuk kedua model *jacket* adalah beban gelombang dan arus. Beban gelombang yang digunakan pada analisa kelelahan disajikan dalam bentuk jumlah kejadian dengan kala ulang 1 tahun yang dapat dilihat pada Tabel 3.1 hingga Tabel 3.16.

- Lokasi Data : 6° 30' 00.00" S dan 112° 51' 00.00" E
- Jumlah Arah : 16 arah
- Arah Datang : Menuju struktur

Tabel 3.1 Data kejadian gelombang arah N

| Cluster: L | Wave Distribution of 100 Years Period | | | | | | | | | | | | | N |
|--------------|---------------------------------------|------|-------|------|-----|-----|-----|-----|-----|------|-------|-------|-------|-------|
| H | T (second) | | | | | | | | | | | | | Total |
| (meter) | 0-1 | 1-2 | 2-3 | 3-4 | 4-5 | 5-6 | 6-7 | 7-8 | 8-9 | 9-10 | 10-11 | 11-12 | 12-13 | |
| 0.0-0.5 | 403 | 3320 | 10045 | 5359 | 824 | 26 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 19977 |
| 0.5-1.0 | 0 | 0 | 722 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 722 |
| Total | 403 | 3320 | 10767 | 5359 | 824 | 26 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 20699 |

Tabel 3.2 Data kejadian gelombang arah NNE

| Cluster: L | Wave Distribution of 100 Years Period | | | | | | | | | | | | | NNE |
|--------------|---------------------------------------|-------------|-------------|-------------|------------|-----------|----------|----------|----------|----------|----------|----------|----------|--------------|
| H (meter) | T (second) | | | | | | | | | | | | | Total |
| | 0-1 | 1-2 | 2-3 | 3-4 | 4-5 | 5-6 | 6-7 | 7-8 | 8-9 | 9-10 | 10-11 | 11-12 | 12-13 | |
| 0.0-0.5 | 231 | 1763 | 6377 | 3135 | 396 | 21 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 11927 |
| 0.5-1.0 | 0 | 0 | 460 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 460 |
| Total | 231 | 1763 | 6837 | 3135 | 396 | 21 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 12387 |

Tabel 3.3 Data kejadian gelombang arah NE

| Cluster: L | Wave Distribution of 100 Years Period | | | | | | | | | | | | | NE |
|--------------|---------------------------------------|------------|-------------|-------------|------------|-----------|-----------|----------|----------|----------|----------|----------|----------|-------------|
| H (meter) | T (second) | | | | | | | | | | | | | Total |
| | 0-1 | 1-2 | 2-3 | 3-4 | 4-5 | 5-6 | 6-7 | 7-8 | 8-9 | 9-10 | 10-11 | 11-12 | 12-13 | |
| 0.0-0.5 | 126 | 969 | 6470 | 1037 | 262 | 85 | 16 | 4 | 0 | 0 | 0 | 0 | 0 | 8969 |
| 0.5-1.0 | 0 | 0 | 294 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 294 |
| Total | 126 | 969 | 6764 | 1037 | 262 | 85 | 16 | 4 | 0 | 0 | 0 | 0 | 0 | 9263 |

Tabel 3.4 Data kejadian gelombang arah ENE

| Cluster: L | Wave Distribution of 100 Years Period | | | | | | | | | | | | | ENE |
|--------------|---------------------------------------|-------------|-------------|-------------|-------------|-------------|------------|----------|----------|----------|----------|----------|----------|--------------|
| H (meter) | T (second) | | | | | | | | | | | | | Total |
| | 0-1 | 1-2 | 2-3 | 3-4 | 4-5 | 5-6 | 6-7 | 7-8 | 8-9 | 9-10 | 10-11 | 11-12 | 12-13 | |
| 0.0-0.5 | 763 | 9288 | 6207 | 1903 | 940 | 307 | 34 | 1 | 0 | 0 | 0 | 0 | 0 | 19443 |
| 0.5-1.0 | 0 | 14 | 395 | 2301 | 2970 | 952 | 97 | 1 | 0 | 0 | 0 | 0 | 0 | 6730 |
| 1.0-1.5 | 0 | 0 | 0 | 238 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 238 |
| Total | 763 | 9302 | 6602 | 4442 | 3910 | 1259 | 131 | 2 | 0 | 0 | 0 | 0 | 0 | 26411 |

Tabel 3.5 Data kejadian gelombang arah E

| Cluster: L | Wave Distribution of 100 Years Period | | | | | | | | | | | | | E |
|--------------|---------------------------------------|--------------|--------------|--------------|--------------|-------------|------------|-----------|----------|----------|----------|----------|----------|---------------|
| H (meter) | T (second) | | | | | | | | | | | | | Total |
| | 0-1 | 1-2 | 2-3 | 3-4 | 4-5 | 5-6 | 6-7 | 7-8 | 8-9 | 9-10 | 10-11 | 11-12 | 12-13 | |
| 0.0-0.5 | 1970 | 15232 | 31614 | 80981 | 16340 | 4117 | 644 | 56 | 1 | 2 | 0 | 0 | 0 | 150957 |
| 0.5-1.0 | 0 | 0 | 0 | 0 | 21272 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 21272 |
| Total | 1970 | 15232 | 31614 | 80981 | 37612 | 4117 | 644 | 56 | 1 | 2 | 0 | 0 | 0 | 172229 |

Tabel 3.6 Data kejadian gelombang arah ESE

| Cluster: L | Wave Distribution of 100 Years Period | | | | | | | | | | | | | ESE |
|--------------|---------------------------------------|---------------|---------------|---------------|---------------|---------------|---------------|--------------|-------------|-------------|------------|-----------|----------|----------------|
| H (meter) | T (second) | | | | | | | | | | | | | Total |
| | 0-1 | 1-2 | 2-3 | 3-4 | 4-5 | 5-6 | 6-7 | 7-8 | 8-9 | 9-10 | 10-11 | 11-12 | 12-13 | |
| 0.0-0.5 | 23697 | 185332 | 387643 | 461869 | 296908 | 77333 | 13927 | 2049 | 264 | 43 | 9 | 1 | 0 | 1449075 |
| 0.5-1.0 | 1 | 869 | 18475 | 124233 | 183827 | 98264 | 31668 | 8613 | 2283 | 516 | 96 | 15 | 4 | 468864 |
| 1.0-1.5 | 0 | 4 | 407 | 8503 | 38574 | 44095 | 27347 | 11729 | 3496 | 668 | 106 | 12 | 2 | 134943 |
| 1.5-2.0 | 0 | 0 | 12 | 414 | 6928 | 18766 | 17217 | 7841 | 2067 | 378 | 62 | 11 | 1 | 53697 |
| 2.0-2.5 | 0 | 0 | 1 | 18 | 1060 | 6401 | 7884 | 3725 | 990 | 174 | 15 | 2 | 0 | 20270 |
| 2.5-3.0 | 0 | 0 | 0 | 2 | 109 | 1756 | 2919 | 1544 | 400 | 52 | 4 | 0 | 0 | 6786 |
| 3.0-3.5 | 0 | 0 | 0 | 0 | 9 | 384 | 985 | 627 | 145 | 10 | 0 | 0 | 0 | 2160 |
| 3.5-4.0 | 0 | 0 | 0 | 0 | 0 | 78 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 78 |
| Total | 23698 | 186205 | 406538 | 595039 | 527415 | 247077 | 101947 | 36128 | 9645 | 1841 | 292 | 41 | 7 | 2135873 |

Tabel 3.7 Data kejadian gelombang arah SE

| Cluster: L | Wave Distribution of 100 Years Period | | | | | | | | | | | | | SE |
|--------------|---------------------------------------|--------------|--------------|---------------|--------------|--------------|-------------|-------------|------------|-----------|----------|----------|----------|---------------|
| H (meter) | T (second) | | | | | | | | | | | | | Total |
| | 0-1 | 1-2 | 2-3 | 3-4 | 4-5 | 5-6 | 6-7 | 7-8 | 8-9 | 9-10 | 10-11 | 11-12 | 12-13 | |
| 0.0-0.5 | 4985 | 39356 | 88597 | 123260 | 71801 | 17327 | 3504 | 620 | 67 | 7 | 2 | 0 | 0 | 349526 |
| 0.5-1.0 | 0 | 30 | 978 | 12319 | 22066 | 12383 | 4119 | 846 | 175 | 31 | 2 | 0 | 0 | 52949 |
| 1.0-1.5 | 0 | 0 | 0 | 0 | 1114 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1114 |
| Total | 4985 | 39386 | 89575 | 135579 | 94981 | 29710 | 7623 | 1466 | 242 | 38 | 4 | 0 | 0 | 403589 |

Tabel 3.8 Data kejadian gelombang arah SSE

| Cluster: L | Wave Distribution of 100 Years Period | | | | | | | | | | | | | SSE |
|--------------|---------------------------------------|-------------|--------------|-------------|-------------|-----------|----------|----------|----------|----------|----------|----------|----------|--------------|
| H (meter) | T (second) | | | | | | | | | | | | | Total |
| | 0-1 | 1-2 | 2-3 | 3-4 | 4-5 | 5-6 | 6-7 | 7-8 | 8-9 | 9-10 | 10-11 | 11-12 | 12-13 | |
| 0.0-0.5 | 675 | 5089 | 12558 | 7663 | 1090 | 41 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 27117 |
| 0.5-1.0 | 0 | 0 | 71 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 71 |
| Total | 675 | 5089 | 12629 | 7663 | 1090 | 41 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 27188 |

Tabel 3.9 Data kejadian gelombang arah S

| Cluster: L | Wave Distribution of 100 Years Period | | | | | | | | | | | | | S |
|--------------|---------------------------------------|-------------|-------------|-------------|------------|----------|----------|----------|----------|----------|----------|----------|----------|-------------|
| H (meter) | T (second) | | | | | | | | | | | | | Total |
| | 0-1 | 1-2 | 2-3 | 3-4 | 4-5 | 5-6 | 6-7 | 7-8 | 8-9 | 9-10 | 10-11 | 11-12 | 12-13 | |
| 0.0-0.5 | 251 | 1984 | 5337 | 1989 | 261 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9830 |
| 0.5-1.0 | 0 | 0 | 44 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 44 |
| Total | 251 | 1984 | 5381 | 1989 | 261 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9874 |

Tabel 3.10 Data kejadian gelombang arah SSW

| Cluster: L | Wave Distribution of 100 Years Period | | | | | | | | | | | | | SSW |
|--------------|---------------------------------------|------------|-------------|-------------|------------|-----------|----------|----------|----------|----------|----------|----------|----------|-------------|
| H (meter) | T (second) | | | | | | | | | | | | | Total |
| | 0-1 | 1-2 | 2-3 | 3-4 | 4-5 | 5-6 | 6-7 | 7-8 | 8-9 | 9-10 | 10-11 | 11-12 | 12-13 | |
| 0.0-0.5 | 68 | 571 | 1204 | 2163 | 559 | 16 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 4583 |
| 0.5-1.0 | 0 | 0 | 82 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 82 |
| Total | 68 | 571 | 1286 | 2163 | 559 | 16 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 4665 |

Tabel 3.11 Data kejadian gelombang arah SW

| Cluster: L | Wave Distribution of 100 Years Period | | | | | | | | | | | | | SW |
|--------------|---------------------------------------|-------------|--------------|--------------|-------------|------------|----------|----------|----------|----------|----------|----------|----------|--------------|
| H (meter) | T (second) | | | | | | | | | | | | | Total |
| | 0-1 | 1-2 | 2-3 | 3-4 | 4-5 | 5-6 | 6-7 | 7-8 | 8-9 | 9-10 | 10-11 | 11-12 | 12-13 | |
| 0.0-0.5 | 648 | 5105 | 11911 | 15379 | 4812 | 272 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 38135 |
| 0.5-1.0 | 0 | 0 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 29 |
| Total | 648 | 5105 | 11940 | 15379 | 4812 | 272 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 38164 |

Tabel 3.12 Data kejadian gelombang arah WSW

| Cluster: L | Wave Distribution of 100 Years Period | | | | | | | | | | | | | WSW |
|--------------|---------------------------------------|--------------|--------------|--------------|--------------|-------------|------------|-----------|----------|----------|----------|----------|----------|---------------|
| H (meter) | T (second) | | | | | | | | | | | | | Total |
| | 0-1 | 1-2 | 2-3 | 3-4 | 4-5 | 5-6 | 6-7 | 7-8 | 8-9 | 9-10 | 10-11 | 11-12 | 12-13 | |
| 0.0-0.5 | 2536 | 20782 | 41592 | 44241 | 13851 | 2712 | 319 | 21 | 0 | 0 | 0 | 0 | 0 | 126054 |
| 0.5-1.0 | 0 | 12 | 739 | 6320 | 6342 | 1161 | 37 | 1 | 0 | 0 | 0 | 0 | 0 | 14612 |
| 1.0-1.5 | 0 | 0 | 0 | 179 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 179 |
| Total | 2536 | 20794 | 42331 | 50740 | 20193 | 3873 | 356 | 22 | 0 | 0 | 0 | 0 | 0 | 140845 |

Tabel 3.13 Data kejadian gelombang arah W

| Cluster: L | Wave Distribution of 100 Years Period | | | | | | | | | | | | | W |
|--------------|---------------------------------------|---------------|---------------|----------------|---------------|---------------|--------------|-------------|------------|-----------|----------|----------|----------|----------------|
| H (meter) | T (second) | | | | | | | | | | | | | Total |
| | 0-1 | 1-2 | 2-3 | 3-4 | 4-5 | 5-6 | 6-7 | 7-8 | 8-9 | 9-10 | 10-11 | 11-12 | 12-13 | |
| 0.0-0.5 | 44934 | 354641 | 716611 | 770837 | 384059 | 92256 | 17988 | 2647 | 304 | 26 | 3 | 0 | 0 | 2384306 |
| 0.5-1.0 | 0 | 1931 | 49167 | 378204 | 464200 | 211107 | 44513 | 5205 | 372 | 19 | 0 | 0 | 0 | 1154718 |
| 1.0-1.5 | 0 | 1 | 166 | 21180 | 98635 | 60754 | 8282 | 442 | 13 | 0 | 0 | 0 | 0 | 189473 |
| 1.5-2.0 | 0 | 0 | 0 | 406 | 9289 | 7368 | 548 | 6 | 0 | 0 | 0 | 0 | 0 | 17617 |
| 2.0-2.5 | 0 | 0 | 0 | 8 | 484 | 508 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 1020 |
| 2.5-3.0 | 0 | 0 | 0 | 0 | 10 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 42 |
| 3.0-3.5 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| Total | 44934 | 356573 | 765944 | 1170635 | 956677 | 372028 | 71351 | 8300 | 689 | 45 | 3 | 0 | 0 | 3747179 |

Tabel 3.14 Data kejadian gelombang arah WNW

| Cluster: L | Wave Distribution of 100 Years Period | | | | | | | | | | | | | WNW |
|------------|---------------------------------------|--------|--------|--------|--------|--------|-------|------|-----|------|-------|-------|-------|---------|
| H | T (second) | | | | | | | | | | | | | Total |
| (meter) | 0-1 | 1-2 | 2-3 | 3-4 | 4-5 | 5-6 | 6-7 | 7-8 | 8-9 | 9-10 | 10-11 | 11-12 | 12-13 | |
| 0.0-0.5 | 26219 | 207860 | 429647 | 398651 | 152945 | 33163 | 5143 | 490 | 11 | 0 | 0 | 0 | 0 | 1254129 |
| 0.5-1.0 | 0 | 1342 | 34129 | 240103 | 238116 | 76475 | 10298 | 566 | 24 | 0 | 0 | 0 | 0 | 601053 |
| 1.0-1.5 | 0 | 2 | 115 | 15805 | 47876 | 17433 | 1176 | 17 | 0 | 0 | 0 | 0 | 0 | 82424 |
| 1.5-2.0 | 0 | 0 | 0 | 331 | 4117 | 1705 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 6181 |
| 2.0-2.5 | 0 | 0 | 0 | 5 | 188 | 100 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 294 |
| 2.5-3.0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| Total | 26219 | 209204 | 463891 | 654895 | 443245 | 128876 | 16646 | 1073 | 35 | 0 | 0 | 0 | 0 | 1944084 |

Tabel 3.15 Data kejadian gelombang arah NW

| Cluster: L | Wave Distribution of 100 Years Period | | | | | | | | | | | | | NW |
|------------|---------------------------------------|-------|-------|-------|------|-----|-----|-----|-----|------|-------|-------|-------|-------|
| H | T (second) | | | | | | | | | | | | | Total |
| (meter) | 0-1 | 1-2 | 2-3 | 3-4 | 4-5 | 5-6 | 6-7 | 7-8 | 8-9 | 9-10 | 10-11 | 11-12 | 12-13 | |
| 0.0-0.5 | 1533 | 11626 | 23613 | 25264 | 6148 | 292 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 68479 |
| 0.5-1.0 | 0 | 97 | 3666 | 18040 | 3219 | 215 | 20 | 1 | 0 | 0 | 0 | 0 | 0 | 25258 |
| 1.0-1.5 | 0 | 0 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 20 |
| Total | 1533 | 11723 | 27299 | 43304 | 9367 | 507 | 23 | 1 | 0 | 0 | 0 | 0 | 0 | 93757 |

Tabel 3.16 Data kejadian gelombang arah NNW

| Cluster: L | Wave Distribution of 100 Years Period | | | | | | | | | | | | | NNW |
|------------|---------------------------------------|------|-------|------|-----|-----|-----|-----|-----|------|-------|-------|-------|-------|
| H | T (second) | | | | | | | | | | | | | Total |
| (meter) | 0-1 | 1-2 | 2-3 | 3-4 | 4-5 | 5-6 | 6-7 | 7-8 | 8-9 | 9-10 | 10-11 | 11-12 | 12-13 | |
| 0.0-0.5 | 376 | 1048 | 310 | 47 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1782 |
| 0.5-1.0 | 253 | 2407 | 2520 | 703 | 74 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5958 |
| 1.0-1.5 | 38 | 1166 | 3520 | 1977 | 169 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6871 |
| 1.5-2.0 | 1 | 379 | 3116 | 2467 | 128 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6091 |
| 2.0-2.5 | 0 | 85 | 2208 | 1895 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4218 |
| 2.5-3.0 | 0 | 15 | 1242 | 1062 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2323 |
| 3.0-3.5 | 0 | 3 | 575 | 469 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1049 |
| 3.5-4.0 | 0 | 0 | 224 | 166 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 391 |
| 4.0-4.5 | 0 | 0 | 84 | 51 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 135 |
| 4.5-5.0 | 0 | 0 | 16 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 27 |
| 5.0-5.5 | 0 | 0 | 9 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 |
| 5.5-6.0 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 6.0-6.5 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Total | 668 | 5103 | 13828 | 8852 | 409 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 28863 |

Untuk gelombang yang digunakan pada analisa *inplace* disajikan dalam bentuk rangkuman Hs dan Tp setiap arah pembebanan yang dapat dilihat pada Tabel 3.17.

Tabel 3.17 Rangkuman Hs dan Tp setiap arah.

| Return Period | Wave Height (m) and Associated Periods (second) For All Direction (to which) | | | | | | | | | | | | | | | | |
|------------------|--|------|------|------|------|------|-------|-------|------|------|------|------|------|------|------|------|------|
| | Omni | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW |
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 |
| 1-Year | | | | | | | | | | | | | | | | | |
| Hs | 1.94 | 0.34 | 0.32 | 0.26 | 0.50 | 0.40 | 1.94 | 0.65 | 0.39 | 0.40 | 0.33 | 0.40 | 0.60 | 1.55 | 1.29 | 0.53 | 0.37 |
| Tp | 6.54 | 3.07 | 2.97 | 2.98 | 3.48 | 5.31 | 6.54 | 4.70 | 3.25 | 3.31 | 3.25 | 3.23 | 3.53 | 5.84 | 5.20 | 3.28 | 3.17 |
| Tz | 5.09 | 2.39 | 2.31 | 2.32 | 2.71 | 4.13 | 5.09 | 3.66 | 2.53 | 2.57 | 2.53 | 2.51 | 2.75 | 4.54 | 4.04 | 2.55 | 2.47 |
| Hmax | 3.88 | 0.68 | 0.64 | 0.52 | 1.00 | 0.80 | 3.88 | 1.30 | 0.78 | 0.80 | 0.66 | 0.80 | 1.20 | 3.10 | 2.58 | 1.06 | 0.74 |
| Tmax | 5.89 | 2.76 | 2.67 | 2.68 | 3.13 | 4.78 | 5.89 | 4.23 | 2.93 | 2.98 | 2.93 | 2.91 | 3.18 | 5.26 | 4.68 | 2.95 | 2.85 |
| 100-Years | | | | | | | | | | | | | | | | | |
| Hs | 4.74 | 1.30 | 1.55 | 1.75 | 1.81 | 1.35 | 4.74 | 3.86 | 1.25 | 1.41 | 1.40 | 1.35 | 2.38 | 3.07 | 2.16 | 1.46 | 1.23 |
| Tp | 10.12 | 4.65 | 5.61 | 5.55 | 6.28 | 8.63 | 10.12 | 10.05 | 6.22 | 5.25 | 5.24 | 5.53 | 7.97 | 7.95 | 6.97 | 5.66 | 4.41 |
| Tz | 7.87 | 3.62 | 4.36 | 4.32 | 4.88 | 6.71 | 7.87 | 7.82 | 4.84 | 4.08 | 4.07 | 4.30 | 6.20 | 6.18 | 5.42 | 4.40 | 3.43 |
| Hmax | 9.48 | 2.60 | 3.10 | 3.50 | 3.62 | 2.70 | 9.48 | 7.72 | 2.50 | 2.82 | 2.80 | 2.70 | 4.76 | 6.14 | 4.32 | 2.92 | 2.46 |
| Tmax | 9.11 | 4.19 | 5.05 | 5.00 | 5.65 | 7.77 | 9.11 | 9.05 | 5.60 | 4.73 | 4.72 | 4.98 | 7.17 | 7.16 | 6.27 | 5.09 | 3.97 |

Sementara beban arus yang digunakan dalam analisa *inplace* disajikan dalam bentuk rangkuman kecepatan arus pada setiap 10% kedalaman di setiap arah pembebanan seperti yang dapat dilihat pada Tabel 3.18.

Tabel 3.18 Data Arus

| Layers and Distance from Water Surface, z (m) | Current Speed (cm/s) and Direction (to which) | | | | | | | | | | | | | | | | | |
|---|---|--------|-------|-------|-------|-------|--------|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | Omni | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | |
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | |
| 1-Year Return Period | | | | | | | | | | | | | | | | | | |
| Layer 10 - Surface (1.0 D) | 0.00 | 61.93 | 18.99 | 18.90 | 19.75 | 33.99 | 61.93 | 61.72 | 21.24 | 13.08 | 10.04 | 10.12 | 10.40 | 17.85 | 44.98 | 61.33 | 34.83 | 23.98 |
| Layer 9 (0.9 D) | -8.11 | 61.00 | 18.33 | 18.05 | 19.45 | 33.48 | 61.00 | 60.80 | 20.92 | 12.88 | 9.89 | 9.97 | 10.24 | 17.39 | 44.29 | 60.48 | 34.16 | 23.21 |
| Layer 8 (0.8 D) | -12.21 | 59.99 | 18.07 | 18.37 | 19.13 | 32.62 | 59.99 | 59.78 | 20.57 | 12.67 | 9.72 | 9.80 | 10.07 | 17.10 | 43.55 | 59.45 | 33.59 | 22.82 |
| Layer 7 (0.7 D) | -18.32 | 58.85 | 17.73 | 18.06 | 18.77 | 32.30 | 58.85 | 58.65 | 20.18 | 12.43 | 9.54 | 9.62 | 9.88 | 16.77 | 42.73 | 58.33 | 32.98 | 22.39 |
| Layer 6 (0.6 D) | -24.42 | 57.57 | 17.35 | 15.71 | 18.38 | 31.60 | 57.57 | 57.38 | 19.75 | 12.16 | 9.33 | 9.41 | 9.67 | 16.41 | 41.80 | 57.06 | 32.24 | 21.90 |
| Layer 5 - Mid Depth (0.5 D) | -30.53 | 56.09 | 16.90 | 15.31 | 17.89 | 30.79 | 56.09 | 55.90 | 19.24 | 11.85 | 9.09 | 9.17 | 9.42 | 15.99 | 40.72 | 55.59 | 31.41 | 21.34 |
| Layer 4 (0.4 D) | -36.63 | 54.33 | 16.37 | 14.83 | 17.33 | 29.62 | 54.33 | 54.15 | 18.83 | 11.48 | 8.81 | 8.88 | 9.12 | 15.48 | 39.44 | 53.85 | 30.42 | 20.87 |
| Layer 3 (0.3 D) | -42.74 | 52.14 | 15.71 | 14.23 | 16.63 | 28.62 | 52.14 | 51.97 | 17.88 | 11.01 | 8.45 | 8.52 | 8.76 | 14.86 | 37.86 | 51.89 | 29.20 | 19.84 |
| Layer 2 (0.2 D) | -48.84 | 49.21 | 14.83 | 13.43 | 15.69 | 27.01 | 49.21 | 49.04 | 16.88 | 10.39 | 7.98 | 8.04 | 8.28 | 14.02 | 35.73 | 48.77 | 27.98 | 18.72 |
| Layer 1 - Near Bed (0.1 D) | -54.95 | 44.57 | 13.43 | 12.10 | 14.21 | 24.40 | 44.57 | 44.42 | 15.29 | 9.41 | 7.23 | 7.28 | 7.48 | 12.70 | 32.30 | 44.17 | 24.90 | 16.90 |
| (1m ASB) | -60.05 | 38.82 | 11.70 | 10.59 | 12.38 | 21.30 | 38.82 | 38.69 | 13.31 | 8.20 | 6.29 | 6.34 | 6.52 | 11.06 | 28.18 | 38.47 | 21.74 | 14.77 |
| 100-Year Return Period | | | | | | | | | | | | | | | | | | |
| Layer 10 - Surface (1.0 D) | 0.00 | 119.11 | 30.78 | 31.50 | 38.14 | 46.78 | 109.77 | 119.11 | 58.05 | 39.91 | 26.40 | 26.81 | 34.97 | 43.67 | 60.32 | 75.88 | 51.79 | 39.98 |
| Layer 9 (0.9 D) | -8.11 | 117.33 | 30.30 | 31.03 | 37.57 | 46.08 | 108.13 | 117.33 | 57.18 | 39.31 | 28.98 | 29.38 | 34.45 | 43.02 | 59.42 | 74.75 | 51.02 | 39.38 |
| Layer 8 (0.8 D) | -12.21 | 115.37 | 29.79 | 30.51 | 36.94 | 45.31 | 106.33 | 115.37 | 56.23 | 38.66 | 28.48 | 28.87 | 33.87 | 42.30 | 58.43 | 73.50 | 50.17 | 38.71 |
| Layer 7 (0.7 D) | -18.32 | 113.19 | 29.23 | 29.94 | 36.25 | 44.45 | 104.32 | 113.19 | 55.17 | 37.93 | 27.94 | 28.33 | 33.23 | 41.50 | 57.32 | 72.11 | 49.22 | 37.97 |
| Layer 6 (0.6 D) | -24.42 | 110.73 | 28.80 | 29.28 | 35.46 | 43.49 | 102.04 | 110.73 | 53.99 | 37.10 | 27.33 | 27.71 | 32.51 | 40.60 | 56.07 | 70.54 | 48.15 | 37.15 |
| Layer 5 - Mid Depth (0.5 D) | -30.53 | 107.88 | 27.88 | 28.53 | 34.54 | 42.37 | 99.42 | 107.88 | 52.58 | 36.15 | 26.83 | 27.00 | 31.87 | 39.55 | 54.63 | 68.73 | 46.91 | 36.19 |
| Layer 4 (0.4 D) | -36.63 | 104.50 | 26.99 | 27.64 | 33.46 | 41.04 | 98.30 | 104.50 | 50.93 | 35.01 | 25.79 | 26.15 | 30.68 | 38.31 | 52.92 | 66.57 | 45.44 | 35.06 |
| Layer 3 (0.3 D) | -42.74 | 100.29 | 25.90 | 26.52 | 32.11 | 39.39 | 92.42 | 100.29 | 48.88 | 33.60 | 24.75 | 25.10 | 29.44 | 36.77 | 50.79 | 63.89 | 43.81 | 33.85 |
| Layer 2 (0.2 D) | -48.84 | 94.64 | 24.44 | 25.03 | 30.31 | 37.17 | 87.22 | 94.64 | 46.13 | 31.71 | 23.36 | 23.69 | 27.78 | 34.70 | 47.93 | 60.29 | 41.15 | 31.75 |
| Layer 1 - Near Bed (0.1 D) | -54.95 | 85.72 | 22.14 | 22.87 | 27.45 | 33.67 | 79.00 | 85.72 | 41.78 | 28.72 | 21.16 | 21.45 | 25.17 | 31.43 | 43.41 | 54.61 | 37.27 | 28.78 |
| (1m ASB) | -60.05 | 74.66 | 19.23 | 19.74 | 23.91 | 29.32 | 68.80 | 74.66 | 36.39 | 25.02 | 18.43 | 18.68 | 21.92 | 27.37 | 37.81 | 47.56 | 32.46 | 25.05 |

3.2.3 Pemodelan Struktur Jacket 3 Kaki Modifikasi

Pemodelan struktur *jacket* 3 kaki modifikasi menggunakan *software* SACS berdasarkan data struktur yang telah didapat. Pemodelan struktur ini nantinya menjadi data awal umur kelelahan yang akan dianalisa sebelum didesain ulang pada bagian *jacket*.

3.2.4 Pemodelan Struktur Jacket 3 Kaki Konvensional

Sebagaimana tujuan dari tugas akhir ini yaitu mengetahui perbandingan umur kelelahan struktur *jacket* 3 kaki modifikasi dan konvensional, maka diperlukan pembandingan kedua yaitu struktur *jacket* 3 kaki model konvensional. Pada tahap ini pemodelan tidak merubah ukuran dari *member*, melainkan hanya merubah konfigurasi *jacket leg* dan *bracing* untuk membatasi desain agar pembandingan setara.

3.2.5 Analisa *Inplace* Dengan Software SACS

Analisa kekuatan statis menggunakan model *jacket* konvensional, pada tahap ini konfigurasi *bracing* akan diubah jika mengalami kegagalan pada hasil analisisnya. Tahap ini mensimulasikan keadaan struktur saat sedang beroperasi dengan semua beban mati, beban hidup, dan beban lingkungan yang bekerja. Alur pengerjaan tahap ini dapat dilihat pada Tabel 3.19.

Tabel 3.19 Alur pengerjaan analisa *inplace*

| SACS | Tipe Analisa | Hasil |
|----------------|-----------------------|-----------------|
| <i>Inplace</i> | Basic Static Analysis | Kekuatan Statis |

Tahap analisa *inplace* memerlukan *file* model (*sacinp.*) sebagai objek analisa yang berisi model *jacket* serta beban mati dan beban hidup, *seastate* (*seainp.*) sebagai beban lingkungan meliputi gelombang, arus, serta beban kombinasi yang sudah difaktorkan untuk kondisi operasi dan kondisi badai, dan *joint can* (*jcninp.*) sebagai *input* daftar *joint* yang dipilih untuk dianalisa. *Output* dari analisa ini adalah kekuatan statis berupa *common solution file* (*sacssf.*) yang dapat dilihat pada *file postvue database* (*psvdb*), *file* ini menunjukkan warna pada tiap member yang mengindikasikan *unity check*.

3.2.6 Analisa *Fatigue* Dengan Software SACS

Tahap lanjutan dari analisa sebelumnya, analisa kekuatan dinamis pertama menyertakan beban lingkungan lain untuk menjalankan analisisnya. Pada tahap ini akan menggunakan metode analisa umur kelelahan yaitu *spectral analysis*. Dari analisa ini akan didapat umur kelelahan pada setiap *joint* dan akan diketahui mana *joint* yang tidak memenuhi umur desain. Alur pengerjaan tahap ini dapat dilihat pada Tabel 3.20.

Tabel 3.20 Alur pengerjaan analisa *fatigue*

| SACS | Tipe Analisa | Hasil |
|-----------------------------|------------------------|--------------------------------|
| PSI (Pile Soil Interaction) | Linearisasi Pondasi | Pile Superelement |
| DYNPAC | Modal Analysis | - Mode Shapes - Mode Matrix |
| Wave Response | Wave Response Analysis | Common Solution Files |
| Fatigue | Fatigue Analysis | Fatigue Results |

a. PSI (Pile Soil Interaction)

Dari *jacket* yang sudah dimodelkan maka perlu dilakukan analisa PSI untuk mendapatkan berapa beban yang bergerak dengan tumpuan *pilehead*. Analisa ini memerlukan *file* model (*sacinp.*) dan *file pile soil interaction* (*psiinp.*) untuk di-*run* dan menghasilkan *output superelement* (*dynsef.*).

b. DYNPAC

Menggunakan *file dynsef.* dari analisis sebelumnya dan model (*sacinp.*) untuk analisis dinamis (mode shape) untuk menghasilkan mode dinamis (*dynmod.*) dan massa dinamis (*dynmas.*). Pada tahap ini juga bisa didapatkan periode natural struktur pada mode dinamis 1 yang tercantum pada *file dynlst.*

c. Wave Response

Memasukan *file dynmod.* dan *dynmas.*, *file* model (*sacinp.*) dan *file wvrinp.* yang berisi jumlah *wave step* dan faktor redaman yang akan menghasilkan fungsi transfer berupa *base shear*, *overturning moment* dan *common solution file* (*saccsf.*)

d. Fatigue

Memasukan *file fatigue input* (*figinp.*) yang berisi umur rencana operasi, *safety factor*, jumlah kejadian gelombang dan lainnya. Selain itu, perlu *pile superelement*, *mode shapes*, fungsi transfer, *common solution files* dari *wave response analysis*, Mode Matrix 30 memasukan *file common solution file* (*saccsf.*) untuk masing-masing arah gelombang dan menghasilkan *file fatigue list* (*figlst.*) yang berisi hasil analisa *fatigue* secara rinci berupa *stress concentration factor*, *damage*, dan umur kelelahan dalam satuan tahun.

3.2.7 Kesimpulan dan Saran

Kesimpulan memuat hasil analisa mulai dari periode natural hingga umur kelelahan masing-masing struktur dengan metode *spectral analysis* Pada tahap ini juga akan dilampirkan hasil perbandingan perkiraan harga, metode fabrikasi, dan metode instalasi yang digunakan oleh masing-masing struktur.

3.3 Rencana Kegiatan Tugas Akhir

Berikut merupakan rencana pengerjaan tugas akhir dimulai dari studi literatur hingga pengumpulan laporan tugas akhir yang dapat dilihat pada Tabel 3.21.

Tabel 3.21 Rencana pengerjaan tugas akhir

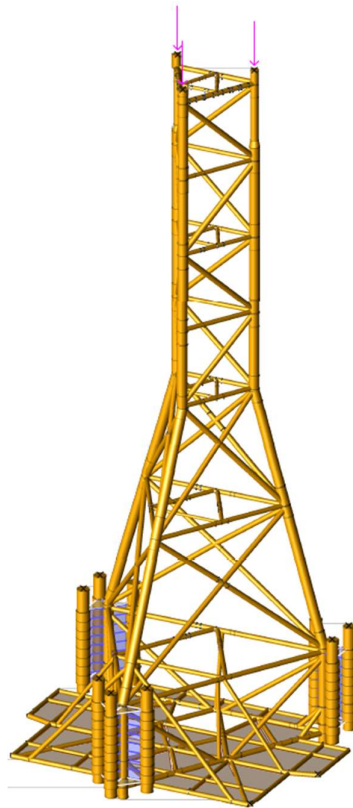
| Nama Kegiatan | Bulan | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|---|----------|---|---|---|-------|---|---|---|-------|---|---|---|-----|---|---|---|------|---|---|---|------|---|---|---|---|---|---|---|--|--|--|--|
| | Februari | | | | Maret | | | | April | | | | Mei | | | | Juni | | | | Juli | | | | | | | | | | | |
| | Minggu | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 1 | 2 | 3 | 4 | 1 | 2 | 3 | 4 | 1 | 2 | 3 | 4 | 1 | 2 | 3 | 4 | 1 | 2 | 3 | 4 | 1 | 2 | 3 | 4 | 1 | 2 | 3 | 4 | | | | |
| Studi literature | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | | | | |
| Pembuatan Laporan | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | | | | | | | | |
| Sidang Proposal (P1) | | | | | | | ■ | | | | | | | | | | | | | | | | | | | | | | | | | |
| Pengumpulan data | | | | | | | | ■ | | | | | | | | | | | | | | | | | | | | | | | | |
| Pemodelan <i>jacket</i> 3 kaki modifikasi | | | | | | | | | ■ | | | | | | | | | | | | | | | | | | | | | | | |
| Analisa <i>fatigue</i> menggunakan <i>software</i> SACS | | | | | | | | | | ■ | | | | | | | | | | | | | | | | | | | | | | |
| Sidang progres penelitian (P2) | | | | | | | | | | | ■ | | | | | | | | | | | | | | | | | | | | | |
| Pemodelan <i>jacket</i> 3 kaki konvensional | | | | | | | | | | | | ■ | ■ | ■ | ■ | ■ | | | | | | | | | | | | | | | | |
| Analisa inplace | | | | | | | | | | | | | | | ■ | | | | | | | | | | | | | | | | | |
| Analisa <i>fatigue</i> menggunakan <i>software</i> SACS | | | | | | | | | | | | | | | | ■ | ■ | ■ | ■ | ■ | | | | | | | | | | | | |
| Penyusunan laporan akhir | | | | | | | | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | ■ | | | | | | | | |
| Seminar tugas akhir | | | | | | | | | | | | | | | | | | | | | | | | | | | ■ | | | | | |
| Sidang akhir (P3) | | | | | | | | | | | | | | | | | | | | | | | | | | | ■ | | | | | |
| Pengumpulan laporan tugas akhir | | | | | | | | | | | | | | | | | | | | | | | | | | | ■ | ■ | | | | |

BAB IV

ANALISA DAN PEMBAHASAN

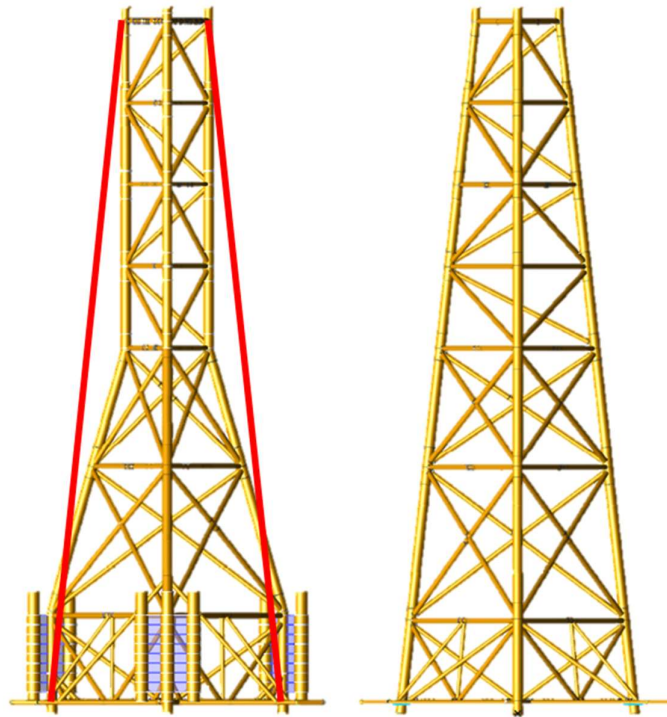
4.1 Pemodelan *Jacket* 3 Kaki Modifikasi dan Konvensional

Pemodelan *jacket* 3 kaki modifikasi menggunakan *software* SACS 5.6 menggunakan data dari struktur milik Husky-CNOOC Madura Limited (HCML). Pada pengerjaan penelitian ini, *jacket* 3 kaki modifikasi hanya dimodelkan bagian kaki dengan bagian *topside* dimodelkan sebagai beban *joint* pada ujung atas kaki letak elevasi *working point*. Hasil pemodelan dapat dilihat pada Gambar 4.1 di bawah.

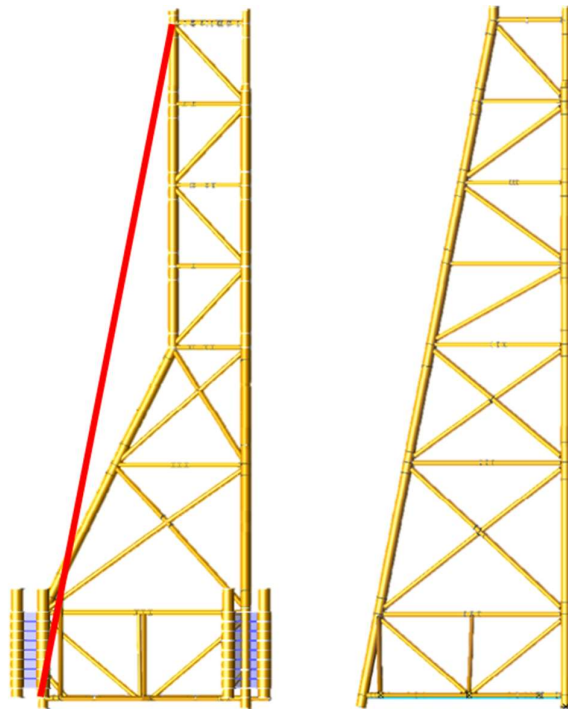


Gambar 4.1 *Jacket* 3 kaki modifikasi dengan beban *topside*

Ada pun *jacket* 3 kaki konvensional difungsikan sebagai struktur pembanding. Agar kedua struktur dapat dikatakan sebanding maka dasar desain pada pemodelan *jacket* konvensional ini mengacu pada 2 aspek yang ada pada *jacket* modifikasi yang meliputi jumlah elevasi dan *material properties*. Kemiringan kaki pada *jacket* ini diambil dari garis lurus antara *joint* di ujung setiap kaki pada elevasi (+) 30' ft hingga (-) 261' 7 5/16" ft. Sedangkan jumlah dan model pondasi pada *jacket* konvensional dibuat berbeda mengacu pada desain pondasi *jacket* konvensional pada umumnya yang berada di dalam kaki dari *jacket*. Berikut ilustrasinya :

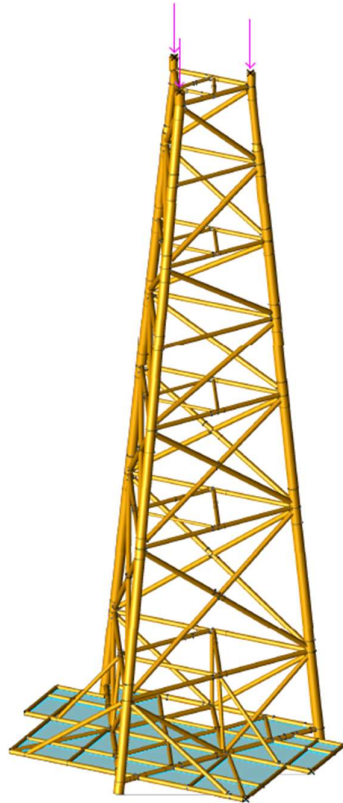


Gambar 4.2 Ilustrasi penentuan *batter jacket* konvensional



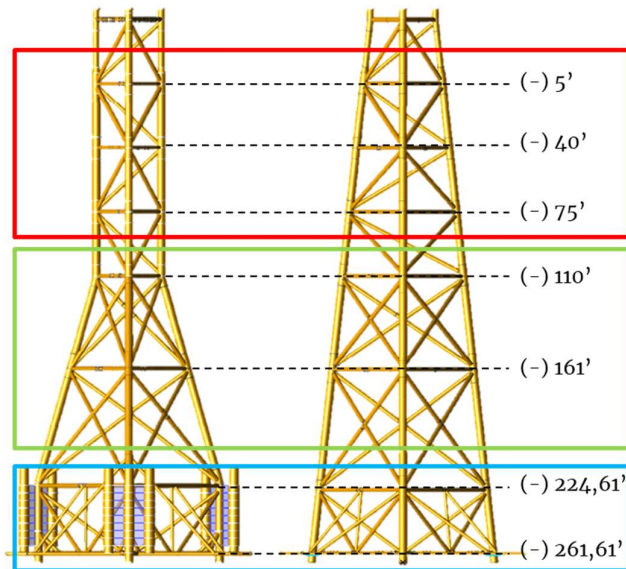
Gambar 4.3 Ilustrasi penentuan *batter jacket* konvensional (lanjutan)

Dengan pengambilan *batter* sesuai pada Gambar 4.2 dan Gambar 4.3 maka hasil pemodelan *jacket* 3 kaki konvensional didapatkan seperti pada Gambar 4.4.



Gambar 4.4 Jacket 3 kaki konvensional dengan beban *topside*.

Selanjutnya untuk mempermudah maka elevasi dari kedua *jacket* dibagi menjadi 3 bagian yaitu *top* (elevasi -5', -40', dan -75'), *middle* (elevasi -110' dan 161'), dan *bottom* (224,61' dan 261,61') seperti pada Gambar 4.5.



Gambar 4.5 Pembagian elevasi

4.2 Analisa *Inplace* Dengan *Software* SACS

Analisa pada tahap ini dilakukan pada kedua model *jacket* untuk mengetahui apakah desain kaki dengan jumlah elevasi dan *material properties* yang sama dengan konfigurasi yang berbeda masih dapat menahan beban yang berkerja pada kaki *jacket* meliputi *selfweight*, beban lingkungan, serta beban *topside*.

4.2.1 Pengolahan Data Lingkungan

Pada tahap analisa *inplace* beban lingkungan yang digunakan meliputi beban gelombang, beban arus, dan beban angin, namun pada penelitian ini beban angin tidak dijadikan pertimbangan dikarenakan tidak adanya member penghalang yang dapat dikenai angin. Sementara kala ulang yang digunakan adalah 1 tahun untuk kondisi operasi dan 100 tahun untuk kondisi badai.

Pada penggunaan data gelombang diperlukan perhitungan untuk menentukan teori gelombang yang tepat diaplikasikan pada kondisi lingkungan yang ada dengan langkah pertama menentukan *apparent wave period* (T_{app}) dibantu grafik *doppler shift due to steady current*. Hasil perhitungan ini dapat dilihat pada Tabel 4.1 dan Tabel 4.2.

Tabel 4.1 Perhitungan *apparent wave period* kondisi operasi

| Operating Condition | | | | | | |
|---------------------|-------|-------------|----------|----------|-------------|---------------|
| Direction | T (s) | V_i (m/s) | d/gT^2 | V_i/gT | T_{app}/T | T_{app} (s) |
| Omni | 6,54 | 0,619 | 0,190 | 0,010 | 1,06 | 6,932 |
| N | 3,31 | 0,100 | 0,742 | 0,003 | 1,02 | 3,376 |
| NNE | 3,25 | 0,101 | 0,769 | 0,003 | 1,02 | 3,315 |
| NE | 3,23 | 0,104 | 0,779 | 0,003 | 1,02 | 3,295 |
| ENE | 3,53 | 0,177 | 0,652 | 0,005 | 1,03 | 3,636 |
| E | 5,84 | 0,450 | 0,238 | 0,008 | 1,05 | 6,132 |
| ESE | 5,20 | 0,614 | 0,301 | 0,012 | 1,07 | 5,564 |
| SE | 3,28 | 0,347 | 0,755 | 0,011 | 1,06 | 3,477 |
| SSE | 3,17 | 0,236 | 0,809 | 0,008 | 1,05 | 3,329 |
| S | 3,07 | 0,187 | 0,862 | 0,006 | 1,04 | 3,193 |
| SSW | 2,97 | 0,169 | 0,921 | 0,006 | 1,04 | 3,089 |
| SW | 2,98 | 0,198 | 0,915 | 0,007 | 1,045 | 3,114 |
| WSW | 3,48 | 0,340 | 0,671 | 0,010 | 1,06 | 3,689 |
| W | 5,31 | 0,619 | 0,288 | 0,012 | 1,07 | 5,682 |
| WNW | 6,54 | 0,617 | 0,190 | 0,010 | 1,06 | 6,932 |
| NW | 4,70 | 0,212 | 0,368 | 0,005 | 1,03 | 4,841 |
| NNW | 3,25 | 0,131 | 0,769 | 0,004 | 1,025 | 3,331 |

Tabel 4.2 Perhitungan *apparent wave period* kondisi badai

| Storm Condition | | | | | | |
|-----------------|-------|----------------------|-------------------|--------------------|---------------------|----------------------|
| Direction | T (s) | V _i (m/s) | d/gT ² | V _i /gT | T _{app} /T | T _{app} (s) |
| Omni | 10,12 | 1,191 | 0,079 | 0,012 | 1,075 | 10,879 |
| N | 5,25 | 0,294 | 0,295 | 0,006 | 1,04 | 5,460 |
| NNE | 5,24 | 0,298 | 0,296 | 0,006 | 1,04 | 5,450 |
| NE | 5,53 | 0,350 | 0,266 | 0,006 | 1,04 | 5,751 |
| ENE | 7,97 | 0,437 | 0,128 | 0,006 | 1,04 | 8,289 |
| E | 7,95 | 0,603 | 0,129 | 0,008 | 1,048 | 8,332 |
| ESE | 6,97 | 0,759 | 0,167 | 0,011 | 1,065 | 7,423 |
| SE | 5,66 | 0,518 | 0,254 | 0,009 | 1,05 | 5,943 |
| SSE | 4,41 | 0,400 | 0,418 | 0,009 | 1,05 | 4,631 |
| S | 4,65 | 0,308 | 0,376 | 0,007 | 1,045 | 4,859 |
| SSW | 5,61 | 0,315 | 0,258 | 0,006 | 1,04 | 5,834 |
| SW | 5,55 | 0,381 | 0,264 | 0,007 | 1,045 | 5,800 |
| WSW | 6,28 | 0,468 | 0,206 | 0,008 | 1,048 | 6,581 |
| W | 8,63 | 1,098 | 0,109 | 0,013 | 1,075 | 9,277 |
| WNW | 10,12 | 1,191 | 0,079 | 0,012 | 1,075 | 10,879 |
| NW | 10,05 | 0,581 | 0,080 | 0,006 | 1,045 | 10,502 |
| NNW | 6,22 | 0,399 | 0,210 | 0,007 | 1,045 | 6,500 |

Setelah diketahui nilai dari *apparent wave period* maka dapat dilanjutkan dengan menentukan teori gelombang yang akan dipakai dengan plot parameter d/gT_{app}^2 dan H/gT_{app}^2 ke grafik *region of applicability* untuk diambil titik perpotongannya. Hasil perhitungan ini dapat dilihat pada Tabel 4.3 dan Tabel 4.4.

Tabel 4.3 Penentuan teori gelombang kondisi operasi

| Operating Condition | | | | | | |
|---------------------|--------|---------|----------------------|----------------------------------|----------------------------------|------------|
| Direction | Hs (m) | Hs (ft) | T _{app} (s) | H/gT _{app} ² | d/gT _{app} ² | Teori Gel. |
| Omni | 1,94 | 6,37 | 6,932 | 0,004 | 0,169 | Stokes 5 |
| N | 0,40 | 1,31 | 3,376 | 0,004 | 0,713 | Stokes 5 |
| NNE | 0,33 | 1,08 | 3,315 | 0,003 | 0,740 | Stokes 5 |
| NE | 0,40 | 1,31 | 3,295 | 0,004 | 0,749 | Stokes 5 |
| ENE | 0,60 | 1,97 | 3,636 | 0,005 | 0,615 | Stokes 5 |
| E | 1,55 | 5,09 | 6,132 | 0,004 | 0,216 | Stokes 5 |
| ESE | 1,29 | 4,23 | 5,564 | 0,004 | 0,263 | Stokes 5 |
| SE | 0,53 | 1,74 | 3,477 | 0,004 | 0,672 | Stokes 5 |
| SSE | 0,37 | 1,21 | 3,329 | 0,003 | 0,734 | Stokes 5 |
| S | 0,34 | 1,12 | 3,193 | 0,003 | 0,797 | Stokes 5 |
| SSW | 0,32 | 1,05 | 3,089 | 0,003 | 0,852 | Stokes 5 |
| SW | 0,26 | 0,85 | 3,114 | 0,003 | 0,838 | Stokes 5 |
| WSW | 0,50 | 1,64 | 3,689 | 0,004 | 0,597 | Stokes 5 |
| W | 0,40 | 1,31 | 5,682 | 0,001 | 0,252 | Stokes 5 |
| WNW | 1,94 | 6,37 | 6,932 | 0,004 | 0,169 | Stokes 5 |
| NW | 0,65 | 2,13 | 4,841 | 0,003 | 0,347 | Stokes 5 |
| NNW | 0,39 | 1,28 | 3,331 | 0,004 | 0,732 | Stokes 5 |

Tabel 4.4 Penentuan teori gelombang kondisi badai

| Storm Condition | | | | | | |
|-----------------|--------|---------|----------|----------------------|----------------------|------------|
| Direction | Hs (m) | Hs (ft) | Tapp (s) | H/gTapp ² | d/gTapp ² | Teori Gel. |
| Omni | 4,74 | 15,55 | 10,879 | 0,004 | 0,069 | Stokes 5 |
| N | 1,41 | 4,63 | 5,460 | 0,005 | 0,273 | Stokes 5 |
| NNE | 1,40 | 4,59 | 5,450 | 0,005 | 0,274 | Stokes 5 |
| NE | 1,35 | 4,43 | 5,751 | 0,004 | 0,246 | Stokes 5 |
| ENE | 2,38 | 7,81 | 8,289 | 0,004 | 0,118 | Stokes 5 |
| E | 3,07 | 10,07 | 8,332 | 0,005 | 0,117 | Stokes 5 |
| ESE | 2,16 | 7,09 | 7,423 | 0,004 | 0,147 | Stokes 5 |
| SE | 1,46 | 4,79 | 5,943 | 0,004 | 0,230 | Stokes 5 |
| SSE | 1,23 | 4,04 | 4,631 | 0,006 | 0,379 | Stokes 5 |
| S | 1,30 | 4,27 | 4,859 | 0,006 | 0,344 | Stokes 5 |
| SSW | 1,55 | 5,09 | 5,834 | 0,005 | 0,239 | Stokes 5 |
| SW | 1,75 | 5,74 | 5,800 | 0,005 | 0,242 | Stokes 5 |
| WSW | 1,81 | 5,94 | 6,581 | 0,004 | 0,188 | Stokes 5 |
| W | 1,35 | 4,43 | 9,277 | 0,002 | 0,094 | Stokes 5 |
| WNW | 4,74 | 15,55 | 10,879 | 0,004 | 0,069 | Stokes 5 |
| NW | 3,86 | 12,66 | 10,502 | 0,004 | 0,074 | Stokes 5 |
| NNW | 1,25 | 4,10 | 6,500 | 0,003 | 0,192 | Stokes 5 |

Dari hasil perhitungan dapat diketahui jika teori gelombang yang dapat diaplikasikan adalah Stokes orde 5, dengan begitu *input* perhitungan beban gelombang dapat mengaplikasikan teori Stokes orde 5.

Sementara *input* perhitungan beban arus dapat langsung dimasukkan dengan penyesuaian kecepatan arus pada setiap ketinggian yang tertera pada data di Tabel 4.5.

Tabel 4.5 Kecepatan arus pada setiap kedalaman di setiap arah.

| Layers and Distance from Water Surface, z (m) | Current Speed (cm/s) and Direction (to which) | | | | | | | | | | | | | | | | | |
|---|---|--------|-------|-------|-------|-------|--------|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | Omni | N | NNE | NE | ENE | E | ESE | SE | SSE | S | SSW | SW | WSW | W | WNW | NW | NNW | |
| Water Depth (m) = 61.05 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | |
| 1-Year Return Period | | | | | | | | | | | | | | | | | | |
| Layer 10 - Surface (1.0 D) | 0.00 | 61.93 | 18.66 | 10.90 | 19.75 | 33.99 | 61.93 | 61.72 | 21.24 | 13.08 | 10.04 | 10.12 | 10.40 | 17.65 | 44.96 | 61.38 | 34.63 | 23.56 |
| Layer 9 (0.6 D) | -6.11 | 61.00 | 18.38 | 10.65 | 19.45 | 33.48 | 61.00 | 60.80 | 20.92 | 12.88 | 9.89 | 9.97 | 10.24 | 17.39 | 44.29 | 60.46 | 34.10 | 23.21 |
| Layer 8 (0.8 D) | -12.21 | 59.99 | 18.07 | 10.37 | 19.15 | 32.62 | 59.99 | 59.78 | 20.57 | 12.67 | 9.72 | 9.80 | 10.07 | 17.10 | 43.55 | 59.45 | 33.59 | 22.82 |
| Layer 7 (0.7 D) | -18.32 | 58.85 | 17.73 | 10.06 | 18.77 | 32.30 | 58.85 | 58.65 | 20.18 | 12.43 | 9.54 | 9.62 | 9.88 | 16.77 | 42.73 | 58.33 | 32.90 | 22.39 |
| Layer 6 (0.6 D) | -24.42 | 57.57 | 17.35 | 15.71 | 18.36 | 31.60 | 57.57 | 57.38 | 19.75 | 12.16 | 9.33 | 9.41 | 9.67 | 16.41 | 41.80 | 57.09 | 32.24 | 21.90 |
| Layer 5 - Mid Depth (0.5 D) | -30.53 | 56.09 | 16.90 | 15.31 | 17.89 | 30.79 | 56.09 | 55.90 | 19.24 | 11.85 | 9.09 | 9.17 | 9.42 | 15.99 | 40.72 | 55.59 | 31.41 | 21.34 |
| Layer 4 (0.4 D) | -36.63 | 54.33 | 16.37 | 14.83 | 17.33 | 29.82 | 54.33 | 54.15 | 18.63 | 11.48 | 8.81 | 8.89 | 9.12 | 15.48 | 39.44 | 53.85 | 30.42 | 20.87 |
| Layer 3 (0.3 D) | -42.74 | 52.14 | 15.71 | 14.23 | 16.63 | 28.82 | 52.14 | 51.97 | 17.88 | 11.01 | 8.45 | 8.52 | 8.76 | 14.86 | 37.86 | 51.68 | 29.20 | 19.84 |
| Layer 2 (0.2D) | -48.84 | 49.21 | 14.83 | 13.43 | 15.69 | 27.01 | 49.21 | 49.04 | 16.88 | 10.39 | 7.98 | 8.04 | 8.26 | 14.02 | 35.73 | 48.77 | 27.50 | 18.72 |
| Layer 1 - Near Bed (0.1 D) | -54.95 | 44.57 | 13.43 | 12.10 | 14.21 | 24.46 | 44.57 | 44.42 | 15.29 | 9.41 | 7.23 | 7.28 | 7.48 | 12.70 | 32.36 | 44.17 | 24.90 | 16.90 |
| (1m ASB) | -60.05 | 38.82 | 11.70 | 10.59 | 12.38 | 21.30 | 38.82 | 38.69 | 13.31 | 8.20 | 6.26 | 6.34 | 6.52 | 11.06 | 28.18 | 38.47 | 21.74 | 14.77 |
| 100-Year Return Period | | | | | | | | | | | | | | | | | | |
| Layer 10 - Surface (1.0 D) | 0.00 | 119.11 | 30.79 | 31.50 | 38.14 | 46.76 | 109.77 | 119.11 | 58.05 | 39.91 | 29.40 | 29.81 | 34.97 | 43.67 | 60.32 | 75.88 | 51.79 | 39.90 |
| Layer 9 (0.6 D) | -6.11 | 117.33 | 30.30 | 31.03 | 37.57 | 46.08 | 108.13 | 117.33 | 57.18 | 39.31 | 28.96 | 29.36 | 34.45 | 43.02 | 59.42 | 74.75 | 51.02 | 39.38 |
| Layer 8 (0.8 D) | -12.21 | 115.37 | 29.79 | 30.51 | 36.94 | 45.31 | 106.33 | 115.37 | 56.23 | 38.66 | 28.48 | 28.87 | 33.87 | 42.30 | 58.43 | 73.50 | 50.17 | 38.71 |
| Layer 7 (0.7 D) | -18.32 | 113.19 | 29.23 | 29.94 | 36.25 | 44.48 | 104.32 | 113.19 | 55.17 | 37.93 | 27.94 | 28.33 | 33.23 | 41.50 | 57.32 | 72.11 | 49.22 | 37.97 |
| Layer 6 (0.6 D) | -24.42 | 110.73 | 28.69 | 29.28 | 35.46 | 43.49 | 102.04 | 110.73 | 53.96 | 37.10 | 27.33 | 27.71 | 32.51 | 40.60 | 56.07 | 70.54 | 48.15 | 37.15 |
| Layer 5 - Mid Depth (0.5 D) | -30.53 | 107.88 | 27.86 | 28.53 | 34.54 | 42.37 | 99.42 | 107.88 | 52.58 | 36.15 | 26.63 | 27.00 | 31.67 | 39.55 | 54.63 | 68.73 | 46.91 | 36.19 |
| Layer 4 (0.4 D) | -36.63 | 104.50 | 26.99 | 27.64 | 33.46 | 41.04 | 96.30 | 104.50 | 50.93 | 35.01 | 25.79 | 26.15 | 30.68 | 38.31 | 52.92 | 66.57 | 45.44 | 35.06 |
| Layer 3 (0.3 D) | -42.74 | 100.26 | 25.90 | 26.52 | 32.11 | 39.39 | 92.42 | 100.26 | 48.88 | 33.60 | 24.75 | 25.10 | 29.44 | 36.77 | 50.79 | 63.89 | 43.81 | 33.65 |
| Layer 2 (0.2D) | -48.84 | 94.84 | 24.44 | 25.03 | 30.31 | 37.17 | 87.22 | 94.84 | 46.13 | 31.71 | 23.36 | 23.69 | 27.79 | 34.70 | 47.93 | 60.29 | 41.15 | 31.75 |
| Layer 1 - Near Bed (0.1 D) | -54.95 | 85.72 | 22.14 | 22.67 | 27.45 | 33.67 | 79.00 | 85.72 | 41.78 | 28.72 | 21.16 | 21.45 | 25.17 | 31.43 | 43.41 | 54.81 | 37.27 | 28.76 |
| (1m ASB) | -60.05 | 74.66 | 19.28 | 19.74 | 23.91 | 29.32 | 68.80 | 74.66 | 36.39 | 25.02 | 18.43 | 18.68 | 21.62 | 27.37 | 37.81 | 47.50 | 32.46 | 25.05 |

4.2.2 Kombinasi Beban

Dari beban lingkungan, *selfweight*, dan beban bangunan atas yang ada maka dibuat kombinasi beban setiap arah dengan 2 kondisi operasi dengan kode 8 dan 0, dan badai dengan kode 9 dan 1 dengan mengaplikasikan faktor kontingensi untuk setiap beban. Kombinasi beban dan faktor kontingensi yang diaplikasikan dapat dilihat pada Tabel 4.6 dan Tabel 4.7.

Tabel 4.6 Kombinasi beban operasi

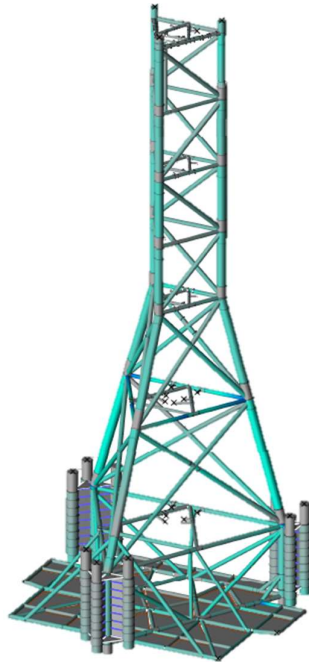
| Load Comb. | Load Cond. Operation | | |
|------------|----------------------|---------------|---------------|
| | Factor = 1 | Factor = 1,07 | Factor = 1,07 |
| 8N | 0N | SELF | TOPS |
| 8NNE | 0NNE | SELF | TOPS |
| 8NE | 0NE | SELF | TOPS |
| 8ENE | 0ENE | SELF | TOPS |
| 8E | 0E | SELF | TOPS |
| 8ESE | 0ESE | SELF | TOPS |
| 8SE | 0SE | SELF | TOPS |
| 8SSE | 0SSE | SELF | TOPS |
| 8S | 0S | SELF | TOPS |
| 8SSW | 0SSW | SELF | TOPS |
| 8SW | 0SW | SELF | TOPS |
| 8WSW | 0WSW | SELF | TOPS |
| 8W | 0W | SELF | TOPS |
| 8WNW | 0WNW | SELF | TOPS |
| 8NW | 0NW | SELF | TOPS |
| 8NNW | 0NNW | SELF | TOPS |

Tabel 4.7 Kombinasi beban badai

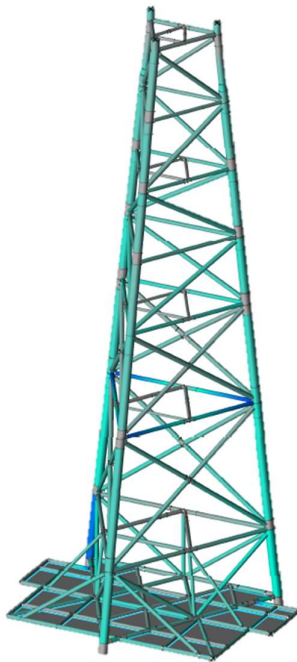
| Load Comb. | Load Cond. Storm | | |
|------------|------------------|---------------|---------------|
| | Factor = 1 | Factor = 1,07 | Factor = 1,07 |
| 9N | 1N | SELF | TOPS |
| 9NNE | 1NNE | SELF | TOPS |
| 9NE | 1NE | SELF | TOPS |
| 9ENE | 1ENE | SELF | TOPS |
| 9E | 1E | SELF | TOPS |
| 9ESE | 1ESE | SELF | TOPS |
| 9SE | 1SE | SELF | TOPS |
| 9SSE | 1SSE | SELF | TOPS |
| 9S | 1S | SELF | TOPS |
| 9SSW | 1SSW | SELF | TOPS |
| 9SW | 1SW | SELF | TOPS |
| 9WSW | 1WSW | SELF | TOPS |
| 9W | 1W | SELF | TOPS |
| 9WNW | 1WNW | SELF | TOPS |
| 9NW | 1NW | SELF | TOPS |
| 9NNW | 1NNW | SELF | TOPS |

4.2.3 Hasil Analisa *Inplace*

Dari analisa *inplace* yang telah dilakukan pada kedua model *jacket*, maka didapatkan hasil seperti pada Gambar 4.6 dan Gambar 4.7.



Gambar 4.6 Hasil analisa *inplace jacket* modifikasi



Gambar 4.7 Hasil analisa *inplace jacket* konvensional

Dari hasil di atas tercatat jika UC terbesar yang dialami oleh *jacket* modifikasi adalah sebesar 0,225 pada *member* 0055 – 0101. Sementara UC terbesar yang dialami *jacket* konvensional adalah sebesar 0,285 pada *member* 0070 – 0114. Dari hasil tersebut maka dapat dikatakan jika kedua model *jacket* dengan konfigurasi kaki yang berbeda di atas memenuhi syarat dikarenakan hasil UC *checking* terbesar bernilai kurang dari 1.

4.3 Analisa Fatigue Dengan Software SACS

4.3.1 Periode dan Frekuensi Natural

Periode natural adalah faktor utama yang harus diketahui untuk analisis kelelahan bangunan lepas pantai. Berikut ini adalah hasil perhitungan periode natural menggunakan *software finite element method* untuk 5 *mode shape* pertama untuk kedua struktur yang ditunjukkan pada Tabel 4.8 untuk *jacket* modifikasi dan Tabel 4.9 untuk *jacket* konvensional.

Tabel 4.8 5 *mode shape* pertama *jacket* modifikasi

| Jacket Modifikasi | | | | |
|-------------------|------------|-----------|------------|--------------|
| MODE | FREQ.(CPS) | GEN. MASS | EIGENVALUE | PERIOD(SECS) |
| 1 | 0,570 | 1,58E+11 | 7,81E+05 | 1,756 |
| 2 | 0,576 | 1,44E+11 | 7,64E+05 | 1,737 |
| 3 | 0,951 | 1,45E+11 | 2,80E+05 | 1,052 |
| 4 | 1,652 | 1,35E+10 | 9,28E+04 | 0,605 |
| 5 | 1,675 | 8,25E+09 | 9,03E+04 | 0,597 |

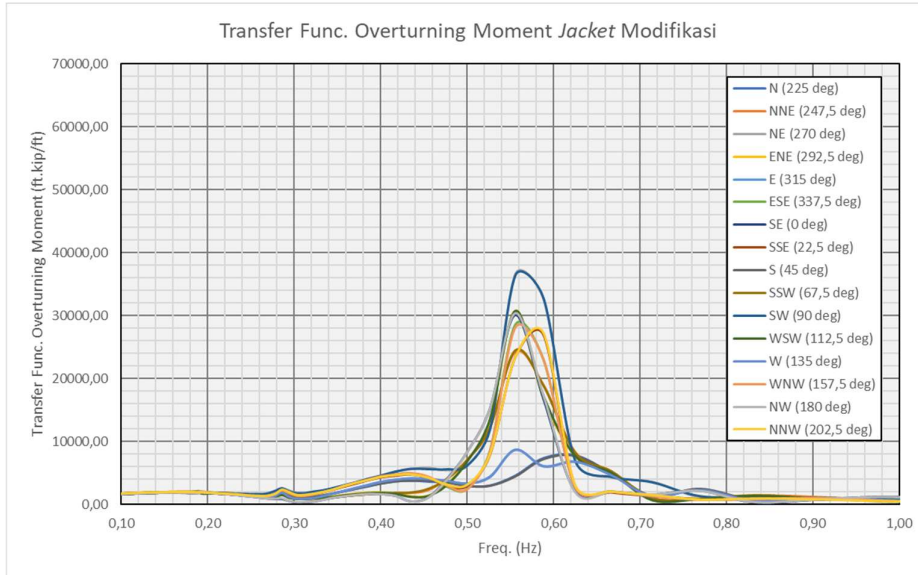
Tabel 4.9 5 *mode shape* pertama *jacket* konvensional

| Jacket Konvensional | | | | |
|---------------------|------------|-----------|------------|---------------|
| MODE | FREQ.(CPS) | GEN. MASS | EIGENVALUE | PERIOD (SECS) |
| 1 | 0,679 | 1,71E+11 | 5,49E+05 | 1,472 |
| 2 | 0,684 | 1,68E+11 | 5,41E+05 | 1,461 |
| 3 | 1,065 | 2,23E+11 | 2,23E+05 | 0,939 |
| 4 | 1,948 | 2,23E+11 | 6,68E+04 | 0,513 |
| 5 | 1,979 | 2,75E+11 | 6,47E+04 | 0,505 |

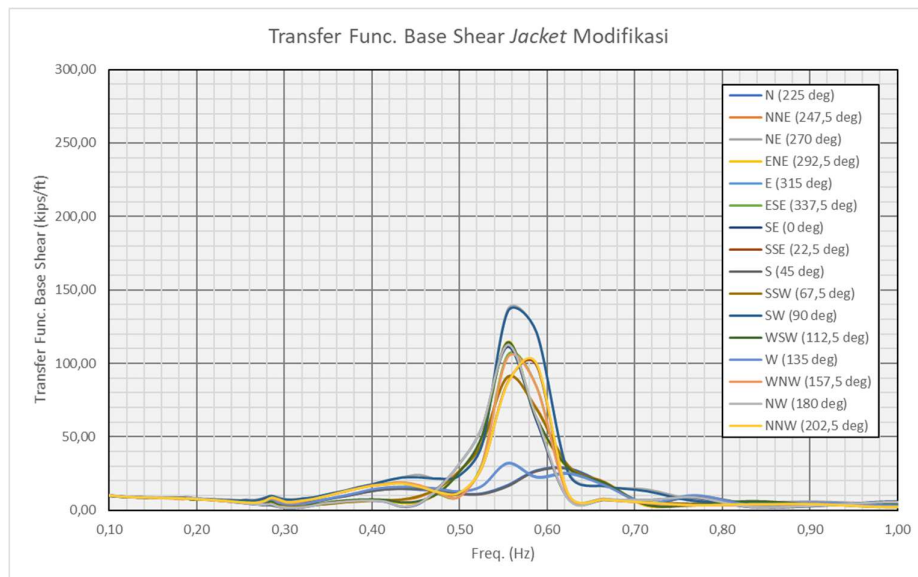
Dari tabel di atas maka dapat dilihat jika periode natural kedua *jacket* memiliki perbedaan yang cukup signifikan terlihat pada mode 1 setiap *jacket* yang merupakan periode dasar atau periode natural struktur dengan 1,756 s untuk *jacket* modifikasi dan 1,472 s untuk *jacket* konvensional.

4.3.2 Response Amplitude Operator (RAO)

Pada tahap ini RAO digunakan sebagai fungsi transfer untuk mengetahui respon struktur terhadap gelombang yang mengenai. Sementara RAO yang digunakan adalah *overturning moment* dan *base shear* seperti yang dapat dilihat pada Gambar 4.8 dan Gambar 4.9 di bawah yang dihasilkan oleh *jacket* modifikasi.



Gambar 4.8 RAO *overturning moment jacket* modifikasi terhadap frekuensi

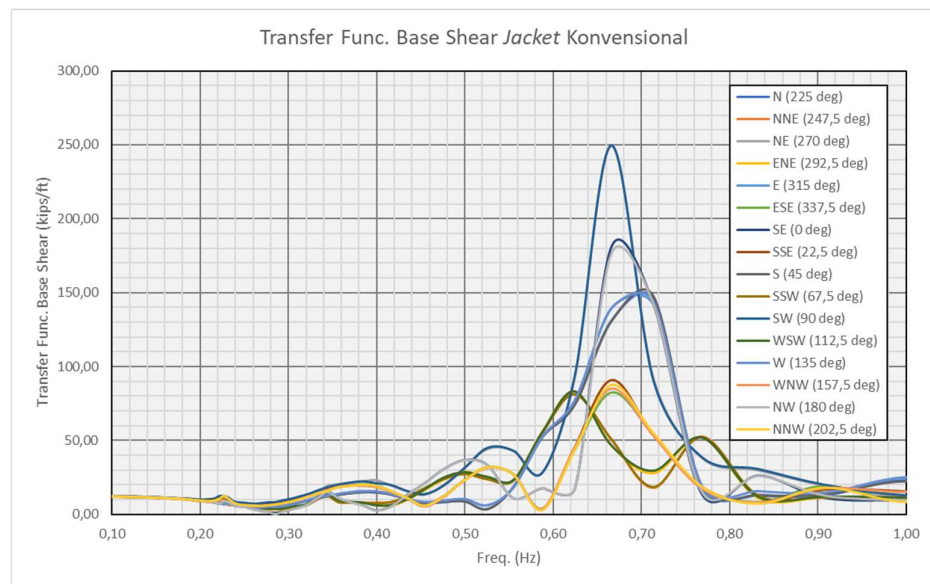


Gambar 4.9 RAO *base shear jacket* modifikasi terhadap frekuensi

Dari kedua grafik di atas dapat dilihat jika beban gelombang yang mengenai *jacket* modifikasi pada tiap arah akan mengalami puncak pada rentang frekuensi 0,5 – 0,6 Hz, hal ini dikarenakan frekuensi gelombang yang mengenai struktur beresonansi dengan frekuensi natural struktur yang berada pada rentang frekuensi yang sama dengan nilai 0,570 Hz seperti ditunjukkan pada Tabel 4.8. Adapun RAO yang dihasilkan oleh *jacket* konvensional dapat dilihat pada Gambar 4.10 dan Gambar 4.11 di bawah.



Gambar 4.10 RAO *overturning moment jacket* konvensional terhadap frekuensi



Gambar 4.11 RAO *base shear jacket* konvensional terhadap frekuensi

Berbeda dengan grafik pada *jacket* modifikasi, grafik pada *jacket* konvensional memiliki puncak pada rentang frekuensi 0,6 – 0,72 Hz, hal ini dikarenakan frekuensi gelombang yang mengenai struktur beresonansi dengan frekuensi natural struktur yang berada pada rentang frekuensi yang sama dengan nilai 0,679 Hz seperti ditunjukkan pada Tabel 4.9.

4.3.3 Dynamic Amplification Factor (DAF)

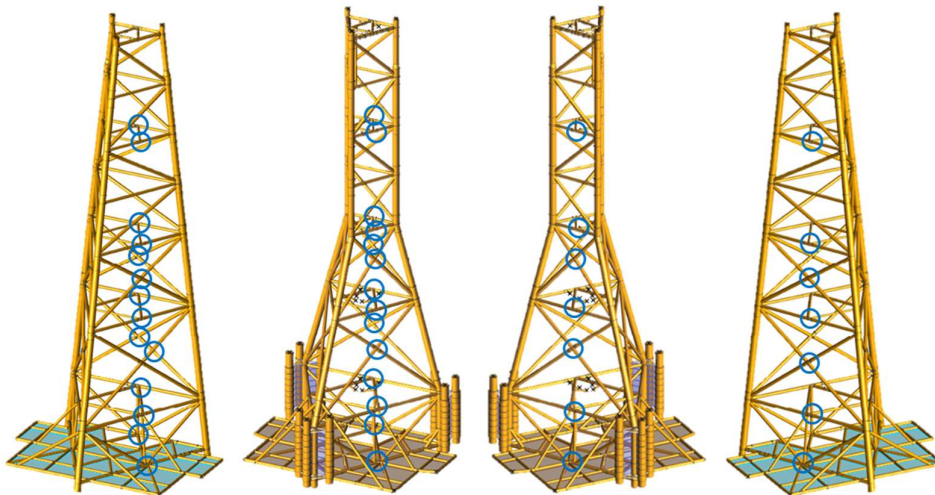
DAF merupakan faktor amplifikasi respon struktur terhadap suatu periode gelombang yang mengenai struktur tersebut, hal ini dikaitkan dengan periode natural struktur yang mana menjadi penting untuk dipertimbangkan dikarenakan jika periode gelombang yang mengenai struktur berada pada daerah periode natural struktur maka akan terjadi resonansi yang dapat mengakibatkan naiknya respon yang dialami struktur akibat gelombang tersebut. Dengan mengaplikasikan koefisien *damping* 2% maka didapatkan hasil perhitungan DAF seperti pada Tabel 4.10.

Tabel 4.10 Hasil perhitungan DAF

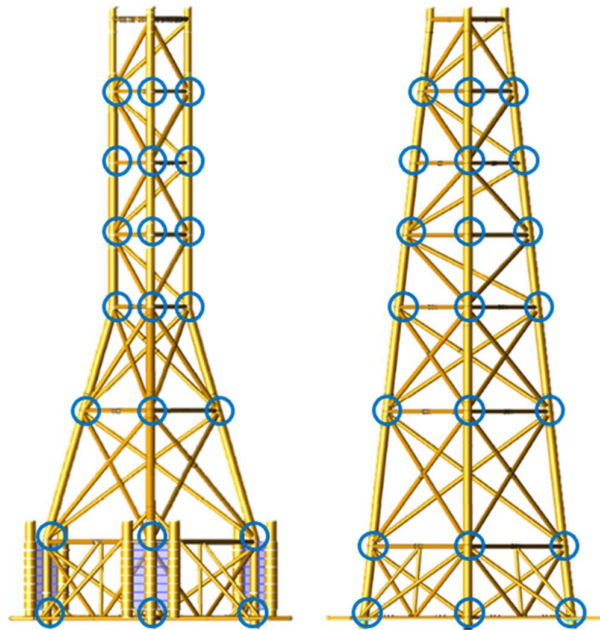
| Wave Direction | Tp (s) | DAF Jacket Konvensional | | | DAF Jacket Modifikasi | | | |
|----------------|--------|-------------------------|--------------------|--------|-----------------------|--------------------|--------|-------|
| | | $\{1-(T_n/T)^2\}^2$ | $(2\beta T_n/T)^2$ | DAF | $\{1-(T_n/T)^2\}^2$ | $(2\beta T_n/T)^2$ | DAF | |
| N | 225 | 3,31 | 0,6436 | 0,0003 | 1,246 | 0,5163 | 0,0005 | 1,391 |
| NNE | 247,5 | 3,25 | 0,6318 | 0,0003 | 1,258 | 0,5014 | 0,0005 | 1,412 |
| NE | 270 | 3,23 | 0,6278 | 0,0003 | 1,262 | 0,4962 | 0,0005 | 1,419 |
| ENE | 292,5 | 3,53 | 0,6825 | 0,0003 | 1,210 | 0,5663 | 0,0004 | 1,328 |
| E | 315 | 5,84 | 0,8770 | 0,0001 | 1,068 | 0,8274 | 0,0001 | 1,099 |
| ESE | 337,5 | 5,20 | 0,8462 | 0,0001 | 1,087 | 0,7849 | 0,0002 | 1,129 |
| SE | 0 | 3,28 | 0,6378 | 0,0003 | 1,252 | 0,5089 | 0,0005 | 1,401 |
| SSE | 22,5 | 3,17 | 0,6152 | 0,0003 | 1,275 | 0,4805 | 0,0005 | 1,442 |
| S | 45 | 3,07 | 0,5931 | 0,0004 | 1,298 | 0,4527 | 0,0005 | 1,485 |
| SSW | 67,5 | 2,97 | 0,5691 | 0,0004 | 1,325 | 0,4231 | 0,0006 | 1,536 |
| SW | 90 | 2,98 | 0,5715 | 0,0004 | 1,322 | 0,4261 | 0,0006 | 1,531 |
| WSW | 112,5 | 3,48 | 0,6742 | 0,0003 | 1,218 | 0,5556 | 0,0004 | 1,341 |
| W | 135 | 5,31 | 0,8522 | 0,0001 | 1,083 | 0,7932 | 0,0002 | 1,123 |
| WNW | 157,5 | 6,54 | 0,9012 | 0,0001 | 1,053 | 0,8610 | 0,0001 | 1,078 |
| NW | 180 | 4,70 | 0,8134 | 0,0002 | 1,109 | 0,7403 | 0,0002 | 1,162 |
| NNW | 202,5 | 3,25 | 0,6318 | 0,0003 | 1,258 | 0,5014 | 0,0005 | 1,412 |

4.3.4 Umur Kelelahan

Pada tahap ini, analisa umur kelelahan hanya terkonsentrasi pada *joint-joint* utama yang menghubungkan *member-member* utama seperti *jacket leg* dan *bracing*. Lokasi setiap *joint* yang dianalisa pada kedua *jacket* dapat dilihat pada Gambar 4.12 dan Gambar 4.13.



Gambar 4.12 Lokasi *joint* yang ditinjau pada *bracing*



Gambar 4.13 Lokasi *joint* yang ditinjau pada *jacket*

Dengan menggunakan metode spektral serta mempertimbangkan faktor dinamis dari struktur, maka hasil analisa umur kelelahan setiap *joint* yang sudah ditunjuk pada Gambar 4.12 dan Gambar 4.13 dapat dilihat pada Tabel 4.11 hingga Tabel 4.13.

Tabel 4.11 Umur kelelahan setiap *joint* bagian *top*.

| Row/Elevasi (dari MSL) | Top | | | | | | Fatigue Life Lebih Besar |
|---------------------------|---------------------|-----------|----------------------|-------------------|-----------|----------------------|-----------------------------|
| | Jacket Konvensional | | | Jacket Modifikasi | | | |
| | Joint | Member | Fatigue Life (tahun) | Joint | Member | Fatigue Life (tahun) | |
| (-) 5' | 0078 | 0061-0078 | 31533,32 | 0012 | 0001-0012 | 36033,51 | Modifikasi |
| | 0091 | 0078-0091 | 150529,8 | 0006 | 0195-0006 | 1302607 | Modifikasi |
| | 0061 | 0067-0061 | 9125,79 | 0009 | 0013-0009 | 13229,9 | Modifikasi |
| (-) 40' | 0067 | 0105-0067 | 983051,7 | 0010 | 0100-0010 | 261460000 | Modifikasi |
| | 0107 | 0105-0107 | infinite | 0098 | 0207-0098 | infinite | |
| | 0092 | 0093-0092 | 15593,67 | 0007 | 0008-0007 | 9886,43 | Konvensional |
| | 0105 | 0107-0105 | infinite | 0100 | 0010-0100 | infinite | |
| | 0106 | 0105-0106 | infinite | 0099 | 0208-0099 | infinite | |
| | 0079 | 0080-0079 | 11138,05 | 0013 | 0014-0013 | 11367,81 | Modifikasi |
| (-) 75' | 0068 | 0069-0068 | 15539,58 | 0011 | 0005-0011 | 13843,78 | Konvensional |
| | 0093 | 0080-0093 | 2236095 | 0008 | 0215-0008 | 306370000 | Modifikasi |
| | 0080 | 0079-0080 | 35491,34 | 0014 | 0013-0014 | 10953,7 | Konvensional |

Tabel 4.12 Umur kelelahan setiap *joint* bagian *middle*.

| Middle | | | | | | | |
|------------------------------------|---------------------|-----------|----------------------|-------------------|-----------|----------------------|-----------------------------|
| Row/Elevasi (dari MSL) | Jacket Konvensional | | | Jacket Modifikasi | | | Fatigue Life Lebih Besar |
| | Joint | Member | Fatigue Life (tahun) | Joint | Member | Fatigue Life (tahun) | |
| (-) 110' dan X-bracing di bawahnya | 0069 | 0070-0069 | 2001440 | 0017 | 0055-0017 | 677,464 | Konvensional |
| | 0113 | 0111-0113 | infinite | 0081 | 0088-0081 | infinite | |
| | 0094 | 0080-0094 | 123072,1 | 0015 | 0049-0015 | 96,1158 | Konvensional |
| | 0111 | 0069-0111 | infinite | 0079 | 0088-0079 | infinite | |
| | 0112 | 0081-0112 | infinite | 0082 | 0089-0082 | infinite | |
| | 0081 | 0068-0081 | 43505,3 | 0016 | 0050-0016 | 101,0301 | Konvensional |
| | 0097 | 0083-0097 | 279810,6 | 0056 | 0015-0056 | 26037000 | Modifikasi |
| | 0098 | 0070-0098 | 1263107 | 0060 | 0015-0060 | 10869000 | Modifikasi |
| | 0099 | 0083-0099 | 1360852 | 0066 | 0050-0066 | 13010,48 | Konvensional |
| (-) 161' dan X-bracing di bawahnya | 0070 | 0071-0070 | 843017,8 | 0055 | 0023-0055 | 79235,86 | Konvensional |
| | 0116 | 0095-0116 | infinite | 0101 | 0049-0101 | infinite | |
| | 0095 | 0096-0095 | 1453852 | 0049 | 0101-0049 | 503315,7 | Konvensional |
| | 0114 | 0070-0114 | infinite | 0096 | 0107-0096 | infinite | |
| | 0115 | 0083-0115 | infinite | 0104 | 0101-0104 | infinite | |
| | 0083 | 0081-0083 | 984899,6 | 0050 | 0022-0050 | 55470,17 | Konvensional |
| | 0100 | 0084-0100 | 10665000 | 0068 | 0049-0068 | 48145000000 | Modifikasi |
| | 0101 | 0095-0101 | 93268000 | 0120 | 0023-0120 | 1008500000 | Modifikasi |
| | 0120 | 0070-0120 | 10520000 | 0072 | 0022-0072 | 1287954 | Konvensional |

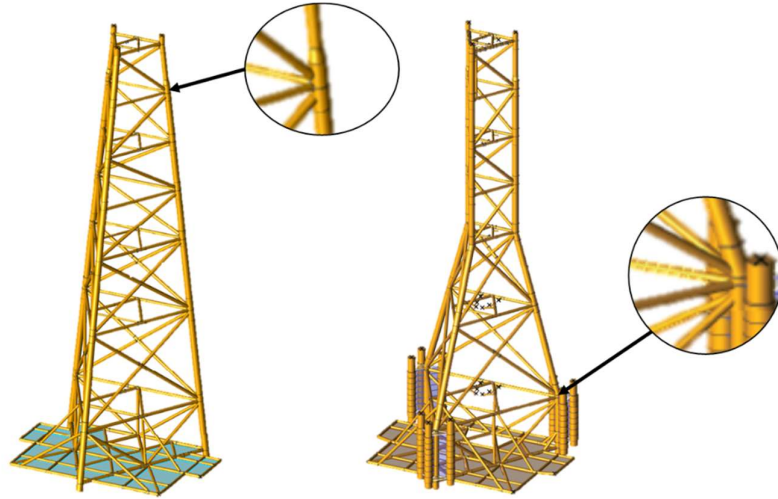
Tabel 4.13 Umur kelelahan setiap *joint* bagian *bottom*.

| Bottom | | | | | | | |
|---------------------------|---------------------|-----------|----------------------|-------------------|-----------|----------------------|-----------------------------|
| Row/Elevasi (dari MSL) | Jacket Konvensional | | | Jacket Modifikasi | | | Fatigue Life Lebih Besar |
| | Joint | Member | Fatigue Life (tahun) | Joint | Member | Fatigue Life (tahun) | |
| (-) 224,61' | 0071 | 0070-0071 | 4758150 | 0023 | 0026-0023 | 149,6136 | Konvensional |
| | 0119 | 0071-0119 | infinite | 0051 | 0052-0051 | infinite | |
| | 0096 | 0095-0096 | 8195252 | 0018 | 0224-0018 | 974,0327 | Konvensional |
| | 0117 | 0071-0117 | infinite | 0039 | 0038-0039 | infinite | |
| | 0118 | 0084-0118 | infinite | 0045 | 0025-0045 | infinite | |
| | 0084 | 0083-0084 | 946588,7 | 0022 | 0025-0022 | 44,98 | Konvensional |
| (-) 261,61' | 0010 | 0071-0010 | 16481000 | 0029 | 0226-0029 | infinite | Modifikasi |
| | 0032 | 0125-0032 | infinite | 0052 | 0165-0052 | infinite | |
| | 0011 | 0096-0011 | 1822043 | 0027 | 0246-0027 | infinite | Modifikasi |
| | 0012 | 0123-0012 | infinite | 0038 | 0025-0038 | infinite | |
| | 0031 | 0084-0031 | 322020000 | 0033 | 0024-0033 | infinite | Modifikasi |
| | 0009 | 0084-0009 | 35093000 | 0028 | 0040-0028 | infinite | Modifikasi |

Dari hasil yang ada maka dapat diketahui umur kelelahan pada setiap *joint* yang ditinjau dari kedua struktur. Dengan hasil yang berbeda maka umur kelelahan kedua struktur secara global dapat diwakili oleh umur kelelahan terendah pada setiap struktur, pada Tabel 4.14 adalah umur terendah pada setiap struktur beserta lokasi *joint*-nya yang ditunjukkan pada Gambar 4.14.

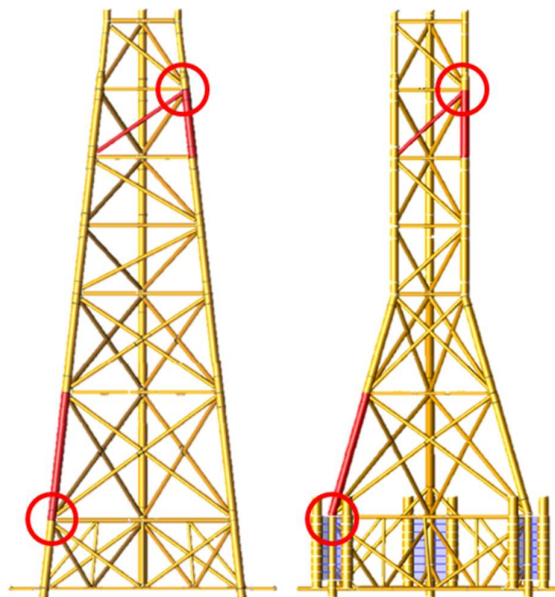
Tabel 4.14 Umur kelelahan terendah pada setiap setiap struktur

| Umur Kelelahan Terendah | | | | | |
|-------------------------|-----------|----------------------|-------------------|-----------|----------------------|
| Jacket Konvensional | | | Jacket Modifikasi | | |
| Joint | Member | Fatigue Life (tahun) | Joint | Member | Fatigue Life (tahun) |
| 0061 | 0067-0061 | 9125,79 | 0022 | 0025-0022 | 44,98 |



Gambar 4.14 Lokasi *joint* dengan umur kelelahan terendah

Namun *joint* dengan posisi yang sama dihasilkan umur kelelahan yang berbeda, hal ini disebabkan oleh beberapa faktor yang salah satunya merupakan SCF. SCF *joint* tertentu dengan posisi yang sama pada kedua struktur dapat memiliki nilai yang berbeda bergantung pada faktor-faktor yang telah disebutkan pada 2.2.6.1.g yang salah satunya merupakan sudut kemiringan antara *chord* dan *brace*. Dari tinjauan yang telah dilakukan pada *joint-joint* kritis dengan umur kelelahan terendah dan *joint* dengan posisi yang sama pada struktur pembandingnya dapat terlihat jika SCF yang dihasilkan berbanding terbalik dengan umur kelelahan pada *joint* tersebut. Posisi *joint-member* yang ditinjau ditunjukkan pada Gambar 4.15.



Gambar 4.15 Posisi *joint* kritis dan *joint* yang sama pada struktur pembanding

Dari Gambar 4.15 maka dapat diambil data SCF pada kedua *jacket* dengan hasil seperti ditunjukkan pada Tabel 4.15.

Tabel 4.15 Hasil SCF pada *joint* kritis dan *joint* di posisi yang sama pada struktur pembandingnya.

| Jacket Konvensional | | | | | | Jacket Modifikasi | | | | | |
|---------------------|-----------|-------|-------|-------|-------|-------------------|-----------|-------|-------|-------|-------|
| Joint | Member | SCF | | | | Joint | Member | SCF | | | |
| | | AX-CR | AX-SD | IN-PL | OU-PL | | | AX-CR | AX-SD | IN-PL | OU-PL |
| 0061 | 0067-0061 | 3,59 | 4,20 | 1,75 | 3,60 | 0009 | 0010-0009 | 3,18 | 3,42 | 1,54 | 2,78 |
| 0084 | 0083-0084 | 3,17 | 3,2 | 1,56 | 2,98 | 0022 | 0025-0022 | 8,18 | 1,52 | 3,68 | 1,50 |

Dari Tabel 4.15 dapat diketahui jika SCF pada *joint* 0061 *member* 0061 – 0067 di *jacket* konvensional lebih tinggi dibanding pada *joint* 0009 *member* 0009 – 0010 pada *jacket* modifikasi. Hal serupa juga terjadi pada *joint* 0022 *member* 0022 – 0025 *jacket* modifikasi yang lebih tinggi dibanding pada *joint* 0084 *member* 0084 – 0083 *jacket* konvensional.

BAB V

KESIMPULAN DAN SARAN

5.1 Kesimpulan

Kesimpulan yang dapat ditarik dari hasil penelitian ini adalah sebagai berikut :

1. Periode natural pada *jacket* modifikasi bernilai lebih tinggi sebesar 1,756 s diakibatkan oleh nilai kekakuan yang lebih rendah dari nilai kekakuan *jacket* konvensional dengan nilai periode natural 1,472 s.
2. Secara keseluruhan, *joint* pada *jacket* modifikasi pada bagian *top* di elevasi (-) 5', (-) 40', dan (-) 75 memiliki umur kelelahan yang lebih tinggi dibandingkan *joint* di titik yang sama pada *jacket* konvensional. Hal ini dikarenakan SCF yang mengalami kenaikan pada *joint* dengan sudut kemiringan *chord* dan *brace* yang tidak siku-siku seperti pada *jacket* konvensional.
3. *Joint* pada *jacket* modifikasi pada bagian *middle* di elevasi (-) 110' dan (-) 161' memiliki umur kelelahan yang lebih rendah dibandingkan *joint* di titik yang sama pada *jacket* konvensional. Hal ini dikarenakan SCF yang mengalami kenaikan pada *joint* dengan sudut kemiringan *chord* dan *brace* yang lebih ekstrem pada *jacket* modifikasi.
4. Berdasarkan konfigurasi struktur, *jacket* konvensional memiliki umur yang lebih panjang dengan umur kelelahan terendah adalah 9125,79 tahun dibanding *jacket* modifikasi dengan umur kelelahan terendah 44,98 tahun.

5.2 Saran

Ada pun saran yang dapat diberikan untuk keperluan pengembangan penelitian adalah sebagai berikut :

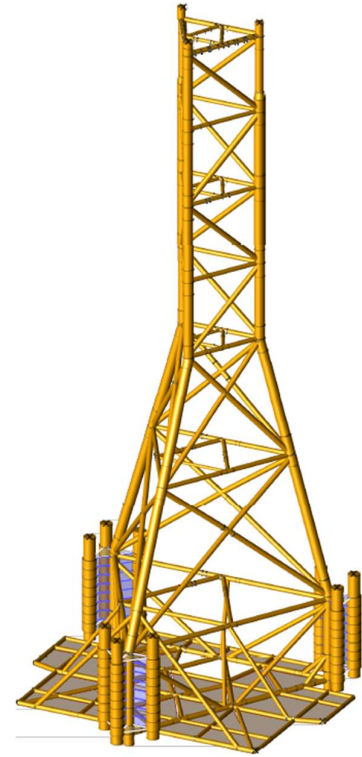
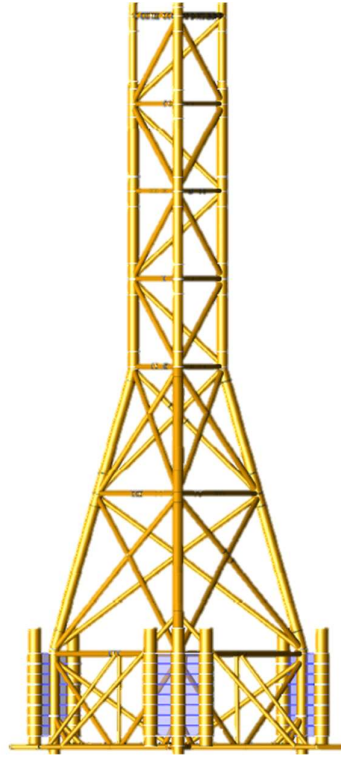
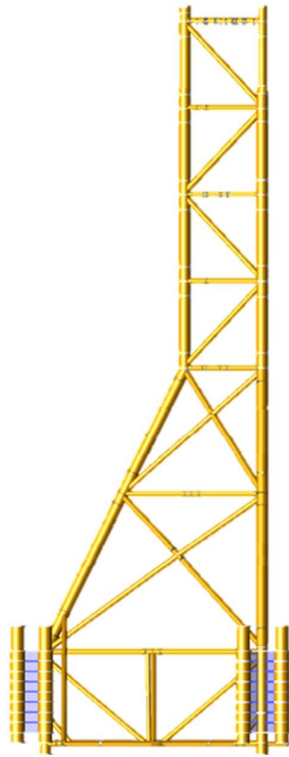
1. Diperlukan analisis local pada *joint* kritis pada *jacket* modifikasi untuk mengetahui parameter-parameter pendukung untuk mengetahui umur kelelahan yang lebih presisi.
2. Dapat dilakukan analisa beban ultimat pada *jacket* modifikasi untuk mengetahui beban maksimum yang dapat ditumpu.
3. Disarankan untuk dilakukan analisa terkait optimasi desain *jacket* modifikasi dengan konsep minimalis untuk penggunaan yang lebih optimal.

DAFTAR PUSTAKA

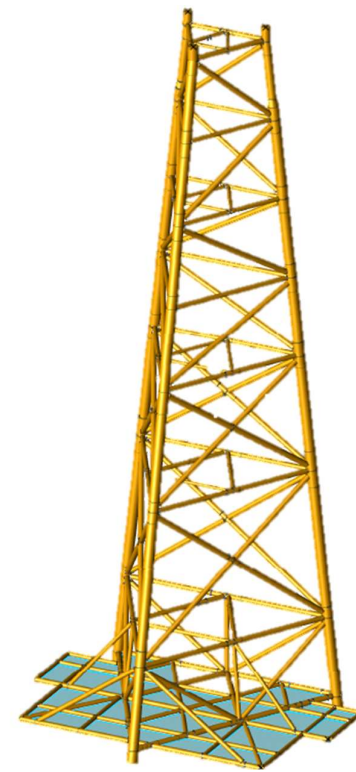
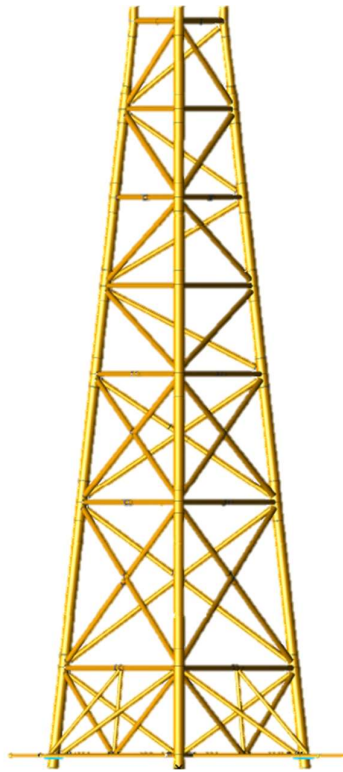
- Almar-Næss, A : *Fatigue Handbook of Offshore Steel Structure.*, Tapir, Trondheim, Norway, 1985.
- American Petroleum Institute : *Recommended Practice for Planning, Designing and Constructing Fixed Offshore Platforms – Working Stress Design.* 21st ed., API Publishing Services, Washington D.C, USA, 2000.
- American Petroleum Institute : *Recommended Practice for Planning, Designing and Constructing Fixed Offshore Platforms – Working Stress Design.* 21st ed., API Publishing Services, Washington D.C, USA, 2010.
- Djarmiko, E. B : *Analisa Kelelahan Struktur Bangunan Laut.* Modul Perkuliahan., Departemen Teknik Kelautan ITS, Institut Teknologi Sepuluh Nopember, Surabaya, Indonesia, 2006.
- Djarmiko, E. B : *Perilaku dan Operabilitas Bangunan Laut di Atas Gelombang Acak.*, Institut Teknologi Sepuluh Nopember, Surabaya, Indonesia, 2012.
- El-Reedy, M. A : *Offshore Structures Design, Construction, and Maintenance.*, Elsevier Ltd., Oxford, UK, 2012.
- Gibstein, M. B : *Stress Concentration in Tubular K-Joints with Diameter Ratio Equal to One.*, Elsevier Ltd., Amsterdam, Netherlands, 1985.
- British Standard ISO 19902:2007 : *Petroleum and Natural Gas Industries – Fixed Steel Offshore Structures.*, BSI Standards Ltd., UK, 2007
- Riyanto, R. D : *Modul Perancangan Struktur Lepas Pantai Terpancang.* Modul Perkuliahan., Departemen Teknik Kelautan ITS, Institut Teknologi Sepuluh Nopember, Surabaya, Indonesia, 2015.
- Saini, D : *A Review Of Stress Concentration Factors In Tubular And Non-Tubular Joints For Design Of Offshore Installations.* Journal of Ocean Engineering and Science Volume 1, Issue 3, 2016.
- Setyadi, H. F : *Analisis Umur Kelelahan Dengan Metode Deterministik dan Spektral Pada Sambungan Tubular Jacket Kaki Tiga Dengan Variasi Kedalaman.* Tugas Akhir Departemen Teknik Kelautan., Institut Teknologi Sepuluh Nopember, Surabaya, Indonesia, 2018.

LAMPIRAN A
SACS MODEL

JACKET MODIFIKASI



JACKET KONVENSIONAL



LAMPIRAN B
SACS INPUT

SEASTATE INPUT JACKET MODIFIKASI (INPLACE)

```

LDOPT          -Z64.20000490.0000-261.609 261.609GLOB          CMBMPTNP      2K
LCSEL          8E  8N  8S  8W  9E  9N  9S  9W  8NE 8NW 8SE 8SW
LCSEL          9NE 9NW 9SE 9SW 8ENE 8ESE 8NNE 8NNW 8SSE 8SSW 8WNW 8WSW
LCSEL          9ENE 9ESE 9NNE 9NNW 9SSE 9SSW 9WNW 9WSW
FILE B
CDM
CDM  22.00 0.500          2.000          0.800          2.000
CDM  24.00 0.500          2.000          0.800          2.000
CDM  26.00 0.500          2.000          0.800          2.000
CDM  28.00 0.500          2.000          0.800          2.000
CDM  30.00 0.500          2.000          0.800          2.000
CDM  53.00 0.500          2.000          0.800          2.000
CDM  54.00 0.500          2.000          0.800          2.000
*
LOADCN DL
DEAD
DEAD      -Z                      M
LOAD
LOADCN OE
WAVE
WAVE1.00STOK  5.09          6.13          315.00      D          MM10 1 0 5
CURR
CURR      0.382  1.274 315.000          0.900          CN FPS WDP
CURR      50.000  1.840 315.000          CN FPS WDP
CURR     100.000  2.032 315.000          CN FPS WDP
LOADCN ON
WAVE
WAVE1.00STOK  1.31          3.38          225.00      D          MM10 1 0 5
CURR
CURR      0.382  0.384 225.000          0.900          CN FPS WDP
CURR      50.000  0.554 225.000          CN FPS WDP
CURR     100.000  0.612 225.000          CN FPS WDP
LOADCN OS
WAVE
WAVE1.00STOK  1.12          3.14          45.00       D          MM10 1 0 5
CURR
CURR      0.382  0.206 45.000          0.900          CN FPS WDP
CURR      50.000  0.298 45.000          CN FPS WDP
CURR     100.000  0.329 45.000          CN FPS WDP
LOADCN OW
WAVE
WAVE1.00STOK  1.31          5.68          135.00      D          MM10 1 0 5
CURR
CURR      0.382  0.924 135.000          0.900          CN FPS WDP
CURR      50.000  1.336 135.000          CN FPS WDP
CURR     100.000  1.475 135.000          CN FPS WDP
LOADCN 1E
WAVE
WAVE1.00STOK 10.07          7.95          315.00      D          MM10 1 0 5
CURR
CURR      0.382  2.257 315.000          0.900          CN FPS WDP
CURR      50.000  3.282 315.000          CN FPS WDP
CURR     100.000  3.601 315.000          CN FPS WDP
LOADCN 1N
WAVE
WAVE1.00STOK  4.63          5.25          225.00      D          MM10 1 0 5
CURR
CURR      0.382  0.632 225.000          0.900          CN FPS WDP
CURR      50.000  0.914 225.000          CN FPS WDP
CURR     100.000  1.009 225.000          CN FPS WDP
LOADCN 1S
WAVE
WAVE1.00STOK  4.27          4.65          45.00       D          MM10 1 0 5
CURR
CURR      0.382  0.605 45.000          0.900          CN FPS WDP
CURR      50.000  0.874 45.000          CN FPS WDP
CURR     100.000  0.964 45.000          CN FPS WDP
LOADCN 1W
WAVE
WAVE1.00STOK  4.43          8.63          135.00      D          MM10 1 0 5
CURR

```

| | | | | | | | | | |
|--------------|---------|-------|---------|--------|-------|--|----|------|-------|
| CURR | 0.382 | 1.240 | 45.000 | | 0.900 | | CN | FPS | WDP |
| CURR | 50.000 | 1.792 | 45.000 | | | | CN | FPS | WDP |
| CURR | 100.000 | 1.979 | 45.000 | | | | CN | FPS | WDP |
| LOADCN ONE | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 1.31 | | 3.30 | 270.00 | D | | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 0.406 | 270.000 | | 0.900 | | CN | FPS | WDP |
| CURR | 50.000 | 0.587 | 270.000 | | | | CN | FPS | WDP |
| CURR | 100.000 | 0.648 | 270.000 | | | | CN | FPS | WDP |
| LOADCN ONW | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 2.13 | | 4.84 | 180.00 | D | | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 0.713 | 180.000 | | 0.900 | | CN | FPS | WDP |
| CURR | 50.000 | 1.030 | 180.000 | | | | CN | FPS | WDP |
| CURR | 100.000 | 1.138 | 180.000 | | | | CN | FPS | WDP |
| LOADCN OSE | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 1.74 | | 3.48 | 0. | D | | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 0.437 | 0.000 | | 0.900 | | CN | FPS | WDP |
| CURR | 50.000 | 0.631 | | | | | CN | FPS | WDP |
| CURR | 100.000 | 0.697 | | | | | CN | FPS | WDP |
| LOADCN OSW | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 0.85 | | 3.11 | 90.00 | D | | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 0.214 | 90.000 | | 0.900 | | CN | FPS | WDP |
| CURR | 50.000 | 0.309 | 90.000 | | | | CN | FPS | WDP |
| CURR | 100.000 | 0.341 | 90.000 | | | | CN | FPS | WDP |
| LOADCN 1NE | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 4.43 | | 5.53 | 270.00 | D | | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 0.784 | 270.000 | | 0.900 | | CN | FPS | WDP |
| CURR | 50.000 | 1.133 | 270.000 | | | | CN | FPS | WDP |
| CURR | 100.000 | 1.251 | 270.000 | | | | CN | FPS | WDP |
| LOADCN 1NW | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 12.66 | | 10.05 | 180.00 | D | | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 1.065 | 180.000 | | 0.900 | | CN | FPS | WDP |
| CURR | 50.000 | 1.539 | 180.000 | | | | CN | FPS | WDP |
| CURR | 100.000 | 1.699 | 180.000 | | | | CN | FPS | WDP |
| LOADCN 1SE | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 4.79 | | 5.66 | 0. | D | | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 1.194 | 0.000 | | 0.900 | | CN | FPS | WDP |
| CURR | 50.000 | 1.725 | | | | | CN | FPS | WDP |
| CURR | 100.000 | 1.904 | | | | | CN | FPS | WDP |
| LOADCN 1SW | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 5.74 | | 5.55 | 90.00 | D | | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 0.719 | 90.000 | | 0.900 | | CN | FPS | WDP |
| CURR | 50.000 | 1.039 | 90.000 | | | | CN | FPS | WDP |
| CURR | 100.000 | 1.147 | 90.000 | | | | CN | FPS | WDP |
| LOADCNOENE | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 1.97 | | 3.64 | 292.50 | D | | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 0.699 | 292.500 | | 0.900 | | CN | FPS | WDP |
| CURR | 50.000 | 1.010 | 292.500 | | | | CN | FPS | WDP |
| CURR | 100.000 | 1.115 | 292.500 | | | | CN | FPS | WDP |
| LOADCNOESE | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 4.23 | | 5.56 | 337.50 | D | | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 1.269 | 337.500 | | 0.900 | | CN | FPS | WDP |
| CURR | 50.000 | 1.834 | 337.500 | | | | CN | FPS | WDP |
| CURR | 100.000 | 2.025 | 337.500 | | | | CN | FPS | WDP |
| LOADCNONNE | | | | | | | | | |

| | | | | | | | | | |
|--------------|---------|-------|---------|--------|-------|--|------------|------|-------|
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 1.08 | | 3.32 | 247.50 | D | | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 0.347 | 247.500 | | 0.900 | | CN FPS WDP | | |
| CURR | 50.000 | 0.502 | 247.500 | | | | CN FPS WDP | | |
| CURR | 100.000 | 0.554 | 247.500 | | | | CN FPS WDP | | |
| LOADCN0NNW | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 1.28 | | 3.33 | 202.50 | D | | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 0.484 | 202.500 | | 0.900 | | CN FPS WDP | | |
| CURR | 50.000 | 0.700 | 202.500 | | | | CN FPS WDP | | |
| CURR | 100.000 | 0.773 | 202.500 | | | | CN FPS WDP | | |
| LOADCN0SSE | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 1.21 | | 3.33 | 22.50 | D | | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 0.269 | 22.500 | | 0.900 | | CN FPS WDP | | |
| CURR | 50.000 | 0.389 | 22.500 | | | | CN FPS WDP | | |
| CURR | 100.000 | 0.429 | 22.500 | | | | CN FPS WDP | | |
| LOADCN0SSW | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 1.05 | | 3.09 | 67.50 | D | | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 0.208 | 67.500 | | 0.900 | | CN FPS WDP | | |
| CURR | 50.000 | 0.301 | 67.500 | | | | CN FPS WDP | | |
| CURR | 100.000 | 0.332 | 67.500 | | | | CN FPS WDP | | |
| LOADCN0WNW | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 6.37 | | 6.93 | 157.50 | D | | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 1.262 | 157.500 | | 0.900 | | CN FPS WDP | | |
| CURR | 50.000 | 1.824 | 157.500 | | | | CN FPS WDP | | |
| CURR | 100.000 | 2.014 | 157.500 | | | | CN FPS WDP | | |
| LOADCN0WSW | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 1.64 | | 3.69 | 112.50 | D | | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 0.363 | 112.500 | | 0.900 | | CN FPS WDP | | |
| CURR | 50.000 | 0.525 | 112.500 | | | | CN FPS WDP | | |
| CURR | 100.000 | 0.579 | 112.500 | | | | CN FPS WDP | | |
| LOADCN1ENE | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 7.81 | | 7.97 | 292.50 | D | | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 0.962 | 292.500 | | 0.900 | | CN FPS WDP | | |
| CURR | 50.000 | 1.390 | 292.500 | | | | CN FPS WDP | | |
| CURR | 100.000 | 1.535 | 292.500 | | | | CN FPS WDP | | |
| LOADCN1ESE | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 7.09 | | 6.97 | 337.50 | D | | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 2.449 | 337.500 | | 0.900 | | CN FPS WDP | | |
| CURR | 50.000 | 3.539 | 337.500 | | | | CN FPS WDP | | |
| CURR | 100.000 | 3.908 | 337.500 | | | | CN FPS WDP | | |
| LOADCN1NNE | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 4.59 | | 5.24 | 247.50 | D | | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 0.648 | 247.500 | | 0.900 | | CN FPS WDP | | |
| CURR | 50.000 | 0.936 | 247.500 | | | | CN FPS WDP | | |
| CURR | 100.000 | 1.033 | 247.500 | | | | CN FPS WDP | | |
| LOADCN1NNW | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 4.10 | | 6.22 | 202.50 | D | | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 0.822 | 202.500 | | 0.900 | | CN FPS WDP | | |
| CURR | 50.000 | 1.187 | 202.500 | | | | CN FPS WDP | | |
| CURR | 100.000 | 1.311 | 202.500 | | | | CN FPS WDP | | |
| LOADCN1SSE | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 4.04 | | 4.41 | 22.50 | D | | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 0.821 | 22.500 | | 0.900 | | CN FPS WDP | | |

| | | | | | | |
|--------------|---------|----------|------------------|--------|---|------------|
| CURR | 50.000 | 1.186 | 22.500 | | | CN FPS WDP |
| CURR | 100.000 | 1.309 | 22.500 | | | CN FPS WDP |
| LOADCN1SSW | | | | | | |
| WAVE | | | | | | |
| WAVE1.00STOK | 5.09 | | 5.61 | 67.50 | D | MM10 1 0 5 |
| CURR | | | | | | |
| CURR | 0.382 | 0.613 | 67.500 | 0.900 | | CN FPS WDP |
| CURR | 50.000 | 0.886 | 67.500 | | | CN FPS WDP |
| CURR | 100.000 | 0.978 | 67.500 | | | CN FPS WDP |
| LOADCN1WNW | | | | | | |
| WAVE | | | | | | |
| WAVE1.00STOK | 15.55 | | 10.12 | 157.50 | D | MM10 1 0 5 |
| CURR | | | | | | |
| CURR | 0.382 | 1.560 | 157.500 | 0.900 | | CN FPS WDP |
| CURR | 50.000 | 2.255 | 157.500 | | | CN FPS WDP |
| CURR | 100.000 | 2.490 | 157.500 | | | CN FPS WDP |
| LOADCN1WSW | | | | | | |
| WAVE | | | | | | |
| WAVE1.00STOK | 5.94 | | 6.28 | 112.50 | D | MM10 1 0 5 |
| CURR | | | | | | |
| CURR | 0.382 | 0.898 | 112.500 | 0.900 | | CN FPS WDP |
| CURR | 50.000 | 1.298 | 112.500 | | | CN FPS WDP |
| CURR | 100.000 | 1.433 | 112.500 | | | CN FPS WDP |
| LCOMB | | | | | | |
| LCOMB 8E | 0E | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 8N | 0N | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 8S | 0S | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 8W | 0W | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 9E | 1E | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 9N | 1N | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 9S | 1S | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 9W | 1W | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 8NE | 0NE | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 8NW | 0NW | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 8SE | 0SE | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 8SW | 0SW | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 9NE | 1NE | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 9NW | 1NW | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 9SE | 1SE | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 9SW | 1SW | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 8ENE | 0ENE | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 8ESE | 0ESE | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 8NNE | 0NNE | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 8NNW | 0NNW | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 8SSE | 0SSE | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 8SSW | 0SSW | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 8WNW | 0WNW | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 8WSW | 0WSW | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 9ENE | 1ENE | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 9ESE | 1ESE | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 9NNE | 1NNE | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 9NNW | 1NNW | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 9SSE | 1SSE | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 9SSW | 1SSW | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 9WNW | 1WNW | 1.0000DL | 1.0700TOPS1.0600 | | | |
| LCOMB 9WSW | 1WSW | 1.0000DL | 1.0700TOPS1.0600 | | | |
| END | | | | | | |

SEASTATE INPUT JACKET KONVENTIONAL (INPLACE)

| | | | | | | | | | | | | |
|--------|--|-------|------|-------|------|-------|------|-------|------|------|----------|------|
| LDOPT | +Z64.20000490.0000-261.609 261.609GLOB | | | | | | | | | | CMBMPTNP | 2K |
| LCSEL | 8E | 8N | 8S | 8W | 9E | 9N | 9S | 9W | 8NE | 8NW | 8SE | 8SW |
| LCSEL | 9NE | 9NW | 9SE | 9SW | 8ENE | 8ESE | 8NNE | 8NNW | 8SSE | 8SSW | 8WNW | 8WSW |
| LCSEL | 9ENE | 9ESE | 9NNE | 9NNW | 9SSE | 9SSW | 9WNW | 9WSW | | | | |
| FILE B | | | | | | | | | | | | |
| CDM | | | | | | | | | | | | |
| CDM | 22.00 | 0.500 | | 2.000 | | 0.800 | | 2.000 | | | | |
| CDM | 24.00 | 0.500 | | 2.000 | | 0.800 | | 2.000 | | | | |
| CDM | 26.00 | 0.500 | | 2.000 | | 0.800 | | 2.000 | | | | |
| CDM | 28.00 | 0.500 | | 2.000 | | 0.800 | | 2.000 | | | | |
| CDM | 30.00 | 0.500 | | 2.000 | | 0.800 | | 2.000 | | | | |

| | | | | | | | | |
|--------------|---------|-------|---------|--------|-------|---|--|------------|
| CDM | 53.00 | 0.500 | 2.000 | 0.800 | 2.000 | | | |
| CDM | 54.00 | 0.500 | 2.000 | 0.800 | 2.000 | | | |
| * | | | | | | | | |
| LOADCNSELF | | | | | | | | |
| DEAD | | | | | | | | |
| DEAD | -Z | | | | | M | | |
| LOAD | | | | | | | | |
| LOADCN OE | | | | | | | | |
| WAVE | | | | | | | | |
| WAVE1.00STOK | 5.09 | | 6.13 | 315.00 | | D | | MM10 1 0 5 |
| CURR | | | | | | | | |
| CURR | 0.382 | 1.274 | 315.000 | | 0.900 | | | CN FPS WDP |
| CURR | 50.000 | 1.840 | 315.000 | | | | | CN FPS WDP |
| CURR | 100.000 | 2.032 | 315.000 | | | | | CN FPS WDP |
| LOADCN ON | | | | | | | | |
| WAVE | | | | | | | | |
| WAVE1.00STOK | 1.31 | | 3.38 | 225.00 | | D | | MM10 1 0 5 |
| CURR | | | | | | | | |
| CURR | 0.382 | 0.384 | 225.000 | | 0.900 | | | CN FPS WDP |
| CURR | 50.000 | 0.554 | 225.000 | | | | | CN FPS WDP |
| CURR | 100.000 | 0.612 | 225.000 | | | | | CN FPS WDP |
| LOADCN OS | | | | | | | | |
| WAVE | | | | | | | | |
| WAVE1.00STOK | 1.12 | | 3.14 | 45.00 | | D | | MM10 1 0 5 |
| CURR | | | | | | | | |
| CURR | 0.382 | 0.206 | 45.000 | | 0.900 | | | CN FPS WDP |
| CURR | 50.000 | 0.298 | 45.000 | | | | | CN FPS WDP |
| CURR | 100.000 | 0.329 | 45.000 | | | | | CN FPS WDP |
| LOADCN OW | | | | | | | | |
| WAVE | | | | | | | | |
| WAVE1.00STOK | 1.31 | | 5.68 | 135.00 | | D | | MM10 1 0 5 |
| CURR | | | | | | | | |
| CURR | 0.382 | 0.924 | 135.000 | | 0.900 | | | CN FPS WDP |
| CURR | 50.000 | 1.336 | 135.000 | | | | | CN FPS WDP |
| CURR | 100.000 | 1.475 | 135.000 | | | | | CN FPS WDP |
| LOADCN 1E | | | | | | | | |
| WAVE | | | | | | | | |
| WAVE1.00STOK | 10.07 | | 7.95 | 315.00 | | D | | MM10 1 0 5 |
| CURR | | | | | | | | |
| CURR | 0.382 | 2.257 | 315.000 | | 0.900 | | | CN FPS WDP |
| CURR | 50.000 | 3.282 | 315.000 | | | | | CN FPS WDP |
| CURR | 100.000 | 3.601 | 315.000 | | | | | CN FPS WDP |
| LOADCN 1N | | | | | | | | |
| WAVE | | | | | | | | |
| WAVE1.00STOK | 4.63 | | 5.25 | 225.00 | | D | | MM10 1 0 5 |
| CURR | | | | | | | | |
| CURR | 0.382 | 0.632 | 225.000 | | 0.900 | | | CN FPS WDP |
| CURR | 50.000 | 0.914 | 225.000 | | | | | CN FPS WDP |
| CURR | 100.000 | 1.009 | 225.000 | | | | | CN FPS WDP |
| LOADCN 1S | | | | | | | | |
| WAVE | | | | | | | | |
| WAVE1.00STOK | 4.27 | | 4.65 | 45.00 | | D | | MM10 1 0 5 |
| CURR | | | | | | | | |
| CURR | 0.382 | 0.605 | 45.000 | | 0.900 | | | CN FPS WDP |
| CURR | 50.000 | 0.874 | 45.000 | | | | | CN FPS WDP |
| CURR | 100.000 | 0.964 | 45.000 | | | | | CN FPS WDP |
| LOADCN 1W | | | | | | | | |
| WAVE | | | | | | | | |
| WAVE1.00STOK | 4.43 | | 8.63 | 135.00 | | D | | MM10 1 0 5 |
| CURR | | | | | | | | |
| CURR | 0.382 | 1.240 | 45.000 | | 0.900 | | | CN FPS WDP |
| CURR | 50.000 | 1.792 | 45.000 | | | | | CN FPS WDP |
| CURR | 100.000 | 1.979 | 45.000 | | | | | CN FPS WDP |
| LOADCN ONE | | | | | | | | |
| WAVE | | | | | | | | |
| WAVE1.00STOK | 1.31 | | 3.30 | 270.00 | | D | | MM10 1 0 5 |
| CURR | | | | | | | | |
| CURR | 0.382 | 0.406 | 270.000 | | 0.900 | | | CN FPS WDP |
| CURR | 50.000 | 0.587 | 270.000 | | | | | CN FPS WDP |
| CURR | 100.000 | 0.648 | 270.000 | | | | | CN FPS WDP |
| LOADCN ONW | | | | | | | | |
| WAVE | | | | | | | | |
| WAVE1.00STOK | 2.13 | | 4.84 | 180.00 | | D | | MM10 1 0 5 |
| CURR | | | | | | | | |

| | | | | | | | | | |
|--------------|---------|-------|---------|--|--------|---|----|------|-------|
| CURR | 0.382 | 0.713 | 180.000 | | 0.900 | | CN | FPS | WDP |
| CURR | 50.000 | 1.030 | 180.000 | | | | CN | FPS | WDP |
| CURR | 100.000 | 1.138 | 180.000 | | | | CN | FPS | WDP |
| LOADCN 0SE | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 1.74 | | 3.48 | | 0. | D | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 0.437 | 0.000 | | 0.900 | | CN | FPS | WDP |
| CURR | 50.000 | 0.631 | | | | | CN | FPS | WDP |
| CURR | 100.000 | 0.697 | | | | | CN | FPS | WDP |
| LOADCN 0SW | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 0.85 | | 3.11 | | 90.00 | D | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 0.214 | 90.000 | | 0.900 | | CN | FPS | WDP |
| CURR | 50.000 | 0.309 | 90.000 | | | | CN | FPS | WDP |
| CURR | 100.000 | 0.341 | 90.000 | | | | CN | FPS | WDP |
| LOADCN 1NE | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 4.43 | | 5.53 | | 270.00 | D | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 0.784 | 270.000 | | 0.900 | | CN | FPS | WDP |
| CURR | 50.000 | 1.133 | 270.000 | | | | CN | FPS | WDP |
| CURR | 100.000 | 1.251 | 270.000 | | | | CN | FPS | WDP |
| LOADCN 1NW | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 12.66 | | 10.05 | | 180.00 | D | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 1.065 | 180.000 | | 0.900 | | CN | FPS | WDP |
| CURR | 50.000 | 1.539 | 180.000 | | | | CN | FPS | WDP |
| CURR | 100.000 | 1.699 | 180.000 | | | | CN | FPS | WDP |
| LOADCN 1SE | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 4.79 | | 5.66 | | 0. | D | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 1.194 | 0.000 | | 0.900 | | CN | FPS | WDP |
| CURR | 50.000 | 1.725 | | | | | CN | FPS | WDP |
| CURR | 100.000 | 1.904 | | | | | CN | FPS | WDP |
| LOADCN 1SW | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 5.74 | | 5.55 | | 90.00 | D | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 0.719 | 90.000 | | 0.900 | | CN | FPS | WDP |
| CURR | 50.000 | 1.039 | 90.000 | | | | CN | FPS | WDP |
| CURR | 100.000 | 1.147 | 90.000 | | | | CN | FPS | WDP |
| LOADCN0ENE | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 1.97 | | 3.64 | | 292.50 | D | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 0.699 | 292.500 | | 0.900 | | CN | FPS | WDP |
| CURR | 50.000 | 1.010 | 292.500 | | | | CN | FPS | WDP |
| CURR | 100.000 | 1.115 | 292.500 | | | | CN | FPS | WDP |
| LOADCN0ESE | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 4.23 | | 5.56 | | 337.50 | D | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 1.269 | 337.500 | | 0.900 | | CN | FPS | WDP |
| CURR | 50.000 | 1.834 | 337.500 | | | | CN | FPS | WDP |
| CURR | 100.000 | 2.025 | 337.500 | | | | CN | FPS | WDP |
| LOADCN0NNE | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 1.08 | | 3.32 | | 247.50 | D | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 0.347 | 247.500 | | 0.900 | | CN | FPS | WDP |
| CURR | 50.000 | 0.502 | 247.500 | | | | CN | FPS | WDP |
| CURR | 100.000 | 0.554 | 247.500 | | | | CN | FPS | WDP |
| LOADCN0NNW | | | | | | | | | |
| WAVE | | | | | | | | | |
| WAVE1.00STOK | 1.28 | | 3.33 | | 202.50 | D | | MM10 | 1 0 5 |
| CURR | | | | | | | | | |
| CURR | 0.382 | 0.484 | 202.500 | | 0.900 | | CN | FPS | WDP |
| CURR | 50.000 | 0.700 | 202.500 | | | | CN | FPS | WDP |
| CURR | 100.000 | 0.773 | 202.500 | | | | CN | FPS | WDP |
| LOADCN0SSE | | | | | | | | | |

| | | | | | | | | |
|--------------|---------|-------|---------|---|-------|------------|-------|--|
| WAVE | | | | | | | | |
| WAVE1.00STOK | 1.21 | 3.33 | 22.50 | D | | MM10 | 1 0 5 | |
| CURR | | | | | | | | |
| CURR | 0.382 | 0.269 | 22.500 | | 0.900 | CN FPS WDP | | |
| CURR | 50.000 | 0.389 | 22.500 | | | CN FPS WDP | | |
| CURR | 100.000 | 0.429 | 22.500 | | | CN FPS WDP | | |
| LOADCN0SSW | | | | | | | | |
| WAVE | | | | | | | | |
| WAVE1.00STOK | 1.05 | 3.09 | 67.50 | D | | MM10 | 1 0 5 | |
| CURR | | | | | | | | |
| CURR | 0.382 | 0.208 | 67.500 | | 0.900 | CN FPS WDP | | |
| CURR | 50.000 | 0.301 | 67.500 | | | CN FPS WDP | | |
| CURR | 100.000 | 0.332 | 67.500 | | | CN FPS WDP | | |
| LOADCN0WNW | | | | | | | | |
| WAVE | | | | | | | | |
| WAVE1.00STOK | 6.37 | 6.93 | 157.50 | D | | MM10 | 1 0 5 | |
| CURR | | | | | | | | |
| CURR | 0.382 | 1.262 | 157.500 | | 0.900 | CN FPS WDP | | |
| CURR | 50.000 | 1.824 | 157.500 | | | CN FPS WDP | | |
| CURR | 100.000 | 2.014 | 157.500 | | | CN FPS WDP | | |
| LOADCN0WSW | | | | | | | | |
| WAVE | | | | | | | | |
| WAVE1.00STOK | 1.64 | 3.69 | 112.50 | D | | MM10 | 1 0 5 | |
| CURR | | | | | | | | |
| CURR | 0.382 | 0.363 | 112.500 | | 0.900 | CN FPS WDP | | |
| CURR | 50.000 | 0.525 | 112.500 | | | CN FPS WDP | | |
| CURR | 100.000 | 0.579 | 112.500 | | | CN FPS WDP | | |
| LOADCN1ENE | | | | | | | | |
| WAVE | | | | | | | | |
| WAVE1.00STOK | 7.81 | 7.97 | 292.50 | D | | MM10 | 1 0 5 | |
| CURR | | | | | | | | |
| CURR | 0.382 | 0.962 | 292.500 | | 0.900 | CN FPS WDP | | |
| CURR | 50.000 | 1.390 | 292.500 | | | CN FPS WDP | | |
| CURR | 100.000 | 1.535 | 292.500 | | | CN FPS WDP | | |
| LOADCN1ESE | | | | | | | | |
| WAVE | | | | | | | | |
| WAVE1.00STOK | 7.09 | 6.97 | 337.50 | D | | MM10 | 1 0 5 | |
| CURR | | | | | | | | |
| CURR | 0.382 | 2.449 | 337.500 | | 0.900 | CN FPS WDP | | |
| CURR | 50.000 | 3.539 | 337.500 | | | CN FPS WDP | | |
| CURR | 100.000 | 3.908 | 337.500 | | | CN FPS WDP | | |
| LOADCN1NNE | | | | | | | | |
| WAVE | | | | | | | | |
| WAVE1.00STOK | 4.59 | 5.24 | 247.50 | D | | MM10 | 1 0 5 | |
| CURR | | | | | | | | |
| CURR | 0.382 | 0.648 | 247.500 | | 0.900 | CN FPS WDP | | |
| CURR | 50.000 | 0.936 | 247.500 | | | CN FPS WDP | | |
| CURR | 100.000 | 1.033 | 247.500 | | | CN FPS WDP | | |
| LOADCN1NNW | | | | | | | | |
| WAVE | | | | | | | | |
| WAVE1.00STOK | 4.10 | 6.22 | 202.50 | D | | MM10 | 1 0 5 | |
| CURR | | | | | | | | |
| CURR | 0.382 | 0.822 | 202.500 | | 0.900 | CN FPS WDP | | |
| CURR | 50.000 | 1.187 | 202.500 | | | CN FPS WDP | | |
| CURR | 100.000 | 1.311 | 202.500 | | | CN FPS WDP | | |
| LOADCN1SSE | | | | | | | | |
| WAVE | | | | | | | | |
| WAVE1.00STOK | 4.04 | 4.41 | 22.50 | D | | MM10 | 1 0 5 | |
| CURR | | | | | | | | |
| CURR | 0.382 | 0.821 | 22.500 | | 0.900 | CN FPS WDP | | |
| CURR | 50.000 | 1.186 | 22.500 | | | CN FPS WDP | | |
| CURR | 100.000 | 1.309 | 22.500 | | | CN FPS WDP | | |
| LOADCN1SSW | | | | | | | | |
| WAVE | | | | | | | | |
| WAVE1.00STOK | 5.09 | 5.61 | 67.50 | D | | MM10 | 1 0 5 | |
| CURR | | | | | | | | |
| CURR | 0.382 | 0.613 | 67.500 | | 0.900 | CN FPS WDP | | |
| CURR | 50.000 | 0.886 | 67.500 | | | CN FPS WDP | | |
| CURR | 100.000 | 0.978 | 67.500 | | | CN FPS WDP | | |
| LOADCN1WNW | | | | | | | | |
| WAVE | | | | | | | | |
| WAVE1.00STOK | 15.55 | 10.12 | 157.50 | D | | MM10 | 1 0 5 | |
| CURR | | | | | | | | |
| CURR | 0.382 | 1.560 | 157.500 | | 0.900 | CN FPS WDP | | |


```

CURR      50.000   2.255 157.500
CURR     100.000   2.490 157.500
LOADCN1WSW
WAVE
WAVE1.00STOK  5.94           6.28           112.50           D           MM10 1 0 5
CURR
CURR      0.382   0.898 112.500           0.900           CN FPS WDP
CURR     50.000   1.298 112.500           CN FPS WDP
CURR     100.000   1.433 112.500           CN FPS WDP
LCOMB
LCOMB 8E  0E  1.0000SELF1.0700TOPS1.0600
LCOMB 8N  0N  1.0000SELF1.0700TOPS1.0600
LCOMB 8S  0S  1.0000SELF1.0700TOPS1.0600
LCOMB 8W  0W  1.0000SELF1.0700TOPS1.0600
LCOMB 9E  1E  1.0000SELF1.0700TOPS1.0600
LCOMB 9N  1N  1.0000SELF1.0700TOPS1.0600
LCOMB 9S  1S  1.0000SELF1.0700TOPS1.0600
LCOMB 9W  1W  1.0000SELF1.0700TOPS1.0600
LCOMB 8NE 0NE 1.0000SELF1.0700TOPS1.0600
LCOMB 8NW 0NW 1.0000SELF1.0700TOPS1.0600
LCOMB 8SE 0SE 1.0000SELF1.0700TOPS1.0600
LCOMB 8SW 0SW 1.0000SELF1.0700TOPS1.0600
LCOMB 9NE 1NE 1.0000SELF1.0700TOPS1.0600
LCOMB 9NW 1NW 1.0000SELF1.0700TOPS1.0600
LCOMB 9SE 1SE 1.0000SELF1.0700TOPS1.0600
LCOMB 9SW 1SW 1.0000SELF1.0700TOPS1.0600
LCOMB 8ENE 0ENE1.0000SELF1.0700TOPS1.0600
LCOMB 8ESE 0ESE1.0000SELF1.0700TOPS1.0600
LCOMB 8NNE 0NNE1.0000SELF1.0700TOPS1.0600
LCOMB 8NNW 0NNW1.0000SELF1.0700TOPS1.0600
LCOMB 8SSE 0SSE1.0000SELF1.0700TOPS1.0600
LCOMB 8SSW 0SSW1.0000SELF1.0700TOPS1.0600
LCOMB 8WNW 0WNW1.0000SELF1.0700TOPS1.0600
LCOMB 8WSW 0WSW1.0000SELF1.0700TOPS1.0600
LCOMB 9ENE 1ENE1.0000SELF1.0700TOPS1.0600
LCOMB 9ESE 1ESE1.0000SELF1.0700TOPS1.0600
LCOMB 9NNE 1NNE1.0000SELF1.0700TOPS1.0600
LCOMB 9NNW 1NNW1.0000SELF1.0700TOPS1.0600
LCOMB 9SSE 1SSE1.0000SELF1.0700TOPS1.0600
LCOMB 9SSW 1SSW1.0000SELF1.0700TOPS1.0600
LCOMB 9WNW 1WNW1.0000SELF1.0700TOPS1.0600
LCOMB 9WSW 1WSW1.0000SELF1.0700TOPS1.0600
END

```

SEASTATE INPUT JACKET MODIFIKASI (SUPERELEMENT)

```

LDOPT      -Z64.20000490.0000-261.609 261.609GLOBEN           CMB
FILE B
*Addition for Superelement*
LOADCN
LOADCNWAVX
WAVE1.00STOK15.547           10.12           0           L           MM10 1 0 5
LOADCNWAVY
WAVE1.00STOK15.547           10.12           90.00           L           MM10 1 0 5
***
LCOMB
LCOMB SUPX WAVX  1.  DL  1.TOPS  1.
LCOMB SUPY WAVY  1.  DL  1.TOPS  1.
END

```

SEASTATE INPUT JACKET KONVENSIONAL (SUPERELEMENT)

```

LDOPT      -Z64.20000490.0000-261.609 261.609GLOB           CMB
FILE B
*Addition for Superelement*
LOADCN
LOADCNWAVX
WAVE1.00STOK15.547           10.12           0           L           MM10 1 0 5

```

```

LOADCNWAVY
WAVEL.00STOK15.547      10.12      90.00      L      MM10 1 0 5
***
LCOMB
LCOMB SUPX WAVX      1.SELF      1.TOPS      1.
LCOMB SUPY WAVY      1.SELF      1.TOPS      1.
END

```

PSI INPUT JACKET MODIFIKASI

```

PSIOPT +ZMN      SM      0.01      0.01 50PTPT      PT      100      0.05      7.85
PLTRQ SD      DT      RT      MT      ST      TS      UCE      PR      LG      XH
LCSEL IN      MASS SUPX SUPY

```

```

PLGRUP
*** PILE FOR ALL
PLGRUP PILE      162.566.3500 21.00      8.00 34.501.2192

```

```

FILE
** PILES
PILE1 01050156 PILE      SOL1
PILE2 02370239 PILE      SOL1
PILE3 02340236 PILE      SOL1
PILE4 00480149 PILE      SOL1
PILE5 00800150 PILE      SOL1
PILE6 00870151 PILE      SOL1
PILE7 02430245 PILE      SOL1
PILE8 00970152 PILE      SOL1
PILE9 02400242 PILE      SOL1

```

```

=====
SOIL
** SCOURING UNTIL 0.9 M DEPTH FROM MUDLINE
**
** DATA WAS TAKEN FROM 54 INCH PILES FACTOR WAS APPLIED AS FOLLOW;
** T-Z FACTOR
** SACS INPUT IS IN KN/CM2 , WHEREAS DATA PROVIDED IS IN KN/M
**
**          1/(100*PI*137.20)      = 2.32e-5 = TFAC
** SACS INPUT IS IN CM FOR Z, WHEREAS DATA PROVIDED IS IN MM,
**

```

```

=====
SOIL TZAXIAL HEAD 30 8      0.10SOL1
SOIL T-Z      SLOCSM      8 0.000 0.900      2.3E-5      1
SOIL      T-Z      0.00 0.000 0.000 0.0000.00000.00000.00000.00000.00000.00000
SOIL      T-Z      0.00000.00000.00000.00000.00000.00000.00000
SOIL T-Z      SLOCSM      8 0.9107.80      2.3E-5      2
SOIL      T-Z      15.320 2.19025.530 4.25038.2907.820045.95010.970
SOIL      T-Z      51.06013.72045.95027.43045.95068.580
SOIL T-Z      SLOCSM      8 7.801      2.3E-5      3
SOIL      T-Z      23.670 2.19039.440 4.25059.1607.820071.00010.970
SOIL      T-Z      78.88013.72071.00027.43071.00068.580
SOIL T-Z      SLOCSM      8 12.000      2.3E-5      4
SOIL      T-Z      33.350 2.19055.580 4.25083.3707.8200100.0510.970
SOIL      T-Z      111.1613.720100.0527.430100.0568.580
SOIL T-Z      SLOCSM      8 12.010      2.3E-5      5
SOIL      T-Z      31.440 2.19052.400 4.25078.6107.820094.33010.970
SOIL      T-Z      104.8113.72094.33027.43094.33068.580
SOIL T-Z      SLOCSM      8 27.000      2.3E-5      6
SOIL      T-Z      59.590 2.19099.320 4.250148.977.8200178.7710.970
SOIL      T-Z      198.6313.720178.7727.430178.7768.580
SOIL T-Z      SLOCSM      8 27.010      2.3E-5      7
SOIL      T-Z      62.500 2.190104.16 4.250156.247.8200187.4910.970
SOIL      T-Z      208.3313.720187.4927.430187.4968.580
SOIL T-Z      SLOCSM      8 31.500      2.3E-5      8
SOIL      T-Z      63.290 2.190105.48 4.250158.227.8200189.8710.970
SOIL      T-Z      210.9713.720189.8727.430189.8768.580
SOIL T-Z      SLOCSM      8 31.501      2.3E-5      9
SOIL      T-Z      59.870 2.19099.780 4.250149.667.8200179.6010.970
SOIL      T-Z      199.5513.720179.6027.430179.6068.580
SOIL T-Z      SLOCSM      8 37.800      2.3E-5      10
SOIL      T-Z      72.350 2.190120.58 4.250180.867.8200217.0410.970
SOIL      T-Z      241.1513.720217.0427.430217.0468.580
SOIL T-Z      SLOCSM      8 37.801      2.3E-5      11
SOIL      T-Z      70.540 2.190117.57 4.250176.367.8200211.6310.970
SOIL      T-Z      235.1513.720211.6327.430211.6368.580

```

| | | | | |
|----------|--------|--------------------------------------|-------------|-------------------------------|
| SOIL T-Z | SLOCSM | 8 50.000 | 2.3E-5 | 12 |
| SOIL | T-Z | 94.040 | 2.190156.73 | 4.250235.107.8200282.1210.970 |
| SOIL | T-Z | 313.4613.720282.1227.430282.1268.580 | | |
| SOIL T-Z | SLOCSM | 8 50.010 | 2.3E-5 | 13 |
| SOIL | T-Z | 93.410 | 2.190155.68 | 4.250233.537.8200280.2310.970 |
| SOIL | T-Z | 311.3713.720280.2327.430280.2368.580 | | |
| SOIL T-Z | SLOCSM | 8 57.000 | 2.3E-5 | 14 |
| SOIL | T-Z | 111.24 | 2.190185.41 | 4.250278.117.8200333.7310.970 |
| SOIL | T-Z | 370.8213.720333.7327.430333.7368.580 | | |
| SOIL T-Z | SLOCSM | 8 57.010 | 2.3E-5 | 15 |
| SOIL | T-Z | 138.75 | 2.190231.24 | 4.250346.877.8200416.2410.970 |
| SOIL | T-Z | 462.4913.720416.2427.430416.2468.580 | | |
| SOIL T-Z | SLOCSM | 8 66.600 | 2.3E-5 | 16 |
| SOIL | T-Z | 122.81 | 2.190204.68 | 4.250307.027.8200368.4210.970 |
| SOIL | T-Z | 409.3613.720368.4227.430368.4268.580 | | |
| SOIL T-Z | SLOCSM | 8 66.610 | 2.3E-5 | 17 |
| SOIL | T-Z | 128.05 | 2.190213.42 | 4.250320.137.8200384.1610.970 |
| SOIL | T-Z | 426.8413.720384.1627.430384.1668.580 | | |
| SOIL T-Z | SLOCSM | 8 72.500 | 2.3E-5 | 18 |
| SOIL | T-Z | 129.27 | 2.190215.45 | 4.250323.187.8200387.8110.970 |
| SOIL | T-Z | 430.9013.720387.8127.430387.8168.580 | | |
| SOIL T-Z | SLOCSM | 8 72.510 | 2.3E-5 | 19 |
| SOIL | T-Z | 147.37 | 2.190245.62 | 4.250368.427.8200442.1110.970 |
| SOIL | T-Z | 491.2313.720442.1127.430442.1168.580 | | |
| SOIL T-Z | SLOCSM | 8 80.000 | 2.3E-5 | 20 |
| SOIL | T-Z | 164.53 | 2.190274.22 | 4.250411.337.8200493.6010.970 |
| SOIL | T-Z | 548.4513.720493.6027.430493.6068.580 | | |
| SOIL T-Z | SLOCSM | 8 80.100 | 2.3E-5 | 21 |
| SOIL | T-Z | 155.93 | 2.190259.88 | 4.250389.827.8200467.7910.970 |
| SOIL | T-Z | 519.7713.720467.7927.430467.7968.580 | | |
| SOIL T-Z | SLOCSM | 8 82.700 | 2.3E-5 | 22 |
| SOIL | T-Z | 184.64 | 2.190307.73 | 4.250461.607.8200553.9210.970 |
| SOIL | T-Z | 615.4613.720553.9227.430553.9268.580 | | |
| SOIL T-Z | SLOCSM | 8 82.710 | 2.3E-5 | 23 |
| SOIL | T-Z | 186.74 | 2.190311.23 | 4.250466.847.8200560.2110.970 |
| SOIL | T-Z | 622.4613.720560.2127.430560.2168.580 | | |
| SOIL T-Z | SLOCSM | 8 88.000 | 2.3E-5 | 24 |
| SOIL | T-Z | 195.18 | 2.190325.30 | 4.250487.957.8200585.5410.970 |
| SOIL | T-Z | 650.5913.720585.5427.430585.5468.580 | | |
| SOIL T-Z | SLOCSM | 8 88.010 | 2.3E-5 | 25 |
| SOIL | T-Z | 192.10 | 2.190320.17 | 4.250480.267.8200576.3110.970 |
| SOIL | T-Z | 640.3513.720576.3127.430576.3168.580 | | |
| SOIL T-Z | SLOCSM | 8 104.10 | 2.3E-5 | 26 |
| SOIL | T-Z | 224.69 | 2.190374.48 | 4.250561.727.8200674.0610.970 |
| SOIL | T-Z | 748.9513.720674.0627.430674.0668.580 | | |
| SOIL T-Z | SLOCSM | 8 104.11 | 2.3E-5 | 27 |
| SOIL | T-Z | 689.44 | 2.540689.44 | 5.080689.4412.700689.4425.400 |
| SOIL | T-Z | 689.4450.800689.44127.00689.44254.00 | | |
| SOIL T-Z | SLOCSM | 8 122.30 | 2.3E-5 | 28 |
| SOIL | T-Z | 732.53 | 2.540732.53 | 5.080732.5312.700732.5325.400 |
| SOIL | T-Z | 732.5350.800732.53127.00732.53254.00 | | |
| SOIL T-Z | SLOCSM | 8 122.31 | 2.3E-5 | 29 |
| SOIL | T-Z | 259.84 | 2.190433.07 | 4.250649.607.8200779.5210.970 |
| SOIL | T-Z | 866.1313.720779.5227.430779.5268.580 | | |
| SOIL T-Z | SLOCSM | 8 125.00 | 2.3E-5 | 30 |
| SOIL | T-Z | 259.84 | 2.190433.12 | 4.250649.687.8200779.6210.970 |
| SOIL | T-Z | 866.2413.720779.5227.430779.6268.580 | | |

*
*

```

**=====
** Q - Z FACTOR
** DIVIDE BY AREA OF PILES AREA (kN TO kN/cm^2)
** PLUGGED AREA = (PI*((137.2)^2)/4 = 14784.21 CM2
** MULTIPLYING FACTOR = 1/14784.20 = 6.76E-5
** SACS INPUT IS IN CM FOR Z, WHEREAS DATA PROVIDED IS IN MM,
**
**=====
SOIL BEARING HEAD 11 0.1 SOL1
SOIL T-Z SLOCSM 8 80.000 6.7E-5 1
SOIL T-Z 0.00000.0000432.19 2.740864.37 17.831158.3 34.291296.657.610
SOIL T-Z 1555.8100.131728.8137.161728.8685.80
SOIL T-Z SLOCSM 8 80.010 6.7E-5 2
SOIL T-Z 0.00000.0000398.94 2.740797.88 17.831069.1 34.291196.857.610
SOIL T-Z 1436.2100.131595.8137.161595.8685.80

```

SOIL T-Z SLOCSM 8 82.700 6.7E-5 3
SOIL T-Z 0.00000.0000515.30 2.7401030.6 17.831381.0 34.291545.957.610
SOIL T-Z 1855.1100.132061.2137.162061.2685.80
SOIL T-Z SLOCSM 8 82.710 6.7E-5 4
SOIL T-Z 0.00000.0000531.92 2.7401063.8 17.831425.6 34.291595.757.610
SOIL T-Z 1914.9100.132127.6137.162127.6685.80
SOIL T-Z SLOCSM 8 88.000 6.7E-5 5
SOIL T-Z 0.00000.0000531.92 2.7401063.8 17.831425.6 34.291595.757.610
SOIL T-Z 1914.9100.132127.6137.162127.6685.80
SOIL T-Z SLOCSM 8 88.010 6.7E-5 6
SOIL T-Z 0.00000.0000515.30 2.7401030.6 17.831381.0 34.291545.957.610
SOIL T-Z 1855.1100.132061.2137.162061.2685.80
SOIL T-Z SLOCSM 8 104.10 6.7E-5 7
SOIL T-Z 0.00000.0000598.41 2.7401196.8 17.831603.7 34.291795.257.610
SOIL T-Z 2154.3100.132393.6137.162393.6685.80
SOIL T-Z SLOCSM 8 104.11 6.7E-5 8
SOIL T-Z 0.00000.0000531.92 2.7401063.8 17.831425.6 34.291595.857.610
SOIL T-Z 1914.9100.132127.7137.162127.7685.80
SOIL T-Z SLOCSM 8 122.30 6.7E-5 9
SOIL T-Z 0.00000.0000565.17 2.7401130.3 17.831514.6 34.291695.557.610
SOIL T-Z 2034.6100.132260.6137.162260.7685.80
SOIL T-Z SLOCSM 8 122.31 6.7E-5 10
SOIL T-Z 0.00000.0000664.90 2.7401329.8 17.831781.9 34.291994.757.610
SOIL T-Z 2393.7100.132659.6137.162659.6685.80
SOIL T-Z SLOCSM 8 125.00 6.7E-5 11
SOIL T-Z 0.00000.0000664.90 2.7401329.8 17.831781.9 34.291994.757.610
SOIL T-Z 2393.7100.132659.6137.162659.6685.80

*

SOIL TORSION HEAD 20000.0SOL1TORSIONAL SPRING

SOIL LATERAL HEAD 93 YEXP137.20 0.10SOL1P-Y
SOIL P-Y SLOCSM 7 0.9000 0.01 1
SOIL P-Y 0.00000.00000.00000.00000.00000.00000.00000.00000.00000.0000
SOIL P-Y 0.00000.00000.00000.0000
SOIL P-Y SLOCSM 7 1.0000 1.00 2
SOIL P-Y 0.00000.00003.86006.86005.530020.5708.390068.58012.070205.74
SOIL P-Y 1.08001028.71.08002057.4
SOIL P-Y SLOCSM 7 2.0000 0.01 3
SOIL P-Y 0.00000.00008.30006.860011.91020.57018.05068.58026.000205.74
SOIL P-Y 4.64001028.74.64002057.4
SOIL P-Y SLOCSM 7 3.0000 1.00 4
SOIL P-Y 0.00000.000013.3406.860019.14020.57029.00068.58041.760205.74
SOIL P-Y 11.1901028.711.1902057.4
SOIL P-Y SLOCSM 7 4.0000 0.01 5
SOIL P-Y 0.00000.000018.9706.860027.21020.57041.23068.58059.380205.74
SOIL P-Y 21.2101028.721.2102057.4
SOIL P-Y SLOCSM 7 5.0000 0.01 6
SOIL P-Y 0.00000.000025.1805.140036.13015.43054.75051.44078.840154.31
SOIL P-Y 35.190771.5335.1901543.0
SOIL P-Y SLOCSM 7 6.0000 1.00 7
SOIL P-Y 0.00000.000031.9905.140045.90015.43069.54051.440100.14154.31
SOIL P-Y 53.650771.5353.6501543.0
SOIL P-Y SLOCSM 7 6.9000 0.01 8
SOIL P-Y 0.00000.000038.6205.140055.41015.43083.95051.440120.89154.31
SOIL P-Y 74.480771.5374.4801543.0
SOIL P-Y SLOCSM 7 7.8000 0.01 9
SOIL P-Y 0.00000.000045.7305.140065.61015.43099.41051.440143.14154.31
SOIL P-Y 99.690771.5399.6901543.0
SOIL P-Y SLOCSM 7 7.8010 0.01 10
SOIL P-Y 0.00000.000091.9405.1400131.9215.430199.8851.440287.83154.31
SOIL P-Y 200.45771.53200.451543.0
SOIL P-Y SLOCSM 7 8.8000 0.01 11
SOIL P-Y 0.00000.0000101.215.1400145.2215.430220.0251.440316.83154.31
SOIL P-Y 248.94771.53248.941543.0
SOIL P-Y SLOCSM 7 9.8000 0.01 12
SOIL P-Y 0.00000.0000110.755.1400158.9015.430240.7651.440346.70154.31
SOIL P-Y 303.36771.53303.361543.0
SOIL P-Y SLOCSM 7 10.900 0.01 13
SOIL P-Y 0.00000.0000121.565.1400174.4115.430264.2651.440380.54154.31
SOIL P-Y 370.34771.53370.341543.0
SOIL P-Y SLOCSM 7 12.000 0.01 14
SOIL P-Y 0.00000.0000127.765.1400183.3115.430277.7551.440399.96154.31
SOIL P-Y 399.96771.53399.961543.0

| | | | | | |
|----------|--------|--|--------|------|----|
| SOIL P-Y | SLOCSM | 7 | 12.010 | 0.01 | 15 |
| SOIL | P-Y | 0.00000.0000113.575.1400162.9515.430246.8951.440355.52154.31 | | | |
| SOIL | P-Y | 355.521543.0355.521543.0 | | | |
| SOIL P-Y | SLOCSM | 7 | 13.900 | 0.01 | 16 |
| SOIL | P-Y | 0.00000.0000120.765.1400173.2715.430262.5251.440378.03154.31 | | | |
| SOIL | P-Y | 378.031543.0378.031543.0 | | | |
| SOIL P-Y | SLOCSM | 7 | 15.800 | 0.01 | 17 |
| SOIL | P-Y | 0.00000.0000127.955.1400183.5915.430278.1651.440400.55154.31 | | | |
| SOIL | P-Y | 400.551543.0400.551543.0 | | | |
| SOIL P-Y | SLOCSM | 7 | 17.700 | 0.01 | 18 |
| SOIL | P-Y | 0.00000.0000135.155.1400193.9115.430293.8051.440423.07154.31 | | | |
| SOIL | P-Y | 423.071543.0423.071543.0 | | | |
| SOIL P-Y | SLOCSM | 7 | 19.600 | 0.01 | 19 |
| SOIL | P-Y | 0.00000.0000142.345.1400204.2315.430309.4351.440445.58154.31 | | | |
| SOIL | P-Y | 445.581543.0445.581543.0 | | | |
| SOIL P-Y | SLOCSM | 7 | 21.500 | 0.01 | 20 |
| SOIL | P-Y | 0.00000.0000149.533.4300214.5510.290325.0734.290468.10102.87 | | | |
| SOIL | P-Y | 468.101028.7468.101028.7 | | | |
| SOIL P-Y | SLOCSM | 7 | 23.400 | 0.01 | 21 |
| SOIL | P-Y | 0.00000.0000156.723.4300224.8710.290340.7134.290490.62102.87 | | | |
| SOIL | P-Y | 490.621028.7490.621028.7 | | | |
| SOIL P-Y | SLOCSM | 7 | 25.200 | 0.01 | 22 |
| SOIL | P-Y | 0.00000.0000163.543.4300234.6410.290355.5234.290511.95102.87 | | | |
| SOIL | P-Y | 511.951028.7511.951028.7 | | | |
| SOIL P-Y | SLOCSM | 7 | 27.000 | 0.01 | 23 |
| SOIL | P-Y | 0.00000.0000170.353.4300244.4210.290370.3334.290533.28102.87 | | | |
| SOIL | P-Y | 533.281028.7533.281028.7 | | | |
| SOIL P-Y | SLOCSM | 7 | 27.010 | 0.01 | 24 |
| SOIL | P-Y | 0.00000.0000187.393.4300268.8610.290407.3734.290586.61102.87 | | | |
| SOIL | P-Y | 586.611028.7586.611028.7 | | | |
| SOIL P-Y | SLOCSM | 7 | 28.100 | 0.01 | 25 |
| SOIL | P-Y | 0.00000.0000181.143.4300259.9010.290393.7934.290567.05102.87 | | | |
| SOIL | P-Y | 567.051028.7567.051028.7 | | | |
| SOIL P-Y | SLOCSM | 7 | 29.200 | 0.01 | 26 |
| SOIL | P-Y | 0.00000.0000174.903.4300250.9410.290380.2134.290547.50102.87 | | | |
| SOIL | P-Y | 547.501028.7547.501028.7 | | | |
| SOIL P-Y | SLOCSM | 7 | 30.300 | 0.01 | 27 |
| SOIL | P-Y | 0.00000.0000168.653.4300241.9710.290366.6334.290527.95102.87 | | | |
| SOIL | P-Y | 527.951028.7527.951028.7 | | | |
| SOIL P-Y | SLOCSM | 7 | 31.500 | 0.01 | 28 |
| SOIL | P-Y | 0.00000.0000161.843.4300232.2010.290351.8234.290506.61102.87 | | | |
| SOIL | P-Y | 506.611028.7506.611028.7 | | | |
| SOIL P-Y | SLOCSM | 7 | 31.510 | 0.01 | 29 |
| SOIL | P-Y | 0.00000.0000144.803.4300207.7610.290314.7834.290453.29102.87 | | | |
| SOIL | P-Y | 453.291028.7453.291028.7 | | | |
| SOIL P-Y | SLOCSM | 7 | 32.500 | 0.01 | 30 |
| SOIL | P-Y | 0.00000.0000149.313.4300214.2210.290324.5834.290467.39102.87 | | | |
| SOIL | P-Y | 467.391028.7467.391028.7 | | | |
| SOIL P-Y | SLOCSM | 7 | 33.500 | 0.01 | 31 |
| SOIL | P-Y | 0.00000.0000153.813.4300220.6910.290334.3834.290481.50102.87 | | | |
| SOIL | P-Y | 481.501028.7481.501028.7 | | | |
| SOIL P-Y | SLOCSM | 7 | 34.500 | 0.01 | 32 |
| SOIL | P-Y | 0.00000.0000158.323.4300227.1510.290344.1734.290495.61102.87 | | | |
| SOIL | P-Y | 495.611028.7495.611028.7 | | | |
| SOIL P-Y | SLOCSM | 7 | 35.600 | 0.01 | 33 |
| SOIL | P-Y | 0.00000.0000163.283.4300234.2710.290354.9534.290511.13102.87 | | | |
| SOIL | P-Y | 511.131028.7511.131028.7 | | | |
| SOIL P-Y | SLOCSM | 7 | 36.700 | 0.01 | 34 |
| SOIL | P-Y | 0.00000.0000168.233.4300241.3810.290365.7334.290526.65102.87 | | | |
| SOIL | P-Y | 526.651028.7526.651028.7 | | | |
| SOIL P-Y | SLOCSM | 7 | 37.800 | 0.01 | 35 |
| SOIL | P-Y | 0.00000.0000173.193.4300248.4910.290376.5034.290542.17102.87 | | | |
| SOIL | P-Y | 542.171028.7542.171028.7 | | | |
| SOIL P-Y | SLOCSM | 7 | 37.800 | 0.01 | 36 |
| SOIL | P-Y | 0.00000.0000164.673.4300236.2710.290357.9934.290515.50102.87 | | | |
| SOIL | P-Y | 515.501028.7515.501028.7 | | | |
| SOIL P-Y | SLOCSM | 7 | 39.800 | 0.01 | 37 |
| SOIL | P-Y | 0.00000.0000172.593.4300247.6210.290375.1934.290540.27102.87 | | | |
| SOIL | P-Y | 540.271028.7540.271028.7 | | | |
| SOIL P-Y | SLOCSM | 7 | 41.800 | 0.01 | 38 |
| SOIL | P-Y | 0.00000.0000180.503.4300258.9810.290392.3934.290565.04102.87 | | | |
| SOIL | P-Y | 565.041028.7565.041028.7 | | | |
| SOIL P-Y | SLOCSM | 7 | 43.800 | 0.01 | 39 |
| SOIL | P-Y | 0.00000.0000188.413.4300270.3310.290409.5934.290589.81102.87 | | | |

| | | |
|----------|--------|--|
| SOIL | P-Y | 589.811028.7589.811028.7 |
| SOIL P-Y | SLOCSM | 7 46.800 0.01 40 |
| SOIL | P-Y | 0.00000.0000200.283.4300287.3610.290435.3934.290626.97102.87 |
| SOIL | P-Y | 626.971028.7626.971028.7 |
| SOIL P-Y | SLOCSM | 7 50.000 0.01 41 |
| SOIL | P-Y | 0.00000.0000212.943.4300305.5210.290462.9234.290666.60102.87 |
| SOIL | P-Y | 666.601028.7666.601028.7 |
| SOIL P-Y | SLOCSM | 7 50.010 0.01 42 |
| SOIL | P-Y | 0.00000.0000210.103.4300301.4510.290456.7434.290657.71102.87 |
| SOIL | P-Y | 657.711028.7657.711028.7 |
| SOIL P-Y | SLOCSM | 7 51.800 0.01 43 |
| SOIL | P-Y | 0.00000.0000221.783.4300318.2110.290482.1434.290694.28102.87 |
| SOIL | P-Y | 694.281028.7694.281028.7 |
| SOIL P-Y | SLOCSM | 7 53.600 0.01 44 |
| SOIL | P-Y | 0.00000.0000233.463.4300334.9710.290507.5334.290730.84102.87 |
| SOIL | P-Y | 730.841028.7730.841028.7 |
| SOIL P-Y | SLOCSM | 7 55.400 0.01 45 |
| SOIL | P-Y | 0.00000.0000245.153.4300351.7310.290532.9334.290767.41102.87 |
| SOIL | P-Y | 767.411028.7767.411028.7 |
| SOIL P-Y | SLOCSM | 7 57.000 0.01 46 |
| SOIL | P-Y | 0.00000.0000255.533.4300366.6310.290555.5034.290799.92102.87 |
| SOIL | P-Y | 799.921028.7799.921028.7 |
| SOIL P-Y | SLOCSM | 7 57.010 0.01 47 |
| SOIL | P-Y | 0.00000.0000397.491.7100570.315.1400864.1117.1501244.351.440 |
| SOIL | P-Y | 1244.3514.351244.3514.35 |
| SOIL P-Y | SLOCSM | 7 58.900 0.01 48 |
| SOIL | P-Y | 0.00000.0000372.201.7100534.035.1400809.1417.1501165.151.440 |
| SOIL | P-Y | 1165.1514.351165.1514.35 |
| SOIL P-Y | SLOCSM | 7 60.800 0.01 49 |
| SOIL | P-Y | 0.00000.0000346.921.7100497.755.1400754.1717.1501086.051.440 |
| SOIL | P-Y | 1086.0514.351086.0514.35 |
| SOIL P-Y | SLOCSM | 7 62.700 0.01 50 |
| SOIL | P-Y | 0.00000.0000321.631.7100461.475.1400699.1917.1501006.851.440 |
| SOIL | P-Y | 1006.8514.351006.8514.35 |
| SOIL P-Y | SLOCSM | 7 64.600 0.01 51 |
| SOIL | P-Y | 0.00000.0000296.341.7100425.195.1400644.2217.150927.6851.440 |
| SOIL | P-Y | 927.68514.35927.68514.35 |
| SOIL P-Y | SLOCSM | 7 66.600 0.01 52 |
| SOIL | P-Y | 0.00000.0000269.731.7100387.005.1400586.3617.150844.3651.440 |
| SOIL | P-Y | 844.36514.35844.36514.35 |
| SOIL P-Y | SLOCSM | 7 66.610 0.01 53 |
| SOIL | P-Y | 0.00000.0000283.921.7100407.375.1400617.2217.150888.8051.440 |
| SOIL | P-Y | 888.80514.35888.80514.35 |
| SOIL P-Y | SLOCSM | 7 68.600 0.01 54 |
| SOIL | P-Y | 0.00000.0000283.921.7100407.375.1400617.2217.150888.8051.440 |
| SOIL | P-Y | 888.80514.35888.80514.35 |
| SOIL P-Y | SLOCSM | 7 70.600 0.01 55 |
| SOIL | P-Y | 0.00000.0000283.921.7100407.375.1400617.2217.150888.8051.440 |
| SOIL | P-Y | 888.80514.35888.80514.35 |
| SOIL P-Y | SLOCSM | 7 72.500 0.01 56 |
| SOIL | P-Y | 0.00000.0000283.921.7100407.375.1400617.2217.150888.8051.440 |
| SOIL | P-Y | 888.80514.35888.80514.35 |
| SOIL P-Y | SLOCSM | 7 72.510 0.01 57 |
| SOIL | P-Y | 0.00000.0000340.711.7100488.845.1400740.6617.1501066.551.440 |
| SOIL | P-Y | 1066.5514.351066.5514.35 |
| SOIL P-Y | SLOCSM | 7 74.400 0.01 58 |
| SOIL | P-Y | 0.00000.0000347.901.7100499.165.1400756.3017.1501089.051.440 |
| SOIL | P-Y | 1089.0514.351089.0514.35 |
| SOIL P-Y | SLOCSM | 7 76.300 0.01 59 |
| SOIL | P-Y | 0.00000.0000355.091.7100509.485.1400771.9417.1501111.551.440 |
| SOIL | P-Y | 1111.5514.351111.5514.35 |
| SOIL P-Y | SLOCSM | 7 78.200 0.01 60 |
| SOIL | P-Y | 0.00000.0000362.281.7100519.805.1400787.5717.1501134.151.440 |
| SOIL | P-Y | 1134.1514.351134.1514.35 |
| SOIL P-Y | SLOCSM | 7 80.000 0.01 61 |
| SOIL | P-Y | 0.00000.0000369.101.7100529.575.1400802.3917.1501155.451.440 |
| SOIL | P-Y | 1155.4514.351155.4514.35 |
| SOIL P-Y | SLOCSM | 7 80.010 0.01 62 |
| SOIL | P-Y | 0.00000.0000340.711.7100488.845.1400740.6617.1501066.551.440 |
| SOIL | P-Y | 1066.5514.351066.5514.35 |
| SOIL P-Y | SLOCSM | 7 81.300 0.01 63 |
| SOIL | P-Y | 0.00000.0000388.551.7100557.495.1400844.6817.1501216.351.440 |
| SOIL | P-Y | 1216.3514.351216.3514.35 |
| SOIL P-Y | SLOCSM | 7 82.700 0.01 64 |

SOIL P-Y 0.00000.0000440.081.7100631.425.1400956.6917.1501377.651.440
 SOIL P-Y 1377.6514.351377.6514.35
 SOIL P-Y SLOCSM 7 82.710 0.01 65
 SOIL P-Y 0.00000.0000454.271.7100651.785.1400987.5517.1501422.051.440
 SOIL P-Y 1422.0514.351422.0514.35
 SOIL P-Y SLOCSM 7 84.500 0.01 66
 SOIL P-Y 0.00000.0000454.271.7100651.785.1400987.5517.1501422.051.440
 SOIL P-Y 1422.0514.351422.0514.35
 SOIL P-Y SLOCSM 7 86.300 0.01 67
 SOIL P-Y 0.00000.0000454.271.7100651.785.1400987.5517.1501422.051.440
 SOIL P-Y 1422.0514.351422.0514.35
 SOIL P-Y SLOCSM 7 88.000 0.01 68
 SOIL P-Y 0.00000.0000454.271.7100651.785.1400987.5517.1501422.051.440
 SOIL P-Y 1422.0514.351422.0514.35
 SOIL P-Y SLOCSM 7 88.010 0.01 69
 SOIL P-Y 0.00000.0000440.081.7100631.425.1400956.6917.1501377.651.440
 SOIL P-Y 1377.6514.351377.6514.35
 SOIL P-Y SLOCSM 7 92.000 0.01 70
 SOIL P-Y 0.00000.0000457.711.7100656.725.1400995.0317.1501432.851.440
 SOIL P-Y 1432.8514.351432.8514.35
 SOIL P-Y SLOCSM 7 100.00 0.01 71
 SOIL P-Y 0.00000.0000492.981.7100707.325.14001071.717.1501543.251.440
 SOIL P-Y 1543.2514.351543.2514.35
 SOIL P-Y SLOCSM 7 104.10 0.01 72
 SOIL P-Y 0.00000.0000511.061.7100733.265.14001111.017.1501599.851.440
 SOIL P-Y 1599.8514.351599.8514.35
 SOIL P-Y SLOCSM 7 104.10 0.01 73
 SOIL P-Y 0.00000.0000454.271.7100651.785.1400987.5517.1501422.051.440
 SOIL P-Y 1422.0514.351422.0514.35
 SOIL P-Y SLOCSM 7 108.00 0.01 74
 SOIL P-Y 0.00000.0000460.361.7100660.515.14001000.717.1501441.151.440
 SOIL P-Y 1441.1514.351441.1514.35
 SOIL P-Y SLOCSM 7 112.00 0.01 75
 SOIL P-Y 0.00000.0000466.601.7100669.475.14001014.317.1501460.651.440
 SOIL P-Y 1460.6514.351460.6514.35
 SOIL P-Y SLOCSM 7 116.00 0.01 76
 SOIL P-Y 0.00000.0000472.841.7100678.425.14001027.917.1501480.151.440
 SOIL P-Y 1480.1514.351480.1514.35
 SOIL P-Y SLOCSM 7 119.00 0.01 77
 SOIL P-Y 0.00000.0000477.521.7100685.135.14001038.017.1501494.851.440
 SOIL P-Y 1494.8514.351494.8514.35
 SOIL P-Y SLOCSM 7 122.30 0.01 78
 SOIL P-Y 0.00000.0000482.671.7100692.525.14001049.217.1501510.951.440
 SOIL P-Y 1510.9514.351510.9514.35
 SOIL P-Y SLOCSM 7 122.30 0.01 79
 SOIL P-Y 0.00000.0000567.841.7100814.735.14001234.417.1501777.551.440
 SOIL P-Y 1777.5514.351777.5514.35
 SOIL P-Y SLOCSM 7 124.00 0.01 80
 SOIL P-Y 0.00000.0000567.841.7100814.735.14001234.417.1501777.551.440
 SOIL P-Y 1777.5514.351777.5514.35
 SOIL P-Y SLOCSM 7 125.00 0.01 81
 SOIL P-Y 0.00000.0000567.841.7100814.735.14001234.417.1501777.551.440
 SOIL P-Y 1777.5514.351777.5514.35
 SOIL P-Y SLOCSM 7 125.01 0.01 82
 SOIL P-Y 0.00000.0000511.061.7100733.265.14001111.017.1501599.851.440
 SOIL P-Y 1599.8514.351599.8514.35
 SOIL P-Y SLOCSM 7 126.50 0.01 83
 SOIL P-Y 0.00000.0000511.061.7100733.265.14001111.017.1501599.851.440
 SOIL P-Y 1599.8514.351599.8514.35
 SOIL P-Y SLOCSM 7 128.00 0.01 84
 SOIL P-Y 0.00000.0000511.061.7100733.265.14001111.017.1501599.851.440
 SOIL P-Y 1599.8514.351599.8514.35
 SOIL P-Y SLOCSM 7 128.01 0.01 85
 SOIL P-Y 0.00000.00003909.45.72005171.17.62007585.811.4308948.013.720
 SOIL P-Y 13598.22.86020536.51.440
 SOIL P-Y SLOCSM 7 128.70 0.01 86
 SOIL P-Y 0.00000.00003930.85.72005199.47.62007627.211.4308996.913.720
 SOIL P-Y 13673.22.86020649.51.440
 SOIL P-Y SLOCSM 7 129.40 0.01 87
 SOIL P-Y 0.00000.00003952.15.72005227.77.62007668.711.4309045.813.720
 SOIL P-Y 13747.22.86020761.51.440
 SOIL P-Y SLOCSM 7 129.41 0.01 88
 SOIL P-Y 0.00000.0000425.881.7100611.055.1400925.8317.1501333.251.440
 SOIL P-Y 1333.2514.351333.2514.35

```

SOIL P-Y      SLOCSM  7 131.70      0.01    89
SOIL          P-Y 0.00000.0000476.671.7100683.925.14001036.217.1501492.151.440
SOIL          P-Y 1492.1514.351492.1514.35
SOIL P-Y      SLOCSM  7 133.00      0.01    90
SOIL          P-Y 0.00000.0000505.381.7100725.115.14001098.617.1501582.051.440
SOIL          P-Y 1582.0514.351582.0514.35
SOIL P-Y      SLOCSM  7 133.00      0.01    91
SOIL          P-Y 0.00000.00008254.75.720010898.7.620015908.11.43018695.13.720
SOIL          P-Y 27902.22.86040086.51.440
SOIL P-Y      SLOCSM  7 134.00      0.01    92
SOIL          P-Y 0.00000.00008316.75.720010980.7.620016028.11.43018836.13.720
SOIL          P-Y 28112.22.86040388.51.440
SOIL P-Y      SLOCSM  7 135.00      0.01    93
SOIL          P-Y 0.00000.00008378.85.720011062.7.620016147.11.43018976.13.720
SOIL          P-Y 28322.22.86040689.51.440
END

```

PSI INPUT JACKET KONVENTIONAL

```

PSIOPT +ZMN      SM      0.01      0.01 50PTPT      PT      100      0.05      7.85
PLTRQ SD  DT  RT  MT  ST  TS      UCE  PR  LG  XH
LCSEL IN      MASS SUPX SUPY
PLGRUP
*** PILE FOR ALL
PLGRUP PIA      96.526.3500 21.00  8.00 34.50 10.872
PLGRUP PIB      96.526.3500 21.00  8.00 34.50 10.746
PILE
** PILES
PILE1 108P107P PIA      SOL1
PILE2 208P207P PIB      SOL1
PILE3 308P307P PIB      SOL1
*=====
SOIL
** SCOURING UNTIL 0.9 M DEPTH FROM MUDLINE
*=====
** DATA WAS TAKEN FROM 54 INCH PILES FACTOR WAS APPLIED AS FOLLOW;
** T-Z FACTOR
** SACS INPUT IS IN KN/CM2 , WHEREAS DATA PROVIDED IS IN KN/M
**
**          1/(100*PI*137.20)      = 2.32e-5 = TFAC
** SACS INPUT IS IN CM FOR Z, WHEREAS DATA PROVIDED IS IN MM,
** =====
SOIL TZAXIAL HEAD 30 8      0.10SOL1
SOIL T-Z      SLOCSM  8 0.000 0.900      2.3E-5      1
SOIL          T-Z 0.00 0.000 0.000 0.0000.00000.00000.00000.00000.00000.0000
SOIL          T-Z 0.00000.00000.00000.00000.00000.00000
SOIL T-Z      SLOCSM  8 0.9107.80      2.3E-5      2
SOIL          T-Z          15.320 2.19025.530 4.25038.2907.820045.95010.970
SOIL          T-Z 51.06013.72045.95027.43045.95068.580
SOIL T-Z      SLOCSM  8 7.801      2.3E-5      3
SOIL          T-Z          23.670 2.19039.440 4.25059.1607.820071.00010.970
SOIL          T-Z 78.88013.72071.00027.43071.00068.580
SOIL T-Z      SLOCSM  8 12.000      2.3E-5      4
SOIL          T-Z          33.350 2.19055.580 4.25083.3707.8200100.0510.970
SOIL          T-Z 111.1613.720100.0527.430100.0568.580
SOIL T-Z      SLOCSM  8 12.010      2.3E-5      5
SOIL          T-Z          31.440 2.19052.400 4.25078.6107.820094.33010.970
SOIL          T-Z 104.8113.72094.33027.43094.33068.580
SOIL T-Z      SLOCSM  8 27.000      2.3E-5      6
SOIL          T-Z          59.590 2.19099.320 4.250148.977.8200178.7710.970
SOIL          T-Z 198.6313.720178.7727.430178.7768.580
SOIL T-Z      SLOCSM  8 27.010      2.3E-5      7
SOIL          T-Z          62.500 2.190104.16 4.250156.247.8200187.4910.970
SOIL          T-Z 208.3313.720187.4927.430187.4968.580
SOIL T-Z      SLOCSM  8 31.500      2.3E-5      8
SOIL          T-Z          63.290 2.190105.48 4.250158.227.8200189.8710.970
SOIL          T-Z 210.9713.720189.8727.430189.8768.580
SOIL T-Z      SLOCSM  8 31.501      2.3E-5      9
SOIL          T-Z          59.870 2.19099.780 4.250149.667.8200179.6010.970
SOIL          T-Z 199.5513.720179.6027.430179.6068.580
SOIL T-Z      SLOCSM  8 37.800      2.3E-5      10
SOIL          T-Z          72.350 2.190120.58 4.250180.867.8200217.0410.970

```



```

SOIL      T-Z 241.1513.720217.0427.430217.0468.580
SOIL T-Z  SLOCSM  8 37.801      2.3E-5  11
SOIL      T-Z      70.540 2.190117.57 4.250176.367.8200211.6310.970
SOIL      T-Z 235.1513.720211.6327.430211.6368.580
SOIL T-Z  SLOCSM  8 50.000      2.3E-5  12
SOIL      T-Z      94.040 2.190156.73 4.250235.107.8200282.1210.970
SOIL      T-Z 313.4613.720282.1227.430282.1268.580
SOIL T-Z  SLOCSM  8 50.010      2.3E-5  13
SOIL      T-Z      93.410 2.190155.68 4.250233.537.8200280.2310.970
SOIL      T-Z 311.3713.720280.2327.430280.2368.580
SOIL T-Z  SLOCSM  8 57.000      2.3E-5  14
SOIL      T-Z      111.24 2.190185.41 4.250278.117.8200333.7310.970
SOIL      T-Z 370.8213.720333.7327.430333.7368.580
SOIL T-Z  SLOCSM  8 57.010      2.3E-5  15
SOIL      T-Z      138.75 2.190231.24 4.250346.877.8200416.2410.970
SOIL      T-Z 462.4913.720416.2427.430416.2468.580
SOIL T-Z  SLOCSM  8 66.600      2.3E-5  16
SOIL      T-Z      122.81 2.190204.68 4.250307.027.8200368.4210.970
SOIL      T-Z 409.3613.720368.4227.430368.4268.580
SOIL T-Z  SLOCSM  8 66.610      2.3E-5  17
SOIL      T-Z      128.05 2.190213.42 4.250320.137.8200384.1610.970
SOIL      T-Z 426.8413.720384.1627.430384.1668.580
SOIL T-Z  SLOCSM  8 72.500      2.3E-5  18
SOIL      T-Z      129.27 2.190215.45 4.250323.187.8200387.8110.970
SOIL      T-Z 430.9013.720387.8127.430387.8168.580
SOIL T-Z  SLOCSM  8 72.510      2.3E-5  19
SOIL      T-Z      147.37 2.190245.62 4.250368.427.8200442.1110.970
SOIL      T-Z 491.2313.720442.1127.430442.1168.580
SOIL T-Z  SLOCSM  8 80.000      2.3E-5  20
SOIL      T-Z      164.53 2.190274.22 4.250411.337.8200493.6010.970
SOIL      T-Z 548.4513.720493.6027.430493.6068.580
SOIL T-Z  SLOCSM  8 80.100      2.3E-5  21
SOIL      T-Z      155.93 2.190259.88 4.250389.827.8200467.7910.970
SOIL      T-Z 519.7713.720467.7927.430467.7968.580
SOIL T-Z  SLOCSM  8 82.700      2.3E-5  22
SOIL      T-Z      184.64 2.190307.73 4.250461.607.8200553.9210.970
SOIL      T-Z 615.4613.720553.9227.430553.9268.580
SOIL T-Z  SLOCSM  8 82.710      2.3E-5  23
SOIL      T-Z      186.74 2.190311.23 4.250466.847.8200560.2110.970
SOIL      T-Z 622.4613.720560.2127.430560.2168.580
SOIL T-Z  SLOCSM  8 88.000      2.3E-5  24
SOIL      T-Z      195.18 2.190325.30 4.250487.957.8200585.5410.970
SOIL      T-Z 650.5913.720585.5427.430585.5468.580
SOIL T-Z  SLOCSM  8 88.010      2.3E-5  25
SOIL      T-Z      192.10 2.190320.17 4.250480.267.8200576.3110.970
SOIL      T-Z 640.3513.720576.3127.430576.3168.580
SOIL T-Z  SLOCSM  8 104.10      2.3E-5  26
SOIL      T-Z      224.69 2.190374.48 4.250561.727.8200674.0610.970
SOIL      T-Z 748.9513.720674.0627.430674.0668.580
SOIL T-Z  SLOCSM  8 104.11      2.3E-5  27
SOIL      T-Z      689.44 2.540689.44 5.080689.4412.700689.4425.400
SOIL      T-Z 689.4450.800689.44127.00689.44254.00
SOIL T-Z  SLOCSM  8 122.30      2.3E-5  28
SOIL      T-Z      732.53 2.540732.53 5.080732.5312.700732.5325.400
SOIL      T-Z 732.5350.800732.53127.00732.53254.00
SOIL T-Z  SLOCSM  8 122.31      2.3E-5  29
SOIL      T-Z      259.84 2.190433.07 4.250649.607.8200779.5210.970
SOIL      T-Z 866.1313.720779.5227.430779.5268.580
SOIL T-Z  SLOCSM  8 125.00      2.3E-5  30
SOIL      T-Z      259.84 2.190433.12 4.250649.687.8200779.6210.970
SOIL      T-Z 866.2413.720779.5227.430779.6268.580

```

*

*

** Q - Z FACTOR

** DIVIDE BY AREA OF PILES AREA (kN TO kN/cm²)

** PLUGGED AREA = (PI*((137.2)²)/4 = 14784.21 CM2

** MULTIPLYING FACTOR = 1/14784.20 = 6.76E-5

** SACS INPUT IS IN CM FOR Z, WHEREAS DATA PROVIDED IS IN MM,

**

SOIL BEARING HEAD 11 0.1 SOL1

SOIL T-Z SLOCSM 8 80.000 6.7E-5 1

SOIL T-Z 0.00000.0000432.19 2.740864.37 17.831158.3 34.291296.657.610

SOIL T-Z 1555.8100.131728.8137.161728.8685.80
SOIL T-Z SLOCSM 8 80.010 6.7E-5 2
SOIL T-Z 0.00000.0000398.94 2.740797.88 17.831069.1 34.291196.857.610
SOIL T-Z 1436.2100.131595.8137.161595.8685.80
SOIL T-Z SLOCSM 8 82.700 6.7E-5 3
SOIL T-Z 0.00000.0000515.30 2.7401030.6 17.831381.0 34.291545.957.610
SOIL T-Z 1855.1100.132061.2137.162061.2685.80
SOIL T-Z SLOCSM 8 82.710 6.7E-5 4
SOIL T-Z 0.00000.0000531.92 2.7401063.8 17.831425.6 34.291595.757.610
SOIL T-Z 1914.9100.132127.6137.162127.6685.80
SOIL T-Z SLOCSM 8 88.000 6.7E-5 5
SOIL T-Z 0.00000.0000531.92 2.7401063.8 17.831425.6 34.291595.757.610
SOIL T-Z 1914.9100.132127.6137.162127.6685.80
SOIL T-Z SLOCSM 8 88.010 6.7E-5 6
SOIL T-Z 0.00000.0000515.30 2.7401030.6 17.831381.0 34.291545.957.610
SOIL T-Z 1855.1100.132061.2137.162061.2685.80
SOIL T-Z SLOCSM 8 104.10 6.7E-5 7
SOIL T-Z 0.00000.0000598.41 2.7401196.8 17.831603.7 34.291795.257.610
SOIL T-Z 2154.3100.132393.6137.162393.6685.80
SOIL T-Z SLOCSM 8 104.11 6.7E-5 8
SOIL T-Z 0.00000.0000531.92 2.7401063.8 17.831425.6 34.291595.857.610
SOIL T-Z 1914.9100.132127.7137.162127.7685.80
SOIL T-Z SLOCSM 8 122.30 6.7E-5 9
SOIL T-Z 0.00000.0000565.17 2.7401130.3 17.831514.6 34.291695.557.610
SOIL T-Z 2034.6100.132260.6137.162260.7685.80
SOIL T-Z SLOCSM 8 122.31 6.7E-5 10
SOIL T-Z 0.00000.0000664.90 2.7401329.8 17.831781.9 34.291994.757.610
SOIL T-Z 2393.7100.132659.6137.162659.6685.80
SOIL T-Z SLOCSM 8 125.00 6.7E-5 11
SOIL T-Z 0.00000.0000664.90 2.7401329.8 17.831781.9 34.291994.757.610
SOIL T-Z 2393.7100.132659.6137.162659.6685.80

*

SOIL TORSION HEAD 2000.0SOL1TORSIONAL SPRING

SOIL LATERAL HEAD 93 YEXP137.20 0.10SOL1P-Y
SOIL P-Y SLOCSM 7 0.9000 0.01 1
SOIL P-Y 0.00000.00000.00000.00000.00000.00000.00000.00000.00000.00000.00000.00000
SOIL P-Y 0.00000.00000.00000.00000.00000
SOIL P-Y SLOCSM 7 1.0000 1.00 2
SOIL P-Y 0.00000.00003.86006.86005.530020.5708.390068.58012.070205.74
SOIL P-Y 1.08001028.71.08002057.4
SOIL P-Y SLOCSM 7 2.0000 0.01 3
SOIL P-Y 0.00000.00008.30006.860011.91020.57018.05068.58026.000205.74
SOIL P-Y 4.64001028.74.64002057.4
SOIL P-Y SLOCSM 7 3.0000 1.00 4
SOIL P-Y 0.00000.000013.3406.860019.14020.57029.00068.58041.760205.74
SOIL P-Y 11.1901028.711.1902057.4
SOIL P-Y SLOCSM 7 4.0000 0.01 5
SOIL P-Y 0.00000.000018.9706.860027.21020.57041.23068.58059.380205.74
SOIL P-Y 21.2101028.721.2102057.4
SOIL P-Y SLOCSM 7 5.0000 0.01 6
SOIL P-Y 0.00000.000025.1805.140036.13015.43054.75051.44078.840154.31
SOIL P-Y 35.190771.5335.1901543.0
SOIL P-Y SLOCSM 7 6.0000 1.00 7
SOIL P-Y 0.00000.000031.9905.140045.90015.43069.54051.440100.14154.31
SOIL P-Y 53.650771.5353.6501543.0
SOIL P-Y SLOCSM 7 6.9000 0.01 8
SOIL P-Y 0.00000.000038.6205.140055.41015.43083.95051.440120.89154.31
SOIL P-Y 74.480771.5374.4801543.0
SOIL P-Y SLOCSM 7 7.8000 0.01 9
SOIL P-Y 0.00000.000045.7305.140065.61015.43099.41051.440143.14154.31
SOIL P-Y 99.690771.5399.6901543.0
SOIL P-Y SLOCSM 7 7.8010 0.01 10
SOIL P-Y 0.00000.000091.9405.1400131.9215.430199.8851.440287.83154.31
SOIL P-Y 200.45771.53200.451543.0
SOIL P-Y SLOCSM 7 8.8000 0.01 11
SOIL P-Y 0.00000.0000101.215.1400145.2215.430220.0251.440316.83154.31
SOIL P-Y 248.94771.53248.941543.0
SOIL P-Y SLOCSM 7 9.8000 0.01 12
SOIL P-Y 0.00000.0000110.755.1400158.9015.430240.7651.440346.70154.31
SOIL P-Y 303.36771.53303.361543.0
SOIL P-Y SLOCSM 7 10.900 0.01 13
SOIL P-Y 0.00000.0000121.565.1400174.4115.430264.2651.440380.54154.31

| | | |
|----------|--------|--|
| SOIL | P-Y | 370.34771.53370.341543.0 |
| SOIL P-Y | SLOCSM | 7 12.000 0.01 14 |
| SOIL | P-Y | 0.00000.0000127.765.1400183.3115.430277.7551.440399.96154.31 |
| SOIL | P-Y | 399.96771.53399.961543.0 |
| SOIL P-Y | SLOCSM | 7 12.010 0.01 15 |
| SOIL | P-Y | 0.00000.0000113.575.1400162.9515.430246.8951.440355.52154.31 |
| SOIL | P-Y | 355.521543.0355.521543.0 |
| SOIL P-Y | SLOCSM | 7 13.900 0.01 16 |
| SOIL | P-Y | 0.00000.0000120.765.1400173.2715.430262.5251.440378.03154.31 |
| SOIL | P-Y | 378.031543.0378.031543.0 |
| SOIL P-Y | SLOCSM | 7 15.800 0.01 17 |
| SOIL | P-Y | 0.00000.0000127.955.1400183.5915.430278.1651.440400.55154.31 |
| SOIL | P-Y | 400.551543.0400.551543.0 |
| SOIL P-Y | SLOCSM | 7 17.700 0.01 18 |
| SOIL | P-Y | 0.00000.0000135.155.1400193.9115.430293.8051.440423.07154.31 |
| SOIL | P-Y | 423.071543.0423.071543.0 |
| SOIL P-Y | SLOCSM | 7 19.600 0.01 19 |
| SOIL | P-Y | 0.00000.0000142.345.1400204.2315.430309.4351.440445.58154.31 |
| SOIL | P-Y | 445.581543.0445.581543.0 |
| SOIL P-Y | SLOCSM | 7 21.500 0.01 20 |
| SOIL | P-Y | 0.00000.0000149.533.4300214.5510.290325.0734.290468.10102.87 |
| SOIL | P-Y | 468.101028.7468.101028.7 |
| SOIL P-Y | SLOCSM | 7 23.400 0.01 21 |
| SOIL | P-Y | 0.00000.0000156.723.4300224.8710.290340.7134.290490.62102.87 |
| SOIL | P-Y | 490.621028.7490.621028.7 |
| SOIL P-Y | SLOCSM | 7 25.200 0.01 22 |
| SOIL | P-Y | 0.00000.0000163.543.4300234.6410.290355.5234.290511.95102.87 |
| SOIL | P-Y | 511.951028.7511.951028.7 |
| SOIL P-Y | SLOCSM | 7 27.000 0.01 23 |
| SOIL | P-Y | 0.00000.0000170.353.4300244.4210.290370.3334.290533.28102.87 |
| SOIL | P-Y | 533.281028.7533.281028.7 |
| SOIL P-Y | SLOCSM | 7 27.010 0.01 24 |
| SOIL | P-Y | 0.00000.0000187.393.4300268.8610.290407.3734.290586.61102.87 |
| SOIL | P-Y | 586.611028.7586.611028.7 |
| SOIL P-Y | SLOCSM | 7 28.100 0.01 25 |
| SOIL | P-Y | 0.00000.0000181.143.4300259.9010.290393.7934.290567.05102.87 |
| SOIL | P-Y | 567.051028.7567.051028.7 |
| SOIL P-Y | SLOCSM | 7 29.200 0.01 26 |
| SOIL | P-Y | 0.00000.0000174.903.4300250.9410.290380.2134.290547.50102.87 |
| SOIL | P-Y | 547.501028.7547.501028.7 |
| SOIL P-Y | SLOCSM | 7 30.300 0.01 27 |
| SOIL | P-Y | 0.00000.0000168.653.4300241.9710.290366.6334.290527.95102.87 |
| SOIL | P-Y | 527.951028.7527.951028.7 |
| SOIL P-Y | SLOCSM | 7 31.500 0.01 28 |
| SOIL | P-Y | 0.00000.0000161.843.4300232.2010.290351.8234.290506.61102.87 |
| SOIL | P-Y | 506.611028.7506.611028.7 |
| SOIL P-Y | SLOCSM | 7 31.510 0.01 29 |
| SOIL | P-Y | 0.00000.0000144.803.4300207.7610.290314.7834.290453.29102.87 |
| SOIL | P-Y | 453.291028.7453.291028.7 |
| SOIL P-Y | SLOCSM | 7 32.500 0.01 30 |
| SOIL | P-Y | 0.00000.0000149.313.4300214.2210.290324.5834.290467.39102.87 |
| SOIL | P-Y | 467.391028.7467.391028.7 |
| SOIL P-Y | SLOCSM | 7 33.500 0.01 31 |
| SOIL | P-Y | 0.00000.0000153.813.4300220.6910.290334.3834.290481.50102.87 |
| SOIL | P-Y | 481.501028.7481.501028.7 |
| SOIL P-Y | SLOCSM | 7 34.500 0.01 32 |
| SOIL | P-Y | 0.00000.0000158.323.4300227.1510.290344.1734.290495.61102.87 |
| SOIL | P-Y | 495.611028.7495.611028.7 |
| SOIL P-Y | SLOCSM | 7 35.600 0.01 33 |
| SOIL | P-Y | 0.00000.0000163.283.4300234.2710.290354.9534.290511.13102.87 |
| SOIL | P-Y | 511.131028.7511.131028.7 |
| SOIL P-Y | SLOCSM | 7 36.700 0.01 34 |
| SOIL | P-Y | 0.00000.0000168.233.4300241.3810.290365.7334.290526.65102.87 |
| SOIL | P-Y | 526.651028.7526.651028.7 |
| SOIL P-Y | SLOCSM | 7 37.800 0.01 35 |
| SOIL | P-Y | 0.00000.0000173.193.4300248.4910.290376.5034.290542.17102.87 |
| SOIL | P-Y | 542.171028.7542.171028.7 |
| SOIL P-Y | SLOCSM | 7 37.800 0.01 36 |
| SOIL | P-Y | 0.00000.0000164.673.4300236.2710.290357.9934.290515.50102.87 |
| SOIL | P-Y | 515.501028.7515.501028.7 |
| SOIL P-Y | SLOCSM | 7 39.800 0.01 37 |
| SOIL | P-Y | 0.00000.0000172.593.4300247.6210.290375.1934.290540.27102.87 |
| SOIL | P-Y | 540.271028.7540.271028.7 |
| SOIL P-Y | SLOCSM | 7 41.800 0.01 38 |

SOIL P-Y 0.00000.0000180.503.4300258.9810.290392.3934.290565.04102.87
SOIL P-Y 565.041028.7565.041028.7
SOIL P-Y SLOCSM 7 43.800 0.01 39
SOIL P-Y 0.00000.0000188.413.4300270.3310.290409.5934.290589.81102.87
SOIL P-Y 589.811028.7589.811028.7
SOIL P-Y SLOCSM 7 46.800 0.01 40
SOIL P-Y 0.00000.0000200.283.4300287.3610.290435.3934.290626.97102.87
SOIL P-Y 626.971028.7626.971028.7
SOIL P-Y SLOCSM 7 50.000 0.01 41
SOIL P-Y 0.00000.0000212.943.4300305.5210.290462.9234.290666.60102.87
SOIL P-Y 666.601028.7666.601028.7
SOIL P-Y SLOCSM 7 50.010 0.01 42
SOIL P-Y 0.00000.0000210.103.4300301.4510.290456.7434.290657.71102.87
SOIL P-Y 657.711028.7657.711028.7
SOIL P-Y SLOCSM 7 51.800 0.01 43
SOIL P-Y 0.00000.0000221.783.4300318.2110.290482.1434.290694.28102.87
SOIL P-Y 694.281028.7694.281028.7
SOIL P-Y SLOCSM 7 53.600 0.01 44
SOIL P-Y 0.00000.0000233.463.4300334.9710.290507.5334.290730.84102.87
SOIL P-Y 730.841028.7730.841028.7
SOIL P-Y SLOCSM 7 55.400 0.01 45
SOIL P-Y 0.00000.0000245.153.4300351.7310.290532.9334.290767.41102.87
SOIL P-Y 767.411028.7767.411028.7
SOIL P-Y SLOCSM 7 57.000 0.01 46
SOIL P-Y 0.00000.0000255.533.4300366.6310.290555.5034.290799.92102.87
SOIL P-Y 799.921028.7799.921028.7
SOIL P-Y SLOCSM 7 57.010 0.01 47
SOIL P-Y 0.00000.0000397.491.7100570.315.1400864.1117.1501244.351.440
SOIL P-Y 1244.3514.351244.3514.35
SOIL P-Y SLOCSM 7 58.900 0.01 48
SOIL P-Y 0.00000.0000372.201.7100534.035.1400809.1417.1501165.151.440
SOIL P-Y 1165.1514.351165.1514.35
SOIL P-Y SLOCSM 7 60.800 0.01 49
SOIL P-Y 0.00000.0000346.921.7100497.755.1400754.1717.1501086.051.440
SOIL P-Y 1086.0514.351086.0514.35
SOIL P-Y SLOCSM 7 62.700 0.01 50
SOIL P-Y 0.00000.0000321.631.7100461.475.1400699.1917.1501006.851.440
SOIL P-Y 1006.8514.351006.8514.35
SOIL P-Y SLOCSM 7 64.600 0.01 51
SOIL P-Y 0.00000.0000296.341.7100425.195.1400644.2217.150927.6851.440
SOIL P-Y 927.68514.35927.68514.35
SOIL P-Y SLOCSM 7 66.600 0.01 52
SOIL P-Y 0.00000.0000269.731.7100387.005.1400586.3617.150844.3651.440
SOIL P-Y 844.36514.35844.36514.35
SOIL P-Y SLOCSM 7 66.610 0.01 53
SOIL P-Y 0.00000.0000283.921.7100407.375.1400617.2217.150888.8051.440
SOIL P-Y 888.80514.35888.80514.35
SOIL P-Y SLOCSM 7 68.600 0.01 54
SOIL P-Y 0.00000.0000283.921.7100407.375.1400617.2217.150888.8051.440
SOIL P-Y 888.80514.35888.80514.35
SOIL P-Y SLOCSM 7 70.600 0.01 55
SOIL P-Y 0.00000.0000283.921.7100407.375.1400617.2217.150888.8051.440
SOIL P-Y 888.80514.35888.80514.35
SOIL P-Y SLOCSM 7 72.500 0.01 56
SOIL P-Y 0.00000.0000283.921.7100407.375.1400617.2217.150888.8051.440
SOIL P-Y 888.80514.35888.80514.35
SOIL P-Y SLOCSM 7 72.510 0.01 57
SOIL P-Y 0.00000.0000340.711.7100488.845.1400740.6617.1501066.551.440
SOIL P-Y 1066.5514.351066.5514.35
SOIL P-Y SLOCSM 7 74.400 0.01 58
SOIL P-Y 0.00000.0000347.901.7100499.165.1400756.3017.1501089.051.440
SOIL P-Y 1089.0514.351089.0514.35
SOIL P-Y SLOCSM 7 76.300 0.01 59
SOIL P-Y 0.00000.0000355.091.7100509.485.1400771.9417.1501111.551.440
SOIL P-Y 1111.5514.351111.5514.35
SOIL P-Y SLOCSM 7 78.200 0.01 60
SOIL P-Y 0.00000.0000362.281.7100519.805.1400787.5717.1501134.151.440
SOIL P-Y 1134.1514.351134.1514.35
SOIL P-Y SLOCSM 7 80.000 0.01 61
SOIL P-Y 0.00000.0000369.101.7100529.575.1400802.3917.1501155.451.440
SOIL P-Y 1155.4514.351155.4514.35
SOIL P-Y SLOCSM 7 80.010 0.01 62
SOIL P-Y 0.00000.0000340.711.7100488.845.1400740.6617.1501066.551.440
SOIL P-Y 1066.5514.351066.5514.35

| | | | | | |
|----------|--------|--|--------|------|----|
| SOIL P-Y | SLOCSM | 7 | 81.300 | 0.01 | 63 |
| SOIL | P-Y | 0.00000.0000388.551.7100557.495.1400844.6817.1501216.351.440 | | | |
| SOIL | P-Y | 1216.3514.351216.3514.35 | | | |
| SOIL P-Y | SLOCSM | 7 | 82.700 | 0.01 | 64 |
| SOIL | P-Y | 0.00000.0000440.081.7100631.425.1400956.6917.1501377.651.440 | | | |
| SOIL | P-Y | 1377.6514.351377.6514.35 | | | |
| SOIL P-Y | SLOCSM | 7 | 82.710 | 0.01 | 65 |
| SOIL | P-Y | 0.00000.0000454.271.7100651.785.1400987.5517.1501422.051.440 | | | |
| SOIL | P-Y | 1422.0514.351422.0514.35 | | | |
| SOIL P-Y | SLOCSM | 7 | 84.500 | 0.01 | 66 |
| SOIL | P-Y | 0.00000.0000454.271.7100651.785.1400987.5517.1501422.051.440 | | | |
| SOIL | P-Y | 1422.0514.351422.0514.35 | | | |
| SOIL P-Y | SLOCSM | 7 | 86.300 | 0.01 | 67 |
| SOIL | P-Y | 0.00000.0000454.271.7100651.785.1400987.5517.1501422.051.440 | | | |
| SOIL | P-Y | 1422.0514.351422.0514.35 | | | |
| SOIL P-Y | SLOCSM | 7 | 88.000 | 0.01 | 68 |
| SOIL | P-Y | 0.00000.0000454.271.7100651.785.1400987.5517.1501422.051.440 | | | |
| SOIL | P-Y | 1422.0514.351422.0514.35 | | | |
| SOIL P-Y | SLOCSM | 7 | 88.010 | 0.01 | 69 |
| SOIL | P-Y | 0.00000.0000440.081.7100631.425.1400956.6917.1501377.651.440 | | | |
| SOIL | P-Y | 1377.6514.351377.6514.35 | | | |
| SOIL P-Y | SLOCSM | 7 | 92.000 | 0.01 | 70 |
| SOIL | P-Y | 0.00000.0000457.711.7100656.725.1400995.0317.1501432.851.440 | | | |
| SOIL | P-Y | 1432.8514.351432.8514.35 | | | |
| SOIL P-Y | SLOCSM | 7 | 100.00 | 0.01 | 71 |
| SOIL | P-Y | 0.00000.0000492.981.7100707.325.14001071.717.1501543.251.440 | | | |
| SOIL | P-Y | 1543.2514.351543.2514.35 | | | |
| SOIL P-Y | SLOCSM | 7 | 104.10 | 0.01 | 72 |
| SOIL | P-Y | 0.00000.0000511.061.7100733.265.14001111.017.1501599.851.440 | | | |
| SOIL | P-Y | 1599.8514.351599.8514.35 | | | |
| SOIL P-Y | SLOCSM | 7 | 104.10 | 0.01 | 73 |
| SOIL | P-Y | 0.00000.0000454.271.7100651.785.1400987.5517.1501422.051.440 | | | |
| SOIL | P-Y | 1422.0514.351422.0514.35 | | | |
| SOIL P-Y | SLOCSM | 7 | 108.00 | 0.01 | 74 |
| SOIL | P-Y | 0.00000.0000460.361.7100660.515.14001000.717.1501441.151.440 | | | |
| SOIL | P-Y | 1441.1514.351441.1514.35 | | | |
| SOIL P-Y | SLOCSM | 7 | 112.00 | 0.01 | 75 |
| SOIL | P-Y | 0.00000.0000466.601.7100669.475.14001014.317.1501460.651.440 | | | |
| SOIL | P-Y | 1460.6514.351460.6514.35 | | | |
| SOIL P-Y | SLOCSM | 7 | 116.00 | 0.01 | 76 |
| SOIL | P-Y | 0.00000.0000472.841.7100678.425.14001027.917.1501480.151.440 | | | |
| SOIL | P-Y | 1480.1514.351480.1514.35 | | | |
| SOIL P-Y | SLOCSM | 7 | 119.00 | 0.01 | 77 |
| SOIL | P-Y | 0.00000.0000477.521.7100685.135.14001038.017.1501494.851.440 | | | |
| SOIL | P-Y | 1494.8514.351494.8514.35 | | | |
| SOIL P-Y | SLOCSM | 7 | 122.30 | 0.01 | 78 |
| SOIL | P-Y | 0.00000.0000482.671.7100692.525.14001049.217.1501510.951.440 | | | |
| SOIL | P-Y | 1510.9514.351510.9514.35 | | | |
| SOIL P-Y | SLOCSM | 7 | 122.30 | 0.01 | 79 |
| SOIL | P-Y | 0.00000.0000567.841.7100814.735.14001234.417.1501777.551.440 | | | |
| SOIL | P-Y | 1777.5514.351777.5514.35 | | | |
| SOIL P-Y | SLOCSM | 7 | 124.00 | 0.01 | 80 |
| SOIL | P-Y | 0.00000.0000567.841.7100814.735.14001234.417.1501777.551.440 | | | |
| SOIL | P-Y | 1777.5514.351777.5514.35 | | | |
| SOIL P-Y | SLOCSM | 7 | 125.00 | 0.01 | 81 |
| SOIL | P-Y | 0.00000.0000567.841.7100814.735.14001234.417.1501777.551.440 | | | |
| SOIL | P-Y | 1777.5514.351777.5514.35 | | | |
| SOIL P-Y | SLOCSM | 7 | 125.01 | 0.01 | 82 |
| SOIL | P-Y | 0.00000.0000511.061.7100733.265.14001111.017.1501599.851.440 | | | |
| SOIL | P-Y | 1599.8514.351599.8514.35 | | | |
| SOIL P-Y | SLOCSM | 7 | 126.50 | 0.01 | 83 |
| SOIL | P-Y | 0.00000.0000511.061.7100733.265.14001111.017.1501599.851.440 | | | |
| SOIL | P-Y | 1599.8514.351599.8514.35 | | | |
| SOIL P-Y | SLOCSM | 7 | 128.00 | 0.01 | 84 |
| SOIL | P-Y | 0.00000.0000511.061.7100733.265.14001111.017.1501599.851.440 | | | |
| SOIL | P-Y | 1599.8514.351599.8514.35 | | | |
| SOIL P-Y | SLOCSM | 7 | 128.01 | 0.01 | 85 |
| SOIL | P-Y | 0.00000.00003909.45.72005171.17.62007585.811.4308948.013.720 | | | |
| SOIL | P-Y | 13598.22.86020536.51.440 | | | |
| SOIL P-Y | SLOCSM | 7 | 128.70 | 0.01 | 86 |
| SOIL | P-Y | 0.00000.00003930.85.72005199.47.62007627.211.4308996.913.720 | | | |
| SOIL | P-Y | 13673.22.86020649.51.440 | | | |
| SOIL P-Y | SLOCSM | 7 | 129.40 | 0.01 | 87 |
| SOIL | P-Y | 0.00000.00003952.15.72005227.77.62007668.711.4309045.813.720 | | | |

```

SOIL          P-Y 13747.22.86020761.51.440
SOIL P-Y     SLOCSM 7 129.41      0.01    88
SOIL          P-Y 0.00000.0000425.881.7100611.055.1400925.8317.1501333.251.440
SOIL          P-Y 1333.2514.351333.2514.35
SOIL P-Y     SLOCSM 7 131.70      0.01    89
SOIL          P-Y 0.00000.0000476.671.7100683.925.14001036.217.1501492.151.440
SOIL          P-Y 1492.1514.351492.1514.35
SOIL P-Y     SLOCSM 7 133.00      0.01    90
SOIL          P-Y 0.00000.0000505.381.7100725.115.14001098.617.1501582.051.440
SOIL          P-Y 1582.0514.351582.0514.35
SOIL P-Y     SLOCSM 7 133.00      0.01    91
SOIL          P-Y 0.00000.00008254.75.720010898.7.620015908.11.43018695.13.720
SOIL          P-Y 27902.22.86040086.51.440
SOIL P-Y     SLOCSM 7 134.00      0.01    92
SOIL          P-Y 0.00000.00008316.75.720010980.7.620016028.11.43018836.13.720
SOIL          P-Y 28112.22.86040388.51.440
SOIL P-Y     SLOCSM 7 135.00      0.01    93
SOIL          P-Y 0.00000.00008378.85.720011062.7.620016147.11.43018976.13.720
SOIL          P-Y 28322.22.86040689.51.440
END

```

DYNAMIC INPUT

```

DYNOPT      EN100CONS                1.          SA-Z
DYNOP2      1.    1.    1.
END

```

WAVE RESPONSE INPUT JACKET MODIFIKASI

```

*WAVE RESPONSE INPUT FOR MBH STRUCTURE
WROPT ENPSL ALL US                100  -1
PLTTFF                      OMBBSB                PFS
DAMP                          2.
END

```

WAVE RESPONSE INPUT JACKET KONVENSIONAL

```

*WAVE RESPONSE INPUT FOR CONVENTIONAL STRUCTURE
WROPT ENPSL ALL US                63  -1
PLTTFF                      OMBBSB                PFS
DAMP                          2.
END

```

SEASTATE INPUT TRANSFER FUNCTION (NORTH)

```

LDOPT      NF+Z64.20000490.0000-261.609 261.609GLOB                CMB
FILE S
CDM
CDM 22      0.5          2.          0.8          2.
CDM 24      0.5          2          0.8          2.
CDM 26      0.5          2          0.8          2.
CDM 28      0.5          2          0.8          2.
CDM 30      0.5          2          0.8          2.
CDM 53      0.5          2          0.8          2.
CDM 54      0.5          2          0.8          2.

*Addition for Fatigue Calc*

*****
*Spectral Analysis *
*****
*For NORTH*
LOADCN 1
GNTRF  AL1200.02665 12.5 0.1          225.  AIRYPF  21.32 1. 0.03
END

```

SEASTATE INPUT TRANSFER FUNCTION (NORTH-NORTHEAST)

```
LDOPT      NF+Z64.20000490.0000-261.609 261.609GLOB      CMB
FILE S
CDM
CDM 22      0.5      2.      0.8      2.
CDM 24      0.5      2      0.8      2.
CDM 26      0.5      2      0.8      2.
CDM 28      0.5      2      0.8      2.
CDM 30      0.5      2      0.8      2.
CDM 53      0.5      2      0.8      2.
CDM 54      0.5      2      0.8      2.

*Addition for Fatigue Calc*

*****
*Spectral Analysis *
*****
*For NORTH-NORTHEAST*
LOADCN 1
GNTRF  AL1200.02665 12.5 0.1      247.5  AIRYPF  21.32 1. 0.03
END
```

SEASTATE INPUT TRANSFER FUNCTION (NORTH-EAST)

```
LDOPT      NF+Z64.20000490.0000-261.609 261.609GLOB      CMB
FILE S
CDM
CDM 22      0.5      2.      0.8      2.
CDM 24      0.5      2      0.8      2.
CDM 26      0.5      2      0.8      2.
CDM 28      0.5      2      0.8      2.
CDM 30      0.5      2      0.8      2.
CDM 53      0.5      2      0.8      2.
CDM 54      0.5      2      0.8      2.

*Addition for Fatigue Calc*

*****
*Spectral Analysis *
*****
*For NORTH-EAST*
LOADCN 1
GNTRF  AL1200.02665 12.5 0.1      270.  AIRYPF  21.32 1. 0.03
END
```

SEASTATE INPUT TRANSFER FUNCTION (EAST-NORTHEAST)

```
LDOPT      NF+Z64.20000490.0000-261.609 261.609GLOB      CMB
FILE S
CDM
CDM 22      0.5      2.      0.8      2.
CDM 24      0.5      2      0.8      2.
CDM 26      0.5      2      0.8      2.
CDM 28      0.5      2      0.8      2.
CDM 30      0.5      2      0.8      2.
CDM 53      0.5      2      0.8      2.
CDM 54      0.5      2      0.8      2.

*Addition for Fatigue Calc*

*****
*Spectral Analysis *
*****
*For EAST-NORTHEAST*
LOADCN 1
```

GNTRF AL1200.02665 12.5 0.1 292.5 AIRYPF 21.32 1. 0.03
END

SEASTATE INPUT TRANSFER FUNCTION (EAST)

LDOPT NF+Z64.20000490.0000-261.609 261.609GLOB CMB
FILE S
CDM
CDM 22 0.5 2. 0.8 2.
CDM 24 0.5 2 0.8 2.
CDM 26 0.5 2 0.8 2.
CDM 28 0.5 2 0.8 2.
CDM 30 0.5 2 0.8 2.
CDM 53 0.5 2 0.8 2.
CDM 54 0.5 2 0.8 2.

Addition for Fatigue Calc

*Spectral Analysis *

For EAST

LOADCN 1
GNTRF AL1200.02665 12.5 0.1 315. AIRYPF 21.32 1. 0.03
END

SEASTATE INPUT TRANSFER FUNCTION (EAST-SOUTHEAST)

LDOPT NF+Z64.20000490.0000-261.609 261.609GLOB CMB
FILE S
CDM
CDM 22 0.5 2. 0.8 2.
CDM 24 0.5 2 0.8 2.
CDM 26 0.5 2 0.8 2.
CDM 28 0.5 2 0.8 2.
CDM 30 0.5 2 0.8 2.
CDM 53 0.5 2 0.8 2.
CDM 54 0.5 2 0.8 2.

Addition for Fatigue Calc

*Spectral Analysis *

For EAST-SOUTHEAST

LOADCN 1
GNTRF AL1200.02665 12.5 0.1 337.5 AIRYPF 21.32 1. 0.03
END

SEASTATE INPUT TRANSFER FUNCTION (SOUTH-EAST)

LDOPT NF+Z64.20000490.0000-261.609 261.609GLOB CMB
FILE S
CDM
CDM 22 0.5 2. 0.8 2.
CDM 24 0.5 2 0.8 2.
CDM 26 0.5 2 0.8 2.
CDM 28 0.5 2 0.8 2.
CDM 30 0.5 2 0.8 2.
CDM 53 0.5 2 0.8 2.
CDM 54 0.5 2 0.8 2.

Addition for Fatigue Calc

*Spectral Analysis *

```

*For SOUTH-EAST*
LOADCN 1
GNTRF AL1200.02665 12.5 0.1 0. AIRYPF 21.32 1. 0.03
END

```

SEASTATE INPUT TRANSFER FUNCTION (SOUTH-SOUTHEAST)

```

LDOPT NF+Z64.20000490.0000-261.609 261.609GLOB CMB
FILE S
CDM
CDM 22 0.5 2. 0.8 2.
CDM 24 0.5 2 0.8 2.
CDM 26 0.5 2 0.8 2.
CDM 28 0.5 2 0.8 2.
CDM 30 0.5 2 0.8 2.
CDM 53 0.5 2 0.8 2.
CDM 54 0.5 2 0.8 2.

```

Addition for Fatigue Calc

```

*****
*Spectral Analysis *
*****
*For SOUTH-SOUTHEAST*
LOADCN 1
GNTRF AL1200.02665 12.5 0.1 22.5 AIRYPF 21.32 1. 0.03
END

```

SEASTATE INPUT TRANSFER FUNCTION (SOUTH)

```

LDOPT NF+Z64.20000490.0000-261.609 261.609GLOB CMB
FILE S
CDM
CDM 22 0.5 2. 0.8 2.
CDM 24 0.5 2 0.8 2.
CDM 26 0.5 2 0.8 2.
CDM 28 0.5 2 0.8 2.
CDM 30 0.5 2 0.8 2.
CDM 53 0.5 2 0.8 2.
CDM 54 0.5 2 0.8 2.

```

Addition for Fatigue Calc

```

*****
*Spectral Analysis *
*****
*For SOUTH*
LOADCN 1
GNTRF AL1200.02665 12.5 0.1 45. AIRYPF 21.32 1. 0.03
END

```

SEASTATE INPUT TRANSFER FUNCTION (SOUTH-SOUTHWEST)

```

LDOPT NF+Z64.20000490.0000-261.609 261.609GLOB CMB
FILE S
CDM
CDM 22 0.5 2. 0.8 2.
CDM 24 0.5 2 0.8 2.
CDM 26 0.5 2 0.8 2.
CDM 28 0.5 2 0.8 2.
CDM 30 0.5 2 0.8 2.
CDM 53 0.5 2 0.8 2.
CDM 54 0.5 2 0.8 2.

```

Addition for Fatigue Calc

```

*****
*Spectral Analysis *
*****
*For SOUTH-SOUTHWEST*
LOADCN 1
GNTRF AL1200.02665 12.5 0.1 67.5 AIRYPF 21.32 1. 0.03
END

```

SEASTATE INPUT TRANSFER FUNCTION (SOUTH-WEST)

```

LDOPT NF+Z64.20000490.0000-261.609 261.609GLOB CMB
FILE S
CDM
CDM 22 0.5 2. 0.8 2.
CDM 24 0.5 2 0.8 2.
CDM 26 0.5 2 0.8 2.
CDM 28 0.5 2 0.8 2.
CDM 30 0.5 2 0.8 2.
CDM 53 0.5 2 0.8 2.
CDM 54 0.5 2 0.8 2.

```

Addition for Fatigue Calc

```

*****
*Spectral Analysis *
*****
*For SOUTH-WEST*
LOADCN 1
GNTRF AL1200.02665 12.5 0.1 90. AIRYPF 21.32 1. 0.03
END

```

SEASTATE INPUT TRANSFER FUNCTION (WEST-SOUTHWEST)

```

LDOPT NF+Z64.20000490.0000-261.609 261.609GLOB CMB
FILE S
CDM
CDM 22 0.5 2. 0.8 2.
CDM 24 0.5 2 0.8 2.
CDM 26 0.5 2 0.8 2.
CDM 28 0.5 2 0.8 2.
CDM 30 0.5 2 0.8 2.
CDM 53 0.5 2 0.8 2.
CDM 54 0.5 2 0.8 2.

```

Addition for Fatigue Calc

```

*****
*Spectral Analysis *
*****
*For WEST-SOUTHWEST*
LOADCN 1
GNTRF AL1200.02665 12.5 0.1 112.5 AIRYPF 21.32 1. 0.03
END

```

SEASTATE INPUT TRANSFER FUNCTION (WEST)

```

LDOPT NF+Z64.20000490.0000-261.609 261.609GLOB CMB
FILE S
CDM
CDM 22 0.5 2. 0.8 2.
CDM 24 0.5 2 0.8 2.
CDM 26 0.5 2 0.8 2.
CDM 28 0.5 2 0.8 2.
CDM 30 0.5 2 0.8 2.
CDM 53 0.5 2 0.8 2.
CDM 54 0.5 2 0.8 2.

```

Addition for Fatigue Calc

*Spectral Analysis *

For WEST

LOADCN 1
GNTRF AL1200.02665 12.5 0.1 135. AIRYPF 21.32 1. 0.03
END

SEASTATE INPUT TRANSFER FUNCTION (WEST-NORTHWEST)

LDOPT NF+Z64.20000490.0000-261.609 261.609GLOB CMB
FILE S
CDM
CDM 22 0.5 2. 0.8 2.
CDM 24 0.5 2 0.8 2.
CDM 26 0.5 2 0.8 2.
CDM 28 0.5 2 0.8 2.
CDM 30 0.5 2 0.8 2.
CDM 53 0.5 2 0.8 2.
CDM 54 0.5 2 0.8 2.

Addition for Fatigue Calc

*Spectral Analysis *

For WEST-NORTHWEST

LOADCN 1
GNTRF AL1200.02665 12.5 0.1 157.5 AIRYPF 21.32 1. 0.03
END

SEASTATE INPUT TRANSFER FUNCTION (NORTH-WEST)

LDOPT NF+Z64.20000490.0000-261.609 261.609GLOB CMB
FILE S
CDM
CDM 22 0.5 2. 0.8 2.
CDM 24 0.5 2 0.8 2.
CDM 26 0.5 2 0.8 2.
CDM 28 0.5 2 0.8 2.
CDM 30 0.5 2 0.8 2.
CDM 53 0.5 2 0.8 2.
CDM 54 0.5 2 0.8 2.

Addition for Fatigue Calc

*Spectral Analysis *

For NORTH-WEST

LOADCN 1
GNTRF AL1200.02665 12.5 0.1 180. AIRYPF 21.32 1. 0.03
END

SEASTATE INPUT TRANSFER FUNCTION (NORTH-NORTHWEST)

LDOPT NF+Z64.20000490.0000-261.609 261.609GLOB CMB
FILE S
CDM
CDM 22 0.5 2. 0.8 2.
CDM 24 0.5 2 0.8 2.
CDM 26 0.5 2 0.8 2.

```

CDM 28 0.5 2 0.8 2.
CDM 30 0.5 2 0.8 2.
CDM 53 0.5 2 0.8 2.
CDM 54 0.5 2 0.8 2.

```

Addition for Fatigue Calc

```

*****
*Spectral Analysis *
*****

```

For NORTH-NORTHWEST

```

LOADCN 1
GNTRF AL1200.02665 12.5 0.1 202.5 AIRYPF 21.32 1. 0.03
END

```

FATIGUE INPUT JACKET MODIFIKASI

Fatigue Input for MBH Structure Spectral Analysis

```

FTOPT F 20. 1. 2. SMAPI SKMXMNSKNE KTLPEFT
FTOPT2 PPTVC PV WS AWS-261.61 261.61TI2 LO
SCFLM 10. 1.5

```

```

MODE 2.
JSLC 0006000900120007001000130098009901000008001100140027
JSLC 000300040005007900810082001500160017005600600660028
JSLC 004900500055009601010104006800720120022400220023
JSLC 001800240025002600390045005100380033005202060211
JSLC 021702180040004300460044004700530037004200540029
JNTSEL SM 0006 0009 0012 0007 0010 0013 0098 0099 0100 0008 0011 0014
JNTSEL SM 0003 0004 0005 0079 0081 0082 0015 0016 0017 0056 0060 0066
JNTSEL SM 0049 0050 0055 0096 0101 0104 0068 0072 0120 0224 0022 0023
JNTSEL SM 0018 0024 0025 0026 0039 0045 0051 0038 0033 0052 0206 0211
JNTSEL SM 0217 0218 0040 0043 0046 0044 0047 0053 0037 0042 0054 0029
JNTSEL SM 0027 0028

```

RELIEF

SEAS

*

*SOUTH (45 deg)

```

FTCASE 1 0.00235 1.485 SPC 45.
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.1 5.74 7.38 9.02 10.66 12.3 13.94 15.58 17.22
SCPER 0.50.0195
SCPER 1.50.1604
SCPER 2.50.48530.0349
SCPER 3.50.2589
SCPER 4.50.0398
SCPER 5.50.0013

```

*

*SOUTH-SOUTHWEST (67,5 deg)

```

FTCASE 2 0.00141 1.536 SPC 67.5
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.1 5.74 7.38 9.02 10.66 12.3 13.94 15.58 17.22
SCPER 0.50.0186
SCPER 1.50.1423
SCPER 2.50.51480.0371
SCPER 3.50.2531
SCPER 4.50.0320
SCPER 5.50.0017
SCPER 6.50.0003

```

*

*SOUTH-WEST (90 deg)

```

FTCASE 3 0.00105 1.531 SPC 90.
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.1 5.74 7.38 9.02 10.66 12.3 13.94 15.58 17.22
SCPER 0.50.0136
SCPER 1.50.1046
SCPER 2.50.69850.0317

```

SCPER 3.50.1120
SCPER 4.50.0283
SCPER 5.50.0092
SCPER 6.50.0017
SCPER 7.50.0004

*

*WEST-SOUTHWEST (112,5 deg)

FTCASE 4 0.003 1.341 SPC 112.5
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.1 5.74 7.38 9.02 10.66 12.3 13.94 15.58 17.22
SCPER 0.50.0289
SCPER 1.50.35170.0005
SCPER 2.50.23500.0150
SCPER 3.50.07210.08710.0090
SCPER 4.50.03560.1125
SCPER 5.50.01160.0360
SCPER 6.50.00130.0037
SCPER 7.50.00004.00004

*

*WEST (135 deg)

FTCASE 5 0.01954 1.123 SPC 135.
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.1 5.74 7.38 9.02 10.66 12.3 13.94 15.58 17.22
SCPER 0.50.0114
SCPER 1.50.0884
SCPER 2.50.1836
SCPER 3.50.4702
SCPER 4.50.09490.1235
SCPER 5.50.0239
SCPER 6.50.0037
SCPER 7.50.0003
SCPER 8.51.e-06
SCPER 9.51.e-05

*

*WEST-NORTHWEST (157,5 deg)

FTCASE 6 0.24230 1.078 SPC 157.5
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.1 5.74 7.38 9.02 10.66 12.3 13.94 15.58 17.22
SCPER 0.51.E-025.E-07
SCPER 1.59.E-024.E-042.E-06
SCPER 2.52.E-019.E-032.E-046.E-065.E-07
SCPER 3.52.e-016.e-024.e-032.e-048.e-069.e-07
SCPER 4.51.e-019.e-022.e-023.e-035.e-045.e-054.e-06
SCPER 5.54.e-025.e-022.e-029.e-033.e-038.e-042.E-044.E-05
SCPER 6.57.e-031.e-021.e-028.e-034.e-031.e-035.e-04
SCPER 7.51.e-034.e-035.e-034.e-032.e-037.e-043.e-04
SCPER 8.51.e-041.e-032.e-031.e-035.e-042.e-047.e-05
SCPER 9.52.e-052.e-043.e-042.e-048.e-052.e-055.e-06
SCPER 10.54.e-064.e-055.e-053.e-057.e-062.e-06
SCPER 11.55.e-077.e-066.e-065.e-069.e-07
SCPER 12.5 2.e-069.e-075.e-07

*

*NORTH-WEST (180 deg)

FTCASE 7 0.04578 1.162 SPC 180.
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.1 5.74 7.38 9.02 10.66 12.3 13.94 15.58 17.22
SCPER 0.50.0124
SCPER 1.50.09750.0001
SCPER 2.50.21950.0024
SCPER 3.50.30540.0305
SCPER 4.50.17790.05470.0028
SCPER 5.50.04290.0307
SCPER 6.50.00870.0102
SCPER 7.50.00150.0021
SCPER 8.50.00020.0004
SCPER 9.52.e-058.e-05

```

SCPER 10.55.e-065.e-06
*
*****
*NORTH-NORTHWEST (202.5 deg)
*****
FTCASE 8 0.00308 1.412 SPC 202.5
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.1 5.74 7.38 9.02 10.66 12.3 13.94 15.58 17.22
SCPER 0.50.0248
SCPER 1.50.1872
SCPER 2.50.46190.0026
SCPER 3.50.2819
SCPER 4.50.0401
SCPER 5.50.0015
SCPER 6.54.e-05
*
*****
*NORTH (225 deg)
*****
FTCASE 9 0.00112 1.391 SPC 225.
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.1 5.74 7.38 9.02 10.66 12.3 13.94 15.58 17.22
SCPER 0.50.0254
SCPER 1.50.2009
SCPER 2.50.54050.0045
SCPER 3.50.2014
SCPER 4.50.0264
SCPER 5.50.0008
*
*****
*NORTH-NORTHEAST (247.5 deg)
*****
FTCASE 10 0.00053 1.412 SPC 247.5
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.1 5.74 7.38 9.02 10.66 12.3 13.94 15.58 17.22
SCPER 0.50.0146
SCPER 1.50.1224
SCPER 2.50.25810.0176
SCPER 3.50.4637
SCPER 4.50.1198
SCPER 5.50.0034
SCPER 6.50.0004
*
*****
*NORTH-EAST (270 deg)
*****
FTCASE 11 0.00433 1.419 SPC 270.
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.1 5.74 7.38 9.02 10.66 12.3 13.94 15.58 17.22
SCPER 0.50.0170
SCPER 1.50.1388
SCPER 2.50.31210.0008
SCPER 3.50.4030
SCPER 4.50.1261
SCPER 5.50.0071
SCPER 6.50.0002
*
*****
*EAST-NORTHEAST (292.5 deg)
*****
FTCASE 12 0.01598 1.328 SPC 292.5
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.1 5.74 7.38 9.02 10.66 12.3 13.94 15.58 17.22
SCPER 0.50.0180
SCPER 1.50.14760.0001
SCPER 2.50.29530.0052
SCPER 3.50.31410.04490.0013
SCPER 4.50.09830.0450
SCPER 5.50.01930.0082
SCPER 6.50.00230.0003
SCPER 7.50.0001
*
*****
*EAST (315 deg)

```

```

*****
FTCASE 13 0.42509 1.099 SPC 315.
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.1 5.74 7.38 9.02 10.66 12.3 13.94 15.58 17.22
SCPER 0.51.E-02
SCPER 1.59.E-025.E-043.E-07
SCPER 2.52.E-011.E-024.E-05
SCPER 3.52.E-011.E-016.E-031.E-042.E-06
SCPER 4.51.E-011.E-013.E-022.E-031.E-043.E-06
SCPER 5.52.E-026.E-022.E-022.E-031.E-049.E-068.E-07
SCPER 6.55.E-031.E-022.E-031.E-045.E-06
SCPER 7.57.E-041.E-031.E-042.E-06
SCPER 8.58.E-051.E-043.E-06
SCPER 9.57.E-065.E-06
SCPER 10.58.E-07
*
*****
*EAST-SOUTHEAST (337.5 deg)
*****
FTCASE 14 0.22054 1.129 SPC 337.5
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.1 5.74 7.38 9.02 10.66 12.3 13.94 15.58 17.22
SCPER 0.51.E-02
SCPER 1.51.E-017.E-041.E-06
SCPER 2.52.E-012.E-026.E-05
SCPER 3.52.E-011.E-018.E-032.E-043.E-06
SCPER 4.58.E-021.E-012.E-022.E-031.E-042.E-06
SCPER 5.52.E-024.E-029.E-039.E-045.E-05
SCPER 6.53.E-035.E-036.E-041.E-055.E-07
SCPER 7.53.E-043.E-049.E-06
SCPER 8.56.E-061.E-05
*
*****
*SOUTH-EAST (0 deg)
*****
FTCASE 15 0.01064 1.401 SPC
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.1 5.74 7.38 9.02 10.66 12.3 13.94 15.58 17.22
SCPER 0.50.0164
SCPER 1.50.12400.0010
SCPER 2.50.25190.03910.0002
SCPER 3.50.26950.1924
SCPER 4.50.06560.0343
SCPER 5.50.00310.0023
SCPER 6.53.E-050.0002
SCPER 7.5 1.E-05
*
*****
*SOUTH-SOUTHEAST (22.5 deg)
*****
FTCASE 16 0.00327 1.442 SPC 22.5
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.1 5.74 7.38 9.02 10.66 12.3 13.94 15.58 17.22
SCPER 0.51.E-029.E-031.E-033.E-05
SCPER 1.54.E-028.E-024.E-021.E-023.E-035.E-041.E-04
SCPER 2.51.E-029.E-021.E-011.E-018.E-024.E-022.E-028.E-033.E-036.E-043.E-04
SCPER 3.52.E-032.E-027.E-029.E-027.E-024.E-022.E-026.E-032.E-034.E-041.E-04
SCPER 4.53.E-053.E-036.E-034.E-031.E-031.E-047.E-053.E-05
SCPER 5.5 3.E-053.E-05
*
SCWAV 18.86 20.5
SCPER 0.5
SCPER 1.5
SCPER 2.51.E-043.E-05
SCPER 3.53.E-05
SCPER 4.5
SCPER 5.5 3.E-05
*
END

```

FATIGUE INPUT JACKET KONVENSIONAL

Fatigue Input for Conventional Structure Spectral Analysis

FTOPT F 20. 1. 2. SMAPI SKMXMNSKNE KTLPEFT
FTOPT2 PTPTVC PV WS AWS-261.61 261.61TI2 LO
SCFLM 10. 1.5
MODE 2.
JSLC 009100780061009200790067010501060107009300680080011401150116010001010120
JSLC 006900810094011101120113009700980099007000830095018901900192019300310032
JSLC 0071008400960117011801190009001000110012
JNTSEL SM 0091 0078 0061 0092 0079 0067 0189 0190 0192 0193 0031 0032
JNTSEL SM 0105 0106 0107 0093 0068 0080 0069 0081 0094 0111 0112 0113
JNTSEL SM 0097 0098 0099 0070 0083 0095 0114 0115 0116 0100 0101 0120
JNTSEL SM 0071 0084 0096 0117 0118 0119 0009 0010 0011 0012
RELIEF
SEAS
*

*SOUTH (45 deg)

FTCASE 1 0.00235 1.298 SPC 45.
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.10 5.74 7.38 9.02 10.66 12.30 13.94 15.58 17.22
SCPER 0.50.0195
SCPER 1.50.1604
SCPER 2.50.48530.0349
SCPER 3.50.2589
SCPER 4.50.0398
SCPER 5.50.0013
*

*SOUTH-SOUTHWEST (67,5 deg)

FTCASE 2 0.00141 1.325 SPC 67.5
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.10 5.74 7.38 9.02 10.66 12.30 13.94 15.58 17.22
SCPER 0.50.0186
SCPER 1.50.1423
SCPER 2.50.51480.0371
SCPER 3.50.2531
SCPER 4.50.0320
SCPER 5.50.0017
SCPER 6.50.0003
*

*SOUTH-WEST (90 deg)

FTCASE 3 0.00105 1.322 SPC 90.
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.10 5.74 7.38 9.02 10.66 12.30 13.94 15.58 17.22
SCPER 0.50.0136
SCPER 1.50.1046
SCPER 2.50.69850.0317
SCPER 3.50.1120
SCPER 4.50.0283
SCPER 5.50.0092
SCPER 6.50.0017
SCPER 7.50.0004
*

*WEST-SOUTHWEST (112,5 deg)

FTCASE 4 0.003 1.218 SPC 112.5
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.10 5.74 7.38 9.02 10.66 12.30 13.94 15.58 17.22
SCPER 0.50.0289
SCPER 1.50.35170.0005
SCPER 2.50.23500.0150
SCPER 3.50.07210.08710.0090
SCPER 4.50.03560.1125
SCPER 5.50.01160.0360
SCPER 6.50.00130.0037
SCPER 7.5.00004.00004


```

*
*****
*WEST (135 deg)
*****
FTCASE 5 0.01954 1.083 SPC 135.
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.10 5.74 7.38 9.02 10.66 12.30 13.94 15.58 17.22
SCPER 0.50.0114
SCPER 1.50.0884
SCPER 2.50.1836
SCPER 3.50.4702
SCPER 4.50.09490.1235
SCPER 5.50.0239
SCPER 6.50.0037
SCPER 7.50.0003
SCPER 8.51.e-06
SCPER 9.51.e-05
*
*****
*WEST-NORTHWEST (157,5 deg)
*****
FTCASE 6 0.24230 1.053 SPC 157.5
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.10 5.74 7.38 9.02 10.66 12.30 13.94 15.58 17.22
SCPER 0.51.E-025.E-07
SCPER 1.59.E-024.E-042.E-06
SCPER 2.52.E-019.E-032.E-046.E-065.E-07
SCPER 3.52.e-016.e-024.e-032.e-048.e-069.e-07
SCPER 4.51.e-019.e-022.e-023.e-035.e-045.e-054.e-06
SCPER 5.54.e-025.e-022.e-029.e-033.e-038.e-042.E-044.E-05
SCPER 6.57.e-031.e-021.e-028.e-034.e-031.e-035.e-04
SCPER 7.51.e-034.e-035.e-034.e-032.e-037.e-043.e-04
SCPER 8.51.e-041.e-032.e-031.e-035.e-042.e-047.e-05
SCPER 9.52.e-052.e-043.e-042.e-048.e-052.e-055.e-06
SCPER 10.54.e-064.e-055.e-053.e-057.e-062.e-06
SCPER 11.55.e-077.e-066.e-065.e-069.e-07
SCPER 12.5 2.e-069.e-075.e-07
*
*****
*NORTH-WEST (180 deg)
*****
FTCASE 7 0.04578 1.109 SPC 180.
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.10 5.74 7.38 9.02 10.66 12.30 13.94 15.58 17.22
SCPER 0.50.0124
SCPER 1.50.09750.0001
SCPER 2.50.21950.0024
SCPER 3.50.30540.0305
SCPER 4.50.17790.05470.0028
SCPER 5.50.04290.0307
SCPER 6.50.00870.0102
SCPER 7.50.00150.0021
SCPER 8.50.00020.0004
SCPER 9.52.e-058.e-05
SCPER 10.55.e-065.e-06
*
*****
*NORTH-NORTHWEST (202.5 deg)
*****
FTCASE 8 0.00308 1.258 SPC 202.5
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.10 5.74 7.38 9.02 10.66 12.30 13.94 15.58 17.22
SCPER 0.50.0248
SCPER 1.50.1872
SCPER 2.50.46190.0026
SCPER 3.50.2819
SCPER 4.50.0401
SCPER 5.50.0015
SCPER 6.54.e-05
*
*****
*NORTH (225 deg)
*****
FTCASE 9 0.00112 1.246 SPC 225.

```

SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.10 5.74 7.38 9.02 10.66 12.30 13.94 15.58 17.22
SCPER 0.50.0254
SCPER 1.50.2009
SCPER 2.50.54050.0045
SCPER 3.50.2014
SCPER 4.50.0264
SCPER 5.50.0008

*

*NORTH-NORTHEAST (247.5 deg)

FTCASE 10 0.00053 1.258 SPC 247.5
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.10 5.74 7.38 9.02 10.66 12.30 13.94 15.58 17.22
SCPER 0.50.0146
SCPER 1.50.1224
SCPER 2.50.25810.0176
SCPER 3.50.4637
SCPER 4.50.1198
SCPER 5.50.0034
SCPER 6.50.0004

*

*NORTH-EAST (270 deg)

FTCASE 11 0.00433 1.262 SPC 270.
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.10 5.74 7.38 9.02 10.66 12.30 13.94 15.58 17.22
SCPER 0.50.0170
SCPER 1.50.1388
SCPER 2.50.31210.0008
SCPER 3.50.4030
SCPER 4.50.1261
SCPER 5.50.0071
SCPER 6.50.0002

*

*EAST-NORTHEAST (292.5 deg)

FTCASE 12 0.01598 1.210 SPC 292.5
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.10 5.74 7.38 9.02 10.66 12.30 13.94 15.58 17.22
SCPER 0.50.0180
SCPER 1.50.14760.0001
SCPER 2.50.29530.0052
SCPER 3.50.31410.04490.0013
SCPER 4.50.09830.0450
SCPER 5.50.01930.0082
SCPER 6.50.00230.0003
SCPER 7.50.0001

*

*EAST (315 deg)

FTCASE 13 0.42509 1.068 SPC 315.
SCATD D 1. 1. N JS 2.
SCWAV 0.82 2.46 4.10 5.74 7.38 9.02 10.66 12.30 13.94 15.58 17.22
SCPER 0.51.E-02
SCPER 1.59.E-025.E-043.E-07
SCPER 2.52.E-011.E-024.E-05
SCPER 3.52.E-011.E-016.E-031.E-042.E-06
SCPER 4.51.E-011.E-013.E-022.E-031.E-043.E-06
SCPER 5.52.E-026.E-022.E-022.E-031.E-049.E-068.E-07
SCPER 6.55.E-031.E-022.E-031.E-045.E-06
SCPER 7.57.E-041.E-031.E-042.E-06
SCPER 8.58.E-051.E-043.E-06
SCPER 9.57.E-065.E-06
SCPER 10.58.E-07

*

*EAST-SOUTHEAST (337.5 deg)

FTCASE 14 0.22054 1.087 SPC 337.5

```
SCATD D    1.    1.    N    JS    2.
SCWAV      0.82  2.46  4.10  5.74  7.38  9.02 10.66 12.30 13.94 15.58 17.22
SCPER      0.51.E-02
SCPER      1.51.E-017.E-041.E-06
SCPER      2.52.E-012.E-026.E-05
SCPER      3.52.E-011.E-018.E-032.E-043.E-06
SCPER      4.58.E-021.E-012.E-022.E-031.E-042.E-06
SCPER      5.52.E-024.E-029.E-039.E-045.E-05
SCPER      6.53.E-035.E-036.E-041.E-055.E-07
SCPER      7.53.E-043.E-049.E-06
SCPER      8.56.E-061.E-05
```

*

*SOUTH-EAST (0 deg)

```
FTCASE 15  0.01064    1.252 SPC
SCATD D    1.    1.    N    JS    2.
SCWAV      0.82  2.46  4.10  5.74  7.38  9.02 10.66 12.30 13.94 15.58 17.22
SCPER      0.50.0164
SCPER      1.50.12400.0010
SCPER      2.50.25190.03910.0002
SCPER      3.50.26950.1924
SCPER      4.50.06560.0343
SCPER      5.50.00310.0023
SCPER      6.53.E-050.0002
SCPER      7.5    1.E-05
```

*

*SOUTH-SOUTHEAST (22.5 deg)

```
FTCASE 16  0.00327    1.275 SPC                22.5
SCATD D    1.    1.    N    JS    2.
SCWAV      0.82  2.46  4.10  5.74  7.38  9.02 10.66 12.30 13.94 15.58 17.22
SCPER      0.51.E-029.E-031.E-033.E-05
SCPER      1.54.E-028.E-024.E-021.E-023.E-035.E-041.E-04
SCPER      2.51.E-029.E-021.E-011.E-018.E-024.E-022.E-028.E-033.E-036.E-043.E-04
SCPER      3.52.E-032.E-027.E-029.E-027.E-024.E-022.E-026.E-032.E-034.E-041.E-04
SCPER      4.53.E-053.E-036.E-034.E-031.E-031.E-047.E-053.E-05
SCPER      5.5    3.E-053.E-05
```

*

SCWAV 18.86 20.50

SCPER 0.5

SCPER 1.5

SCPER 2.51.E-043.E-05

SCPER 3.53.E-05

SCPER 4.5

SCPER 5.5 3.E-05

*

END

LAMPIRAN C
SACS OUTPUT

MASS PARTICIPATION FACTOR JACKET MODIFIKASI

MASS PARTICIPATION FACTOR REPORT

BASED ON RETAINED DEGREES OF FREEDOM

| MODE | ***** MASS PARTICIPATION FACTORS ***** | | | ***** CUMULATIVE FACTORS ***** | | |
|------|--|-----------|-----------|--------------------------------|----------|----------|
| | X | Y | Z | X | Y | Z |
| 1 | 0.0972425 | 0.2604275 | 0.0001317 | 0.097243 | 0.260428 | 0.000132 |
| 2 | 0.2378604 | 0.1049412 | 0.0000449 | 0.335103 | 0.365369 | 0.000177 |
| 3 | 0.0028464 | 0.0001643 | 0.0000006 | 0.337949 | 0.365533 | 0.000177 |
| 4 | 0.0468949 | 0.0000442 | 0.0000057 | 0.384844 | 0.365577 | 0.000183 |
| 5 | 0.0000392 | 0.0626628 | 0.0030970 | 0.384883 | 0.428240 | 0.003280 |
| 6 | 0.0000024 | 0.0001928 | 0.0007197 | 0.384886 | 0.428433 | 0.004000 |
| 7 | 0.0001749 | 0.2326048 | 0.0352949 | 0.385061 | 0.661038 | 0.039295 |
| 8 | 0.2573470 | 0.0003366 | 0.0000967 | 0.642408 | 0.661374 | 0.039391 |
| 9 | 0.0000036 | 0.0020535 | 0.0254609 | 0.642411 | 0.663428 | 0.064852 |
| 10 | 0.0093062 | 0.0000516 | 0.0004732 | 0.651717 | 0.663479 | 0.065325 |
| 11 | 0.0007331 | 0.0000024 | 0.0000230 | 0.652451 | 0.663482 | 0.065348 |
| 12 | 0.0000022 | 0.0005889 | 0.0013368 | 0.652453 | 0.664071 | 0.066685 |
| 13 | 0.0000163 | 0.0176208 | 0.0084477 | 0.652469 | 0.681691 | 0.075133 |
| 14 | 0.0163334 | 0.0017964 | 0.0205301 | 0.668802 | 0.683488 | 0.095663 |
| 15 | 0.0183388 | 0.0146080 | 0.2008255 | 0.687141 | 0.698096 | 0.296488 |
| 16 | 0.0218270 | 0.0103249 | 0.1499586 | 0.708968 | 0.708421 | 0.446447 |
| 17 | 0.0005458 | 0.0142691 | 0.0253085 | 0.709514 | 0.722690 | 0.471755 |
| 18 | 0.0101857 | 0.0424925 | 0.0066453 | 0.719700 | 0.765182 | 0.478401 |
| 19 | 0.0471763 | 0.0085345 | 0.0061220 | 0.766876 | 0.773717 | 0.484523 |
| 20 | 0.0035900 | 0.0032032 | 0.0147721 | 0.770466 | 0.776920 | 0.499295 |
| 21 | 0.0082266 | 0.0050855 | 0.0044671 | 0.778693 | 0.782005 | 0.503762 |
| 22 | 0.0004704 | 0.0158509 | 0.1560811 | 0.779163 | 0.797856 | 0.659843 |
| 23 | 0.0043837 | 0.0023848 | 0.0316717 | 0.783547 | 0.800241 | 0.691515 |
| 24 | 0.0001224 | 0.0133142 | 0.0001162 | 0.783669 | 0.813555 | 0.691631 |
| 25 | 0.0053818 | 0.0000644 | 0.0000051 | 0.789051 | 0.813620 | 0.691636 |
| 26 | 0.0001305 | 0.0001201 | 0.0329627 | 0.789181 | 0.813740 | 0.724599 |
| 27 | 0.0171537 | 0.0000053 | 0.0002115 | 0.806335 | 0.813745 | 0.724810 |
| 28 | 0.0000136 | 0.0013836 | 0.0098225 | 0.806349 | 0.815129 | 0.734633 |
| 29 | 0.0158564 | 0.0011281 | 0.0000001 | 0.822205 | 0.816257 | 0.734633 |
| 30 | 0.0006813 | 0.0634511 | 0.0089934 | 0.822886 | 0.879708 | 0.743626 |
| 31 | 0.0097306 | 0.0125439 | 0.0001487 | 0.832617 | 0.892252 | 0.743775 |
| 32 | 0.0003577 | 0.0553490 | 0.0000036 | 0.832975 | 0.947601 | 0.743779 |
| 33 | 0.0341419 | 0.0010922 | 0.0000196 | 0.867117 | 0.948693 | 0.743798 |
| 34 | 0.0262502 | 0.0039808 | 0.0086725 | 0.893367 | 0.952674 | 0.752471 |
| 35 | 0.0386279 | 0.0208455 | 0.0070022 | 0.931995 | 0.973519 | 0.759473 |
| 36 | 0.0027323 | 0.0032869 | 0.0023552 | 0.934727 | 0.976806 | 0.761828 |
| 37 | 0.0030772 | 0.0028189 | 0.0032137 | 0.937804 | 0.979625 | 0.765042 |
| 38 | 0.0007199 | 0.0001130 | 0.0002784 | 0.938524 | 0.979738 | 0.765320 |
| 39 | 0.0010239 | 0.0003159 | 0.0000310 | 0.939548 | 0.980054 | 0.765351 |
| 40 | 0.0316991 | 0.0003003 | 0.0000451 | 0.971247 | 0.980354 | 0.765396 |
| 41 | 0.0000052 | 0.0000104 | 0.0010081 | 0.971252 | 0.980365 | 0.766404 |
| 42 | 0.0026155 | 0.0061888 | 0.0000093 | 0.973868 | 0.986553 | 0.766414 |
| 43 | 0.0101855 | 0.0000017 | 0.0001114 | 0.984053 | 0.986555 | 0.766525 |
| 44 | 0.0001576 | 0.0002369 | 0.0000099 | 0.984211 | 0.986792 | 0.766535 |
| 45 | 0.0000822 | 0.0000162 | 0.0002462 | 0.984293 | 0.986808 | 0.766781 |
| 46 | 0.0006901 | 0.0001500 | 0.0005670 | 0.984983 | 0.986958 | 0.767348 |
| 47 | 0.0002487 | 0.0008553 | 0.0000114 | 0.985232 | 0.987814 | 0.767359 |
| 48 | 0.0059199 | 0.0000200 | 0.0000650 | 0.991152 | 0.987834 | 0.767424 |
| 49 | 0.0000290 | 0.0000029 | 0.0000024 | 0.991181 | 0.987837 | 0.767427 |
| 50 | 0.0001724 | 0.0000064 | 0.0000081 | 0.991353 | 0.987843 | 0.767435 |
| 51 | 0.0010738 | 0.0001334 | 0.0000009 | 0.992427 | 0.987976 | 0.767436 |
| 52 | 0.0000107 | 0.0007476 | 0.0060152 | 0.992438 | 0.988724 | 0.773451 |
| 53 | 0.0000002 | 0.0000005 | 0.0083560 | 0.992438 | 0.988724 | 0.781807 |
| 54 | 0.0000004 | 0.0000398 | 0.0012692 | 0.992438 | 0.988764 | 0.783076 |
| 55 | 0.0000379 | 0.0000001 | 0.0000091 | 0.992476 | 0.988764 | 0.783085 |
| 56 | 0.0000056 | 0.0011696 | 0.0114901 | 0.992482 | 0.989934 | 0.794575 |
| 57 | 0.0000441 | 0.0018493 | 0.0527912 | 0.992526 | 0.991783 | 0.847367 |
| 58 | 0.0000045 | 0.0000588 | 0.0172662 | 0.992530 | 0.991842 | 0.864633 |
| 59 | 0.0000000 | 0.0000000 | 0.0000282 | 0.992530 | 0.991842 | 0.864661 |
| 60 | 0.0000007 | 0.0000010 | 0.0000573 | 0.992531 | 0.991843 | 0.864718 |
| 61 | 0.0000884 | 0.0000023 | 0.0002889 | 0.992619 | 0.991845 | 0.865007 |
| 62 | 0.0000024 | 0.0000150 | 0.0008235 | 0.992622 | 0.991860 | 0.865831 |
| 63 | 0.0001151 | 0.0000045 | 0.0000014 | 0.992737 | 0.991865 | 0.865832 |
| 64 | 0.0001441 | 0.0000061 | 0.0000318 | 0.992881 | 0.991871 | 0.865864 |
| 65 | 0.0001074 | 0.0007559 | 0.0002020 | 0.992988 | 0.992627 | 0.866066 |
| 66 | 0.0001608 | 0.0000137 | 0.0008575 | 0.993149 | 0.992640 | 0.866923 |
| 67 | 0.0008547 | 0.0000541 | 0.0003568 | 0.994004 | 0.992695 | 0.867280 |
| 68 | 0.0001858 | 0.0003737 | 0.0004503 | 0.994190 | 0.993068 | 0.867731 |
| 69 | 0.0000405 | 0.0000007 | 0.0000024 | 0.994230 | 0.993069 | 0.867733 |

| | | | | | | |
|-----|-----------|-----------|-----------|----------|----------|----------|
| 70 | 0.0001098 | 0.0004055 | 0.0003103 | 0.994340 | 0.993475 | 0.868043 |
| 71 | 0.0002765 | 0.0000844 | 0.0013389 | 0.994617 | 0.993559 | 0.869382 |
| 72 | 0.0000004 | 0.0008169 | 0.0000669 | 0.994617 | 0.994376 | 0.869449 |
| 73 | 0.0000005 | 0.0000154 | 0.0003013 | 0.994617 | 0.994391 | 0.869750 |
| 74 | 0.0000070 | 0.0000053 | 0.0002547 | 0.994624 | 0.994397 | 0.870005 |
| 75 | 0.0000010 | 0.0000000 | 0.0000851 | 0.994625 | 0.994397 | 0.870090 |
| 76 | 0.0000005 | 0.0000176 | 0.0001494 | 0.994626 | 0.994414 | 0.870240 |
| 77 | 0.0000049 | 0.0000000 | 0.0006340 | 0.994631 | 0.994414 | 0.870874 |
| 78 | 0.0004227 | 0.0000075 | 0.0000338 | 0.995053 | 0.994422 | 0.870907 |
| 79 | 0.0001439 | 0.0000063 | 0.0000289 | 0.995197 | 0.994428 | 0.870936 |
| 80 | 0.0000510 | 0.0000005 | 0.0014680 | 0.995248 | 0.994428 | 0.872404 |
| 81 | 0.0000002 | 0.0000002 | 0.0023562 | 0.995248 | 0.994429 | 0.874760 |
| 82 | 0.0000001 | 0.0000079 | 0.0058376 | 0.995249 | 0.994437 | 0.880598 |
| 83 | 0.0000002 | 0.0000011 | 0.0026279 | 0.995249 | 0.994438 | 0.883226 |
| 84 | 0.0000001 | 0.0000037 | 0.0002040 | 0.995249 | 0.994441 | 0.883430 |
| 85 | 0.0000009 | 0.0000014 | 0.0021265 | 0.995250 | 0.994443 | 0.885556 |
| 86 | 0.0000007 | 0.0000079 | 0.0105768 | 0.995250 | 0.994451 | 0.896133 |
| 87 | 0.0000003 | 0.0000069 | 0.0047489 | 0.995251 | 0.994457 | 0.900882 |
| 88 | 0.0000011 | 0.0000015 | 0.0003850 | 0.995252 | 0.994459 | 0.901267 |
| 89 | 0.0000004 | 0.0000009 | 0.0053542 | 0.995252 | 0.994460 | 0.906621 |
| 90 | 0.0000388 | 0.0000094 | 0.0000302 | 0.995291 | 0.994469 | 0.906651 |
| 91 | 0.0000012 | 0.0000050 | 0.0023120 | 0.995292 | 0.994474 | 0.908964 |
| 92 | 0.0000006 | 0.0000006 | 0.0000940 | 0.995293 | 0.994475 | 0.909058 |
| 93 | 0.0000021 | 0.0000039 | 0.0015335 | 0.995295 | 0.994479 | 0.910591 |
| 94 | 0.0000005 | 0.0000001 | 0.0000721 | 0.995295 | 0.994479 | 0.910663 |
| 95 | 0.0000026 | 0.0000034 | 0.0001043 | 0.995298 | 0.994482 | 0.910767 |
| 96 | 0.0000005 | 0.0000030 | 0.0002625 | 0.995298 | 0.994485 | 0.911030 |
| 97 | 0.0000000 | 0.0000002 | 0.0008000 | 0.995299 | 0.994485 | 0.911830 |
| 98 | 0.0000005 | 0.0000059 | 0.0078920 | 0.995299 | 0.994491 | 0.919722 |
| 99 | 0.0000001 | 0.0000025 | 0.0318927 | 0.995299 | 0.994494 | 0.951615 |
| 100 | 0.0000001 | 0.0000000 | 0.0004191 | 0.995299 | 0.994494 | 0.952034 |

MASS PARTICIPATION FACTOR JACKET KONVENSSIONAL

MASS PARTICIPATION FACTOR REPORT

BASED ON RETAINED DEGREES OF FREEDOM

| MODE | ***** MASS PARTICIPATION FACTORS ***** | | | ***** CUMULATIVE FACTORS ***** | | |
|------|--|-----------|-----------|--------------------------------|----------|----------|
| | X | Y | Z | X | Y | Z |
| 1 | 0.0258566 | 0.5868069 | 0.0023828 | 0.025857 | 0.586807 | 0.002383 |
| 2 | 0.5746101 | 0.0263989 | 0.0001052 | 0.600467 | 0.613206 | 0.002488 |
| 3 | 0.0005217 | 0.0000137 | 0.0000003 | 0.600988 | 0.613219 | 0.002488 |
| 4 | 0.2352151 | 0.0001350 | 0.0000702 | 0.836203 | 0.613354 | 0.002558 |
| 5 | 0.0002289 | 0.2831510 | 0.0024916 | 0.836432 | 0.896505 | 0.005050 |
| 6 | 0.0596448 | 0.0000140 | 0.0000056 | 0.896077 | 0.896519 | 0.005056 |
| 7 | 0.0041415 | 0.0003805 | 0.0017229 | 0.900219 | 0.896900 | 0.006779 |
| 8 | 0.0648649 | 0.0020996 | 0.0026902 | 0.965084 | 0.899000 | 0.009469 |
| 9 | 0.0020396 | 0.0545230 | 0.0045917 | 0.967123 | 0.953523 | 0.014061 |
| 10 | 0.0002120 | 0.0007251 | 0.7326047 | 0.967335 | 0.954248 | 0.746665 |
| 11 | 0.0052199 | 0.0001478 | 0.0000088 | 0.972555 | 0.954395 | 0.746674 |
| 12 | 0.0114453 | 0.0001325 | 0.0006904 | 0.984001 | 0.954528 | 0.747364 |
| 13 | 0.0002177 | 0.0306826 | 0.0002067 | 0.984218 | 0.985211 | 0.747571 |
| 14 | 0.0006437 | 0.0012510 | 0.0001352 | 0.984862 | 0.986462 | 0.747706 |
| 15 | 0.0018851 | 0.0001902 | 0.0000041 | 0.986747 | 0.986652 | 0.747711 |
| 16 | 0.0000075 | 0.0000741 | 0.0096618 | 0.986754 | 0.986726 | 0.757372 |
| 17 | 0.0001950 | 0.0008863 | 0.0246679 | 0.986949 | 0.987612 | 0.782040 |
| 18 | 0.0011487 | 0.0005095 | 0.0062494 | 0.988098 | 0.988122 | 0.788290 |
| 19 | 0.0006300 | 0.0010053 | 0.0219438 | 0.988728 | 0.989127 | 0.810233 |
| 20 | 0.0025530 | 0.0000042 | 0.0005366 | 0.991281 | 0.989131 | 0.810770 |
| 21 | 0.0055082 | 0.0001945 | 0.0004452 | 0.996789 | 0.989326 | 0.811215 |
| 22 | 0.0001111 | 0.0037086 | 0.0020894 | 0.996901 | 0.993034 | 0.813305 |
| 23 | 0.0000138 | 0.0032771 | 0.0035098 | 0.996914 | 0.996311 | 0.816814 |
| 24 | 0.0005964 | 0.0001480 | 0.0000375 | 0.997511 | 0.996459 | 0.816852 |
| 25 | 0.0000008 | 0.0000295 | 0.0001464 | 0.997512 | 0.996489 | 0.816998 |
| 26 | 0.0000291 | 0.0001483 | 0.0000828 | 0.997541 | 0.996637 | 0.817081 |
| 27 | 0.0003612 | 0.0000118 | 0.0022039 | 0.997902 | 0.996649 | 0.819285 |
| 28 | 0.0000020 | 0.0000272 | 0.0000395 | 0.997904 | 0.996676 | 0.819324 |
| 29 | 0.0000105 | 0.0010728 | 0.0112835 | 0.997914 | 0.997749 | 0.830608 |
| 30 | 0.0000274 | 0.0008429 | 0.0043673 | 0.997942 | 0.998592 | 0.834975 |
| 31 | 0.0000007 | 0.0001405 | 0.0304755 | 0.997942 | 0.998732 | 0.865451 |
| 32 | 0.0011212 | 0.0000014 | 0.0003555 | 0.999064 | 0.998734 | 0.865806 |
| 33 | 0.0006022 | 0.0000431 | 0.0000725 | 0.999666 | 0.998777 | 0.865879 |
| 34 | 0.0000037 | 0.0004394 | 0.0738651 | 0.999669 | 0.999216 | 0.939744 |
| 35 | 0.0001215 | 0.0002367 | 0.0031468 | 0.999791 | 0.999453 | 0.942891 |
| 36 | 0.0000181 | 0.0000002 | 0.0068924 | 0.999809 | 0.999453 | 0.949783 |
| 37 | 0.0000047 | 0.0000995 | 0.0001503 | 0.999814 | 0.999553 | 0.949933 |
| 38 | 0.0000074 | 0.0000095 | 0.0000888 | 0.999821 | 0.999562 | 0.950022 |
| 39 | 0.0000234 | 0.0000066 | 0.0001761 | 0.999844 | 0.999569 | 0.950198 |
| 40 | 0.0000371 | 0.0000185 | 0.0002931 | 0.999882 | 0.999587 | 0.950491 |
| 41 | 0.0000015 | 0.0000088 | 0.0000240 | 0.999883 | 0.999596 | 0.950515 |

| | | | | | | |
|----|-----------|-----------|-----------|----------|----------|----------|
| 42 | 0.0000003 | 0.0000388 | 0.0000006 | 0.999883 | 0.999635 | 0.950516 |
| 43 | 0.0000203 | 0.0000027 | 0.0000204 | 0.999904 | 0.999638 | 0.950536 |
| 44 | 0.0000002 | 0.0000178 | 0.0000993 | 0.999904 | 0.999655 | 0.950636 |
| 45 | 0.0000006 | 0.0000010 | 0.0000000 | 0.999904 | 0.999656 | 0.950636 |
| 46 | 0.0000005 | 0.0000022 | 0.0000001 | 0.999905 | 0.999659 | 0.950636 |
| 47 | 0.0000002 | 0.0001528 | 0.0203942 | 0.999905 | 0.999811 | 0.971030 |
| 48 | 0.0000002 | 0.0000389 | 0.0043869 | 0.999905 | 0.999850 | 0.975417 |
| 49 | 0.0000119 | 0.0000079 | 0.0027007 | 0.999917 | 0.999858 | 0.978118 |
| 50 | 0.0000409 | 0.0000168 | 0.0000004 | 0.999958 | 0.999875 | 0.978118 |
| 51 | 0.0000028 | 0.0000734 | 0.0058861 | 0.999961 | 0.999948 | 0.984004 |
| 52 | 0.0000000 | 0.0000454 | 0.0076298 | 0.999961 | 0.999994 | 0.991634 |
| 53 | 0.0000045 | 0.0000000 | 0.0049490 | 0.999966 | 0.999994 | 0.996583 |
| 54 | 0.0000312 | 0.0000000 | 0.0008055 | 0.999997 | 0.999994 | 0.997388 |
| 55 | 0.0000000 | 0.0000059 | 0.0023093 | 0.999997 | 1.000000 | 0.999698 |
| 56 | 0.0000019 | 0.0000002 | 0.0000268 | 0.999999 | 1.000000 | 0.999725 |
| 57 | 0.0000012 | 0.0000000 | 0.0002535 | 1.000000 | 1.000000 | 0.999978 |
| 58 | 0.0000000 | 0.0000000 | 0.0000218 | 1.000000 | 1.000000 | 1.000000 |
| 59 | 0.0000000 | 0.0000000 | 0.0000001 | 1.000000 | 1.000000 | 1.000000 |
| 60 | 0.0000000 | 0.0000000 | 0.0000000 | 1.000000 | 1.000000 | 1.000000 |
| 61 | 0.0000000 | 0.0000000 | 0.0000000 | 1.000000 | 1.000000 | 1.000000 |
| 62 | 0.0000000 | 0.0000000 | 0.0000000 | 1.000000 | 1.000000 | 1.000000 |
| 63 | 0.0000000 | 0.0000000 | 0.0000000 | 1.000000 | 1.000000 | 1.000000 |

DEFLECTION REPORT JACKET MODIFIKASI

**** MAXIMUM DEFLECTIONS FOR MODES ****

| MODE | X-DIRECTION | | Y-DIRECTION | | Z-DIRECTION | |
|------|-------------|-------|-------------|-------|-------------|-------|
| | DEFL. IN | JOINT | DEFL. IN | JOINT | DEFL. IN | JOINT |
| 1 | 0.64 | 0058 | 1.00 | 0062 | 0.13 | 0062 |
| 2 | 1.00 | 0058 | 0.66 | 0064 | 0.14 | 0064 |
| 3 | 0.97 | 0058 | 1.00 | 0062 | 0.02 | 0271 |
| 4 | 1.00 | 0120 | 0.57 | 0120 | 0.27 | 0120 |
| 5 | 0.48 | 0068 | 1.00 | 0072 | 0.14 | 0068 |
| 6 | 0.74 | 0068 | 1.00 | 0072 | 0.22 | 0068 |
| 7 | 0.43 | 0068 | 1.00 | 0066 | 0.39 | 0096 |
| 8 | 1.00 | 0060 | 0.33 | 0068 | 0.21 | 0120 |
| 9 | 0.01 | 0060 | 0.02 | 0224 | 1.00 | 0096 |
| 10 | 1.00 | 0008 | 0.81 | 0010 | 0.25 | 0164 |
| 11 | 0.04 | 0060 | 0.02 | 0056 | 1.00 | 0104 |
| 12 | 0.02 | 0060 | 0.06 | 0066 | 1.00 | 0096 |
| 13 | 0.33 | 0056 | 1.00 | 0066 | 0.25 | 0104 |
| 14 | 1.00 | 0060 | 0.55 | 0056 | 0.33 | 0101 |
| 15 | 1.00 | 0224 | 0.82 | 0066 | 1.05 | 0164 |
| 16 | 1.00 | 0224 | 0.77 | 0066 | 1.04 | 0123 |
| 17 | 0.65 | 0062 | 1.00 | 0066 | 0.47 | 0019 |
| 18 | 0.18 | 0062 | 1.00 | 0066 | 0.26 | 0164 |
| 19 | 0.83 | 0060 | 1.00 | 0066 | 0.57 | 0123 |
| 20 | 1.00 | 0056 | 0.54 | 0056 | 0.26 | 0056 |
| 21 | 1.00 | 0060 | 0.53 | 0060 | 0.35 | 0409 |
| 22 | 0.20 | 0056 | 0.21 | 0143 | 1.09 | 0128 |
| 23 | 0.42 | 0060 | 0.40 | 0056 | 1.10 | 0171 |
| 24 | 0.19 | 0064 | 1.00 | 0058 | 0.80 | 0307 |
| 25 | 0.85 | 0224 | 0.38 | 0056 | 1.31 | 0171 |
| 26 | 0.32 | 0060 | 1.00 | 0224 | 0.58 | 0164 |
| 27 | 1.00 | 0012 | 0.67 | 0012 | 0.37 | 0128 |
| 28 | 0.18 | 0141 | 0.15 | 0224 | 1.40 | 0133 |
| 29 | 1.00 | 0006 | 0.39 | 0143 | 0.58 | 0128 |
| 30 | 0.27 | 0051 | 0.79 | 0114 | 1.50 | 0133 |
| 31 | 1.00 | 0008 | 0.95 | 0143 | 0.78 | 0128 |
| 32 | 0.49 | 0055 | 1.46 | 0114 | 0.59 | 0171 |
| 33 | 1.12 | 0141 | 1.10 | 0143 | 0.70 | 0051 |
| 34 | 1.98 | 0103 | 1.58 | 0103 | 1.76 | 0137 |
| 35 | 0.50 | 0145 | 0.68 | 0103 | 1.00 | 0099 |
| 36 | 0.06 | 0145 | 0.07 | 0103 | 1.00 | 0100 |
| 37 | 0.63 | 0010 | 0.50 | 0137 | 1.00 | 0098 |
| 38 | 0.87 | 0006 | 1.00 | 0004 | 0.78 | 0062 |
| 39 | 0.35 | 0055 | 0.97 | 0017 | 1.00 | 0100 |
| 40 | 1.21 | 0102 | 0.61 | 0136 | 0.61 | 0171 |
| 41 | 0.05 | 0145 | 0.07 | 0039 | 1.00 | 0079 |
| 42 | 0.84 | 0145 | 0.53 | 0137 | 1.46 | 0133 |
| 43 | 1.00 | 0045 | 1.01 | 0136 | 0.57 | 0171 |
| 44 | 0.39 | 0145 | 0.46 | 0137 | 1.00 | 0100 |
| 45 | 1.00 | 0045 | 0.98 | 0136 | 0.71 | 0051 |
| 46 | 1.00 | 0010 | 0.91 | 0010 | 0.30 | 0100 |
| 47 | 0.69 | 0050 | 1.00 | 0013 | 0.80 | 0072 |
| 48 | 0.91 | 0110 | 0.87 | 0050 | 1.00 | 0068 |
| 49 | 0.02 | 0008 | 0.01 | 0006 | 1.00 | 0100 |

| | | | | | | |
|-----|------|------|------|------|------|------|
| 50 | 0.04 | 0008 | 0.02 | 0055 | 1.00 | 0098 |
| 51 | 0.56 | 0008 | 0.21 | 0008 | 1.00 | 0099 |
| 52 | 0.25 | 0008 | 0.54 | 0010 | 1.00 | 0079 |
| 53 | 0.06 | 0008 | 0.10 | 0010 | 1.01 | 0188 |
| 54 | 0.02 | 0055 | 0.04 | 0008 | 1.00 | 0079 |
| 55 | 0.03 | 0215 | 0.01 | 0016 | 1.00 | 0081 |
| 56 | 0.34 | 0051 | 1.00 | 0039 | 0.32 | 0187 |
| 57 | 0.49 | 0055 | 1.00 | 0039 | 0.89 | 0072 |
| 58 | 0.23 | 0050 | 0.30 | 0049 | 1.00 | 0019 |
| 59 | 0.04 | 0070 | 0.04 | 0002 | 1.00 | 0278 |
| 60 | 0.05 | 0260 | 0.06 | 0188 | 1.00 | 0019 |
| 61 | 1.00 | 0015 | 0.91 | 0016 | 0.72 | 0056 |
| 62 | 0.87 | 0016 | 1.00 | 0008 | 0.62 | 0060 |
| 63 | 0.93 | 0007 | 0.99 | 0010 | 1.02 | 0290 |
| 64 | 1.03 | 0272 | 0.70 | 0008 | 0.51 | 0290 |
| 65 | 0.49 | 0101 | 1.00 | 0096 | 0.13 | 0178 |
| 66 | 0.86 | 0007 | 1.00 | 0096 | 0.31 | 0079 |
| 67 | 0.97 | 0101 | 1.00 | 0001 | 1.07 | 0127 |
| 68 | 0.76 | 0289 | 1.00 | 0001 | 0.44 | 0021 |
| 69 | 0.75 | 0006 | 1.25 | 0046 | 1.40 | 0178 |
| 70 | 0.67 | 0137 | 1.00 | 0096 | 0.50 | 0138 |
| 71 | 1.00 | 0104 | 0.76 | 0106 | 1.14 | 0031 |
| 72 | 0.87 | 0137 | 1.00 | 0051 | 0.41 | 0171 |
| 73 | 0.52 | 0000 | 1.00 | 0002 | 0.28 | 0275 |
| 74 | 1.00 | 0101 | 0.67 | 0108 | 0.35 | 0005 |
| 75 | 1.00 | 0104 | 0.80 | 0014 | 0.24 | 0071 |
| 76 | 1.00 | 0104 | 0.83 | 0106 | 0.30 | 0015 |
| 77 | 1.00 | 0101 | 0.80 | 0108 | 0.14 | 0013 |
| 78 | 1.99 | 0136 | 1.00 | 0045 | 0.43 | 0128 |
| 79 | 1.00 | 0101 | 0.90 | 0108 | 0.40 | 0016 |
| 80 | 1.00 | 0013 | 0.93 | 0002 | 0.29 | 0049 |
| 81 | 1.00 | 0017 | 0.79 | 0015 | 0.90 | 0066 |
| 82 | 0.75 | 0014 | 1.00 | 0008 | 0.81 | 0072 |
| 83 | 0.75 | 0009 | 0.75 | 0012 | 1.00 | 0068 |
| 84 | 0.12 | 0055 | 0.28 | 0068 | 1.00 | 0072 |
| 85 | 0.25 | 0010 | 0.28 | 0120 | 1.00 | 0120 |
| 86 | 0.76 | 0290 | 0.89 | 0012 | 1.00 | 0072 |
| 87 | 1.00 | 0013 | 0.81 | 0006 | 0.94 | 0120 |
| 88 | 1.00 | 0045 | 0.63 | 0045 | 0.73 | 0171 |
| 89 | 0.44 | 0009 | 0.53 | 0079 | 1.00 | 0068 |
| 90 | 1.00 | 0039 | 0.53 | 0051 | 0.13 | 0128 |
| 91 | 0.50 | 0009 | 0.66 | 0006 | 1.00 | 0072 |
| 92 | 0.98 | 0081 | 0.36 | 0081 | 1.00 | 0013 |
| 93 | 0.77 | 0012 | 1.00 | 0006 | 0.50 | 0164 |
| 94 | 0.66 | 0068 | 1.00 | 0068 | 0.26 | 0068 |
| 95 | 0.67 | 0082 | 1.00 | 0120 | 0.16 | 0120 |
| 96 | 1.00 | 0072 | 0.34 | 0120 | 0.09 | 0068 |
| 97 | 0.74 | 0000 | 1.00 | 0001 | 0.38 | 0292 |
| 98 | 1.00 | 0082 | 0.41 | 0082 | 0.17 | 0060 |
| 99 | 1.00 | 0081 | 0.46 | 0068 | 0.49 | 0056 |
| 100 | 0.70 | 0308 | 1.00 | 0002 | 0.25 | 0278 |

DEFLECTION REPORT *JACKET* KONVENSIONAL

**** MAXIMUM DEFLECTIONS FOR MODES ****

| MODE | X-DIRECTION | | Y-DIRECTION | | Z-DIRECTION | |
|------|-------------|-------|-------------|-------|-------------|-------|
| | DEFL. IN | JOINT | DEFL. IN | JOINT | DEFL. IN | JOINT |
| 1 | -0.216 | 0004 | 1.000 | 0004 | -0.116 | 0061 |
| 2 | 1.000 | 0005 | 0.233 | 0005 | -0.106 | 0079 |
| 3 | 1.000 | 0091 | -0.861 | 0005 | -0.069 | 0078 |
| 4 | 1.000 | 0081 | -0.389 | 0081 | 0.201 | 0079 |
| 5 | 0.062 | 0070 | 1.000 | 0081 | -0.318 | 0092 |
| 6 | 1.000 | 0095 | -0.605 | 0070 | -0.104 | 0005 |
| 7 | -0.753 | 0067 | 1.000 | 0079 | -0.081 | 0004 |
| 8 | 1.000 | 0093 | -0.330 | 0067 | 0.208 | 0078 |
| 9 | 0.222 | 0067 | 1.000 | 0067 | -0.301 | 0091 |
| 10 | -0.098 | 0067 | 0.253 | 0079 | 1.000 | 0005 |
| 11 | 1.000 | 0096 | -0.485 | 0081 | -0.044 | 0005 |
| 12 | 1.000 | 0078 | -0.696 | 0078 | -0.153 | 0061 |
| 13 | 0.392 | 0071 | 1.000 | 0071 | -0.163 | 0095 |
| 14 | 1.000 | 0080 | -0.960 | 0084 | 0.148 | 0080 |
| 15 | 1.000 | 0091 | -0.347 | 0061 | -0.062 | 0005 |
| 16 | -0.519 | 0070 | 1.000 | 0071 | 0.208 | 0096 |
| 17 | -0.374 | 0093 | 1.000 | 0093 | -0.393 | 0093 |
| 18 | 1.000 | 0093 | 0.580 | 0093 | -0.208 | 0093 |
| 19 | 1.000 | 0093 | -0.923 | 0083 | -0.266 | 0096 |
| 20 | 0.939 | 0091 | 1.000 | 0067 | 0.128 | 0071 |

| | | | | | | |
|----|--------|------|--------|------|--------|------|
| 21 | 1.000 | 0095 | -0.672 | 0067 | -0.177 | 0084 |
| 22 | 1.000 | 0071 | -0.693 | 0079 | 0.222 | 0095 |
| 23 | -0.733 | 0071 | 1.000 | 0093 | 0.251 | 0091 |
| 24 | 1.000 | 0067 | -0.569 | 0081 | -0.511 | 0005 |
| 25 | 0.841 | 0067 | 1.000 | 0067 | -0.623 | 0004 |
| 26 | -0.802 | 0093 | 1.000 | 0079 | -0.818 | 0005 |
| 27 | -0.563 | 0005 | 1.000 | 0079 | -0.858 | 0004 |
| 28 | 1.000 | 0091 | 0.822 | 0067 | -0.328 | 0005 |
| 29 | 0.794 | 0083 | -0.943 | 0091 | 1.000 | 0004 |
| 30 | -0.625 | 0069 | 1.000 | 0095 | 0.204 | 0081 |
| 31 | 1.000 | 0070 | 0.730 | 0081 | 0.506 | 0004 |
| 32 | 1.000 | 0094 | -0.725 | 0083 | -0.221 | 0083 |
| 33 | -0.833 | 0068 | 1.000 | 0093 | 0.221 | 0080 |
| 34 | 0.144 | 0005 | 0.875 | 0091 | 1.000 | 0003 |
| 35 | 0.764 | 0069 | 1.000 | 0093 | -0.254 | 0093 |
| 36 | -0.627 | 0005 | 1.000 | 0093 | 0.393 | 0070 |
| 37 | 1.000 | 0081 | 0.954 | 0094 | -0.241 | 0094 |
| 38 | 1.000 | 0092 | -0.450 | 0079 | -0.180 | 0081 |
| 39 | -0.525 | 0081 | 0.910 | 0094 | 1.000 | 0068 |
| 40 | -0.780 | 0061 | 0.826 | 0091 | 1.000 | 0080 |
| 41 | 1.000 | 0079 | 0.689 | 0080 | -0.290 | 0094 |
| 42 | 0.865 | 0080 | 0.975 | 0080 | 1.000 | 0094 |
| 43 | 1.000 | 0061 | -0.978 | 0091 | 0.684 | 0081 |
| 44 | 1.000 | 0079 | -0.694 | 0080 | 0.370 | 0092 |
| 45 | 1.000 | 0068 | -0.867 | 0092 | 0.383 | 0092 |
| 46 | -0.861 | 0091 | 1.000 | 0078 | -0.169 | 0079 |
| 47 | 0.617 | 0068 | 1.000 | 0092 | -0.816 | 0092 |
| 48 | 0.425 | 0079 | 1.000 | 0091 | -0.344 | 0091 |
| 49 | 0.442 | 0061 | 0.309 | 0091 | 1.000 | 0067 |
| 50 | 0.159 | 0061 | -0.185 | 0092 | 1.000 | 0079 |
| 51 | 0.796 | 0061 | 1.000 | 0091 | -0.771 | 0096 |
| 52 | -0.365 | 0078 | 0.568 | 0091 | 1.000 | 0092 |
| 53 | -0.295 | 0084 | -0.181 | 0092 | 1.000 | 0084 |
| 54 | 0.219 | 0071 | -0.112 | 0071 | 1.000 | 0071 |
| 55 | 0.238 | 0071 | -0.321 | 0091 | 1.000 | 0094 |
| 56 | 0.111 | 0004 | -0.159 | 0092 | 1.000 | 0061 |
| 57 | 0.143 | 0084 | -0.201 | 0092 | 1.000 | 0078 |
| 58 | 0.153 | 0069 | 0.054 | 0091 | 1.000 | 0069 |
| 59 | -0.125 | 0081 | 0.051 | 0079 | 1.000 | 0078 |
| 60 | -0.006 | 0079 | 0.208 | 0091 | 1.000 | 0091 |
| 61 | -0.132 | 0079 | -0.055 | 0093 | 1.000 | 0079 |
| 62 | 0.111 | 0067 | -0.125 | 0093 | 1.000 | 0067 |
| 63 | 0.104 | 0067 | 0.192 | 0093 | 1.000 | 0067 |

PERIODE DAN FREKUENSI NATURAL JACKET MODIFIKASI

SACS IV-FREQUENCIES AND GENERALIZED MASS

| MODE | FREQ. (CPS) | GEN. MASS | EIGENVALUE | PERIOD (SECS) |
|------|-------------|---------------|---------------|---------------|
| 1 | 0.569524 | 1.5788947E+04 | 7.8093631E-02 | 1.7558511 |
| 2 | 0.575792 | 1.4433508E+04 | 7.6402772E-02 | 1.7367385 |
| 3 | 0.950519 | 1.4537399E+04 | 2.8036152E-02 | 1.0520566 |
| 4 | 1.652198 | 1.3460341E+03 | 9.2793173E-03 | 0.6052543 |
| 5 | 1.674733 | 8.2495141E+02 | 9.0312737E-03 | 0.5971101 |
| 6 | 1.853042 | 1.2204671E+03 | 7.3768269E-03 | 0.5396531 |
| 7 | 2.243213 | 9.3498630E+03 | 5.0338374E-03 | 0.4457891 |
| 8 | 2.374719 | 1.1139978E+04 | 4.4917529E-03 | 0.4211025 |
| 9 | 2.629026 | 4.0353359E+02 | 3.6648010E-03 | 0.3803690 |
| 10 | 2.873253 | 8.9540429E+03 | 3.0682630E-03 | 0.3480376 |
| 11 | 3.312709 | 2.5673932E+02 | 2.3082008E-03 | 0.3018677 |
| 12 | 3.488805 | 2.3744114E+02 | 2.0810704E-03 | 0.2866311 |
| 13 | 3.519529 | 1.1495001E+03 | 2.0448961E-03 | 0.2841290 |
| 14 | 3.570003 | 1.8700697E+03 | 1.9874813E-03 | 0.2801118 |

| | | | | |
|----|-----------|---------------|---------------|-----------|
| 15 | 3.739531 | 8.3287186E+03 | 1.8113649E-03 | 0.2674132 |
| 16 | 3.756513 | 6.2058367E+03 | 1.7950251E-03 | 0.2662043 |
| 17 | 3.877387 | 3.3525407E+03 | 1.6848526E-03 | 0.2579056 |
| 18 | 4.061175 | 1.1494513E+03 | 1.5358079E-03 | 0.2462342 |
| 19 | 4.075049 | 3.3867750E+03 | 1.5253681E-03 | 0.2453958 |
| 20 | 4.170618 | 1.1319993E+03 | 1.4562617E-03 | 0.2397726 |
| 21 | 4.174724 | 3.0979838E+03 | 1.4533988E-03 | 0.2395368 |
| 22 | 4.377894 | 2.0709920E+03 | 1.3216294E-03 | 0.2284203 |
| 23 | 4.418812 | 2.8029379E+03 | 1.2972667E-03 | 0.2263052 |
| 24 | 4.589345 | 5.8796679E+03 | 1.2026490E-03 | 0.2178960 |
| 25 | 4.906429 | 4.2068443E+03 | 1.0522266E-03 | 0.2038142 |
| 26 | 5.262823 | 2.3598159E+03 | 9.1453990E-04 | 0.1900121 |
| 27 | 5.595036 | 5.6126489E+03 | 8.0915999E-04 | 0.1787298 |
| 28 | 5.844546 | 9.0305928E+02 | 7.4154695E-04 | 0.1710997 |
| 29 | 6.108065 | 3.9216140E+03 | 6.7894236E-04 | 0.1637180 |
| 30 | 6.394052 | 8.8485559E+03 | 6.1956656E-04 | 0.1563954 |
| 31 | 6.963937 | 6.5532666E+03 | 5.2231273E-04 | 0.1435969 |
| 32 | 7.165427 | 1.4304481E+04 | 4.9335110E-04 | 0.1395590 |
| 33 | 7.404097 | 1.5096813E+04 | 4.6205748E-04 | 0.1350604 |
| 34 | 7.786418 | 2.0563934E+04 | 4.1779650E-04 | 0.1284288 |
| 35 | 7.869100 | 2.9287894E+03 | 4.0906293E-04 | 0.1270793 |
| 36 | 7.932322 | 2.2396287E+02 | 4.0256834E-04 | 0.1260665 |
| 37 | 8.017698 | 6.1480658E+03 | 3.9404048E-04 | 0.1247241 |
| 38 | 8.149948 | 1.2292184E+04 | 3.8135594E-04 | 0.1227002 |
| 39 | 8.238332 | 8.1896343E+03 | 3.7321719E-04 | 0.1213838 |
| 40 | 8.366790 | 7.5766448E+03 | 3.6184491E-04 | 0.1195201 |
| 41 | 8.585814 | 2.4084260E+02 | 3.4361907E-04 | 0.1164712 |
| 42 | 8.627019 | 3.0392547E+03 | 3.4034452E-04 | 0.1159149 |
| 43 | 8.725210 | 6.5940211E+03 | 3.3272734E-04 | 0.1146104 |
| 44 | 9.036565 | 5.5803680E+03 | 3.1019408E-04 | 0.1106615 |
| 45 | 9.277259 | 7.3779837E+03 | 2.9430722E-04 | 0.1077905 |
| 46 | 9.550099 | 6.7964498E+03 | 2.7773109E-04 | 0.1047110 |
| 47 | 9.754215 | 7.4233304E+03 | 2.6622912E-04 | 0.1025198 |
| 48 | 10.152127 | 1.0807850E+04 | 2.4576846E-04 | 0.0985015 |
| 49 | 10.208952 | 1.0817677E+02 | 2.4304008E-04 | 0.0979532 |
| 50 | 10.302658 | 1.1776712E+02 | 2.3863914E-04 | 0.0970623 |
| 51 | 10.458476 | 1.3611133E+03 | 2.3158126E-04 | 0.0956162 |
| 52 | 10.559289 | 1.5178984E+03 | 2.2718043E-04 | 0.0947034 |
| 53 | 10.709291 | 3.7282772E+02 | 2.2086088E-04 | 0.0933769 |
| 54 | 10.879506 | 1.2536114E+02 | 2.1400399E-04 | 0.0919159 |
| 55 | 11.031666 | 1.3850670E+02 | 2.0814118E-04 | 0.0906481 |
| 56 | 11.214822 | 8.0105007E+02 | 2.0139815E-04 | 0.0891677 |

| | | | | |
|----|-----------|---------------|---------------|-----------|
| 57 | 12.028049 | 5.4171104E+03 | 1.7508537E-04 | 0.0831390 |
| 58 | 12.442949 | 1.7630637E+03 | 1.6360388E-04 | 0.0803668 |
| 59 | 13.282972 | 1.8507856E+02 | 1.4356539E-04 | 0.0752844 |
| 60 | 13.570673 | 1.3624296E+02 | 1.3754267E-04 | 0.0736883 |
| 61 | 13.966228 | 4.7112242E+03 | 1.2986196E-04 | 0.0716013 |
| 62 | 14.203646 | 5.4170364E+03 | 1.2555689E-04 | 0.0704045 |
| 63 | 14.868138 | 8.8688038E+03 | 1.1458482E-04 | 0.0672579 |
| 64 | 15.044207 | 4.5778800E+03 | 1.1191843E-04 | 0.0664708 |
| 65 | 15.348871 | 5.2444866E+02 | 1.0751953E-04 | 0.0651514 |
| 66 | 15.435015 | 5.3963096E+03 | 1.0632273E-04 | 0.0647878 |
| 67 | 15.927654 | 1.1063910E+04 | 9.9847362E-05 | 0.0627839 |
| 68 | 16.324713 | 3.1298134E+03 | 9.5049348E-05 | 0.0612568 |
| 69 | 16.347169 | 2.0265817E+04 | 9.4788386E-05 | 0.0611727 |
| 70 | 16.499932 | 3.7877532E+03 | 9.3041329E-05 | 0.0606063 |
| 71 | 16.527620 | 7.5138887E+03 | 9.2729862E-05 | 0.0605048 |
| 72 | 16.675800 | 4.2653333E+03 | 9.1089200E-05 | 0.0599671 |
| 73 | 17.078079 | 2.0851660E+03 | 8.6848477E-05 | 0.0585546 |
| 74 | 17.373536 | 1.0807781E+03 | 8.3919674E-05 | 0.0575588 |
| 75 | 17.822779 | 3.4403960E+03 | 7.9742414E-05 | 0.0561080 |
| 76 | 18.198976 | 1.7848832E+03 | 7.6479728E-05 | 0.0549481 |
| 77 | 18.328273 | 1.1886647E+03 | 7.5404479E-05 | 0.0545605 |
| 78 | 18.767121 | 3.1651704E+03 | 7.1919215E-05 | 0.0532847 |
| 79 | 18.836543 | 2.7915505E+03 | 7.1390075E-05 | 0.0530883 |
| 80 | 19.256283 | 5.2001702E+03 | 6.8311737E-05 | 0.0519311 |
| 81 | 19.491851 | 5.6925916E+03 | 6.6670559E-05 | 0.0513035 |
| 82 | 20.916816 | 5.2931586E+03 | 5.7896070E-05 | 0.0478084 |
| 83 | 21.370161 | 4.3032693E+03 | 5.5465718E-05 | 0.0467942 |
| 84 | 21.666913 | 9.5016103E+02 | 5.3956795E-05 | 0.0461533 |
| 85 | 21.858157 | 1.1477837E+03 | 5.3016757E-05 | 0.0457495 |
| 86 | 22.270360 | 5.3561549E+03 | 5.1072342E-05 | 0.0449027 |
| 87 | 22.713718 | 6.2504389E+03 | 4.9097998E-05 | 0.0440263 |
| 88 | 23.586332 | 1.5207945E+03 | 4.5532283E-05 | 0.0423974 |
| 89 | 24.056820 | 4.9319163E+03 | 4.3768717E-05 | 0.0415683 |
| 90 | 24.682416 | 5.4186093E+02 | 4.1578124E-05 | 0.0405147 |
| 91 | 25.482644 | 5.6398349E+03 | 3.9007784E-05 | 0.0392424 |
| 92 | 25.909910 | 7.2895350E+03 | 3.7731877E-05 | 0.0385953 |
| 93 | 26.550811 | 4.8136197E+03 | 3.5932270E-05 | 0.0376636 |
| 94 | 27.458062 | 1.6124981E+03 | 3.3596998E-05 | 0.0364192 |
| 95 | 27.593419 | 1.3598131E+03 | 3.3268193E-05 | 0.0362405 |
| 96 | 28.524107 | 7.2093953E+02 | 3.1132653E-05 | 0.0350581 |
| 97 | 29.150447 | 1.4070057E+03 | 2.9809165E-05 | 0.0343048 |
| 98 | 30.128338 | 5.8205788E+02 | 2.7905504E-05 | 0.0331913 |

| | | | | |
|-----|-----------|---------------|---------------|-----------|
| 99 | 30.379620 | 2.4223353E+03 | 2.7445778E-05 | 0.0329168 |
| 100 | 31.519215 | 8.2447653E+02 | 2.5497022E-05 | 0.0317267 |

PERIODE DAN FREKUENSI NATURAL JACKET
KONVENSIONAL

SACS IV-FREQUENCIES AND GENERALIZED MASS

| MODE | FREQ. (CPS) | GEN. MASS | EIGENVALUE | PERIOD (SECS) |
|------|-------------|---------------|---------------|---------------|
| 1 | 0.679433 | 1.7116757E+04 | 5.4871522E-02 | 1.4718155 |
| 2 | 0.684375 | 1.6837030E+04 | 5.4081920E-02 | 1.4611874 |
| 3 | 1.065044 | 2.2311543E+04 | 2.2330836E-02 | 0.9389282 |
| 4 | 1.947745 | 2.2315462E+04 | 6.6769176E-03 | 0.5134142 |
| 5 | 1.979276 | 2.7539562E+04 | 6.4658787E-03 | 0.5052353 |
| 6 | 2.012561 | 1.4408683E+04 | 6.2537725E-03 | 0.4968793 |
| 7 | 3.054517 | 1.5829372E+04 | 2.7149084E-03 | 0.3273840 |
| 8 | 3.331179 | 1.2751263E+04 | 2.2826762E-03 | 0.3001940 |
| 9 | 3.386124 | 1.2641760E+04 | 2.2091974E-03 | 0.2953229 |
| 10 | 3.705438 | 1.6514941E+04 | 1.8448500E-03 | 0.2698736 |
| 11 | 4.333332 | 7.5880574E+03 | 1.3489512E-03 | 0.2307693 |
| 12 | 4.600538 | 1.2063834E+04 | 1.1968037E-03 | 0.2173659 |
| 13 | 4.904015 | 1.0888063E+04 | 1.0532626E-03 | 0.2039145 |
| 14 | 5.331783 | 1.0835479E+04 | 8.9103612E-04 | 0.1875545 |
| 15 | 5.484406 | 4.7944835E+03 | 8.4213357E-04 | 0.1823351 |
| 16 | 5.963011 | 1.2447792E+04 | 7.1237553E-04 | 0.1677005 |
| 17 | 6.381387 | 1.3920724E+04 | 6.2202812E-04 | 0.1567057 |
| 18 | 6.596688 | 9.1934427E+03 | 5.8208764E-04 | 0.1515912 |
| 19 | 6.718475 | 1.8125695E+04 | 5.6117573E-04 | 0.1488433 |
| 20 | 7.046078 | 1.0736156E+04 | 5.1020571E-04 | 0.1419229 |
| 21 | 7.518049 | 1.1647910E+04 | 4.4815677E-04 | 0.1330132 |
| 22 | 7.576628 | 1.9176238E+04 | 4.4125361E-04 | 0.1319848 |
| 23 | 7.684158 | 1.3320912E+04 | 4.2899046E-04 | 0.1301379 |
| 24 | 7.790261 | 1.3439417E+04 | 4.1738444E-04 | 0.1283654 |
| 25 | 8.068178 | 1.5926347E+04 | 3.8912519E-04 | 0.1239437 |
| 26 | 8.111425 | 8.3828429E+03 | 3.8498690E-04 | 0.1232829 |
| 27 | 8.376970 | 1.1720418E+04 | 3.6096601E-04 | 0.1193749 |
| 28 | 8.788889 | 4.7711690E+03 | 3.2792330E-04 | 0.1137800 |
| 29 | 9.172722 | 1.9180403E+04 | 3.0105356E-04 | 0.1090189 |
| 30 | 9.754943 | 5.4839692E+03 | 2.6618939E-04 | 0.1025121 |
| 31 | 9.798817 | 1.1470735E+04 | 2.6381104E-04 | 0.1020531 |
| 32 | 10.000314 | 9.5180089E+03 | 2.5328701E-04 | 0.0999969 |
| 33 | 10.068534 | 1.0751078E+04 | 2.4986635E-04 | 0.0993193 |
| 34 | 10.438768 | 1.3053724E+04 | 2.3245654E-04 | 0.0957967 |

| | | | | |
|----|-----------|---------------|---------------|-----------|
| 35 | 10.828820 | 6.4145145E+03 | 2.1601206E-04 | 0.0923462 |
| 36 | 10.945770 | 1.4506407E+04 | 2.1142075E-04 | 0.0913595 |
| 37 | 11.831097 | 7.7798274E+03 | 1.8096318E-04 | 0.0845230 |
| 38 | 12.211660 | 4.0793745E+03 | 1.6985989E-04 | 0.0818889 |
| 39 | 13.170034 | 9.6939156E+03 | 1.4603819E-04 | 0.0759299 |
| 40 | 13.605126 | 1.1451494E+04 | 1.3684695E-04 | 0.0735017 |
| 41 | 14.123155 | 6.6354275E+03 | 1.2699213E-04 | 0.0708057 |
| 42 | 14.190108 | 1.3011552E+04 | 1.2579659E-04 | 0.0704716 |
| 43 | 14.788360 | 8.6130288E+03 | 1.1582443E-04 | 0.0676207 |
| 44 | 15.618273 | 5.5274528E+03 | 1.0384228E-04 | 0.0640276 |
| 45 | 15.784487 | 5.4495713E+03 | 1.0166684E-04 | 0.0633533 |
| 46 | 18.027775 | 4.8023809E+03 | 7.7939206E-05 | 0.0554700 |
| 47 | 18.519841 | 1.0267047E+04 | 7.3852594E-05 | 0.0539961 |
| 48 | 19.001717 | 3.4135573E+03 | 7.0154341E-05 | 0.0526268 |
| 49 | 21.072541 | 6.5899500E+03 | 5.7043535E-05 | 0.0474551 |
| 50 | 21.475495 | 5.9769503E+03 | 5.4922951E-05 | 0.0465647 |
| 51 | 22.248912 | 7.7491149E+03 | 5.1170854E-05 | 0.0449460 |
| 52 | 26.226036 | 6.4964435E+03 | 3.6827728E-05 | 0.0381300 |
| 53 | 27.838093 | 4.7219514E+03 | 3.2685964E-05 | 0.0359220 |
| 54 | 28.177405 | 3.9551365E+03 | 3.1903494E-05 | 0.0354894 |
| 55 | 31.451071 | 9.3872127E+03 | 2.5607628E-05 | 0.0317954 |
| 56 | 32.684362 | 3.8082497E+03 | 2.3711565E-05 | 0.0305957 |
| 57 | 33.220270 | 5.5886072E+03 | 2.2952708E-05 | 0.0301021 |
| 58 | 40.782196 | 2.4901281E+03 | 1.5229969E-05 | 0.0245205 |
| 59 | 42.507804 | 3.0514208E+03 | 1.4018544E-05 | 0.0235251 |
| 60 | 49.203215 | 1.1306396E+03 | 1.0462929E-05 | 0.0203239 |
| 61 | 51.724502 | 2.0348641E+03 | 9.4677681E-06 | 0.0193332 |
| 62 | 54.631557 | 1.5592576E+03 | 8.4869783E-06 | 0.0183044 |
| 63 | 55.681805 | 2.1321892E+03 | 8.1698415E-06 | 0.0179592 |

BASE SHEAR DAN OVERTURNING MOMENT REPORT JACKET MODIFIKASI

BASE SHEAR AND OVERTURNING MOMENT COEFFICIENTS

| MODE | SHEAR (X) KIPS | SHEAR (Y) KIPS | MOMENT (X) IN-KIP | MOMENT (Y) IN-KIP |
|------|-------------------|-------------------|----------------------|----------------------|
| 1 | 112.717 | -181.060 | 16679.418 | 13826.543 |
| 2 | -172.281 | -112.323 | 10140.610 | -22244.992 |
| 3 | -51.544 | -12.154 | -2667.119 | 4499.451 |
| 4 | -192.342 | -5.797 | -12708.866 | 428307.584 |
| 5 | 4.471 | -175.545 | -377780.954 | -10649.742 |
| 6 | -1.632 | -14.501 | -27940.580 | 3389.191 |
| 7 | 57.064 | -2042.825 | -3659971.955 | -106738.913 |
| 8 | -2677.842 | -95.064 | -171155.898 | 4784273.498 |
| 9 | 2.332 | -54.772 | -140888.414 | -4112.269 |
| 10 | -668.348 | 48.845 | 117647.049 | 1631231.157 |
| 11 | -42.224 | 2.383 | 6292.559 | 120120.964 |
| 12 | -2.487 | -39.620 | -101654.332 | 5807.474 |
| 13 | 15.038 | -485.304 | -1280730.158 | -35776.005 |
| 14 | -624.687 | 203.348 | 597321.568 | 1576260.770 |
| 15 | -1532.737 | -1342.756 | -4209909.081 | 4129718.096 |

| | | | | |
|-----|------------|------------|---------------|---------------|
| 16 | -1456.550 | 983.309 | 3131307.213 | 3779124.949 |
| 17 | -180.363 | 905.194 | 2610550.987 | 434202.779 |
| 18 | 500.498 | 1003.421 | 2828279.818 | -1271652.523 |
| 19 | -1861.571 | 777.189 | 2126188.383 | 4738535.300 |
| 20 | 310.977 | -288.331 | -789890.400 | -804938.096 |
| 21 | 780.306 | 602.201 | 1758975.060 | -2009360.803 |
| 22 | 167.772 | -955.927 | -2365183.501 | -605145.389 |
| 23 | -607.012 | -439.460 | -1006528.891 | 1963167.145 |
| 24 | -158.434 | -1622.234 | -5073567.452 | 420107.598 |
| 25 | 1015.860 | -109.047 | -186396.283 | -1599802.195 |
| 26 | 136.323 | -128.372 | -1868191.255 | -408928.324 |
| 27 | -2724.128 | 46.891 | 190481.758 | 8612720.696 |
| 28 | 33.538 | 332.386 | 61329.359 | -59509.390 |
| 29 | -2609.161 | 683.098 | 1966531.652 | 8526614.939 |
| 30 | 890.262 | 8433.080 | 23829497.248 | -3075214.466 |
| 31 | -3434.538 | 3827.658 | 11375405.368 | 11649561.414 |
| 32 | 1029.958 | -12576.308 | -36829798.352 | -3113761.602 |
| 33 | -11037.974 | -1937.856 | -5834550.386 | 35608348.356 |
| 34 | -12492.630 | 4775.204 | 16194614.567 | 38657267.516 |
| 35 | 5841.223 | -4211.904 | -12828267.895 | -17334577.680 |
| 36 | -436.527 | 469.956 | 1457253.226 | 1337378.572 |
| 37 | -2479.734 | -2329.643 | -7270640.694 | 5954816.286 |
| 38 | 1752.290 | 681.610 | 2979567.637 | -6147240.965 |
| 39 | 1743.020 | -950.262 | -4399795.325 | -5408756.461 |
| 40 | -9621.401 | 919.166 | 2299823.240 | 27974846.477 |
| 41 | -23.223 | -32.190 | -49379.361 | 59674.094 |
| 42 | 1860.990 | 2809.883 | 7583982.163 | -5586358.078 |
| 43 | 5533.222 | 71.133 | 387051.565 | -16633724.368 |
| 44 | 679.169 | 817.319 | 1113132.879 | -2027459.643 |
| 45 | -594.560 | 259.201 | 1143180.864 | 376518.304 |
| 46 | -1751.731 | 801.623 | 1526680.945 | 4814192.682 |
| 47 | 1146.630 | 2087.037 | 3771341.788 | -3434295.667 |
| 48 | 7311.359 | -416.722 | -392110.851 | -17626234.652 |
| 49 | -51.726 | 16.119 | 26476.697 | 100514.910 |
| 50 | -134.115 | -25.420 | -54099.613 | 263295.127 |
| 51 | -1172.735 | -405.682 | -835231.691 | 2228355.718 |
| 52 | -126.175 | -1033.991 | -2047352.561 | 655254.439 |
| 53 | 8.893 | 13.214 | -64907.052 | -91109.190 |
| 54 | -7.582 | 72.763 | 36182.575 | -9911.445 |
| 55 | -78.151 | 4.636 | 3108.429 | 52684.667 |
| 56 | 74.628 | 1059.761 | 3360454.755 | -239277.446 |
| 57 | 626.966 | 3986.179 | 10087693.710 | -1850279.029 |
| 58 | 122.476 | 433.925 | 1373094.703 | -258286.506 |
| 59 | 1.653 | -2.359 | 9364.738 | 79195.996 |
| 60 | -16.444 | -18.952 | -35381.190 | 15091.044 |
| 61 | 1116.487 | -176.538 | 362329.531 | -1047073.365 |
| 62 | 204.183 | -500.216 | -2599489.688 | -1119124.851 |
| 63 | 1980.616 | 382.820 | 585192.452 | -5282312.916 |
| 64 | -1630.243 | 329.196 | -104215.971 | 3347818.591 |
| 65 | -495.755 | -1291.291 | -2393432.558 | 1496557.422 |
| 66 | 1968.284 | -563.013 | 216377.799 | -6012235.674 |
| 67 | 6918.547 | 1709.104 | 4088230.636 | -18770167.125 |
| 68 | -1802.440 | -2509.042 | -8530831.197 | 3990166.773 |
| 69 | -2148.098 | 273.126 | 1065675.204 | 7052169.533 |
| 70 | 1556.746 | 2937.205 | 9458813.939 | -4464518.152 |
| 71 | -3491.804 | 1893.581 | 8096381.458 | 6550761.864 |
| 72 | -101.036 | 4518.769 | 12536087.962 | 92186.057 |
| 73 | 79.740 | 454.957 | 1192759.982 | 1072942.393 |
| 74 | -233.254 | 199.275 | -695501.693 | -4278711.267 |
| 75 | -167.477 | 5.557 | 3024727.031 | 729053.418 |
| 76 | -84.985 | -510.492 | 5412862.079 | 390790.140 |
| 77 | 226.311 | 6.661 | -1539670.360 | 1803882.239 |
| 78 | 3612.910 | 471.653 | 4562078.890 | -13295731.493 |
| 79 | 1994.446 | 409.031 | -6244759.617 | 168458.272 |
| 80 | 1693.838 | 168.139 | 8035855.752 | -1526654.888 |
| 81 | 114.191 | -104.906 | 8400391.155 | 4159123.757 |
| 82 | 85.540 | -777.003 | 3447099.162 | 2265831.417 |
| 83 | 110.446 | 271.125 | 975568.973 | 4966327.624 |
| 84 | -32.214 | 242.586 | -2121793.318 | -772974.318 |
| 85 | -133.563 | 165.882 | 1169773.383 | -2606475.767 |
| 86 | 266.170 | 888.607 | 5784140.677 | -84970.706 |
| 87 | 210.052 | -931.150 | -1388075.276 | 1252518.016 |
| 88 | -203.669 | 233.141 | 3038712.879 | 790045.443 |
| 89 | -221.533 | 331.034 | -19296710.454 | -866326.191 |
| 90 | 783.413 | 379.439 | 1016624.744 | -2852034.576 |
| 91 | 466.444 | -945.025 | 15210790.199 | 525523.186 |
| 92 | -395.783 | 372.507 | 6597047.393 | -27932186.209 |
| 93 | -628.366 | 836.556 | -23971778.235 | -420032.538 |
| 94 | 184.541 | -88.467 | 8159720.276 | -4010973.125 |
| 95 | 399.148 | -449.840 | 851183.756 | 11596261.422 |
| 96 | -138.688 | 328.208 | 1382664.389 | -5536846.974 |
| 97 | 55.623 | -107.958 | -469602.436 | 6522398.333 |
| 98 | -139.056 | -462.113 | -1413825.820 | 6745203.180 |
| 99 | 147.398 | 629.010 | 5093955.879 | 929258.227 |
| 100 | 61.378 | 28.169 | 138646.664 | 347286.130 |

BASE SHEAR DAN OVERTURNING MOMENT REPORT **JACKET KONVENSIONAL**

BASE SHEAR AND OVERTURNING MOMENT COEFFICIENTS

| MODE | SHEAR (X) KIPS | SHEAR (Y) KIPS | MOMENT (X) IN-KIP | MOMENT (Y) IN-KIP |
|------|-------------------|-------------------|----------------------|----------------------|
|------|-------------------|-------------------|----------------------|----------------------|

| | | | | |
|----|-----------|-----------|---------------|---------------|
| 1 | 84.711 | -397.684 | -103927.588 | -23884.907 |
| 2 | -401.843 | -84.879 | -22235.530 | 113383.694 |
| 3 | -33.756 | 5.387 | 2877.889 | 14340.571 |
| 4 | -2397.443 | 56.595 | 135146.442 | 5862983.417 |
| 5 | -85.802 | -2973.632 | -7269834.993 | 203265.353 |
| 6 | -1035.727 | 15.645 | 43882.203 | 2606699.214 |
| 7 | -658.935 | 196.819 | 555421.204 | 1881753.866 |
| 8 | 2783.723 | -493.551 | -1438376.377 | -8149045.688 |
| 9 | 507.850 | 2587.535 | 7517226.062 | -1523403.246 |
| 10 | -224.118 | -408.412 | -1531474.512 | 666093.938 |
| 11 | -1030.834 | -170.920 | -571911.372 | 3395152.246 |
| 12 | -2169.309 | 230.039 | 786791.038 | 7197150.293 |
| 13 | -322.983 | -3778.436 | -12765138.969 | 1162338.604 |
| 14 | -654.880 | 899.682 | 2927174.094 | 2080711.150 |
| 15 | -788.753 | 246.871 | 759359.698 | 2978502.715 |
| 16 | 94.559 | -293.544 | 454955.559 | -640523.007 |
| 17 | 585.229 | -1229.512 | -5534898.243 | -2406905.162 |
| 18 | -1233.532 | 809.529 | 2625951.466 | 5253969.028 |
| 19 | -1330.528 | -1656.235 | -5380622.822 | 5224091.252 |
| 20 | 2267.223 | -90.309 | -383010.644 | -8628541.942 |
| 21 | 3949.005 | 731.313 | 2569749.443 | -14860382.970 |
| 22 | -730.931 | 4161.241 | 15820050.516 | 2847269.555 |
| 23 | 220.994 | -3353.452 | -12020816.645 | -999643.677 |
| 24 | 1498.644 | 735.804 | 3490567.530 | -4907978.938 |
| 25 | -63.024 | 383.717 | 2080808.982 | -461303.722 |
| 26 | 283.368 | -630.691 | -1403022.432 | 257407.748 |
| 27 | -1259.347 | 223.959 | 1187985.949 | 2591398.126 |
| 28 | 66.220 | -239.134 | 24619.138 | -37685.597 |
| 29 | 329.586 | 3280.776 | 8009540.651 | -411277.274 |
| 30 | 321.971 | 1758.669 | 5266865.278 | -782256.697 |
| 31 | 73.933 | -1047.917 | -3294273.665 | 55998.052 |
| 32 | -2849.589 | -99.361 | -248163.458 | 8659165.721 |
| 33 | 2249.890 | -592.853 | -2096629.140 | -6621059.585 |
| 34 | 210.062 | 2243.191 | 8841805.834 | -846017.681 |
| 35 | -902.821 | 1242.098 | 3364280.998 | 2382525.936 |
| 36 | -534.803 | 55.645 | -227000.713 | 765872.906 |
| 37 | -233.780 | -1058.376 | -4183368.219 | 1605201.080 |
| 38 | 225.516 | 252.512 | 1454185.886 | -1937295.417 |
| 39 | -720.774 | 376.986 | -4403911.421 | -3489163.697 |
| 40 | 1053.076 | 731.617 | -1382458.431 | 5845797.539 |
| 41 | 175.736 | 413.636 | -2415853.601 | -2180976.336 |
| 42 | 102.828 | -1229.769 | 8588642.649 | -270496.556 |
| 43 | 797.812 | 289.048 | -2223219.342 | 6144860.216 |
| 44 | 62.973 | -658.175 | 2745568.890 | 1029131.779 |
| 45 | 122.603 | 160.395 | -967647.376 | -2202406.813 |
| 46 | 139.046 | 287.659 | -1005512.794 | 147555.252 |
| 47 | 141.746 | -3693.030 | -5351173.326 | -142612.388 |
| 48 | 90.171 | -1130.722 | 212021.498 | 980779.612 |
| 49 | 1083.219 | -871.595 | 14944129.910 | 6489445.457 |
| 50 | -1990.106 | -1257.533 | 8183865.269 | -12535228.597 |
| 51 | -637.548 | 3209.623 | -3393447.324 | -4246618.076 |
| 52 | -45.268 | -3211.504 | -4587697.642 | -233453.208 |
| 53 | 989.089 | 21.730 | -21521858.932 | 7222101.705 |
| 54 | -2433.377 | -41.064 | -7848244.829 | -17533691.545 |
| 55 | -104.445 | -1999.295 | -11949082.385 | -951270.550 |
| 56 | 793.477 | -240.224 | 4481005.800 | 6764984.466 |
| 57 | -796.371 | -47.786 | 9319813.808 | -6773645.503 |
| 58 | -85.649 | -126.142 | -1828568.859 | -1035760.728 |
| 59 | 125.495 | -7.414 | -158681.877 | 1667087.983 |
| 60 | -0.257 | 0.066 | 214188.779 | 11651.660 |
| 61 | 6.190 | 3.235 | -38374.280 | 106419.888 |
| 62 | -9.078 | 1.616 | 71943.455 | -84943.353 |
| 63 | -4.740 | -1.997 | -141253.958 | -50143.298 |

FATIGUE REPORT JACKET MODIFIKASI

* * * M E M B E R F A T I G U E R E P O R T * * *
(DAMAGE ORDER)

| JOINT | MEMBER | GRUP ID | TYPE ID | ORIGINAL | | JNT TYP | MEM TYP | CHORD LEN. (FT) | GAP (IN) | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | |
|-------|-----------|------------|------------|------------|------------|------------|------------|-----------------------|-------------|--------------------------|-------|-------|-------|-----------------|-----|----------|----------|------------|
| | | | | OD (IN) | WT (IN) | | | | | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC | LIFE | OD (IN) |
| 0022 | 0022-0072 | B06 | TUB | 28.00 | 1.250 | K | BRC | 129.01 | 3.94 | 3.23 | 2.70 | 2.72 | 2.07 | .91224-5 | B | 2192413. | | |
| 0022 | 0050-0022 | JB6 | TUB | 54.00 | 2.500 | K | CHD | 129.01 | | 3.76 | 3.47 | 1.50 | 2.14 | .12449-4 | B | 1606548. | | |
| 0022 | 0068-0022 | B11 | TUB | 28.00 | 1.250 | Y | BRC | 129.01 | | 4.30 | 3.41 | 2.64 | 2.16 | .67811-7 | T | 29494.+4 | | |
| 0022 | 0050-0022 | JB6 | TUB | 54.00 | 2.500 | Y | CHD | 129.01 | | 5.11 | 4.67 | 1.50 | 2.23 | .25365-6 | TR | 78850.+3 | | |
| 0022 | 0022-0025 | JC1 | TUB | 54.00 | 2.500 | K | BRC | 129.01 | 3.94 | 8.18 | 1.52 | 3.68 | 1.50 | .4446397 | T | 44.98024 | | |
| 0022 | 0050-0022 | JB6 | TUB | 54.00 | 2.500 | K | CHD | 129.01 | | 8.93 | 1.63 | 1.50 | 1.58 | .1678258 | T | 119.1712 | | |
| ----- | | | | | | | | | | | | | | | | | | |
| 0015 | 0015-0056 | B09 | TUB | 30.00 | 1.375 | Y | BRC | 112.19 | | 4.27 | 5.37 | 2.46 | 3.75 | .20601-2 | L | 9708.417 | | |
| 0015 | 0015-0049 | JA5 | TUB | 54.00 | 2.500 | Y | CHD | 112.19 | | 6.31 | 6.39 | 1.96 | 4.15 | .44952-2 | L | 4449.186 | | |
| 0015 | 0015-0060 | B09 | TUB | 30.00 | 1.375 | Y | BRC | 112.19 | | 4.27 | 5.37 | 2.46 | 3.75 | .78626-2 | R | 2543.692 | | |
| 0015 | 0015-0049 | JA5 | TUB | 54.00 | 2.500 | Y | CHD | 112.19 | | 6.31 | 6.39 | 1.96 | 4.15 | .0162113 | R | 1233.705 | | |
| 0015 | 0003-0015 | JC1 | TUB | 54.00 | 2.500 | Y | BRC | 112.19 | | 8.23 | 1.67 | 3.10 | 1.50 | .1586710 | T | 126.0470 | | |
| 0015 | 0015-0049 | JA5 | TUB | 54.00 | 2.500 | Y | CHD | 112.19 | 10.00 | 1.50 | 1.77 | 1.94 | | .2080824 | T | 96.11578 | | |

```

-----
0016 0016-0056 B08 TUB 28.00 1.250 Y BRC 104.14 3.90 4.62 2.45 3.14 .45719-6 R 43746.+3
0016 0016-0050 JB5 TUB 54.00 2.500 Y CHD 104.14 5.05 5.38 1.71 3.23 .13893-5 R 14396.+3

```

```

SACS V8i SELECTseries 3 (v5.6) ITS
ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

```

DATE 07-AUG-2020 TIME 21:02:24 FTG PAGE 276

* * * M E M B E R F A T I G U E R E P O R T * * *
(DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | |
|-------|-----------|------|------|----------|-------|-----|-----|--------|------|--------------------------|------|------|----------|-----------------|----------|----------|----------|------|
| | | | | OD | WT | | | | | (IN) | (IN) | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | | | | | | | | | (IN) | (IN) |
| 0016 | 0016-0066 | B08 | TUB | 28.00 | 1.250 | Y | BRC | 104.14 | 2.87 | 5.33 | 2.41 | 3.28 | .0122636 | L | 1630.845 | | | |
| 0016 | 0016-0050 | JB5 | TUB | 54.00 | 2.500 | Y | CHD | 104.14 | 2.44 | 6.56 | 1.78 | 3.38 | .0334462 | L | 597.9749 | | | |
| 0016 | 0004-0016 | JC1 | TUB | 54.00 | 2.500 | Y | BRC | 104.14 | 5.72 | 1.50 | 3.68 | 1.50 | .1209764 | T | 165.3216 | | | |
| 0016 | 0016-0050 | JB5 | TUB | 54.00 | 2.500 | Y | CHD | 104.14 | 7.73 | 1.50 | 1.50 | 1.50 | .1979608 | T | 101.0301 | | | |
| ----- | | | | | | | | | | | | | | | | | | |
| 0023 | 0023-0072 | B08 | TUB | 28.00 | 1.250 | K | BRC | 129.01 | 8.68 | 3.14 | 2.74 | 2.71 | 2.09 | .12278-4 | B | 1628895. | | |
| 0023 | 0055-0023 | JB6 | TUB | 54.00 | 2.500 | K | CHD | 129.01 | 3.75 | 3.54 | 1.50 | 2.15 | .27033-4 | B | 739832.2 | | | |
| 0023 | 0120-0023 | B08 | TUB | 28.00 | 1.250 | Y | BRC | 129.01 | 4.30 | 3.41 | 2.64 | 2.16 | .10889-5 | T | 18368.+3 | | | |
| 0023 | 0055-0023 | JB6 | TUB | 54.00 | 2.500 | Y | CHD | 129.01 | 5.11 | 4.67 | 1.50 | 2.23 | .39512-5 | TL | 5061730. | | | |
| 0023 | 0023-0026 | JC1 | TUB | 54.00 | 2.500 | K | BRC | 129.01 | 8.68 | 8.06 | 1.52 | 3.68 | 1.50 | .1336777 | T | 149.6136 | | |

0023 0055-0023 JB6 TUB 54.00 2.500 K CHD 129.01 8.84 1.67 1.50 1.59 .0462733 T 432.2148

0017 0017-0066 B03 TUB 28.00 1.250 Y BRC 104.14 2.69 5.38 2.41 3.25 .72133-2 R 2772.646

0017 0017-0055 JB5 TUB 54.00 2.500 Y CHD 104.14 1.95 6.73 1.78 3.35 .0207479 R 963.9536

0017 0017-0060 B08 TUB 28.00 1.250 Y BRC 104.14 3.90 4.62 2.45 3.14 .10844-5 L 18444.+3

0017 0017-0055 JB5 TUB 54.00 2.500 Y CHD 104.14 5.05 5.38 1.71 3.23 .21659-5 L 9234000.

SACS V8i SELECTseries 3 (v5.6) ITS
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

DATE 07-AUG-2020 TIME 21:02:24 FTG PAGE 277

* * * MEMBER FATIGUE REPORT * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | |
|-------|-----------|------|------|----------|-------|-----|-----|--------|------|--------------------------|------|-------|----------|-----------------|----------|--------|----------|------|
| | | | | OD | WT | | | | | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | (IN) | (IN) |
| 0017 | 0005-0017 | JC1 | TUB | 54.00 | 2.500 | Y | BRC | 104.14 | 5.13 | 1.50 | 3.68 | 1.50 | .76788-2 | T | 2604.575 | | | |
| 0017 | 0017-0055 | JB5 | TUB | 54.00 | 2.500 | Y | CHD | 104.14 | 7.13 | 1.50 | 1.50 | 1.50 | .0295219 | T | 677.4640 | | | |
| 0018 | 0018-0068 | B08 | TUB | 28.00 | 1.250 | Y | BRC | 35.40 | 2.79 | 2.21 | 2.83 | 1.54 | .4363-10 | B | 45844.+7 | | | |
| 0018 | 0224-0018 | JA8 | TUB | 54.00 | 2.500 | Y | CHD | 35.40 | 2.55 | 2.29 | 1.50 | 1.59 | .0000000 | T | INFINITE | | | |
| 0018 | 0120-0018 | B08 | TUB | 28.00 | 1.250 | Y | BRC | 35.40 | 2.79 | 2.21 | 2.83 | 1.54 | .25931-8 | B | 77127.+5 | | | |
| 0018 | 0224-0018 | JA8 | TUB | 54.00 | 2.500 | Y | CHD | 35.40 | 2.55 | 2.29 | 1.50 | 1.59 | .3790-10 | B | 52765.+7 | | | |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|--|------|------|------|------|----------|---|----------|
| 0018 | 0018-0024 | JC1 | TUB | 54.00 | 2.500 | Y | BRC | 35.40 | | 3.45 | 1.54 | 3.12 | 1.50 | .0189897 | T | 1053.205 |
| 0018 | 0224-0018 | JA8 | TUB | 54.00 | 2.500 | Y | CHD | 35.40 | | 6.35 | 1.50 | 1.75 | 1.88 | .0205332 | T | 974.0327 |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|------|------|------|------|------|----------|---|----------|
| 0003 | 0011-0003 | B08 | TUB | 28.00 | 1.250 | K | BRC | 35.82 | 3.00 | 2.76 | 3.23 | 2.55 | 2.64 | .45583-3 | L | 43876.30 |
| 0003 | 0008-0003 | JA4 | TUB | 54.00 | 2.500 | K | CHD | 35.82 | | 2.69 | 3.56 | 1.56 | 2.72 | .81233-3 | L | 24620.51 |
| 0003 | 0014-0003 | B08 | TUB | 28.00 | 1.250 | K | BRC | 35.82 | 3.00 | 2.76 | 3.24 | 2.55 | 2.63 | .19995-2 | R | 10002.64 |
| 0003 | 0008-0003 | JA4 | TUB | 54.00 | 2.500 | K | CHD | 35.82 | | 2.69 | 3.57 | 1.56 | 2.71 | .33814-2 | R | 5914.739 |
| 0003 | 0086-0003 | B27 | TUB | 24.00 | 0.750 | K | BRC | 35.82 | 3.00 | 2.82 | 3.53 | 2.06 | 3.65 | .89481-7 | R | 22351.+4 |
| 0003 | 0008-0003 | JA4 | TUB | 54.00 | 2.500 | K | CHD | 35.82 | | 2.08 | 2.59 | 1.50 | 2.74 | .70174-9 | R | 28500.+6 |

SACS V8i SELECTseries 3 (v5.6)
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

ITS

DATE 07-AUG-2020 TIME 21:02:24 FTG PAGE 278

* * * M E M B E R F A T I G U E R E P O R T * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|------|--------------------------|------|-------|-------|-----------------|-------|----------|----------|------|
| | | | | OD | WT | | | | | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | (IN) | (IN) |
| 0003 | 0085-0003 | B28 | TUB | 24.00 | 0.750 | K | BRC | 35.82 | 3.00 | 2.83 | 3.27 | 2.06 | 3.78 | .70100-7 | BL | 28531.+4 | | |
| 0003 | 0008-0003 | JA4 | TUB | 54.00 | 2.500 | K | CHD | 35.82 | | 2.16 | 2.47 | 1.50 | 2.83 | .65388-9 | BL | 30587.+6 | | |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|------|------|------|------|------|----------|---|----------|
| 0004 | 0011-0004 | B08 | TUB | 28.00 | 1.250 | K | BRC | 35.98 | 3.00 | 2.69 | 3.04 | 2.55 | 2.77 | .14917-2 | L | 13407.43 |
|------|-----------|-----|-----|-------|-------|---|-----|-------|------|------|------|------|------|----------|---|----------|

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|------|------|------|------|------|----------|---|----------|
| 0004 | 0014-0004 | JB4 | TUB | 54.00 | 2.500 | K | CHD | 35.98 | | 2.69 | 3.33 | 1.57 | 2.85 | .22753-2 | L | 8790.230 |
| 0004 | 0079-0004 | B24 | TUB | 24.00 | 0.750 | K | BRC | 35.98 | 3.00 | 2.83 | 3.41 | 2.06 | 3.71 | .13399-3 | R | 149263.9 |
| 0004 | 0014-0004 | JB4 | TUB | 54.00 | 2.500 | K | CHD | 35.98 | | 2.12 | 2.53 | 1.50 | 2.78 | .15998-4 | R | 1250151. |
| 0004 | 0004-0082 | B26 | TUB | 24.00 | 0.750 | T | BRC | 35.98 | | 2.75 | 4.74 | 2.06 | 3.09 | .36539-6 | R | 54736.+3 |
| 0004 | 0014-0004 | JB4 | TUB | 54.00 | 2.500 | T | CHD | 35.98 | | 1.73 | 3.14 | 1.50 | 2.32 | .26598-8 | R | 75193.+5 |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|----|-----|-------|------|------|------|------|------|----------|----|----------|
| 0007 | 0009-0007 | B07 | TUB | 32.00 | 1.500 | TK | BRC | 70.00 | 6.00 | 2.87 | 2.90 | 2.66 | 3.15 | .56015-4 | TL | 357046.1 |
| 0007 | 0006-0007 | JA2 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 3.57 | 3.69 | 1.86 | 3.73 | .19328-3 | L | 103474.2 |
| 0007 | 0012-0007 | B07 | TUB | 32.00 | 1.500 | TK | BRC | 70.00 | 6.00 | 2.81 | 2.83 | 2.66 | 3.16 | .19616-3 | TR | 101956.2 |
| 0007 | 0006-0007 | JA2 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 3.49 | 3.56 | 1.86 | 3.75 | .49718-3 | TR | 40226.56 |
| 0007 | 0007-0011 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 70.00 | 6.00 | 2.83 | 2.90 | 2.55 | 2.86 | .37785-3 | T | 52931.55 |
| 0007 | 0007-0008 | JA3 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 3.10 | 3.26 | 1.56 | 2.95 | .45302-3 | TR | 44148.14 |

SACS V8i SELECTseries 3 (v5.6)
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

ITS

DATE 07-AUG-2020 TIME 21:02:24 FTG PAGE 279

* * * MEMBER FATIGUE REPORT * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | |
|-------|--------|------|------|----------|------|-----|-----|-------|------|--------------------------|------|-------|-------|-----------------|-------|--------|----------|------|
| | | | | OD | WT | | | | | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | (IN) | (IN) |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|----|-----|-------|------|------|------|------|------|----------|---|----------|
| 0007 | 0007-0014 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 70.00 | 6.00 | 2.82 | 2.89 | 2.55 | 2.87 | .19131-2 | T | 10454.51 |
| 0007 | 0007-0008 | JA3 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 3.09 | 3.25 | 1.56 | 2.96 | .20230-2 | T | 9886.430 |
| 0007 | 0007-0207 | B21 | TUB | 22.00 | 0.750 | TK | BRC | 70.00 | 6.00 | 2.99 | 3.21 | 2.04 | 3.80 | .0000000 | T | INFINITE |
| 0007 | 0006-0007 | JA2 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 2.34 | 2.42 | 1.50 | 2.79 | .0000000 | T | INFINITE |
| 0007 | 0007-0208 | B22 | TUB | 22.00 | 0.750 | TK | BRC | 70.00 | 6.00 | 2.99 | 3.26 | 2.04 | 3.77 | .54814-8 | T | 36487.+5 |
| 0007 | 0006-0007 | JA2 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 2.34 | 2.44 | 1.50 | 2.76 | .3291-10 | T | 60780.+7 |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|----|-----|-------|------|------|------|------|------|----------|----|----------|
| 0014 | 0007-0014 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 70.00 | 6.00 | 2.60 | 2.61 | 2.55 | 2.80 | .16109-2 | TL | 12415.58 |
| 0014 | 0013-0014 | JB3 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 2.81 | 2.83 | 1.56 | 2.89 | .18259-2 | TL | 10953.70 |
| 0014 | 0014-0003 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 70.00 | 6.00 | 2.62 | 2.64 | 2.55 | 2.81 | .12045-2 | T | 16604.72 |
| 0014 | 0014-0004 | JB4 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 2.84 | 2.88 | 1.56 | 2.89 | .11944-2 | T | 16745.41 |
| 0014 | 0014-0011 | B23 | TUB | 24.00 | 0.750 | T | BRC | 70.00 | | 3.03 | 4.97 | 2.06 | 3.09 | .10267-7 | TL | 19479.+5 |
| 0014 | 0013-0014 | JB3 | TUB | 54.00 | 2.500 | T | CHD | 70.00 | | 2.43 | 3.14 | 1.50 | 2.32 | .3534-10 | TL | 56592.+7 |
| 0014 | 0014-0215 | B23 | TUB | 24.00 | 0.750 | TK | BRC | 70.00 | 6.00 | 2.86 | 2.87 | 2.06 | 3.97 | .20319-6 | BR | 98432.+3 |
| 0014 | 0013-0014 | JB3 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 2.28 | 2.29 | 1.50 | 2.98 | .26232-8 | BR | 76244.+5 |

SACS V8i SELECTseries 3 (v5.6)
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

ITS

DATE 07-AUG-2020 TIME 21:02:24 FTG PAGE 280

* * * MEMBER FATIGUE REPORT * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | | REQUIRED | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|------|--------------------------|------|------|------|-----------------|-------|----------|-------|----------|------|
| | | | | OD | WT | | | | | TYP | TYP | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC |
| | ID | ID | ID | (IN) | (IN) | | | (FT) | (IN) | | | | | | | | | (IN) | (IN) |
| 0013 | 0009-0013 | B02 | TUB | 26.00 | 1.250 | TK | BRC | 70.00 | 6.00 | 2.73 | 2.76 | 2.55 | 2.68 | .87556-3 | TR | 22842.49 | | | |
| 0013 | 0012-0013 | JB2 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 2.92 | 2.98 | 1.54 | 2.71 | .11376-2 | R | 17580.46 | | | |
| 0013 | 0013-0011 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 70.00 | 6.00 | 2.79 | 2.85 | 2.55 | 2.79 | .16581-2 | T | 12062.23 | | | |
| 0013 | 0013-0014 | JB3 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 3.04 | 3.19 | 1.56 | 2.87 | .17594-2 | TL | 11367.81 | | | |
| 0013 | 0013-0100 | B19 | TUB | 22.00 | 0.750 | TK | BRC | 70.00 | 6.00 | 2.97 | 3.18 | 2.04 | 3.74 | .12901-6 | T | 15503.+4 | | | |
| 0013 | 0012-0013 | JB2 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 2.32 | 2.40 | 1.50 | 2.74 | .24115-8 | T | 82936.+5 | | | |
| 0013 | 0099-0013 | B20 | TUB | 22.00 | 0.750 | T | BRC | 70.00 | | 3.04 | 4.92 | 2.04 | 2.93 | .26032-8 | BR | 76829.+5 | | | |
| 0013 | 0012-0013 | JB2 | TUB | 54.00 | 2.500 | T | CHD | 70.00 | | 2.39 | 3.08 | 1.50 | 2.15 | .0000000 | T | INFINITE | | | |
| ----- | | | | | | | | | | | | | | | | | | | |
| 0066 | 0016-0066 | B08 | TUB | 28.00 | 1.250 | T | BRC | 70.78 | | 2.75 | 2.69 | 2.31 | 1.57 | .34924-3 | BR | 57266.42 | | | |
| 0066 | 0066-0050 | B04 | TUB | 28.00 | 1.375 | T | CHD | 70.78 | | 2.31 | 3.60 | 2.81 | 2.20 | .15372-2 | R | 13010.48 | | | |
| 0066 | 0066-0055 | B08 | TUB | 28.00 | 1.250 | T | BRC | 70.78 | | 2.73 | 2.69 | 2.32 | 1.57 | .29116-3 | TR | 68691.11 | | | |
| 0066 | 0017-0066 | B03 | TUB | 28.00 | 1.375 | T | CHD | 70.78 | | 2.28 | 3.60 | 2.81 | 2.19 | .14855-2 | R | 13463.13 | | | |
| ----- | | | | | | | | | | | | | | | | | | | |
| 0009 | 0000-0009 | B01 | TUB | 28.00 | 1.375 | TK | BRC | 70.00 | 6.00 | 2.90 | 2.96 | 2.61 | 3.06 | .43076-4 | TR | 464291.5 | | | |
| 0009 | 0002-0009 | JB1 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 3.33 | 3.48 | 1.70 | 3.32 | .72446-4 | TR | 276066.5 | | | |

* * * M E M B E R F A T I G U E R E P O R T * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|------|--------------------------|------|------|------|-----------------|-------|----------|----------|--------|------|
| | | | | OD | WT | | | | | TYP | TYP | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | | (IN) | (IN) |
| 0009 | 0001-0009 | B01 | TUB | 28.00 | 1.375 | TK | BRC | 70.00 | 6.00 | 2.87 | 2.93 | 2.60 | 2.95 | .32975-3 | T | 60652.33 | | | |
| 0009 | 0002-0009 | JB1 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 3.29 | 3.43 | 1.70 | 3.20 | .38254-3 | T | 52282.80 | | | |
| 0009 | 0009-0013 | B02 | TUB | 26.00 | 1.250 | TK | BRC | 70.00 | 6.00 | 2.96 | 3.08 | 2.55 | 2.75 | .15117-2 | T | 13229.90 | | | |
| 0009 | 0009-0010 | JB2 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 3.18 | 3.42 | 1.54 | 2.78 | .14359-2 | T | 13928.95 | | | |
| 0009 | 0009-0007 | B07 | TUB | 32.00 | 1.500 | TK | BRC | 70.00 | 6.00 | 3.19 | 3.30 | 2.66 | 3.19 | .46666-4 | T | 428575.5 | | | |
| 0009 | 0009-0010 | JB2 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 4.05 | 4.45 | 1.86 | 3.78 | .11063-3 | T | 180784.7 | | | |
| 0009 | 0009-0193 | B17 | TUB | 22.00 | 1.000 | TK | BRC | 70.00 | 6.00 | 3.42 | 4.13 | 2.16 | 4.11 | .95348-5 | R | 2097582. | | | |
| 0009 | 0002-0009 | JB1 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 3.13 | 3.45 | 1.51 | 3.52 | .22117-5 | R | 9042758. | | | |
| 0009 | 0012-0009 | B17 | TUB | 22.00 | 1.000 | TK | BRC | 70.00 | 6.00 | 3.33 | 4.13 | 2.16 | 3.79 | .15125-5 | TL | 13224.+3 | | | |
| 0009 | 0002-0009 | JB1 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 3.03 | 3.39 | 1.51 | 3.25 | .21164-6 | TL | 94499.+3 | | | |
| ----- | | | | | | | | | | | | | | | | | | | |
| 0011 | 0007-0011 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 70.00 | 6.00 | 2.61 | 2.62 | 2.55 | 2.80 | .29217-3 | TR | 68452.48 | | | |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|----|-----|-------|------|------|------|------|------|----------|----|----------|
| 0011 | 0010-0011 | JB3 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 2.82 | 2.85 | 1.56 | 2.89 | .32471-3 | TR | 61593.24 |
| 0011 | 0011-0003 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 70.00 | 6.00 | 2.65 | 2.68 | 2.55 | 2.80 | .29759-3 | T | 67207.05 |
| 0011 | 0011-0005 | JB4 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 2.87 | 2.93 | 1.56 | 2.88 | .31320-3 | TL | 63856.29 |

SACS V8i SELECTseries 3 (v5.6)
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

ITS

DATE 07-AUG-2020 TIME 21:02:24 FTG PAGE 282

* * * MEMBER FATIGUE REPORT * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|------|--------------------------|------|------|------|-----------------|-------|----------|----------|--------|------|
| | | | | OD | WT | | | | | TYP | TYP | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | | (IN) | (IN) |
| 0011 | 0011-0004 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 70.00 | 6.00 | 2.69 | 2.73 | 2.55 | 2.79 | .13068-2 | TR | 15304.80 | | | |
| 0011 | 0011-0005 | JB4 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 2.91 | 3.01 | 1.57 | 2.87 | .14447-2 | TR | 13843.78 | | | |
| 0011 | 0013-0011 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 70.00 | 6.00 | 2.67 | 2.70 | 2.55 | 2.79 | .12636-2 | T | 15827.67 | | | |
| 0011 | 0010-0011 | JB3 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 2.89 | 2.96 | 1.56 | 2.87 | .12967-2 | T | 15423.79 | | | |
| 0011 | 0011-0214 | B23 | TUB | 24.00 | 0.750 | TK | BRC | 70.00 | 6.00 | 2.86 | 2.87 | 2.06 | 3.97 | .52719-8 | BL | 37937.+5 | | | |
| 0011 | 0010-0011 | JB3 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 2.28 | 2.29 | 1.50 | 2.98 | .3203-10 | BL | 62445.+7 | | | |
| 0011 | 0014-0011 | B23 | TUB | 24.00 | 0.750 | TK | BRC | 70.00 | 6.00 | 2.87 | 2.99 | 2.06 | 3.94 | .64412-7 | BL | 31050.+4 | | | |
| 0011 | 0010-0011 | JB3 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 2.29 | 2.34 | 1.50 | 2.96 | .56287-9 | BL | 35532.+6 | | | |
| ----- | | | | | | | | | | | | | | | | | | | |
| 0005 | 0005-0079 | B25 | TUB | 24.00 | 0.750 | T | BRC | 35.98 | | 2.75 | 4.74 | 2.06 | 3.09 | .94962-3 | R | 21061.10 | | | |

| | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|------|------|------|------|----------|---|----------|
| 0005 | 0011-0005 | JB4 | TUB | 54.00 | 2.500 | T | CHD | 35.98 | 1.73 | 3.14 | 1.50 | 2.32 | .92816-4 | R | 215480.2 |
| 0005 | 0005-0081 | B26 | TUB | 24.00 | 0.750 | T | BRC | 35.98 | 2.75 | 4.74 | 2.06 | 3.09 | .95504-6 | L | 20942.+3 |
| 0005 | 0011-0005 | JB4 | TUB | 54.00 | 2.500 | T | CHD | 35.98 | 1.73 | 3.14 | 1.50 | 2.32 | .10846-7 | L | 18440.+5 |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|----|-----|-------|------|------|------|------|----------|----------|----------|----------|
| 0012 | 0000-0012 | B01 | TUB | 28.00 | 1.375 | TK | BRC | 70.00 | 6.00 | 2.85 | 2.89 | 2.61 | 3.09 | .32304-3 | TL | 61912.48 |
| 0012 | 0001-0012 | JB1 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | 3.27 | 3.36 | 1.70 | 3.35 | .55504-3 | TL | 36033.51 | |

SACS V8i SELECTseries 3 (v5.6)
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

ITS

DATE 07-AUG-2020 TIME 21:02:24 FTG PAGE 283

* * * M E M B E R F A T I G U E R E P O R T * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|------|--------------------------|------|------|------|-----------------|-------|----------|----------|--------|------|
| | | | | OD | WT | | | | | TYP | TYP | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | | (IN) | (IN) |
| 0012 | 0012-0007 | B07 | TUB | 32.00 | 1.500 | TK | BRC | 70.00 | 6.00 | 3.12 | 3.21 | 2.66 | 3.23 | .23332-3 | T | 85719.66 | | | |
| 0012 | 0012-0013 | JB2 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 3.95 | 4.29 | 1.86 | 3.82 | .43919-3 | T | 45538.35 | | | |
| 0012 | 0012-0009 | B17 | TUB | 22.00 | 1.000 | T | BRC | 70.00 | | 3.17 | 5.50 | 2.16 | 3.34 | .12340-4 | L | 1620700. | | | |
| 0012 | 0001-0012 | JB1 | TUB | 54.00 | 2.500 | T | CHD | 70.00 | | 3.18 | 4.23 | 1.51 | 2.87 | .13277-5 | L | 15064.+3 | | | |
| 0012 | 0012-0192 | B17 | TUB | 22.00 | 1.000 | TK | BRC | 70.00 | 6.00 | 3.43 | 4.07 | 2.16 | 4.14 | .67594-5 | L | 2958833. | | | |
| 0012 | 0001-0012 | JB1 | TUB | 54.00 | 2.500 | TK | CHD | 70.00 | | 3.13 | 3.42 | 1.51 | 3.55 | .14594-5 | L | 13704.+3 | | | |

```

-----
0050 0066-0050 B04 TUB 28.00 1.250 TK BRC 116.57 4.90 2.24 1.99 2.91 1.98 .47411-4 T 421842.4
0050 0016-0050 JB5 TUB 54.00 2.500 TK CHD 116.57 2.45 2.28 1.50 2.04 .73102-4 TR 273591.6
0050 0068-0050 B08 TUB 28.00 1.250 TK BRC 116.57 6.00 3.68 3.81 2.40 3.66 .37960-7 R 52687.+4
0050 0050-0022 JB6 TUB 54.00 2.500 TK CHD 116.57 4.21 4.21 1.81 3.77 .86367-7 R 23157.+4
0050 0072-0050 B08 TUB 28.00 1.250 TK BRC 116.57 4.90 3.86 4.01 2.36 3.96 .30326-3 TL 65949.13
0050 0050-0022 JB6 TUB 54.00 2.500 TK CHD 116.57 4.36 4.34 1.87 4.07 .36055-3 TL 55470.17
0050 0056-0050 B09 TUB 30.00 1.375 TK BRC 116.57 6.00 2.26 2.12 2.90 2.22 .33926-6 TL 58952.+3
0050 0016-0050 JB5 TUB 54.00 2.500 TK CHD 116.57 2.70 2.62 1.50 2.45 .15568-5 TL 12847.+3

```

SACS V8i SELECTseries 3 (v5.6)
ID=a6hrm6momGt6eWi+d2ZtdnqX1mlncWV5aJZrepeFdmQ=

ITS

DATE 07-AUG-2020 TIME 21:02:24 FTG PAGE 284

* * * M E M B E R F A T I G U E R E P O R T * * *
(DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | |
|-------|-----------|------|------|----------|-------|-----|-----|--------|------|--------------------------|------|-------|-------|-----------------|-------|----------|----------|------|
| | | | | OD | WT | | | | | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC |
| | ID | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | (IN) | (IN) |
| 0050 | 0050-0106 | B30 | TUB | 24.00 | 0.750 | TK | BRC | 116.57 | 4.90 | 2.86 | 2.94 | 2.08 | 3.70 | .13059-6 | TL | 15315.+4 | | |
| 0050 | 0016-0050 | JB5 | TUB | 54.00 | 2.500 | TK | CHD | 116.57 | | 2.37 | 2.36 | 1.50 | 2.77 | .27121-8 | L | 73744.+5 | | |
| 0050 | 0050-0104 | B32 | TUB | 24.00 | 0.750 | TK | BRC | 116.57 | 6.00 | 3.03 | 3.08 | 2.06 | 3.74 | .72818-6 | BR | 27466.+3 | | |
| 0050 | 0016-0050 | JB5 | TUB | 54.00 | 2.500 | TK | CHD | 116.57 | | 2.52 | 2.51 | 1.50 | 2.81 | .64917-7 | BR | 30808.+4 | | |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|----|-----|--------|------|------|------|------|------|----------|----|----------|
| 0055 | 0072-0055 | B05 | TUB | 28.00 | 1.250 | TK | BRC | 116.57 | 4.90 | 3.86 | 4.08 | 2.36 | 4.00 | .18469-3 | TR | 108291.7 |
| 0055 | 0055-0023 | JB6 | TUB | 54.00 | 2.500 | TK | CHD | 116.57 | | 4.41 | 4.38 | 1.87 | 4.12 | .25241-3 | TR | 79235.86 |
| 0055 | 0055-0120 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 116.57 | 4.11 | 3.67 | 3.80 | 2.40 | 3.67 | .57407-6 | BL | 34839.+3 |
| 0055 | 0055-0023 | JB6 | TUB | 54.00 | 2.500 | TK | CHD | 116.57 | | 4.20 | 4.20 | 1.81 | 3.78 | .11555-5 | L | 17308.+3 |
| 0055 | 0066-0055 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 116.57 | 4.90 | 2.26 | 1.99 | 2.91 | 2.01 | .74614-4 | T | 268047.7 |
| 0055 | 0017-0055 | JB5 | TUB | 54.00 | 2.500 | TK | CHD | 116.57 | | 2.47 | 2.29 | 1.50 | 2.06 | .10850-3 | TL | 184338.7 |
| 0055 | 0060-0055 | B09 | TUB | 30.00 | 1.375 | TK | BRC | 116.57 | 4.11 | 2.22 | 2.09 | 2.90 | 2.24 | .55303-5 | TR | 3616414. |
| 0055 | 0017-0055 | JB5 | TUB | 54.00 | 2.500 | TK | CHD | 116.57 | | 2.62 | 2.55 | 1.50 | 2.48 | .15181-4 | TR | 1317395. |
| 0055 | 0055-0107 | B31 | TUB | 24.00 | 0.750 | TK | BRC | 116.57 | 4.90 | 2.87 | 2.97 | 2.08 | 3.78 | .35580-7 | BR | 56211.+4 |
| 0055 | 0017-0055 | JB5 | TUB | 54.00 | 2.500 | TK | CHD | 116.57 | | 2.38 | 2.37 | 1.50 | 2.83 | .10160-8 | R | 19686.+6 |

SACS V8i SELECTseries 3 (v5.6)

ITS

ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

DATE 07-AUG-2020 TIME 21:02:24 FTG PAGE 285

* * * M E M B E R F A T I G U E R E P O R T * * *
(DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | |
|-------|-----------|------|------|----------|-------|-----|-----|--------|------|--------------------------|------|-------|-------|-----------------|-------|----------|----------|------|
| | | | | OD | WT | | | | | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | (IN) | (IN) |
| 0055 | 0055-0101 | B32 | TUB | 24.00 | 0.750 | TK | BRC | 116.57 | 4.11 | 2.93 | 2.99 | 2.06 | 3.80 | .71629-5 | BL | 2792180. | | |
| 0055 | 0017-0055 | JB5 | TUB | 54.00 | 2.500 | TK | CHD | 116.57 | | 2.40 | 2.39 | 1.50 | 2.84 | .89840-6 | BL | 22262.+3 | | |

```

-----
0049 0049-0120 B08 TUB 28.00 1.250 TK BRC 109.11 4.14 3.63 3.92 2.35 4.19 .13954-4 TR 1433295.
0049 0049-0224 JA6 TUB 54.00 2.500 TK CHD 109.11 4.06 4.06 1.89 4.32 .13139-4 TR 1522173.
0049 0056-0049 B08 TUB 28.00 1.250 TK BRC 109.11 4.14 1.81 1.78 3.03 2.05 .0000000 T INFINITE
0049 0015-0049 JA5 TUB 54.00 2.500 TK CHD 109.11 2.01 1.98 1.50 2.11 .0000000 T INFINITE
0049 0060-0049 B08 TUB 28.00 1.250 TK BRC 109.11 4.14 1.81 1.78 3.03 2.05 .0000000 T INFINITE
0049 0015-0049 JA5 TUB 54.00 2.500 TK CHD 109.11 2.01 1.98 1.50 2.11 .0000000 T INFINITE
0049 0049-0068 B10 TUB 28.00 1.250 TK BRC 109.11 4.14 3.63 3.93 2.35 4.19 .25682-5 L 7787658.
0049 0049-0224 JA6 TUB 54.00 2.500 TK CHD 109.11 4.06 4.06 1.89 4.31 .29557-5 L 6766616.
0049 0101-0049 B33 TUB 24.00 0.750 TK BRC 109.11 4.14 2.70 2.78 2.10 4.02 .39736-4 R 503315.7
0049 0015-0049 JA5 TUB 54.00 2.500 TK CHD 109.11 2.21 2.21 1.50 3.02 .42983-5 R 4653000.
0049 0104-0049 B33 TUB 24.00 0.750 TK BRC 109.11 4.14 2.70 2.78 2.10 4.03 .52294-5 L 3824520.
0049 0015-0049 JA5 TUB 54.00 2.500 TK CHD 109.11 2.21 2.21 1.50 3.02 .28809-6 L 69422.+3

```

SACS V8i SELECTseries 3 (v5.6) ITS
ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

DATE 07-AUG-2020 TIME 21:02:24 FTG PAGE 286

* * * MEMBER FATIGUE REPORT * * *
(DAMAGE ORDER)

ORIGINAL

CHORD

REQUIRED

| JOINT | MEMBER | GRUP | TYPE | OD | WT | JNT | MEM | LEN. | GAP | * STRESS | CONC. | FACTORS | FATIGUE RESULTS | | | OD | WT | | |
|-------|-----------|------|------|-------|-------|-----|-----|--------|-------|----------|-------|---------|-----------------|----------|-----|-----|----------|------|------|
| | ID | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC | LIFE | (IN) | (IN) |
| 0072 | 0023-0072 | B08 | TUB | 28.00 | 1.250 | Y | BRC | 103.48 | | 3.34 | 2.55 | 2.35 | 1.69 | .98809-5 | T | | 2024104. | | |
| 0072 | 0072-0055 | B05 | TUB | 28.00 | 1.375 | Y | CHD | 103.48 | | 3.02 | 3.34 | 2.72 | 2.31 | .14287-4 | R | | 1399864. | | |
| 0072 | 0072-0050 | B08 | TUB | 28.00 | 1.250 | Y | BRC | 103.48 | | 3.20 | 2.51 | 2.36 | 1.65 | .12038-4 | B | | 1661386. | | |
| 0072 | 0022-0072 | B06 | TUB | 28.00 | 1.375 | Y | CHD | 103.48 | | 2.89 | 3.29 | 2.70 | 2.21 | .15529-4 | BR | | 1287954. | | |
| ----- | | | | | | | | | | | | | | | | | | | |
| 0006 | 0194-0006 | B17 | TUB | 22.00 | 1.000 | T | BRC | 70.00 | | 3.17 | 5.50 | 2.16 | 3.34 | .13565-5 | L | | 14744.+3 | | |
| 0006 | 0000-0006 | JA1 | TUB | 54.00 | 2.500 | T | CHD | 70.00 | | 3.18 | 4.23 | 1.51 | 2.87 | .13320-6 | L | | 15015.+4 | | |
| 0006 | 0195-0006 | B17 | TUB | 22.00 | 1.000 | T | BRC | 70.00 | | 3.17 | 5.50 | 2.16 | 3.34 | .15354-4 | L | | 1302607. | | |
| 0006 | 0000-0006 | JA1 | TUB | 54.00 | 2.500 | T | CHD | 70.00 | | 3.18 | 4.23 | 1.51 | 2.87 | .26218-5 | BL | | 7628282. | | |
| ----- | | | | | | | | | | | | | | | | | | | |
| 0024 | 0024-0033 | B12 | TUB | 26.00 | 1.000 | K | BRC | 25.08 | 20.89 | 2.64 | 3.39 | 2.34 | 2.67 | .0000000 | T | | INFINITE | | |
| 0024 | 0024-0042 | JA7 | TUB | 54.00 | 2.500 | K | CHD | 25.08 | | 2.04 | 3.09 | 1.50 | 2.39 | .0000000 | T | | INFINITE | | |
| 0024 | 0024-0052 | B12 | TUB | 26.00 | 1.000 | K | BRC | 25.08 | 20.89 | 2.64 | 3.40 | 2.34 | 2.67 | .0000000 | T | | INFINITE | | |
| 0024 | 0024-0042 | JA7 | TUB | 54.00 | 2.500 | K | CHD | 25.08 | | 2.04 | 3.09 | 1.50 | 2.38 | .0000000 | T | | INFINITE | | |
| 0024 | 0045-0024 | B38 | TUB | 26.00 | 1.000 | K | BRC | 25.08 | 20.89 | 2.71 | 5.02 | 2.20 | 3.69 | .23175-6 | L | | 86300.+3 | | |
| 0024 | 0024-0042 | JA7 | TUB | 54.00 | 2.500 | K | CHD | 25.08 | | 2.09 | 4.26 | 1.59 | 3.30 | .24148-7 | L | | 82822.+4 | | |

* * * M E M B E R F A T I G U E R E P O R T * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|-------|--------------------------|------|------|------|-----------------|------|----------|----------|-------|-------|
| | | | | OD | WT | | | | | (IN) | (IN) | TYP | TYP | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | | | | | | | | | | (IN) | (IN) |
| 0024 | 0051-0024 | B38 | TUB | 26.00 | 1.000 | K | BRC | 25.08 | 20.89 | 2.70 | 5.03 | 2.20 | 3.69 | .30719-5 | L | 6510661. | | | |
| 0024 | 0024-0042 | JA7 | TUB | 54.00 | 2.500 | K | CHD | 25.08 | | 2.08 | 4.26 | 1.59 | 3.30 | .71411-6 | L | 28007.+3 | | | |
| ----- | | | | | | | | | | | | | | | | | | | |
| 0060 | 0017-0060 | B08 | TUB | 28.00 | 1.250 | T | BRC | 67.26 | | 3.03 | 4.72 | 2.42 | 3.05 | .29516-8 | R | 67760.+5 | | | |
| 0060 | 0015-0060 | B09 | TUB | 30.00 | 1.375 | T | CHD | 67.26 | | 2.84 | 7.55 | 2.99 | 5.34 | .18401-5 | R | 10869.+3 | | | |
| 0060 | 0060-0049 | B08 | TUB | 28.00 | 1.250 | T | BRC | 67.26 | | 2.83 | 4.72 | 2.42 | 2.99 | .59650-9 | R | 33529.+6 | | | |
| 0060 | 0060-0055 | B09 | TUB | 30.00 | 1.375 | T | CHD | 67.26 | | 2.53 | 7.62 | 2.99 | 5.23 | .50798-6 | R | 39371.+3 | | | |
| ----- | | | | | | | | | | | | | | | | | | | |
| 0026 | 0026-0038 | B12 | TUB | 26.00 | 1.000 | K | BRC | 26.65 | 20.61 | 2.68 | 3.22 | 2.34 | 2.82 | .0000000 | T | INFINITE | | | |
| 0026 | 0047-0026 | JB7 | TUB | 54.00 | 2.500 | K | CHD | 26.65 | | 2.25 | 2.98 | 1.50 | 2.52 | .0000000 | T | INFINITE | | | |
| 0026 | 0026-0052 | B12 | TUB | 26.00 | 1.000 | K | BRC | 26.65 | 20.89 | 2.69 | 2.90 | 2.34 | 2.95 | .0000000 | T | INFINITE | | | |
| 0026 | 0047-0026 | JB7 | TUB | 54.00 | 2.500 | K | CHD | 26.65 | | 2.46 | 2.76 | 1.50 | 2.63 | .0000000 | T | INFINITE | | | |
| 0026 | 0026-0133 | B36 | TUB | 26.00 | 1.000 | K | BRC | 26.65 | 20.61 | 2.80 | 4.87 | 2.20 | 3.71 | .65119-7 | L | 30713.+4 | | | |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|-------|------|------|------|------|----------|---|----------|
| 0026 | 0047-0026 | JB7 | TUB | 54.00 | 2.500 | K | CHD | 26.65 | | 2.25 | 4.14 | 1.59 | 3.32 | .87028-8 | L | 22981.+5 |
| 0026 | 0026-0051 | B37 | TUB | 26.00 | 1.000 | K | BRC | 26.65 | 20.89 | 2.94 | 4.57 | 2.20 | 3.74 | .11990-5 | R | 16681.+3 |
| 0026 | 0047-0026 | JB7 | TUB | 54.00 | 2.500 | K | CHD | 26.65 | | 2.46 | 3.96 | 1.59 | 3.35 | .24119-6 | R | 82923.+3 |

SACS V8i SELECTseries 3 (v5.6)
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

ITS

DATE 07-AUG-2020 TIME 21:02:24 FTG PAGE 288

* * * MEMBER FATIGUE REPORT * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | | | | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|-------|--------------------------|------|------|------|-----------------|------|----------|----------|-------|-------|-------|--------|
| | | | | OD | WT | | | | | (IN) | (IN) | TYP | TYP | LEN. | (FT) | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | | | | (IN) | (IN) |
| 0056 | 0016-0056 | B08 | TUB | 28.00 | 1.250 | T | BRC | 67.12 | | 2.94 | 4.72 | 2.42 | 3.03 | .64759-9 | L | 30884.+6 | | | | | |
| 0056 | 0015-0056 | B09 | TUB | 30.00 | 1.375 | T | CHD | 67.12 | | 2.70 | 7.58 | 2.99 | 5.29 | .76814-6 | L | 26037.+3 | | | | | |
| 0056 | 0056-0049 | B08 | TUB | 28.00 | 1.250 | T | BRC | 67.12 | | 2.78 | 4.72 | 2.42 | 2.98 | .19638-9 | L | 10184.+7 | | | | | |
| 0056 | 0056-0050 | B09 | TUB | 30.00 | 1.375 | T | CHD | 67.12 | | 2.47 | 7.64 | 2.99 | 5.21 | .35703-6 | L | 56017.+3 | | | | | |
| ----- | | | | | | | | | | | | | | | | | | | | | |
| 0025 | 0025-0033 | B12 | TUB | 26.00 | 1.000 | K | BRC | 26.65 | 20.89 | 2.69 | 2.91 | 2.34 | 2.95 | .0000000 | T | INFINITE | | | | | |
| 0025 | 0046-0025 | JB7 | TUB | 54.00 | 2.500 | K | CHD | 26.65 | | 2.46 | 2.76 | 1.50 | 2.63 | .0000000 | T | INFINITE | | | | | |
| 0025 | 0025-0038 | B12 | TUB | 26.00 | 1.000 | K | BRC | 26.65 | 20.61 | 2.68 | 3.24 | 2.34 | 2.81 | .0000000 | T | INFINITE | | | | | |
| 0025 | 0046-0025 | JB7 | TUB | 54.00 | 2.500 | K | CHD | 26.65 | | 2.23 | 2.99 | 1.50 | 2.52 | .0000000 | T | INFINITE | | | | | |
| 0025 | 0025-0132 | B35 | TUB | 26.00 | 1.000 | K | BRC | 26.65 | 20.61 | 2.80 | 4.89 | 2.20 | 3.71 | .77406-7 | R | 25838.+4 | | | | | |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|-------|------|------|------|------|----------|---|----------|
| 0025 | 0046-0025 | JB7 | TUB | 54.00 | 2.500 | K | CHD | 26.65 | | 2.24 | 4.16 | 1.59 | 3.32 | .10176-7 | R | 19653.+5 |
| 0025 | 0025-0045 | B37 | TUB | 26.00 | 1.000 | K | BRC | 26.65 | 20.89 | 2.93 | 4.59 | 2.20 | 3.74 | .21803-6 | L | 91732.+3 |
| 0025 | 0046-0025 | JB7 | TUB | 54.00 | 2.500 | K | CHD | 26.65 | | 2.45 | 3.97 | 1.59 | 3.34 | .31715-7 | L | 63062.+4 |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|--|------|------|------|------|----------|----|----------|
| 0010 | 0010-0100 | B18 | TUB | 22.00 | 0.750 | T | BRC | 70.00 | | 3.04 | 4.92 | 2.04 | 2.93 | .76494-7 | BR | 26146.+4 |
| 0010 | 0009-0010 | JB2 | TUB | 54.00 | 2.500 | T | CHD | 70.00 | | 2.39 | 3.08 | 1.50 | 2.15 | .58014-9 | BR | 34475.+6 |

SACS V8i SELECTseries 3 (v5.6)
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

ITS

DATE 07-AUG-2020 TIME 21:02:24 FTG PAGE 289

* * * M E M B E R F A T I G U E R E P O R T * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|------|--------------------------|------|-------|-------|-----------------|-------|----------|----------|------|
| | | | | OD | WT | | | | | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | (IN) | (IN) |
| 0010 | 0098-0010 | B20 | TUB | 22.00 | 0.750 | T | BRC | 70.00 | | 3.04 | 4.92 | 2.04 | 2.93 | .3627-10 | BL | 55147.+7 | | |
| 0010 | 0009-0010 | JB2 | TUB | 54.00 | 2.500 | T | CHD | 70.00 | | 2.39 | 3.08 | 1.50 | 2.15 | .0000000 | T | INFINITE | | |

| | | | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|--|------|------|------|------|----------|----|----------|--|--|
| 0008 | 0214-0008 | B23 | TUB | 24.00 | 0.750 | T | BRC | 70.00 | | 3.03 | 4.97 | 2.06 | 3.09 | .98426-9 | TL | 20320.+6 | | |
| 0008 | 0007-0008 | JA3 | TUB | 54.00 | 2.500 | T | CHD | 70.00 | | 2.43 | 3.14 | 1.50 | 2.32 | .0000000 | T | INFINITE | | |
| 0008 | 0215-0008 | B23 | TUB | 24.00 | 0.750 | T | BRC | 70.00 | | 3.03 | 4.97 | 2.06 | 3.09 | .65280-7 | TR | 30637.+4 | | |
| 0008 | 0007-0008 | JA3 | TUB | 54.00 | 2.500 | T | CHD | 70.00 | | 2.43 | 3.14 | 1.50 | 2.32 | .52231-9 | TR | 38291.+6 | | |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|--|------|------|------|------|----------|----|----------|
| 0120 | 0055-0120 | B08 | TUB | 28.00 | 1.250 | Y | BRC | 97.46 | | 2.94 | 2.79 | 2.44 | 1.65 | .10109-8 | T | 19785.+6 |
| 0120 | 0120-0023 | B08 | TUB | 28.00 | 1.250 | Y | CHD | 97.46 | | 2.93 | 4.08 | 3.05 | 2.62 | .19831-7 | TL | 10085.+5 |
| 0120 | 0120-0018 | B08 | TUB | 28.00 | 1.250 | Y | BRC | 97.46 | | 2.95 | 2.82 | 2.43 | 1.65 | .55553-9 | T | 36002.+6 |
| 0120 | 0049-0120 | B08 | TUB | 28.00 | 1.250 | Y | CHD | 97.46 | | 2.92 | 4.13 | 3.07 | 2.66 | .18066-7 | L | 11070.+5 |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|------|------|------|------|------|----------|---|----------|
| 0081 | 0081-0088 | F06 | TUB | 18.00 | 0.750 | K | BRC | 26.07 | 2.28 | 3.19 | 3.55 | 2.68 | 5.24 | .0000000 | T | INFINITE |
| 0081 | 0005-0081 | B26 | TUB | 24.00 | 1.000 | K | CHD | 26.07 | | 4.81 | 5.29 | 2.54 | 7.67 | .56714-9 | L | 35265.+6 |
| 0081 | 0083-0081 | F06 | TUB | 18.00 | 0.750 | K | BRC | 26.07 | 2.28 | 3.40 | 4.14 | 2.65 | 5.17 | .0000000 | T | INFINITE |

SACS V8i SELECTseries 3 (v5.6) ITS
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

DATE 07-AUG-2020 TIME 21:02:24 FTG PAGE 290

* * * MEMBER FATIGUE REPORT * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|------|--------------------------|------|-------|-------|-----------------|-------|----------|----------|------|
| | | | | OD | WT | | | | | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | (IN) | (IN) |
| 0081 | 0081-0085 | B29 | TUB | 24.00 | 1.000 | K | CHD | 26.07 | | 5.34 | 6.17 | 2.60 | 7.55 | .0000000 | T | INFINITE | | |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|------|------|------|------|------|----------|---|----------|
| 0082 | 0082-0089 | F06 | TUB | 18.00 | 0.750 | K | BRC | 25.50 | 2.28 | 3.24 | 3.71 | 2.68 | 5.13 | .0000000 | T | INFINITE |
| 0082 | 0004-0082 | B26 | TUB | 24.00 | 1.000 | K | CHD | 25.50 | | 4.95 | 5.58 | 2.54 | 7.50 | .16406-9 | R | 12191.+7 |

0082 0084-0082 F06 TUB 18.00 0.750 K BRC 25.50 2.28 3.45 4.37 2.65 5.03 .0000000 T INFINITE
 0082 0082-0086 B29 TUB 24.00 1.000 K CHD 25.50 5.52 6.55 2.60 7.36 .0000000 T INFINITE

 0100 0209-0100 F05 TUB 18.00 0.750 K BRC 36.00 6.66 3.95 3.79 2.52 4.65 .0000000 T INFINITE
 0100 0010-0100 B18 TUB 22.00 1.000 K CHD 36.00 6.63 5.84 2.48 7.00 .0000000 T INFINITE
 0100 0210-0100 F05 TUB 18.00 0.750 K BRC 36.00 6.66 4.03 3.86 2.52 4.62 .0000000 T INFINITE
 0100 0013-0100 B19 TUB 22.00 1.000 K CHD 36.00 6.82 5.96 2.48 6.95 .4248-10 R 47084.+7

 0068 0018-0068 B08 TUB 28.00 1.250 Y BRC 97.46 2.99 2.58 2.34 1.61 .3373-10 T 59295.+7
 0068 0049-0068 B10 TUB 28.00 1.375 Y CHD 97.46 2.61 3.41 2.74 2.19 .4154-10 TR 48145.+7
 0068 0068-0050 B08 TUB 28.00 1.250 Y BRC 97.46 2.98 2.55 2.34 1.61 .0000000 T INFINITE
 0068 0068-0022 B11 TUB 28.00 1.375 Y CHD 97.46 2.62 3.37 2.73 2.16 .3542-10 R 56464.+7

SACS V8i SELECTseries 3 (v5.6) ITS
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

DATE 07-AUG-2020 TIME 21:02:24 FTG PAGE 291

* * * MEMBER FATIGUE REPORT * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | |
|-------|--------|------|------|----------|------|-----|-----|-------|------|--------------------------|------|-------|-------|-----------------|-------|--------|----------|------|
| | | | | OD | WT | | | | | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | (IN) | (IN) |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|------|------|------|------|------|----------|---|----------|
| 0098 | 0098-0209 | F05 | TUB | 18.00 | 0.750 | K | BRC | 26.07 | 2.12 | 3.46 | 3.49 | 2.56 | 4.40 | .0000000 | T | INFINITE |
| 0098 | 0098-0010 | B20 | TUB | 22.00 | 1.000 | K | CHD | 26.07 | | 5.52 | 5.39 | 2.39 | 6.62 | .0000000 | T | INFINITE |
| 0098 | 0204-0098 | F05 | TUB | 18.00 | 0.750 | K | BRC | 26.07 | 2.12 | 3.46 | 3.60 | 2.53 | 4.55 | .0000000 | T | INFINITE |
| 0098 | 0207-0098 | B17 | TUB | 22.00 | 1.000 | K | CHD | 26.07 | | 5.56 | 5.43 | 2.43 | 6.85 | .0000000 | T | INFINITE |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|------|------|------|------|------|----------|---|----------|
| 0099 | 0099-0210 | F05 | TUB | 18.00 | 0.750 | K | BRC | 25.50 | 2.12 | 3.33 | 3.38 | 2.56 | 4.49 | .0000000 | T | INFINITE |
| 0099 | 0099-0013 | B20 | TUB | 22.00 | 1.000 | K | CHD | 25.50 | | 5.24 | 5.16 | 2.39 | 6.76 | .0000000 | T | INFINITE |
| 0099 | 0205-0099 | F05 | TUB | 18.00 | 0.750 | K | BRC | 25.50 | 2.12 | 3.33 | 3.47 | 2.53 | 4.64 | .0000000 | T | INFINITE |
| 0099 | 0208-0099 | B17 | TUB | 22.00 | 1.000 | K | CHD | 25.50 | | 5.26 | 5.17 | 2.43 | 6.99 | .0000000 | T | INFINITE |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|------|------|------|------|------|----------|---|----------|
| 0079 | 0088-0079 | F06 | TUB | 18.00 | 0.750 | K | BRC | 36.00 | 6.65 | 4.02 | 4.66 | 2.63 | 5.23 | .0000000 | T | INFINITE |
| 0079 | 0005-0079 | B25 | TUB | 24.00 | 1.000 | K | CHD | 36.00 | | 6.75 | 7.01 | 2.66 | 7.66 | .0000000 | T | INFINITE |
| 0079 | 0089-0079 | F06 | TUB | 18.00 | 0.750 | K | BRC | 36.00 | 6.65 | 3.96 | 4.54 | 2.63 | 5.28 | .0000000 | T | INFINITE |
| 0079 | 0079-0004 | B24 | TUB | 24.00 | 1.000 | K | CHD | 36.00 | | 6.58 | 6.82 | 2.66 | 7.73 | .0000000 | T | INFINITE |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|------|------|------|------|------|----------|---|----------|
| 0096 | 0096-0108 | F08 | TUB | 22.00 | 0.750 | K | BRC | 14.00 | 6.38 | 2.78 | 3.10 | 2.47 | 4.15 | .0000000 | T | INFINITE |
|------|-----------|-----|-----|-------|-------|---|-----|-------|------|------|------|------|------|----------|---|----------|

SACS V8i SELECTseries 3 (v5.6)
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

ITS

DATE 07-AUG-2020 TIME 21:02:24 FTG PAGE 292

* * * MEMBER FATIGUE REPORT * * *

(DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|------|--------------------------|------|-------|-------|-----------------|-------|----------|----------|------|
| | | | | OD | WT | | | | | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC |
| | ID | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | (IN) | (IN) |
| 0096 | 0107-0096 | B34 | TUB | 24.00 | 1.000 | K | CHD | 14.00 | | 4.48 | 4.47 | 2.40 | 6.54 | .0000000 | T | INFINITE | | |
| 0096 | 0096-0109 | F08 | TUB | 22.00 | 0.750 | K | BRC | 14.00 | 6.38 | 2.78 | 3.09 | 2.47 | 4.16 | .0000000 | T | INFINITE | | |
| 0096 | 0106-0096 | B34 | TUB | 24.00 | 1.000 | K | CHD | 14.00 | | 4.47 | 4.46 | 2.40 | 6.55 | .0000000 | T | INFINITE | | |
| ----- | | | | | | | | | | | | | | | | | | |
| 0101 | 0101-0104 | F07 | TUB | 16.00 | 0.500 | K | BRC | 64.96 | 1.73 | 3.83 | 3.96 | 2.47 | 4.87 | .0000000 | T | INFINITE | | |
| 0101 | 0101-0049 | B33 | TUB | 24.00 | 1.000 | K | CHD | 64.96 | | 5.42 | 4.97 | 1.89 | 5.48 | .0000000 | T | INFINITE | | |
| 0101 | 0111-0101 | F11 | TUB | 22.00 | 0.750 | K | BRC | 64.96 | 1.73 | 5.17 | 3.35 | 2.47 | 4.16 | .0000000 | T | INFINITE | | |
| 0101 | 0055-0101 | B32 | TUB | 24.00 | 1.000 | K | CHD | 64.96 | | 6.98 | 5.95 | 2.40 | 6.54 | .0000000 | T | INFINITE | | |
| ----- | | | | | | | | | | | | | | | | | | |
| 0104 | 0101-0104 | F07 | TUB | 16.00 | 0.500 | K | BRC | 64.96 | 1.73 | 3.89 | 4.04 | 2.47 | 4.82 | .0000000 | T | INFINITE | | |
| 0104 | 0104-0049 | B33 | TUB | 24.00 | 1.000 | K | CHD | 64.96 | | 5.56 | 5.08 | 1.89 | 5.42 | .0000000 | T | INFINITE | | |
| 0104 | 0110-0104 | F10 | TUB | 22.00 | 0.750 | K | BRC | 64.96 | 1.73 | 5.25 | 3.37 | 2.47 | 4.14 | .0000000 | T | INFINITE | | |
| 0104 | 0050-0104 | B32 | TUB | 24.00 | 1.000 | K | CHD | 64.96 | | 7.07 | 6.01 | 2.40 | 6.52 | .0000000 | T | INFINITE | | |
| ----- | | | | | | | | | | | | | | | | | | |
| 0047 | 0047-0044 | B12 | TUB | 26.00 | 1.000 | Y | BRC | 33.00 | | 2.73 | 2.95 | 2.43 | 2.11 | .0000000 | T | INFINITE | | |

0047 0226-0047 JB7 TUB 54.00 2.500 Y CHD 33.00 2.09 2.69 1.50 1.89 .0000000 T INFINITE

SACS V8i SELECTseries 3 (v5.6) ITS
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

DATE 07-AUG-2020 TIME 21:02:24 FTG PAGE 293

* * * M E M B E R F A T I G U E R E P O R T * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | REQUIRED | | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|------|--------------------------|------|------|------|-----------------|-------|----------|-------|--------|
| | | | | OD | WT | | | | | TYP | TYP | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE |
| | ID | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | (IN) | (IN) |
| 0047 | 0047-0053 | B12 | TUB | 26.00 | 1.000 | Y | BRC | 33.00 | | 2.73 | 2.95 | 2.43 | 2.11 | .0000000 | T | INFINITE | | |
| 0047 | 0226-0047 | JB7 | TUB | 54.00 | 2.500 | Y | CHD | 33.00 | | 2.09 | 2.69 | 1.50 | 1.89 | .0000000 | T | INFINITE | | |
| ----- | | | | | | | | | | | | | | | | | | |
| 0044 | 0047-0044 | B12 | TUB | 26.00 | 1.000 | Y | BRC | 13.17 | | 2.73 | 2.30 | 2.53 | 2.19 | .0000000 | T | INFINITE | | |
| 0044 | 0029-0044 | B45 | TUB | 28.00 | 1.375 | Y | CHD | 13.17 | | 3.97 | 2.79 | 1.89 | 3.38 | .0000000 | T | INFINITE | | |
| ----- | | | | | | | | | | | | | | | | | | |
| 0029 | 0029-0044 | B45 | TUB | 28.00 | 1.000 | T | BRC | 9.00 | | 2.40 | 3.79 | 2.21 | 3.35 | .0000000 | T | INFINITE | | |
| 0029 | 0029-0226 | JB7 | TUB | 54.00 | 2.500 | T | CHD | 9.00 | | 1.50 | 3.45 | 1.61 | 3.06 | .0000000 | T | INFINITE | | |
| 0029 | 0029-0053 | B45 | TUB | 28.00 | 1.000 | T | BRC | 9.00 | | 2.40 | 3.79 | 2.21 | 3.35 | .0000000 | T | INFINITE | | |
| 0029 | 0029-0226 | JB7 | TUB | 54.00 | 2.500 | T | CHD | 9.00 | | 1.50 | 3.45 | 1.61 | 3.06 | .0000000 | T | INFINITE | | |
| ----- | | | | | | | | | | | | | | | | | | |
| 0053 | 0047-0053 | B12 | TUB | 26.00 | 1.000 | Y | BRC | 13.38 | | 2.74 | 2.30 | 2.53 | 2.19 | .0000000 | T | INFINITE | | |

0053 0029-0053 B45 TUB 28.00 1.375 Y CHD 13.38 4.00 2.80 1.89 3.38 .0000000 T INFINITE

 0043 0046-0043 B12 TUB 26.00 1.000 Y BRC 13.17 2.73 2.30 2.53 2.19 .0000000 T INFINITE

0043 0028-0043 B45 TUB 28.00 1.375 Y CHD 13.17 3.97 2.79 1.89 3.38 .0000000 T INFINITE

SACS V8i SELECTseries 3 (v5.6) ITS
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

DATE 07-AUG-2020 TIME 21:02:24 FTG PAGE 294

* * * MEMBER FATIGUE REPORT * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|-----|--------------------------|------|------|------|-----------------|------|----------|----------|-------|
| | | | | OD | WT | | | | | (IN) | (IN) | TYP | TYP | LEN. | (IN) | AX-CR | AX-SD | IN-PL |
| 0046 | 0046-0040 | B12 | TUB | 26.00 | 1.000 | Y | BRC | 33.00 | | 2.73 | 2.95 | 2.43 | 2.11 | .0000000 | T | INFINITE | | |
| 0046 | 0227-0046 | JB7 | TUB | 54.00 | 2.500 | Y | CHD | 33.00 | | 2.09 | 2.69 | 1.50 | 1.89 | .0000000 | T | INFINITE | | |
| 0046 | 0046-0043 | B12 | TUB | 26.00 | 1.000 | Y | BRC | 33.00 | | 2.73 | 2.95 | 2.43 | 2.11 | .0000000 | T | INFINITE | | |
| 0046 | 0227-0046 | JB7 | TUB | 54.00 | 2.500 | Y | CHD | 33.00 | | 2.09 | 2.69 | 1.50 | 1.89 | .0000000 | T | INFINITE | | |

 0028 0028-0040 B45 TUB 28.00 1.000 T BRC 9.00 2.40 3.79 2.21 3.35 .0000000 T INFINITE

0028 0028-0227 JB7 TUB 54.00 2.500 T CHD 9.00 1.50 3.45 1.61 3.06 .0000000 T INFINITE

0028 0028-0043 B45 TUB 28.00 1.000 T BRC 9.00 2.40 3.79 2.21 3.35 .0000000 T INFINITE

0028 0028-0227 JB7 TUB 54.00 2.500 T CHD 9.00 1.50 3.45 1.61 3.06 .0000000 T INFINITE


```

-----
0040 0046-0040 B12 TUB 26.00 1.000 Y BRC 13.38      2.74 2.30 2.53 2.19 .0000000 T INFINITE
0040 0028-0040 B45 TUB 28.00 1.375 Y CHD 13.38      4.00 2.80 1.89 3.38 .0000000 T INFINITE
-----

```

```

0038 0025-0038 B12 TUB 26.00 1.000 TK BRC 20.71 32.70 2.04 1.83 2.70 1.92 .0000000 T INFINITE
0038 0186-0038 B48 TUB 28.00 1.375 TK CHD 20.71      2.95 2.60 1.66 2.95 .0000000 T INFINITE
0038 0026-0038 B12 TUB 26.00 1.000 TK BRC 20.71 32.70 2.03 1.83 2.70 1.92 .0000000 T INFINITE

```

SACS V8i SELECTseries 3 (v5.6) ITS
ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

DATE 07-AUG-2020 TIME 21:02:24 FTG PAGE 295

* * * M E M B E R F A T I G U E R E P O R T * * *
(DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|-------|--------------------------|------|------|------|-----------------|------|----------|----------|-------|-------|
| | | | | OD | WT | | | | | (IN) | (IN) | TYP | TYP | (FT) | (IN) | AX-CR | AX-SD | IN-PL | OU-PL |
| | ID | ID | | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | | (IN) | (IN) |
| 0038 | 0030-0038 | BH0 | TUB | 28.00 | 1.375 | TK | CHD | 20.71 | | 2.93 | 2.61 | 1.66 | 2.96 | .0000000 | T | INFINITE | | | |
| 0038 | 0038-0039 | BV1 | TUB | 22.00 | 0.750 | TK | BRC | 20.71 | 32.70 | 3.42 | 3.45 | 2.24 | 4.29 | .0000000 | T | INFINITE | | | |
| 0038 | 0186-0038 | B48 | TUB | 28.00 | 1.375 | TK | CHD | 20.71 | | 4.53 | 4.55 | 2.00 | 5.33 | .0000000 | T | INFINITE | | | |
| 0038 | 0038-0155 | F17 | TUB | 26.00 | 1.000 | K | BRC | 20.71 | 14.42 | 2.72 | 2.64 | 2.38 | 3.43 | .0000000 | T | INFINITE | | | |
| 0038 | 0030-0038 | BH0 | TUB | 28.00 | 1.375 | K | CHD | 20.71 | | 4.15 | 3.79 | 2.17 | 5.29 | .0000000 | T | INFINITE | | | |
| 0038 | 0038-0180 | F17 | TUB | 26.00 | 1.000 | K | BRC | 20.71 | 14.42 | 2.70 | 2.63 | 2.38 | 3.44 | .0000000 | T | INFINITE | | | |

0038 0186-0038 B48 TUB 28.00 1.375 K CHD 20.71 4.12 3.79 2.17 5.31 .0000000 T INFINITE

 0039 0038-0039 BV1 TUB 22.00 0.750 T BRC 14.00 2.76 4.42 2.25 4.15 .0000000 T INFINITE

0039 0133-0039 B39 TUB 26.00 1.250 T CHD 14.00 3.49 4.67 2.14 5.59 .0000000 T INFINITE

0039 0134-0039 F13 TUB 24.00 0.750 K BRC 14.00 6.45 2.56 2.62 2.29 3.20 .0000000 T INFINITE

0039 0133-0039 B39 TUB 26.00 1.250 K CHD 14.00 3.37 3.12 1.87 4.44 .0000000 T INFINITE

0039 0135-0039 F13 TUB 24.00 0.750 K BRC 14.00 6.45 2.56 2.62 2.29 3.20 .0000000 T INFINITE

0039 0132-0039 B39 TUB 26.00 1.250 K CHD 14.00 3.37 3.13 1.87 4.45 .0000000 T INFINITE

 0217 0051-0217 F20 TUB 22.00 0.750 Y BRC 28.49 3.86 4.05 2.64 4.00 .0000000 T INFINITE

SACS V8i SELECTseries 3 (v5.6) ITS
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

DATE 07-AUG-2020 TIME 21:02:24 FTG PAGE 296

* * * M E M B E R F A T I G U E R E P O R T * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|------|--------------------------|------|------|------|-----------------|-------|----------|----------|--------|------|
| | | | | OD | WT | | | | | TYP | TYP | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC |
| | ID | ID | | (IN) | (IN) | | | (FT) | (IN) | | | | | | | | | (IN) | (IN) |
| 0217 | 0158-0217 | F21 | TUB | 26.00 | 1.000 | Y | CHD | 28.49 | | 6.71 | 6.83 | 2.44 | 6.14 | .0000000 | T | INFINITE | | | |

 0051 0051-0052 BV1 TUB 22.00 0.750 T BRC 100.83 8.46 5.13 2.25 4.17 .0000000 T INFINITE

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|--------|-------|------|------|------|----------|----------|----------|----------|
| 0051 | 0026-0051 | B37 | TUB | 26.00 | 1.250 | T | CHD | 100.83 | 10.00 | 4.69 | 2.15 | 5.61 | .0000000 | T | INFINITE | |
| 0051 | 0051-0045 | F12 | TUB | 24.00 | 1.000 | K | BRC | 100.83 | 3.09 | 5.89 | 3.14 | 2.44 | 3.67 | .0000000 | T | INFINITE |
| 0051 | 0051-0024 | B38 | TUB | 26.00 | 1.250 | K | CHD | 100.83 | 6.59 | 6.32 | 2.39 | 5.96 | .0000000 | T | INFINITE | |
| 0051 | 0051-0137 | F16 | TUB | 24.00 | 0.750 | K | BRC | 100.83 | 3.09 | 6.29 | 3.03 | 2.28 | 3.44 | .0000000 | T | INFINITE |
| 0051 | 0026-0051 | B37 | TUB | 26.00 | 1.250 | K | CHD | 100.83 | 7.17 | 5.31 | 1.88 | 4.77 | .0000000 | T | INFINITE | |
| 0051 | 0051-0217 | F20 | TUB | 22.00 | 0.750 | Y | BRC | 100.83 | 8.46 | 4.83 | 2.28 | 3.87 | .0000000 | T | INFINITE | |
| 0051 | 0026-0051 | B37 | TUB | 26.00 | 1.250 | Y | CHD | 100.83 | 10.00 | 6.40 | 2.08 | 5.21 | .0000000 | T | INFINITE | |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|--------|-------|------|------|------|----------|----------|----------|----------|
| 0045 | 0033-0045 | BV1 | TUB | 22.00 | 0.750 | T | BRC | 100.83 | 8.46 | 5.13 | 2.25 | 4.17 | .0000000 | T | INFINITE | |
| 0045 | 0025-0045 | B37 | TUB | 26.00 | 1.250 | T | CHD | 100.83 | 10.00 | 4.69 | 2.15 | 5.61 | .0000000 | T | INFINITE | |
| 0045 | 0051-0045 | F12 | TUB | 24.00 | 1.000 | K | BRC | 100.83 | 0.49 | 5.91 | 3.08 | 2.44 | 3.72 | .0000000 | T | INFINITE |
| 0045 | 0045-0024 | B38 | TUB | 26.00 | 1.250 | K | CHD | 100.83 | 6.47 | 6.20 | 2.39 | 6.03 | .0000000 | T | INFINITE | |
| 0045 | 0045-0136 | F15 | TUB | 24.00 | 0.750 | K | BRC | 100.83 | 0.49 | 6.27 | 2.98 | 2.28 | 3.49 | .0000000 | T | INFINITE |

SACS V8i SELECTseries 3 (v5.6) ITS
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

DATE 07-AUG-2020 TIME 21:02:24 FTG PAGE 297

* * * MEMBER FATIGUE REPORT * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD LEN. | GAP | * | STRESS | CONC. | FACTORS | * | FATIGUE | RESULTS | REQUIRED | |
|-------|--------|------|------|----------|----|-----|-----|---------------|-----|---|--------|-------|---------|---|---------|---------|----------|----|
| | | | | OD | WT | | | | | | | | | | | | OD | WT |

| ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC LIFE | (IN) | (IN) |
|-------|-----------|------|------|-------|-------|------|------|--------|-------|-------|-------|--------|----------|----------|----------|----------|
| 0045 | 0025-0045 | B37 | TUB | 26.00 | 1.250 | K | CHD | 100.83 | 7.08 | 5.22 | 1.88 | 4.85 | .0000000 | T | INFINITE | |
| 0045 | 0045-0218 | F20 | TUB | 22.00 | 0.750 | Y | BRC | 100.83 | 8.46 | 4.83 | 2.28 | 3.87 | .0000000 | T | INFINITE | |
| 0045 | 0025-0045 | B37 | TUB | 26.00 | 1.250 | Y | CHD | 100.83 | 10.00 | 6.40 | 2.08 | 5.21 | .0000000 | T | INFINITE | |
| ----- | | | | | | | | | | | | | | | | |
| 0218 | 0045-0218 | F20 | TUB | 22.00 | 0.750 | Y | BRC | 28.49 | 3.86 | 4.05 | 2.64 | 4.00 | .0000000 | T | INFINITE | |
| 0218 | 0168-0218 | F21 | TUB | 26.00 | 1.000 | Y | CHD | 28.49 | 6.71 | 6.83 | 2.44 | 6.14 | .0000000 | T | INFINITE | |
| ----- | | | | | | | | | | | | | | | | |
| 0052 | 0024-0052 | B12 | TUB | 26.00 | 1.000 | TK | BRC | 50.42 | 55.20 | 2.09 | 1.84 | 2.69 | 2.03 | .0000000 | T | INFINITE |
| 0052 | 0052-0165 | B42 | TUB | 28.00 | 1.375 | TK | CHD | 50.42 | 3.04 | 2.75 | 1.67 | 3.13 | .0000000 | T | INFINITE | |
| 0052 | 0026-0052 | B12 | TUB | 26.00 | 1.000 | TK | BRC | 50.42 | 55.20 | 2.00 | 1.84 | 2.69 | 1.92 | .0000000 | T | INFINITE |
| 0052 | 0177-0052 | B43 | TUB | 28.00 | 1.375 | TK | CHD | 50.42 | 2.91 | 2.73 | 1.67 | 2.97 | .0000000 | T | INFINITE | |
| 0052 | 0051-0052 | BV1 | TUB | 22.00 | 0.750 | TK | BRC | 50.42 | 55.20 | 3.19 | 3.19 | 2.23 | 4.56 | .0000000 | T | INFINITE |
| 0052 | 0052-0165 | B42 | TUB | 28.00 | 1.375 | TK | CHD | 50.42 | 4.10 | 4.07 | 2.00 | 5.67 | .0000000 | T | INFINITE | |
| 0052 | 0155-0052 | F18 | TUB | 26.00 | 1.000 | K | BRC | 50.42 | 5.25 | 3.36 | 2.94 | 2.37 | 3.16 | .0000000 | T | INFINITE |
| 0052 | 0177-0052 | B43 | TUB | 28.00 | 1.375 | K | CHD | 50.42 | 4.79 | 4.43 | 2.20 | 4.88 | .0000000 | T | INFINITE | |
| 0052 | 0148-0052 | F19 | TUB | 26.00 | 1.000 | K | BRC | 50.42 | 5.25 | 3.23 | 2.83 | 2.37 | 3.30 | .0000000 | T | INFINITE |

SACS V8i SELECTseries 3 (v5.6) ITS
ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

* * * M E M B E R F A T I G U E R E P O R T * * *
(DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|-------|--------------------------|------|------|------|-----------------|-------|----------|----------|--------|------|
| | | | | OD | WT | | | | | TYP | TYP | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC |
| | ID | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | | (IN) | (IN) |
| 0052 | 0052-0165 | B42 | TUB | 28.00 | 1.375 | K | CHD | 50.42 | | 4.67 | 4.26 | 2.18 | 5.09 | .0000000 | T | INFINITE | | | |
| 0052 | 0052-0158 | F21 | TUB | 26.00 | 1.000 | Y | BRC | 50.42 | | 3.38 | 3.27 | 2.37 | 2.29 | .0000000 | T | INFINITE | | | |
| 0052 | 0177-0052 | B43 | TUB | 28.00 | 1.375 | Y | CHD | 50.42 | | 4.04 | 4.91 | 2.19 | 3.53 | .0000000 | T | INFINITE | | | |
| ----- | | | | | | | | | | | | | | | | | | | |
| 0033 | 0024-0033 | B12 | TUB | 26.00 | 1.000 | TK | BRC | 50.42 | 55.20 | 2.10 | 1.84 | 2.69 | 2.03 | .0000000 | T | INFINITE | | | |
| 0033 | 0033-0166 | B42 | TUB | 28.00 | 1.375 | TK | CHD | 50.42 | | 3.05 | 2.76 | 1.67 | 3.13 | .0000000 | T | INFINITE | | | |
| 0033 | 0025-0033 | B12 | TUB | 26.00 | 1.000 | TK | BRC | 50.42 | 55.20 | 2.00 | 1.84 | 2.69 | 1.92 | .0000000 | T | INFINITE | | | |
| 0033 | 0178-0033 | B43 | TUB | 28.00 | 1.375 | TK | CHD | 50.42 | | 2.91 | 2.73 | 1.67 | 2.97 | .0000000 | T | INFINITE | | | |
| 0033 | 0033-0045 | BV1 | TUB | 22.00 | 0.750 | TK | BRC | 50.42 | 55.20 | 3.19 | 3.19 | 2.23 | 4.56 | .0000000 | T | INFINITE | | | |
| 0033 | 0033-0166 | B42 | TUB | 28.00 | 1.375 | TK | CHD | 50.42 | | 4.10 | 4.07 | 2.00 | 5.67 | .0000000 | T | INFINITE | | | |
| 0033 | 0180-0033 | F18 | TUB | 26.00 | 1.000 | K | BRC | 50.42 | 5.25 | 3.36 | 2.95 | 2.37 | 3.16 | .0000000 | T | INFINITE | | | |
| 0033 | 0178-0033 | B43 | TUB | 28.00 | 1.375 | K | CHD | 50.42 | | 4.80 | 4.43 | 2.20 | 4.88 | .0000000 | T | INFINITE | | | |
| 0033 | 0148-0033 | F19 | TUB | 26.00 | 1.000 | K | BRC | 50.42 | 5.25 | 3.23 | 2.83 | 2.37 | 3.31 | .0000000 | T | INFINITE | | | |
| 0033 | 0033-0166 | B42 | TUB | 28.00 | 1.375 | K | CHD | 50.42 | | 4.68 | 4.25 | 2.18 | 5.10 | .0000000 | T | INFINITE | | | |

0033 0033-0168 F21 TUB 26.00 1.000 Y BRC 50.42 3.38 3.27 2.37 2.29 .0000000 T INFINITE

SACS V8i SELECTseries 3 (v5.6) ITS
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

DATE 07-AUG-2020 TIME 21:02:24 FTG PAGE 299

* * * M E M B E R F A T I G U E R E P O R T * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|------|--------------------------|------|------|------|-----------------|-------|----------|----------|--------|------|
| | | | | OD | WT | | | | | TYP | TYP | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | | (IN) | (IN) |
| 0033 | 0178-0033 | B43 | TUB | 28.00 | 1.375 | Y | CHD | 50.42 | | 4.05 | 4.91 | 2.19 | 3.54 | .0000000 | T | INFINITE | | | |
| ----- | | | | | | | | | | | | | | | | | | | |
| 0211 | 0224-0211 | F21 | TUB | 26.00 | 1.000 | Y | BRC | 28.49 | | 4.79 | 2.50 | 2.65 | 2.78 | .0000000 | T | INFINITE | | | |
| 0211 | 0121-0211 | F21 | TUB | 26.00 | 1.000 | Y | CHD | 28.49 | | 10.00 | 3.48 | 2.68 | 5.27 | .0000000 | T | INFINITE | | | |
| ----- | | | | | | | | | | | | | | | | | | | |
| 0224 | 0224-0206 | F21 | TUB | 26.00 | 1.000 | Y | BRC | 70.72 | | 3.21 | 3.38 | 2.39 | 2.26 | .0000000 | T | INFINITE | | | |
| 0224 | 0224-0018 | JA8 | TUB | 53.00 | 2.500 | Y | CHD | 70.72 | | 2.98 | 3.31 | 1.50 | 2.03 | .0000000 | T | INFINITE | | | |
| 0224 | 0224-0211 | F21 | TUB | 26.00 | 1.000 | Y | BRC | 70.72 | | 3.21 | 3.38 | 2.39 | 2.26 | .0000000 | T | INFINITE | | | |
| 0224 | 0224-0018 | JA8 | TUB | 53.00 | 2.500 | Y | CHD | 70.72 | | 2.98 | 3.31 | 1.50 | 2.03 | .0000000 | T | INFINITE | | | |
| ----- | | | | | | | | | | | | | | | | | | | |
| 0206 | 0224-0206 | F21 | TUB | 26.00 | 1.000 | Y | BRC | 28.49 | | 4.79 | 2.50 | 2.65 | 2.78 | .0000000 | T | INFINITE | | | |
| 0206 | 0159-0206 | F21 | TUB | 26.00 | 1.000 | Y | CHD | 28.49 | | 10.00 | 3.48 | 2.68 | 5.27 | .0000000 | T | INFINITE | | | |

```

-----
0054 0042-0054 B12 TUB 26.00 1.000 Y BRC 16.70 3.02 2.34 2.53 2.20 .0000000 T INFINITE
0054 0054-0160 BH0 TUB 28.00 1.375 Y CHD 16.70 4.47 3.02 1.89 3.39 .0000000 T INFINITE
-----

```

```

0037 0042-0037 B12 TUB 26.00 1.000 Y BRC 16.70 3.02 2.34 2.53 2.20 .0000000 T INFINITE

```

```

SACS V8i SELECTseries 3 (v5.6) ITS
ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

```

```

DATE 07-AUG-2020 TIME 21:02:24 FTG PAGE 300

```

```

* * * MEMBER FATIGUE REPORT * * *
(DAMAGE ORDER)

```

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | | REQUIRED | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|------|--------------------------|------|------|----------|-----------------|----------|-------|-------|----------|------|
| | | | | OD | WT | | | | | TYP | TYP | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC |
| | | ID | ID | (IN) | (IN) | | | (FT) | (IN) | | | | | | | | | (IN) | (IN) |
| 0037 | 0037-0161 | BH0 | TUB | 28.00 | 1.375 | Y | CHD | 16.70 | 4.47 | 3.02 | 1.89 | 3.39 | .0000000 | T | INFINITE | | | | |

```

-----
0027 0160-0027 B40 TUB 28.00 1.000 T BRC 9.08 2.40 3.81 2.21 3.36 .0000000 T INFINITE
0027 0027-0246 JA7 TUB 54.00 2.500 T CHD 9.08 1.50 3.47 1.61 3.06 .0000000 T INFINITE
0027 0161-0027 B40 TUB 28.00 1.000 T BRC 9.08 2.40 3.81 2.21 3.36 .0000000 T INFINITE
0027 0027-0246 JA7 TUB 54.00 2.500 T CHD 9.08 1.50 3.47 1.61 3.06 .0000000 T INFINITE
-----

```

```

0042 0042-0037 B12 TUB 26.00 1.000 Y BRC 32.92 2.73 2.95 2.43 2.11 .0000000 T INFINITE

```

| | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|------|------|------|------|----------|---|----------|
| 0042 | 0042-0225 | JA7 | TUB | 54.00 | 2.500 | Y | CHD | 32.92 | 2.09 | 2.69 | 1.50 | 1.89 | .0000000 | T | INFINITE |
| 0042 | 0042-0054 | B12 | TUB | 26.00 | 1.000 | Y | BRC | 32.92 | 2.73 | 2.95 | 2.43 | 2.11 | .0000000 | T | INFINITE |
| 0042 | 0042-0225 | JA7 | TUB | 54.00 | 2.500 | Y | CHD | 32.92 | 2.09 | 2.69 | 1.50 | 1.89 | .0000000 | T | INFINITE |

FATIGUE REPORT JACKET KONVENSIONAL

* * * M E M B E R F A T I G U E R E P O R T * * *
(DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|------|--------------------------|------|------|------|-----------------|-------|----------|----------|--------|
| | | | | OD | WT | | | | | TYP | TYP | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE |
| | | ID | ID | (IN) | (IN) | | | (FT) | (IN) | | | | | | | | (IN) | (IN) |
| 0061 | 0003-0061 | B01 | TUB | 28.00 | 1.375 | TK | BRC | 70.43 | 6.05 | 2.90 | 2.92 | 2.63 | 3.10 | .87914-5 | TL | 2274963. | | |
| 0061 | 0061-0005 | JB1 | TUB | 54.00 | 2.500 | TK | CHD | 70.43 | | 3.39 | 3.50 | 1.66 | 3.36 | .25484-4 | L | 784806.9 | | |
| 0061 | 0004-0061 | B01 | TUB | 28.00 | 1.375 | TK | BRC | 70.43 | 6.07 | 2.84 | 2.84 | 2.65 | 2.83 | .27938-3 | T | 71588.20 | | |
| 0061 | 0061-0005 | JB1 | TUB | 54.00 | 2.500 | TK | CHD | 70.43 | | 3.31 | 3.40 | 1.64 | 3.07 | .21853-3 | T | 91519.79 | | |
| 0061 | 0061-0092 | B07 | TUB | 32.00 | 1.500 | TK | BRC | 70.43 | 6.05 | 3.43 | 4.13 | 2.53 | 4.04 | .39611-4 | TL | 504916.4 | | |
| 0061 | 0061-0067 | JB2 | TUB | 54.00 | 2.500 | TK | CHD | 70.43 | | 4.47 | 5.13 | 2.08 | 4.78 | .12916-3 | TL | 154844.3 | | |
| 0061 | 0061-0079 | B02 | TUB | 26.00 | 1.250 | TK | BRC | 70.43 | 6.07 | 3.24 | 4.05 | 2.40 | 3.57 | .20127-2 | TR | 9936.713 | | |
| 0061 | 0061-0067 | JB2 | TUB | 54.00 | 2.500 | TK | CHD | 70.43 | | 3.59 | 4.20 | 1.75 | 3.60 | .21916-2 | TR | 9125.788 | | |
| 0061 | 0091-0061 | B13 | TUB | 22.00 | 1.000 | TK | BRC | 70.43 | 6.05 | 3.35 | 4.04 | 2.16 | 4.37 | .16388-3 | R | 122040.9 | | |
| 0061 | 0061-0005 | JB1 | TUB | 54.00 | 2.500 | TK | CHD | 70.43 | | 3.05 | 3.36 | 1.51 | 3.75 | .50327-4 | R | 397404.8 | | |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|----|-----|-------|------|------|------|------|------|----------|----|----------|
| 0061 | 0061-0078 | B13 | TUB | 22.00 | 1.000 | TK | BRC | 70.43 | 6.07 | 3.24 | 4.00 | 2.17 | 3.94 | .26377-3 | TL | 75824.64 |
| 0061 | 0061-0005 | JB1 | TUB | 54.00 | 2.500 | TK | CHD | 70.43 | | 2.93 | 3.28 | 1.51 | 3.38 | .78769-4 | TL | 253906.5 |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|----|-----|-------|------|------|------|------|------|----------|----|----------|
| 0079 | 0061-0079 | B02 | TUB | 26.00 | 1.250 | TK | BRC | 70.43 | 6.05 | 2.91 | 2.97 | 2.52 | 2.92 | .74270-3 | TR | 26928.67 |
| 0079 | 0078-0079 | JB2 | TUB | 54.00 | 2.500 | TK | CHD | 70.43 | | 3.16 | 3.25 | 1.57 | 2.95 | .83011-3 | TR | 24093.22 |

SACS V8i SELECTseries 3 (v5.6)
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

ITS

DATE 15-JUL-2020 TIME 16:51:31 FTG PAGE 273

* * * MEMBER FATIGUE REPORT * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|------|--------------------------|------|-------|-------|-----------------|-------|----------|----------|------|
| | | | | OD | WT | | | | | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | (IN) | (IN) |
| 0079 | 0079-0068 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 70.43 | 6.05 | 3.36 | 3.96 | 2.38 | 3.81 | .16693-2 | T | 11980.94 | | |
| 0079 | 0079-0080 | JB3 | TUB | 54.00 | 2.500 | TK | CHD | 70.43 | | 3.75 | 4.15 | 1.83 | 3.92 | .17956-2 | T | 11138.05 | | |
| 0079 | 0079-0105 | B15 | TUB | 22.00 | 0.750 | TK | BRC | 70.43 | 6.05 | 2.86 | 3.13 | 2.04 | 4.05 | .95237-6 | T | 21000.+3 | | |
| 0079 | 0078-0079 | JB2 | TUB | 54.00 | 2.500 | TK | CHD | 70.43 | | 2.20 | 2.30 | 1.50 | 2.97 | .31195-7 | T | 64114.+4 | | |
| 0079 | 0079-0106 | B14 | TUB | 22.00 | 0.750 | T | BRC | 70.43 | | 3.05 | 4.91 | 2.04 | 2.92 | .57875-5 | R | 3455741. | | |
| 0079 | 0078-0079 | JB2 | TUB | 54.00 | 2.500 | T | CHD | 70.43 | | 2.39 | 3.08 | 1.50 | 2.15 | .59859-7 | R | 33412.+4 | | |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|----|-----|-------|------|------|------|------|------|----------|---|----------|
| 0068 | 0092-0068 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 70.43 | 6.05 | 3.00 | 3.09 | 2.46 | 3.39 | .85653-4 | T | 233499.2 |
|------|-----------|-----|-----|-------|-------|----|-----|-------|------|------|------|------|------|----------|---|----------|

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|----|-----|-------|------|------|------|------|------|----------|----|----------|
| 0068 | 0067-0068 | JB3 | TUB | 54.00 | 2.500 | TK | CHD | 70.43 | | 3.27 | 3.36 | 1.70 | 3.50 | .96040-4 | TR | 208246.8 |
| 0068 | 0068-0094 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 70.43 | 6.05 | 3.36 | 3.56 | 2.38 | 3.88 | .81042-4 | T | 246785.2 |
| 0068 | 0068-0069 | JB4 | TUB | 54.00 | 2.500 | TK | CHD | 70.43 | | 3.62 | 3.75 | 1.83 | 3.99 | .82196-4 | T | 243321.3 |
| 0068 | 0079-0068 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 70.43 | 6.05 | 2.96 | 3.07 | 2.48 | 3.28 | .84284-3 | T | 23729.34 |
| 0068 | 0067-0068 | JB3 | TUB | 54.00 | 2.500 | TK | CHD | 70.43 | | 3.25 | 3.37 | 1.67 | 3.38 | .81247-3 | TL | 24616.25 |
| 0068 | 0068-0081 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 70.43 | 6.05 | 3.44 | 3.79 | 2.37 | 3.97 | .12645-2 | T | 15817.13 |
| 0068 | 0068-0069 | JB4 | TUB | 54.00 | 2.500 | TK | CHD | 70.43 | | 3.74 | 3.95 | 1.86 | 4.09 | .12870-2 | T | 15539.58 |

SACS V8i SELECTseries 3 (v5.6)
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

ITS

DATE 15-JUL-2020 TIME 16:51:31 FTG PAGE 274

* * * M E M B E R F A T I G U E R E P O R T * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|------|--------------------------|------|-------|-------|-----------------|-------|----------|----------|------|
| | | | | OD | WT | | | | | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC |
| | ID | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | (IN) | (IN) |
| 0068 | 0093-0068 | B17 | TUB | 24.00 | 0.750 | TK | BRC | 70.43 | 6.05 | 2.76 | 2.81 | 2.06 | 4.32 | .63089-6 | R | 31701.+3 | | |
| 0068 | 0067-0068 | JB3 | TUB | 54.00 | 2.500 | TK | CHD | 70.43 | | 2.17 | 2.18 | 1.50 | 3.24 | .13301-7 | R | 15036.+5 | | |
| 0068 | 0068-0080 | B17 | TUB | 24.00 | 0.750 | TK | BRC | 70.43 | 6.05 | 2.75 | 2.90 | 2.06 | 4.31 | .44996-7 | T | 44448.+4 | | |
| 0068 | 0067-0068 | JB3 | TUB | 54.00 | 2.500 | TK | CHD | 70.43 | | 2.16 | 2.21 | 1.50 | 3.23 | .30023-9 | T | 66615.+6 | | |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|----|-----|-------|------|------|------|------|------|----------|----|----------|
| 0092 | 0078-0092 | B07 | TUB | 32.00 | 1.500 | TK | BRC | 71.29 | 6.05 | 2.92 | 2.93 | 2.66 | 3.31 | .62770-4 | TR | 318625.3 |
| 0092 | 0091-0092 | JA2 | TUB | 54.00 | 2.500 | TK | CHD | 71.29 | | 3.70 | 3.76 | 1.86 | 3.92 | .15233-3 | TR | 131289.9 |
| 0092 | 0061-0092 | B07 | TUB | 32.00 | 1.500 | TK | BRC | 71.29 | 6.05 | 2.95 | 2.98 | 2.66 | 3.29 | .24546-4 | TL | 814796.1 |
| 0092 | 0091-0092 | JA2 | TUB | 54.00 | 2.500 | TK | CHD | 71.29 | | 3.75 | 3.85 | 1.86 | 3.90 | .87260-4 | L | 229200.4 |
| 0092 | 0092-0080 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 71.29 | 6.05 | 3.44 | 4.08 | 2.37 | 3.94 | .11080-2 | T | 18050.95 |
| 0092 | 0092-0093 | JA3 | TUB | 54.00 | 2.500 | TK | CHD | 71.29 | | 3.85 | 4.26 | 1.85 | 4.06 | .12826-2 | T | 15593.67 |
| 0092 | 0092-0068 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 71.29 | 6.05 | 3.44 | 4.11 | 2.37 | 3.94 | .18186-3 | TR | 109973.7 |
| 0092 | 0092-0093 | JA3 | TUB | 54.00 | 2.500 | TK | CHD | 71.29 | | 3.86 | 4.28 | 1.85 | 4.06 | .24379-3 | TR | 82039.10 |
| 0092 | 0092-0106 | B14 | TUB | 22.00 | 0.750 | TK | BRC | 71.29 | 6.05 | 2.85 | 3.12 | 2.04 | 4.07 | .25328-6 | R | 78965.+3 |
| 0092 | 0091-0092 | JA2 | TUB | 54.00 | 2.500 | TK | CHD | 71.29 | | 2.19 | 2.30 | 1.50 | 2.99 | .34585-8 | TR | 57828.+5 |

SACS V8i SELECTseries 3 (v5.6)
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

ITS

DATE 15-JUL-2020 TIME 16:51:31 FTG PAGE 275

* * * M E M B E R F A T I G U E R E P O R T * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|------|--------------------------|------|------|------|-----------------|-------|----------|----------|--------|------|
| | | | | OD | WT | | | | | TYP | TYP | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | | (IN) | (IN) |
| 0092 | 0092-0107 | B14 | TUB | 22.00 | 0.750 | TK | BRC | 71.29 | 6.05 | 2.84 | 3.09 | 2.04 | 4.10 | .27351-6 | R | 73123.+3 | | | |
| 0092 | 0091-0092 | JA2 | TUB | 54.00 | 2.500 | TK | CHD | 71.29 | | 2.19 | 2.28 | 1.50 | 3.01 | .31715-8 | TR | 63062.+5 | | | |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|----|-----|-------|------|------|------|------|------|----------|----|----------|
| 0078 | 0003-0078 | B01 | TUB | 28.00 | 1.375 | TK | BRC | 70.43 | 6.05 | 2.86 | 2.87 | 2.63 | 3.13 | .64929-4 | T | 308027.1 |
| 0078 | 0078-0004 | JB1 | TUB | 54.00 | 2.500 | TK | CHD | 70.43 | | 3.33 | 3.41 | 1.66 | 3.40 | .81629-4 | TR | 245011.9 |
| 0078 | 0078-0092 | B07 | TUB | 32.00 | 1.500 | TK | BRC | 70.43 | 6.05 | 3.42 | 4.05 | 2.53 | 4.06 | .20884-3 | T | 95767.74 |
| 0078 | 0078-0079 | JB2 | TUB | 54.00 | 2.500 | TK | CHD | 70.43 | | 4.42 | 5.02 | 2.08 | 4.81 | .43004-3 | TL | 46507.10 |
| 0078 | 0091-0078 | B13 | TUB | 22.00 | 1.000 | TK | BRC | 70.43 | 6.05 | 3.36 | 3.98 | 2.16 | 4.41 | .21975-3 | L | 91011.92 |
| 0078 | 0078-0004 | JB1 | TUB | 54.00 | 2.500 | TK | CHD | 70.43 | | 3.04 | 3.32 | 1.51 | 3.79 | .67331-4 | L | 297038.7 |
| 0078 | 0061-0078 | B13 | TUB | 22.00 | 1.000 | Y | BRC | 70.43 | | 3.18 | 5.44 | 2.17 | 3.31 | .63425-3 | L | 31533.32 |
| 0078 | 0078-0004 | JB1 | TUB | 54.00 | 2.500 | Y | CHD | 70.43 | | 3.19 | 4.20 | 1.51 | 2.84 | .16481-3 | BL | 121351.8 |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|----|-----|-------|------|------|------|------|------|----------|----|----------|
| 0080 | 0092-0080 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 70.43 | 6.05 | 3.00 | 3.09 | 2.46 | 3.40 | .53142-3 | T | 37635.17 |
| 0080 | 0079-0080 | JB3 | TUB | 54.00 | 2.500 | TK | CHD | 70.43 | | 3.27 | 3.35 | 1.70 | 3.50 | .56352-3 | TL | 35491.34 |
| 0080 | 0080-0094 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 70.43 | 6.05 | 3.36 | 3.52 | 2.38 | 3.88 | .48291-3 | T | 41415.38 |
| 0080 | 0080-0081 | JB4 | TUB | 54.00 | 2.500 | TK | CHD | 70.43 | | 3.61 | 3.72 | 1.83 | 4.00 | .47744-3 | T | 41890.50 |

SACS V8i SELECTseries 3 (v5.6)
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

ITS

DATE 15-JUL-2020 TIME 16:51:31 FTG PAGE 276

* * * MEMBER FATIGUE REPORT * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * | STRESS | CONC. | FACTORS | * | FATIGUE | RESULTS | REQUIRED | |
|-------|--------|------|------|----------|----|-----|-----|-------|-----|---|--------|-------|---------|---|---------|---------|----------|----|
| | | | | OD | WT | | | | | | | | | | | | OD | WT |

| ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC LIFE | (IN) | (IN) |
|-------|-----------|------|------|-------|-------|------|------|-------|-------|-------|-------|--------|------|----------|------|----------|
| 0080 | 0093-0080 | B17 | TUB | 24.00 | 0.750 | TK | BRC | 70.43 | 6.05 | 2.76 | 2.80 | 2.06 | 4.33 | .15498-5 | L | 12905.+3 |
| 0080 | 0079-0080 | JB3 | TUB | 54.00 | 2.500 | TK | CHD | 70.43 | | 2.16 | 2.18 | 1.50 | 3.25 | .13069-6 | L | 15303.+4 |
| 0080 | 0068-0080 | B17 | TUB | 24.00 | 0.750 | Y | BRC | 70.43 | | 3.03 | 4.92 | 2.06 | 3.06 | .31923-6 | L | 62651.+3 |
| 0080 | 0079-0080 | JB3 | TUB | 54.00 | 2.500 | Y | CHD | 70.43 | | 2.44 | 3.13 | 1.50 | 2.29 | .21162-8 | L | 94509.+5 |
| ----- | | | | | | | | | | | | | | | | |
| 0081 | 0068-0081 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 86.53 | 6.02 | 3.02 | 3.14 | 2.45 | 3.49 | .45971-3 | T | 43505.30 |
| 0081 | 0080-0081 | JB4 | TUB | 54.00 | 2.500 | TK | CHD | 86.53 | | 3.30 | 3.38 | 1.72 | 3.60 | .45913-3 | TR | 43560.58 |
| 0081 | 0081-0097 | B08 | TUB | 28.00 | 1.250 | K | BRC | 86.53 | 3.00 | 3.19 | 3.67 | 2.42 | 3.68 | .11911-5 | TL | 16791.+3 |
| 0081 | 0083-0081 | JB5 | TUB | 54.00 | 2.500 | K | CHD | 86.53 | | 3.60 | 3.89 | 1.77 | 3.79 | .13981-5 | TL | 14305.+3 |
| 0081 | 0081-0099 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 86.53 | 6.02 | 3.31 | 3.64 | 2.40 | 3.68 | .61680-4 | TR | 324255.7 |
| 0081 | 0083-0081 | JB5 | TUB | 54.00 | 2.500 | TK | CHD | 86.53 | | 3.70 | 3.88 | 1.79 | 3.79 | .77904-4 | TR | 256724.9 |
| 0081 | 0081-0111 | B19 | TUB | 24.00 | 0.750 | TK | BRC | 86.53 | 6.02 | 2.79 | 2.91 | 2.06 | 4.20 | .69209-5 | B | 2889802. |
| 0081 | 0080-0081 | JB4 | TUB | 54.00 | 2.500 | TK | CHD | 86.53 | | 2.21 | 2.24 | 1.50 | 3.15 | .53032-6 | BL | 37713.+3 |
| 0081 | 0081-0112 | B18 | TUB | 24.00 | 0.750 | K | BRC | 86.53 | 3.00 | 2.79 | 2.96 | 2.06 | 4.21 | .93747-6 | TR | 21334.+3 |
| 0081 | 0080-0081 | JB4 | TUB | 54.00 | 2.500 | K | CHD | 86.53 | | 2.22 | 2.25 | 1.50 | 3.15 | .40563-7 | TR | 49306.+4 |

SACS V8i SELECTseries 3 (v5.6)
ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

ITS

* * * M E M B E R F A T I G U E R E P O R T * * *
(DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|------|--------------------------|------|------|------|-----------------|-------|----------|----------|--------|------|
| | | | | OD | WT | | | | | TYP | TYP | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC |
| | ID | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | | | | | | | | | | (IN) | (IN) |
| 0094 | 0080-0094 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 87.58 | 6.02 | 2.93 | 2.95 | 2.47 | 3.43 | .16251-3 | T | 123072.1 | | | |
| 0094 | 0093-0094 | JA4 | TUB | 54.00 | 2.500 | TK | CHD | 87.58 | | 3.18 | 3.20 | 1.68 | 3.54 | .16240-3 | T | 123155.5 | | | |
| 0094 | 0068-0094 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 87.58 | 6.02 | 2.92 | 2.95 | 2.47 | 3.44 | .23690-4 | T | 844247.6 | | | |
| 0094 | 0093-0094 | JA4 | TUB | 54.00 | 2.500 | TK | CHD | 87.58 | | 3.17 | 3.20 | 1.68 | 3.54 | .23619-4 | TL | 846792.3 | | | |
| 0094 | 0094-0097 | B05 | TUB | 30.00 | 1.375 | TK | BRC | 87.58 | 6.02 | 3.51 | 3.80 | 2.45 | 4.02 | .58131-4 | TL | 344051.8 | | | |
| 0094 | 0094-0095 | JA5 | TUB | 54.00 | 2.500 | TK | CHD | 87.58 | | 4.17 | 4.32 | 1.99 | 4.45 | .10996-3 | TL | 181886.3 | | | |
| 0094 | 0094-0098 | B05 | TUB | 30.00 | 1.375 | TK | BRC | 87.58 | 6.02 | 3.51 | 3.81 | 2.45 | 4.01 | .59664-5 | R | 3352128. | | | |
| 0094 | 0094-0095 | JA5 | TUB | 54.00 | 2.500 | TK | CHD | 87.58 | | 4.18 | 4.33 | 1.99 | 4.44 | .15916-4 | R | 1256573. | | | |
| 0094 | 0094-0112 | B18 | TUB | 24.00 | 0.750 | TK | BRC | 87.58 | 6.02 | 2.76 | 2.79 | 2.07 | 4.14 | .15506-5 | BL | 12898.+3 | | | |
| 0094 | 0093-0094 | JA4 | TUB | 54.00 | 2.500 | TK | CHD | 87.58 | | 2.18 | 2.19 | 1.50 | 3.10 | .70118-7 | BL | 28523.+4 | | | |
| 0094 | 0094-0113 | B18 | TUB | 24.00 | 0.750 | TK | BRC | 87.58 | 6.02 | 2.76 | 2.80 | 2.07 | 4.12 | .36474-7 | BR | 54833.+4 | | | |
| 0094 | 0093-0094 | JA4 | TUB | 54.00 | 2.500 | TK | CHD | 87.58 | | 2.19 | 2.19 | 1.50 | 3.09 | .35879-9 | B | 55743.+6 | | | |
| ----- | | | | | | | | | | | | | | | | | | | |
| 0091 | 0091-0078 | B13 | TUB | 22.00 | 1.000 | Y | BRC | 71.29 | | 3.19 | 5.38 | 2.17 | 3.27 | .13286-3 | R | 150529.8 | | | |
| 0091 | 0003-0091 | JA1 | TUB | 54.00 | 2.500 | Y | CHD | 71.29 | | 3.20 | 4.18 | 1.50 | 2.80 | .21928-4 | R | 912074.7 | | | |

SACS V8i SELECTseries 3 (v5.6)
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

ITS

DATE 15-JUL-2020 TIME 16:51:31 FTG PAGE 278

* * * M E M B E R F A T I G U E R E P O R T * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | |
|-------|-----------|------|------|----------|-------|-----|-----|--------|------|--------------------------|------|-------|-------|-----------------|-------|----------|----------|------|
| | | | | OD | WT | | | | | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | (IN) | (IN) |
| 0091 | 0091-0061 | B13 | TUB | 22.00 | 1.000 | Y | BRC | 71.29 | | 3.19 | 5.38 | 2.17 | 3.27 | .85283-4 | L | 234513.5 | | |
| 0091 | 0003-0091 | JA1 | TUB | 54.00 | 2.500 | Y | CHD | 71.29 | | 3.20 | 4.18 | 1.50 | 2.80 | .16587-4 | L | 1205732. | | |
| ----- | | | | | | | | | | | | | | | | | | |
| 0097 | 0081-0097 | B08 | TUB | 28.00 | 1.250 | Y | BRC | 80.08 | | 2.81 | 4.06 | 2.48 | 2.61 | .68153-6 | L | 29346.+3 | | |
| 0097 | 0083-0097 | B05 | TUB | 30.00 | 1.375 | Y | CHD | 80.08 | | 2.58 | 6.83 | 2.83 | 4.56 | .63141-4 | L | 316752.1 | | |
| 0097 | 0095-0097 | B08 | TUB | 28.00 | 1.250 | Y | BRC | 80.08 | | 2.76 | 4.08 | 2.48 | 2.61 | .73385-6 | L | 27253.+3 | | |
| 0097 | 0094-0097 | B05 | TUB | 30.00 | 1.375 | Y | CHD | 80.08 | | 2.52 | 6.86 | 2.83 | 4.57 | .71477-4 | L | 279810.6 | | |
| ----- | | | | | | | | | | | | | | | | | | |
| 0070 | 0070-0098 | B05 | TUB | 30.00 | 1.375 | TK | BRC | 117.29 | 6.00 | 2.97 | 2.98 | 2.56 | 3.41 | .34155-6 | T | 58557.+3 | | |
| 0070 | 0070-0069 | JB5 | TUB | 54.00 | 2.500 | TK | CHD | 117.29 | | 3.50 | 3.50 | 1.80 | 3.77 | .88294-6 | TR | 22652.+3 | | |
| 0070 | 0070-0099 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 117.29 | 6.00 | 2.79 | 2.79 | 2.52 | 3.14 | .10934-4 | T | 1829193. | | |
| 0070 | 0070-0069 | JB5 | TUB | 54.00 | 2.500 | TK | CHD | 117.29 | | 3.08 | 3.08 | 1.61 | 3.23 | .14880-4 | T | 1344114. | | |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|----|-----|--------|------|------|------|------|------|----------|---|----------|
| 0070 | 0070-0101 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 117.29 | 6.00 | 3.15 | 3.21 | 2.44 | 3.53 | .14554-5 | L | 13742.+3 |
| 0070 | 0070-0071 | JB6 | TUB | 54.00 | 2.500 | TK | CHD | 117.29 | | 3.48 | 3.49 | 1.73 | 3.64 | .24267-5 | L | 8241657. |
| 0070 | 0070-0114 | B16 | TUB | 24.00 | 0.750 | TK | BRC | 117.29 | 6.00 | 2.80 | 2.83 | 2.06 | 4.19 | .19228-7 | T | 10402.+5 |
| 0070 | 0070-0069 | JB5 | TUB | 54.00 | 2.500 | TK | CHD | 117.29 | | 2.23 | 2.22 | 1.50 | 3.14 | .24573-9 | T | 81389.+6 |

SACS V8i SELECTseries 3 (v5.6) ITS
 ID=a6hrm6momGt6eWi+dZ2tdnqXlmlncWV5aJZrepeFdmQ=

DATE 15-JUL-2020 TIME 16:51:31 FTG PAGE 279

* * * MEMBER FATIGUE REPORT * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | |
|-------|-----------|------|------|----------|-------|-----|-----|--------|------|--------------------------|------|------|------|-----------------|------|----------|----------|-------|
| | | | | OD | WT | | | | | (IN) | (IN) | TYP | TYP | LEN. | (IN) | AX-CR | AX-SD | IN-PL |
| 0070 | 0070-0116 | B20 | TUB | 24.00 | 0.750 | TK | BRC | 117.29 | 6.00 | 2.85 | 2.88 | 2.06 | 4.33 | .34557-7 | R | 57876.+4 | | |
| 0070 | 0070-0069 | JB5 | TUB | 54.00 | 2.500 | TK | CHD | 117.29 | | 2.28 | 2.27 | 1.50 | 3.25 | .18434-8 | T | 10849.+6 | | |
| 0070 | 0070-0120 | B04 | TUB | 28.00 | 1.250 | TK | BRC | 117.29 | 6.00 | 3.23 | 3.31 | 2.42 | 3.58 | .13148-4 | R | 1521096. | | |
| 0070 | 0070-0071 | JB6 | TUB | 54.00 | 2.500 | TK | CHD | 117.29 | | 3.57 | 3.57 | 1.76 | 3.69 | .23724-4 | R | 843017.8 | | |
| ----- | | | | | | | | | | | | | | | | | | |
| 0084 | 0084-0100 | B06 | TUB | 28.00 | 1.250 | TK | BRC | 101.23 | 6.00 | 2.86 | 2.87 | 2.53 | 2.97 | .42007-5 | T | 4761136. | | |
| 0084 | 0083-0084 | JB6 | TUB | 54.00 | 2.500 | TK | CHD | 101.23 | | 3.19 | 3.22 | 1.60 | 3.06 | .49235-5 | TL | 4062161. | | |
| 0084 | 0084-0117 | B21 | TUB | 26.00 | 1.000 | TK | BRC | 101.23 | 6.00 | 3.13 | 3.25 | 2.20 | 4.27 | .0000000 | T | INFINITE | | |
| 0084 | 0083-0084 | JB6 | TUB | 54.00 | 2.500 | TK | CHD | 101.23 | | 2.88 | 2.89 | 1.58 | 3.82 | .0000000 | T | INFINITE | | |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|----|-----|--------|------|------|------|------|------|----------|----|----------|
| 0084 | 0084-0118 | B22 | TUB | 26.00 | 1.000 | TK | BRC | 101.23 | 6.00 | 3.14 | 3.31 | 2.20 | 4.28 | .11962-5 | R | 16719.+3 |
| 0084 | 0083-0084 | JB6 | TUB | 54.00 | 2.500 | TK | CHD | 101.23 | | 2.91 | 2.92 | 1.59 | 3.83 | .13493-6 | TR | 14823.+4 |
| 0084 | 0084-0120 | B04 | TUB | 28.00 | 1.250 | TK | BRC | 101.23 | 6.00 | 2.83 | 2.82 | 2.55 | 2.90 | .19180-4 | T | 1042750. |
| 0084 | 0083-0084 | JB6 | TUB | 54.00 | 2.500 | TK | CHD | 101.23 | | 3.17 | 3.20 | 1.56 | 2.98 | .21129-4 | T | 946588.7 |
| 0084 | 0084-0031 | B09 | TUB | 26.00 | 1.000 | TK | BRC | 101.23 | 6.00 | 2.79 | 2.81 | 2.32 | 3.10 | .15344-5 | T | 13035.+3 |
| 0084 | 0084-0009 | JB7 | TUB | 54.00 | 2.500 | TK | CHD | 101.23 | | 2.70 | 2.71 | 1.50 | 2.77 | .54866-6 | T | 36452.+3 |

SACS V8i SELECTseries 3 (v5.6)
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

ITS

DATE 15-JUL-2020 TIME 16:51:31 FTG PAGE 280

* * * M E M B E R F A T I G U E R E P O R T * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | | | | |
|-------|-----------|------|------|----------|-------|-----|-----|--------|------|--------------------------|------|------|------|-----------------|------|----------|----------|-------|-------|--------|------|
| | | | | OD | WT | | | | | (IN) | (IN) | TYP | TYP | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | | | | | | | | | | | | (IN) | (IN) |
| 0084 | 0084-0012 | B09 | TUB | 26.00 | 1.000 | TK | BRC | 101.23 | 6.00 | 2.95 | 2.97 | 2.29 | 3.23 | .27823-5 | T | 7188282. | | | | | |
| 0084 | 0084-0009 | JB7 | TUB | 54.00 | 2.500 | TK | CHD | 101.23 | | 2.87 | 2.87 | 1.50 | 2.89 | .13507-5 | T | 14807.+3 | | | | | |
| ----- | | | | | | | | | | | | | | | | | | | | | |
| 0067 | 0067-0105 | B15 | TUB | 22.00 | 0.750 | Y | BRC | 70.43 | | 3.05 | 4.87 | 2.04 | 2.90 | .20345-4 | R | 983051.7 | | | | | |
| 0067 | 0061-0067 | JB2 | TUB | 54.00 | 2.500 | Y | CHD | 70.43 | | 2.39 | 3.06 | 1.50 | 2.13 | .56971-6 | R | 35106.+3 | | | | | |
| 0067 | 0067-0107 | B14 | TUB | 22.00 | 0.750 | T | BRC | 70.43 | | 3.05 | 4.91 | 2.04 | 2.92 | .36085-5 | L | 5542470. | | | | | |
| 0067 | 0061-0067 | JB2 | TUB | 54.00 | 2.500 | T | CHD | 70.43 | | 2.39 | 3.08 | 1.50 | 2.15 | .59504-7 | L | 33611.+4 | | | | | |

```

-----
0083 0083-0097 B05 TUB 30.00 1.375 TK BRC 117.29 6.00 3.00 3.00 2.56 3.40 .88731-5 TL 2254010.
0083 0083-0081 JB5 TUB 54.00 2.500 TK CHD 117.29 3.55 3.55 1.80 3.76 .20307-4 TL 984899.6
0083 0083-0099 B03 TUB 28.00 1.250 TK BRC 117.29 6.01 2.78 2.78 2.52 3.14 .41656-6 TR 48013.+3
0083 0083-0081 JB5 TUB 54.00 2.500 TK CHD 117.29 3.06 3.06 1.61 3.23 .82632-6 TR 24204.+3
0083 0083-0100 B08 TUB 28.00 1.250 TK BRC 117.29 6.00 3.16 3.22 2.44 3.53 .35545-5 L 5626669.
0083 0083-0084 JB6 TUB 54.00 2.500 TK CHD 117.29 3.50 3.50 1.73 3.63 .56733-5 L 3525264.
0083 0083-0114 B16 TUB 24.00 0.750 TK BRC 117.29 6.01 2.79 2.84 2.06 4.27 .13690-7 T 14609.+5
0083 0083-0081 JB5 TUB 54.00 2.500 TK CHD 117.29 2.22 2.21 1.50 3.20 .25233-9 T 79262.+6

```

SACS V8i SELECTseries 3 (v5.6)
ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

ITS

DATE 15-JUL-2020 TIME 16:51:31 FTG PAGE 281

* * * M E M B E R F A T I G U E R E P O R T * * *
(DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | |
|-------|-----------|------|------|----------|-------|-----|-----|--------|------|--------------------------|------|-------|-------|-----------------|-------|----------|----------|------|
| | | | | OD | WT | | | | | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | (IN) | (IN) |
| 0083 | 0083-0115 | B20 | TUB | 24.00 | 0.750 | TK | BRC | 117.29 | 6.00 | 2.84 | 2.88 | 2.06 | 4.34 | .51499-7 | B | 38836.+4 | | |
| 0083 | 0083-0081 | JB5 | TUB | 54.00 | 2.500 | TK | CHD | 117.29 | | 2.27 | 2.27 | 1.50 | 3.25 | .26595-8 | B | 75202.+5 | | |
| 0083 | 0083-0120 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 117.29 | 6.01 | 3.23 | 3.35 | 2.42 | 3.61 | .28719-5 | R | 6964028. | | |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|----|-----|--------|------|------|------|------|------|----------|----|----------|
| 0095 | 0094-0095 | JA5 | TUB | 54.00 | 2.500 | TK | CHD | 118.71 | | 3.05 | 3.04 | 1.57 | 3.06 | .39346-7 | R | 50831.+4 |
| 0095 | 0095-0098 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 118.71 | 6.01 | 2.74 | 2.73 | 2.55 | 2.97 | .32580-8 | L | 61386.+5 |
| 0095 | 0094-0095 | JA5 | TUB | 54.00 | 2.500 | TK | CHD | 118.71 | | 3.04 | 3.04 | 1.57 | 3.06 | .17634-7 | L | 11341.+5 |
| 0095 | 0095-0100 | B06 | TUB | 28.00 | 1.250 | TK | BRC | 118.71 | 6.00 | 3.28 | 3.40 | 2.41 | 3.67 | .84409-5 | L | 2369417. |
| 0095 | 0096-0095 | JA6 | TUB | 54.00 | 2.500 | TK | CHD | 118.71 | | 3.65 | 3.64 | 1.78 | 3.78 | .13757-4 | L | 1453852. |
| 0095 | 0095-0101 | B06 | TUB | 28.00 | 1.250 | TK | BRC | 118.71 | 6.01 | 3.28 | 3.39 | 2.41 | 3.68 | .23453-5 | R | 8527675. |
| 0095 | 0096-0095 | JA6 | TUB | 54.00 | 2.500 | TK | CHD | 118.71 | | 3.64 | 3.64 | 1.78 | 3.79 | .36867-5 | R | 5424960. |
| 0095 | 0095-0115 | B20 | TUB | 24.00 | 0.750 | TK | BRC | 118.71 | 6.00 | 2.75 | 2.79 | 2.07 | 4.22 | .33326-7 | TL | 60014.+4 |
| 0095 | 0094-0095 | JA5 | TUB | 54.00 | 2.500 | TK | CHD | 118.71 | | 2.18 | 2.17 | 1.50 | 3.16 | .23830-9 | TL | 83927.+6 |
| 0095 | 0095-0116 | B20 | TUB | 24.00 | 0.750 | TK | BRC | 118.71 | 6.01 | 2.75 | 2.79 | 2.07 | 4.22 | .24596-7 | T | 81313.+4 |
| 0095 | 0094-0095 | JA5 | TUB | 54.00 | 2.500 | TK | CHD | 118.71 | | 2.18 | 2.17 | 1.50 | 3.16 | .24248-8 | T | 82481.+5 |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|--|------|------|------|------|----------|---|----------|
| 0011 | 0163-0011 | B24 | TUB | 28.00 | 1.375 | Y | BRC | 40.77 | | 2.91 | 5.95 | 2.38 | 4.32 | .22329-6 | L | 89569.+3 |
| 0011 | 0096-0011 | JA7 | TUB | 54.00 | 2.500 | Y | CHD | 40.77 | | 3.36 | 6.12 | 2.09 | 4.68 | .33220-6 | L | 60205.+3 |
| 0011 | 0164-0011 | B24 | TUB | 28.00 | 1.375 | Y | BRC | 40.77 | | 2.91 | 5.95 | 2.38 | 4.32 | .72768-5 | R | 2748446. |

SACS V8i SELECTseries 3 (v5.6)
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

ITS

DATE 15-JUL-2020 TIME 16:51:31 FTG PAGE 283

* * * MEMBER FATIGUE REPORT * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | | REQUIRED | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|------|--------------------------|------|------|------|-----------------|-------|----------|-------|----------|------|
| | | | | OD | WT | | | | | TYP | TYP | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | | (IN) | (IN) |
| 0011 | 0096-0011 | JA7 | TUB | 54.00 | 2.500 | Y | CHD | 40.77 | | 3.36 | 6.12 | 2.09 | 4.68 | .10977-4 | R | 1822043. | | | |
| ----- | | | | | | | | | | | | | | | | | | | |
| 0069 | 0069-0098 | B08 | TUB | 28.00 | 1.250 | K | BRC | 86.53 | 3.00 | 3.17 | 3.62 | 2.42 | 3.69 | .97269-6 | L | 20562.+3 | | | |
| 0069 | 0070-0069 | JB5 | TUB | 54.00 | 2.500 | K | CHD | 86.53 | | 3.57 | 3.84 | 1.77 | 3.80 | .15692-5 | L | 12745.+3 | | | |
| 0069 | 0069-0099 | B03 | TUB | 28.00 | 1.250 | K | BRC | 86.53 | 3.00 | 3.20 | 3.70 | 2.40 | 3.81 | .87496-5 | TR | 2285806. | | | |
| 0069 | 0070-0069 | JB5 | TUB | 54.00 | 2.500 | K | CHD | 86.53 | | 3.60 | 3.87 | 1.79 | 3.92 | .99928-5 | TR | 2001440. | | | |
| 0069 | 0069-0111 | B19 | TUB | 24.00 | 0.750 | K | BRC | 86.53 | 3.00 | 2.78 | 2.98 | 2.06 | 4.21 | .55037-5 | T | 3633902. | | | |
| 0069 | 0068-0069 | JB4 | TUB | 54.00 | 2.500 | K | CHD | 86.53 | | 2.20 | 2.24 | 1.50 | 3.16 | .38582-6 | T | 51837.+3 | | | |
| 0069 | 0069-0113 | B18 | TUB | 24.00 | 0.750 | K | BRC | 86.53 | 3.00 | 2.80 | 3.01 | 2.06 | 4.18 | .27500-7 | T | 72728.+4 | | | |
| 0069 | 0068-0069 | JB4 | TUB | 54.00 | 2.500 | K | CHD | 86.53 | | 2.23 | 2.27 | 1.50 | 3.13 | .26003-9 | T | 76913.+6 | | | |
| ----- | | | | | | | | | | | | | | | | | | | |
| 0093 | 0093-0080 | B17 | TUB | 24.00 | 0.750 | Y | BRC | 71.29 | | 3.04 | 4.86 | 2.07 | 3.02 | .89442-5 | R | 2236095. | | | |
| 0093 | 0092-0093 | JA3 | TUB | 54.00 | 2.500 | Y | CHD | 71.29 | | 2.45 | 3.12 | 1.50 | 2.27 | .25512-6 | R | 78394.+3 | | | |
| 0093 | 0093-0068 | B17 | TUB | 24.00 | 0.750 | Y | BRC | 71.29 | | 3.04 | 4.86 | 2.07 | 3.02 | .63332-6 | L | 31579.+3 | | | |
| 0093 | 0092-0093 | JA3 | TUB | 54.00 | 2.500 | Y | CHD | 71.29 | | 2.45 | 3.12 | 1.50 | 2.27 | .10827-7 | L | 18473.+5 | | | |

0071 0071-0101 B06 TUB 28.00 1.250 TK BRC 101.23 6.00 2.86 2.87 2.53 2.97 .18748-6 TR 10668.+4

SACS V8i SELECTseries 3 (v5.6)

ITS

ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

DATE 15-JUL-2020 TIME 16:51:31 FTG PAGE 284

* * * M E M B E R F A T I G U E R E P O R T * * *
(DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | | |
|-------|-----------|------|------|----------|-------|-----|-----|--------|------|--------------------------|------|------|------|-----------------|-------|----------|----------|--------|------|
| | | | | OD | WT | | | | | TYP | TYP | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | | (IN) | (IN) |
| 0071 | 0070-0071 | JB6 | TUB | 54.00 | 2.500 | TK | CHD | 101.23 | | 3.19 | 3.22 | 1.60 | 3.06 | .30158-6 | R | 66318.+3 | | | |
| 0071 | 0071-0117 | B21 | TUB | 26.00 | 1.000 | TK | BRC | 101.23 | 6.00 | 3.12 | 3.24 | 2.20 | 4.27 | .0000000 | T | INFINITE | | | |
| 0071 | 0070-0071 | JB6 | TUB | 54.00 | 2.500 | TK | CHD | 101.23 | | 2.87 | 2.88 | 1.58 | 3.82 | .0000000 | T | INFINITE | | | |
| 0071 | 0071-0119 | B22 | TUB | 26.00 | 1.000 | TK | BRC | 101.23 | 6.00 | 3.13 | 3.26 | 2.20 | 4.29 | .15387-6 | L | 12998.+4 | | | |
| 0071 | 0070-0071 | JB6 | TUB | 54.00 | 2.500 | TK | CHD | 101.23 | | 2.89 | 2.89 | 1.59 | 3.84 | .13873-7 | TL | 14417.+5 | | | |
| 0071 | 0071-0120 | B08 | TUB | 28.00 | 1.250 | TK | BRC | 101.23 | 6.00 | 2.80 | 2.79 | 2.55 | 2.90 | .33465-5 | T | 5976474. | | | |
| 0071 | 0070-0071 | JB6 | TUB | 54.00 | 2.500 | TK | CHD | 101.23 | | 3.14 | 3.15 | 1.56 | 2.99 | .42033-5 | T | 4758150. | | | |
| 0071 | 0071-0032 | B09 | TUB | 26.00 | 1.000 | TK | BRC | 101.23 | 6.00 | 2.79 | 2.80 | 2.32 | 3.10 | .47849-7 | T | 41798.+4 | | | |
| 0071 | 0071-0010 | JB7 | TUB | 54.00 | 2.500 | TK | CHD | 101.23 | | 2.69 | 2.70 | 1.50 | 2.77 | .73934-8 | T | 27051.+5 | | | |
| 0071 | 0071-0012 | B09 | TUB | 26.00 | 1.000 | TK | BRC | 101.23 | 6.00 | 2.94 | 2.96 | 2.29 | 3.28 | .27473-5 | T | 7279996. | | | |
| 0071 | 0071-0010 | JB7 | TUB | 54.00 | 2.500 | TK | CHD | 101.23 | | 2.85 | 2.86 | 1.50 | 2.93 | .12177-5 | T | 16425.+3 | | | |

```

-----
0096 0096-0100 B08 TUB 28.00 1.250 TK BRC 102.46 6.00 2.77 2.74 2.58 2.75 .17254-5 T 11591.+3
0096 0096-0095 JA6 TUB 54.00 2.500 TK CHD 102.46 3.13 3.13 1.53 2.84 .24404-5 TR 8195252.
0096 0096-0101 B08 TUB 28.00 1.250 TK BRC 102.46 6.01 2.78 2.74 2.58 2.75 .15397-6 TL 12989.+4

```

SACS V8i SELECTseries 3 (v5.6)

ITS

ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

DATE 15-JUL-2020 TIME 16:51:31 FTG PAGE 285

* * * MEMBER FATIGUE REPORT * * *
(DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | |
|-------|-----------|------|------|----------|-------|-----|-----|--------|------|--------------------------|------|-------|-------|-----------------|-------|----------|----------|------|
| | | | | OD | WT | | | | | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | (IN) | (IN) |
| 0096 | 0096-0095 | JA6 | TUB | 54.00 | 2.500 | TK | CHD | 102.46 | | 3.13 | 3.14 | 1.53 | 2.84 | .34592-6 | TL | 57817.+3 | | |
| 0096 | 0096-0118 | B22 | TUB | 26.00 | 1.000 | TK | BRC | 102.46 | 6.00 | 3.09 | 3.23 | 2.21 | 4.23 | .14641-6 | L | 13661.+4 | | |
| 0096 | 0096-0095 | JA6 | TUB | 54.00 | 2.500 | TK | CHD | 102.46 | | 2.86 | 2.86 | 1.57 | 3.78 | .20826-7 | TL | 96034.+4 | | |
| 0096 | 0096-0119 | B22 | TUB | 26.00 | 1.000 | TK | BRC | 102.46 | 6.01 | 3.09 | 3.23 | 2.21 | 4.22 | .19599-7 | R | 10205.+5 | | |
| 0096 | 0096-0095 | JA6 | TUB | 54.00 | 2.500 | TK | CHD | 102.46 | | 2.86 | 2.86 | 1.57 | 3.78 | .20934-8 | TR | 95540.+5 | | |
| 0096 | 0096-0031 | B09 | TUB | 26.00 | 1.000 | TK | BRC | 102.46 | 6.00 | 3.06 | 3.10 | 2.27 | 3.37 | .20885-5 | T | 9576237. | | |
| 0096 | 0096-0011 | JA7 | TUB | 54.00 | 2.500 | TK | CHD | 102.46 | | 2.97 | 2.98 | 1.50 | 3.01 | .70416-6 | T | 28403.+3 | | |
| 0096 | 0096-0032 | B09 | TUB | 26.00 | 1.000 | TK | BRC | 102.46 | 6.01 | 3.07 | 3.10 | 2.27 | 3.37 | .83844-7 | T | 23854.+4 | | |
| 0096 | 0096-0011 | JA7 | TUB | 54.00 | 2.500 | TK | CHD | 102.46 | | 2.98 | 2.99 | 1.50 | 3.01 | .21957-7 | T | 91088.+4 | | |

| | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|--------|------|------|------|------|----------|---|----------|
| 0096 | 0096-0189 | F09 | TUB | 26.00 | 1.000 | Y | BRC | 102.46 | 3.38 | 4.18 | 2.33 | 2.65 | .0000000 | T | INFINITE |
| 0096 | 0096-0011 | JA7 | TUB | 54.00 | 2.500 | Y | CHD | 102.46 | 3.42 | 4.18 | 1.50 | 2.37 | .0000000 | T | INFINITE |
| 0096 | 0096-0190 | F09 | TUB | 26.00 | 1.000 | Y | BRC | 102.46 | 3.37 | 4.18 | 2.33 | 2.65 | .0000000 | T | INFINITE |
| 0096 | 0096-0011 | JA7 | TUB | 54.00 | 2.500 | Y | CHD | 102.46 | 3.39 | 4.19 | 1.50 | 2.37 | .0000000 | T | INFINITE |

| | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|--------|------|------|------|------|----------|---|----------|
| 0120 | 0083-0120 | B08 | TUB | 28.00 | 1.250 | Y | BRC | 100.99 | 2.59 | 2.49 | 2.35 | 1.52 | .21617-6 | T | 92521.+3 |
|------|-----------|-----|-----|-------|-------|---|-----|--------|------|------|------|------|----------|---|----------|

SACS V8i SELECTseries 3 (v5.6) ITS
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

DATE 15-JUL-2020 TIME 16:51:31 FTG PAGE 286

* * * M E M B E R F A T I G U E R E P O R T * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | |
|-------|-----------|------|------|----------|-------|-----|-----|--------|------|--------------------------|------|-------|----------|-----------------|----------|--------|----------|------|
| | | | | OD | WT | | | | | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | (IN) | (IN) |
| 0120 | 0084-0120 | B04 | TUB | 28.00 | 1.375 | Y | CHD | 100.99 | 2.22 | 3.32 | 2.72 | 1.95 | .15968-5 | R | 12525.+3 | | | |
| 0120 | 0071-0120 | B08 | TUB | 28.00 | 1.250 | Y | BRC | 100.99 | 2.67 | 2.50 | 2.35 | 1.54 | .35172-6 | B | 56864.+3 | | | |
| 0120 | 0070-0120 | B04 | TUB | 28.00 | 1.375 | Y | CHD | 100.99 | 2.31 | 3.33 | 2.72 | 1.99 | .19011-5 | R | 10520.+3 | | | |

| | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|------|------|------|------|----------|---|----------|
| 0100 | 0083-0100 | B08 | TUB | 28.00 | 1.250 | Y | BRC | 98.55 | 2.64 | 2.50 | 2.35 | 1.53 | .35214-6 | T | 56795.+3 |
| 0100 | 0084-0100 | B06 | TUB | 28.00 | 1.375 | Y | CHD | 98.55 | 2.27 | 3.33 | 2.72 | 1.98 | .18753-5 | L | 10665.+3 |

0100 0096-0100 B08 TUB 28.00 1.250 Y BRC 98.55 2.64 2.51 2.35 1.54 .19790-6 B 10106.+4
 0100 0095-0100 B06 TUB 28.00 1.375 Y CHD 98.55 2.27 3.34 2.73 1.98 .17711-5 L 11293.+3

 0010 0161-0010 B24 TUB 28.00 1.375 T BRC 40.29 2.90 6.09 2.37 4.40 .42280-8 R 47303.+5
 0010 0071-0010 JB7 TUB 54.00 2.500 T CHD 40.29 3.35 6.20 2.11 4.78 .49321-8 R 40551.+5
 0010 0123-0010 B23 TUB 28.00 1.375 Y BRC 40.29 2.90 6.03 2.38 4.37 .74005-6 L 27025.+3
 0010 0071-0010 JB7 TUB 54.00 2.500 Y CHD 40.29 3.35 6.17 2.10 4.74 .12135-5 L 16481.+3

 0009 0158-0009 B24 TUB 28.00 1.375 T BRC 40.29 2.90 6.09 2.37 4.40 .37372-6 L 53516.+3
 0009 0084-0009 JB7 TUB 54.00 2.500 T CHD 40.29 3.35 6.20 2.11 4.78 .56991-6 L 35093.+3

SACS V8i SELECTseries 3 (v5.6) ITS
 ID=a6hrm6momGt6eWi+d2ZtdnqX1mlncWV5aJZrepeFdmQ=

DATE 15-JUL-2020 TIME 16:51:31 FTG PAGE 287

* * * M E M B E R F A T I G U E R E P O R T * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|------|--------------------------|------|-------|----------|-----------------|----------|--------|----------|-----|
| | | | | OD | WT | | | | | (IN) | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC |
| 0009 | 0122-0009 | B23 | TUB | 28.00 | 1.375 | Y | BRC | 40.29 | 2.90 | 6.03 | 2.38 | 4.37 | .19945-6 | R | 10028.+4 | | | |
| 0009 | 0084-0009 | JB7 | TUB | 54.00 | 2.500 | Y | CHD | 40.29 | 3.35 | 6.17 | 2.10 | 4.74 | .32528-6 | R | 61486.+3 | | | |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|--|------|------|------|------|----------|---|----------|
| 0101 | 0070-0101 | B08 | TUB | 28.00 | 1.250 | Y | BRC | 98.55 | | 2.65 | 2.50 | 2.35 | 1.54 | .68643-8 | T | 29136.+5 |
| 0101 | 0071-0101 | B06 | TUB | 28.00 | 1.375 | Y | CHD | 98.55 | | 2.28 | 3.33 | 2.72 | 1.98 | .13233-6 | L | 15114.+4 |
| 0101 | 0096-0101 | B08 | TUB | 28.00 | 1.250 | Y | BRC | 98.55 | | 2.64 | 2.51 | 2.35 | 1.53 | .10322-7 | B | 19376.+5 |
| 0101 | 0095-0101 | B06 | TUB | 28.00 | 1.375 | Y | CHD | 98.55 | | 2.27 | 3.34 | 2.73 | 1.98 | .21444-6 | L | 93268.+3 |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|----|-----|-------|--------|------|------|------|------|----------|---|----------|
| 0031 | 0127-0031 | F09 | TUB | 26.00 | 1.000 | K | BRC | 50.42 | -14.25 | 3.23 | 2.67 | 2.78 | 4.31 | .0000000 | T | INFINITE |
| 0031 | 0126-0031 | B23 | TUB | 28.00 | 1.375 | K | CHD | 50.42 | | 4.28 | 3.37 | 2.46 | 6.64 | .19479-7 | R | 10267.+5 |
| 0031 | 0031-0129 | F09 | TUB | 26.00 | 1.000 | K | BRC | 50.42 | -14.25 | 2.91 | 2.85 | 2.87 | 4.65 | .0000000 | T | INFINITE |
| 0031 | 0121-0031 | B23 | TUB | 28.00 | 1.375 | K | CHD | 50.42 | | 2.86 | 2.91 | 2.57 | 7.17 | .24957-9 | R | 80137.+6 |
| 0031 | 0084-0031 | B09 | TUB | 26.00 | 1.000 | TK | BRC | 50.42 | -29.03 | 2.06 | 1.90 | 3.38 | 2.42 | .62108-7 | B | 32202.+4 |
| 0031 | 0121-0031 | B23 | TUB | 28.00 | 1.375 | TK | CHD | 50.42 | | 1.95 | 1.77 | 2.00 | 3.73 | .18090-7 | B | 11056.+5 |
| 0031 | 0096-0031 | B09 | TUB | 26.00 | 1.000 | TK | BRC | 50.42 | -29.03 | 1.81 | 1.72 | 3.41 | 2.43 | .17758-7 | B | 11263.+5 |
| 0031 | 0126-0031 | B23 | TUB | 28.00 | 1.375 | TK | CHD | 50.42 | | 1.81 | 1.71 | 1.99 | 3.75 | .79110-8 | B | 25281.+5 |

SACS V8i SELECTseries 3 (v5.6)
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

ITS

DATE 15-JUL-2020 TIME 16:51:31 FTG PAGE 288

* * * MEMBER FATIGUE REPORT * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | | |
|-------|--------|------|------|----------|------|---------|-------|------|--------------------------|------|-------|-------|-----------------|-------|--------|----------|------|------|
| | | | | OD | WT | | | | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC | LIFE |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | (IN) | (IN) |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|----|-----|-------|--------|------|------|------|------|----------|---|----------|
| 0031 | 0118-0031 | BV1 | TUB | 22.00 | 0.750 | TK | BRC | 50.42 | -29.03 | 2.83 | 2.83 | 2.71 | 5.54 | .28130-8 | L | 71098.+5 |
| 0031 | 0126-0031 | B23 | TUB | 28.00 | 1.375 | TK | CHD | 50.42 | | 2.72 | 2.70 | 2.40 | 6.90 | .31831-7 | L | 62832.+4 |
| 0031 | 0031-0152 | F09 | TUB | 26.00 | 1.000 | Y | BRC | 50.42 | | 4.74 | 3.30 | 2.37 | 2.72 | .0000000 | T | INFINITE |
| 0031 | 0121-0031 | B23 | TUB | 28.00 | 1.375 | Y | CHD | 50.42 | | 7.46 | 5.23 | 2.18 | 4.20 | .0000000 | T | INFINITE |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|----|-----|-------|--------|------|------|------|------|----------|---|----------|
| 0032 | 0032-0127 | F09 | TUB | 26.00 | 1.000 | K | BRC | 50.42 | -14.25 | 3.25 | 2.67 | 2.78 | 4.30 | .0000000 | T | INFINITE |
| 0032 | 0125-0032 | B23 | TUB | 28.00 | 1.375 | K | CHD | 50.42 | | 4.32 | 3.38 | 2.46 | 6.63 | .42082-7 | L | 47526.+4 |
| 0032 | 0032-0128 | F09 | TUB | 26.00 | 1.000 | K | BRC | 50.42 | -14.25 | 2.90 | 2.84 | 2.87 | 4.67 | .0000000 | T | INFINITE |
| 0032 | 0124-0032 | B23 | TUB | 28.00 | 1.375 | K | CHD | 50.42 | | 2.83 | 2.89 | 2.57 | 7.20 | .20019-8 | L | 99907.+5 |
| 0032 | 0071-0032 | B09 | TUB | 26.00 | 1.000 | TK | BRC | 50.42 | -29.03 | 2.06 | 1.90 | 3.38 | 2.42 | .29505-8 | B | 67784.+5 |
| 0032 | 0124-0032 | B23 | TUB | 28.00 | 1.375 | TK | CHD | 50.42 | | 1.95 | 1.78 | 2.00 | 3.73 | .20772-7 | B | 96285.+4 |
| 0032 | 0096-0032 | B09 | TUB | 26.00 | 1.000 | TK | BRC | 50.42 | -29.03 | 1.81 | 1.72 | 3.41 | 2.43 | .20729-8 | B | 96485.+5 |
| 0032 | 0125-0032 | B23 | TUB | 28.00 | 1.375 | TK | CHD | 50.42 | | 1.81 | 1.71 | 1.99 | 3.75 | .13705-7 | B | 14593.+5 |
| 0032 | 0119-0032 | BV1 | TUB | 22.00 | 0.750 | TK | BRC | 50.42 | -29.03 | 2.83 | 2.83 | 2.71 | 5.54 | .0000000 | T | INFINITE |
| 0032 | 0125-0032 | B23 | TUB | 28.00 | 1.375 | TK | CHD | 50.42 | | 2.72 | 2.70 | 2.40 | 6.89 | .24431-9 | R | 81863.+6 |

SACS V8i SELECTseries 3 (v5.6)
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

ITS

DATE 15-JUL-2020 TIME 16:51:31 FTG PAGE 289

* * * MEMBER FATIGUE REPORT * * *

(DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | | | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|--------|--------------------------|------|------|----------|-----------------|----------|----------|----------|-------|-------|-------|
| | | | | OD | WT | | | | | LEN. | (IN) | (IN) | TYP | TYP | (FT) | (IN) | AX-CR | AX-SD | IN-PL | OU-PL |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | | | | | | | | | | | (IN) | (IN) |
| 0032 | 0032-0153 | F09 | TUB | 26.00 | 1.000 | Y | BRC | 50.42 | | 4.74 | 3.30 | 2.37 | 2.72 | .0000000 | T | INFINITE | | | | |
| 0032 | 0124-0032 | B23 | TUB | 28.00 | 1.375 | Y | CHD | 50.42 | | 7.47 | 5.23 | 2.18 | 4.20 | .0000000 | T | INFINITE | | | | |
| ----- | | | | | | | | | | | | | | | | | | | | |
| 0118 | 0118-0117 | F07 | TUB | 24.00 | 0.750 | K | BRC | 88.51 | 3.23 | 6.00 | 3.02 | 2.28 | 3.35 | .0000000 | T | INFINITE | | | | |
| 0118 | 0084-0118 | B22 | TUB | 26.00 | 1.250 | K | CHD | 88.51 | | 7.45 | 5.17 | 1.87 | 4.65 | .0000000 | T | INFINITE | | | | |
| 0118 | 0119-0118 | F08 | TUB | 24.00 | 1.000 | K | BRC | 88.51 | 3.23 | 6.15 | 3.15 | 2.44 | 3.64 | .0000000 | T | INFINITE | | | | |
| 0118 | 0096-0118 | B22 | TUB | 26.00 | 1.250 | K | CHD | 88.51 | | 6.80 | 6.17 | 2.39 | 5.91 | .0000000 | T | INFINITE | | | | |
| 0118 | 0118-0031 | BV1 | TUB | 22.00 | 0.750 | T | BRC | 88.51 | | 7.65 | 5.08 | 2.25 | 4.17 | .23486-9 | BR | 85156.+6 | | | | |
| 0118 | 0084-0118 | B22 | TUB | 26.00 | 1.250 | T | CHD | 88.51 | 10.00 | 4.69 | 2.15 | 5.61 | .13601-7 | B | 14705.+5 | | | | | |
| 0118 | 0118-0192 | F10 | TUB | 22.00 | 0.750 | Y | BRC | 88.51 | | 7.65 | 4.78 | 2.28 | 3.88 | .0000000 | T | INFINITE | | | | |
| 0118 | 0084-0118 | B22 | TUB | 26.00 | 1.250 | Y | CHD | 88.51 | 10.00 | 6.08 | 2.08 | 5.22 | .18518-9 | B | 10800.+7 | | | | | |
| ----- | | | | | | | | | | | | | | | | | | | | |
| 0012 | 0128-0012 | F09 | TUB | 26.00 | 1.000 | K | BRC | 50.42 | -13.08 | 3.08 | 2.77 | 2.96 | 4.56 | .0000000 | T | INFINITE | | | | |
| 0012 | 0123-0012 | B23 | TUB | 28.00 | 1.375 | K | CHD | 50.42 | | 3.20 | 2.65 | 2.53 | 7.04 | .0000000 | T | INFINITE | | | | |
| 0012 | 0129-0012 | F09 | TUB | 26.00 | 1.000 | K | BRC | 50.42 | -13.08 | 3.06 | 2.76 | 2.96 | 4.58 | .0000000 | T | INFINITE | | | | |

0012 0122-0012 B23 TUB 28.00 1.375 K CHD 50.42 3.15 2.62 2.53 7.06 .0000000 T INFINITE

SACS V8i SELECTseries 3 (v5.6) ITS
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

DATE 15-JUL-2020 TIME 16:51:31 FTG PAGE 290

* * * M E M B E R F A T I G U E R E P O R T * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|--------|--------------------------|------|------|------|-----------------|-------|----------|----------|--------|------|
| | | | | OD | WT | | | | | TYP | TYP | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | | (IN) | (IN) |
| 0012 | 0084-0012 | B09 | TUB | 26.00 | 1.000 | TK | BRC | 50.42 | -29.00 | 1.99 | 1.89 | 3.39 | 2.47 | .50146-9 | B | 39884.+6 | | | |
| 0012 | 0122-0012 | B23 | TUB | 28.00 | 1.375 | TK | CHD | 50.42 | | 1.84 | 1.72 | 1.98 | 3.80 | .24724-9 | BL | 80892.+6 | | | |
| 0012 | 0071-0012 | B09 | TUB | 26.00 | 1.000 | TK | BRC | 50.42 | -29.00 | 1.80 | 1.72 | 3.40 | 2.46 | .29288-9 | B | 68286.+6 | | | |
| 0012 | 0123-0012 | B23 | TUB | 28.00 | 1.375 | TK | CHD | 50.42 | | 1.80 | 1.71 | 1.99 | 3.80 | .29320-9 | BL | 68213.+6 | | | |
| 0012 | 0117-0012 | BV1 | TUB | 22.00 | 0.750 | TK | BRC | 50.42 | -29.00 | 2.84 | 2.84 | 2.69 | 5.55 | .17958-9 | R | 11137.+7 | | | |
| 0012 | 0122-0012 | B23 | TUB | 28.00 | 1.375 | TK | CHD | 50.42 | | 2.75 | 2.71 | 2.39 | 6.90 | .28789-8 | R | 69471.+5 | | | |

| | | | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|------|------|------|------|------|----------|---|----------|--|--|
| 0119 | 0119-0117 | F07 | TUB | 24.00 | 0.750 | K | BRC | 88.51 | 3.22 | 6.03 | 3.02 | 2.28 | 3.34 | .0000000 | T | INFINITE | | |
| 0119 | 0071-0119 | B22 | TUB | 26.00 | 1.250 | K | CHD | 88.51 | | 7.49 | 5.19 | 1.87 | 4.64 | .0000000 | T | INFINITE | | |
| 0119 | 0119-0118 | F08 | TUB | 24.00 | 1.000 | K | BRC | 88.51 | 3.22 | 6.38 | 3.19 | 2.44 | 3.62 | .0000000 | T | INFINITE | | |
| 0119 | 0096-0119 | B22 | TUB | 26.00 | 1.250 | K | CHD | 88.51 | | 7.00 | 6.32 | 2.39 | 5.88 | .0000000 | T | INFINITE | | |
| 0119 | 0119-0032 | BV1 | TUB | 22.00 | 0.750 | T | BRC | 88.51 | | 7.65 | 5.08 | 2.25 | 4.17 | .0000000 | T | INFINITE | | |

| | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|-------|------|------|------|----------|---|----------|
| 0119 | 0071-0119 | B22 | TUB | 26.00 | 1.250 | T | CHD | 88.51 | 10.00 | 4.69 | 2.15 | 5.61 | .25051-8 | T | 79838.+5 |
| 0119 | 0119-0193 | F10 | TUB | 22.00 | 0.750 | Y | BRC | 88.51 | 7.65 | 4.78 | 2.28 | 3.88 | .0000000 | T | INFINITE |
| 0119 | 0071-0119 | B22 | TUB | 26.00 | 1.250 | Y | CHD | 88.51 | 10.00 | 6.08 | 2.08 | 5.22 | .0000000 | T | INFINITE |

SACS V8i SELECTseries 3 (v5.6) ITS
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

DATE 15-JUL-2020 TIME 16:51:31 FTG PAGE 291

* * * MEMBER FATIGUE REPORT * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|------|--------------------------|------|------|------|-----------------|------|----------|----------|-------|-------|
| | | | | OD | WT | | | | | (IN) | (IN) | TYP | TYP | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | | | | | | | | | | (IN) | (IN) |
| 0192 | 0118-0192 | F10 | TUB | 22.00 | 0.750 | Y | BRC | 27.16 | | 3.75 | 3.75 | 2.67 | 3.73 | .0000000 | T | INFINITE | | | |
| 0192 | 0152-0192 | F09 | TUB | 26.00 | 1.000 | Y | CHD | 27.16 | | 6.36 | 6.45 | 2.37 | 5.72 | .21434-9 | TR | 93309.+6 | | | |
| ----- | | | | | | | | | | | | | | | | | | | |
| 0114 | 0114-0116 | F06 | TUB | 22.00 | 0.750 | K | BRC | 73.94 | 3.18 | 6.06 | 3.48 | 2.47 | 4.19 | .0000000 | T | INFINITE | | | |
| 0114 | 0070-0114 | B16 | TUB | 24.00 | 1.000 | K | CHD | 73.94 | | 7.39 | 6.50 | 2.40 | 6.61 | .19493-9 | R | 10260.+7 | | | |
| 0114 | 0114-0115 | F06 | TUB | 22.00 | 0.750 | K | BRC | 73.94 | 3.18 | 6.06 | 3.48 | 2.47 | 4.19 | .0000000 | T | INFINITE | | | |
| 0114 | 0083-0114 | B16 | TUB | 24.00 | 1.000 | K | CHD | 73.94 | | 7.40 | 6.50 | 2.40 | 6.60 | .0000000 | T | INFINITE | | | |
| ----- | | | | | | | | | | | | | | | | | | | |
| 0113 | 0113-0111 | F04 | TUB | 18.00 | 0.750 | K | BRC | 62.59 | 3.21 | 4.86 | 4.39 | 2.65 | 5.21 | .0000000 | T | INFINITE | | | |
| 0113 | 0069-0113 | B18 | TUB | 24.00 | 1.000 | K | CHD | 62.59 | | 7.19 | 7.19 | 2.60 | 7.62 | .15954-9 | L | 12536.+7 | | | |

0113 0113-0112 F04 TUB 18.00 0.750 K BRC 62.59 3.21 4.72 4.29 2.65 5.25 .0000000 T INFINITE
 0113 0094-0113 B18 TUB 24.00 1.000 K CHD 62.59 6.97 6.97 2.60 7.68 .0000000 T INFINITE

 0115 0114-0115 F06 TUB 22.00 0.750 K BRC 73.93 3.23 5.29 3.34 2.47 4.15 .0000000 T INFINITE
 0115 0083-0115 B20 TUB 24.00 1.000 K CHD 73.93 6.74 6.08 2.40 6.54 .0000000 T INFINITE
 0115 0116-0115 F05 TUB 16.00 0.500 K BRC 73.93 3.23 3.99 3.98 2.47 4.82 .0000000 T INFINITE

SACS V8i SELECTseries 3 (v5.6) ITS
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

DATE 15-JUL-2020 TIME 16:51:31 FTG PAGE 292

* * * M E M B E R F A T I G U E R E P O R T * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|------|--------------------------|------|-------|-------|-----------------|-------|----------|----------|------|
| | | | | OD | WT | | | | | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC |
| | | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | (IN) | (IN) |
| 0115 | 0095-0115 | B20 | TUB | 24.00 | 1.000 | K | CHD | 73.93 | | 5.77 | 5.11 | 1.89 | 5.42 | .15853-9 | R | 12616.+7 | | |

 0193 0119-0193 F10 TUB 22.00 0.750 Y BRC 27.16 3.75 3.75 2.67 3.73 .0000000 T INFINITE
 0193 0153-0193 F09 TUB 26.00 1.000 Y CHD 27.16 6.36 6.45 2.37 5.72 .0000000 T INFINITE

 0190 0096-0190 F09 TUB 26.00 1.000 Y BRC 27.16 4.62 1.96 2.81 1.89 .0000000 T INFINITE
 0190 0186-0190 F09 TUB 26.00 1.000 Y CHD 27.16 8.83 2.38 2.26 3.59 .0000000 T INFINITE

```

-----
0189 0096-0189 F09 TUB 26.00 1.000 Y BRC 27.16 4.62 1.96 2.81 1.89 .0000000 T INFINITE
0189 0184-0189 F09 TUB 26.00 1.000 Y CHD 27.16 8.83 2.38 2.26 3.59 .0000000 T INFINITE
-----

```

```

-----
0117 0119-0117 F07 TUB 24.00 0.750 K BRC 88.51 3.23 4.31 2.67 2.28 3.46 .0000000 T INFINITE
0117 0071-0117 B21 TUB 26.00 1.250 K CHD 88.51 5.43 4.17 1.87 4.81 .0000000 T INFINITE
0117 0118-0117 F07 TUB 24.00 0.750 K BRC 88.51 3.23 4.31 2.66 2.28 3.46 .0000000 T INFINITE
0117 0084-0117 B21 TUB 26.00 1.250 K CHD 88.51 5.43 4.17 1.87 4.81 .0000000 T INFINITE
0117 0117-0012 BV1 TUB 22.00 0.750 T BRC 88.51 7.65 5.08 2.25 4.17 .0000000 T INFINITE
-----

```

SACS V8i SELECTseries 3 (v5.6) ITS
ID=a6hrm6momGt6eWi+d2ZtdngXlmlncWV5aJZrepeFdmQ= DATE 15-JUL-2020 TIME 16:51:31 FTG PAGE 293

* * * M E M B E R F A T I G U E R E P O R T * * *
(DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | REQUIRED | |
|-------|-----------|------|------|----------|-------|-----|-----|-------|-------|--------------------------|------|-------|----------|-----------------|----------|--------|----------|------|
| | | | | OD | WT | | | | | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC |
| | ID | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | (IN) | (IN) |
| 0117 | 0071-0117 | B21 | TUB | 26.00 | 1.250 | T | CHD | 88.51 | 10.00 | 4.69 | 2.15 | 5.62 | .0000000 | T | INFINITE | | | |

```

-----
0116 0114-0116 F06 TUB 22.00 0.750 K BRC 73.93 3.23 5.52 3.39 2.47 4.12 .0000000 T INFINITE
0116 0070-0116 B20 TUB 24.00 1.000 K CHD 73.93 6.97 6.25 2.40 6.49 .0000000 T INFINITE
-----

```


0116 0116-0115 F05 TUB 16.00 0.500 K BRC 73.93 3.23 4.10 4.08 2.47 4.75 .0000000 T INFINITE
 0116 0095-0116 B20 TUB 24.00 1.000 K CHD 73.93 6.00 5.28 1.89 5.35 .0000000 T INFINITE

 0111 0113-0111 F04 TUB 18.00 0.750 K BRC 62.60 3.21 4.59 4.20 2.65 5.30 .0000000 T INFINITE
 0111 0069-0111 B19 TUB 24.00 1.000 K CHD 62.60 6.77 6.77 2.60 7.75 .0000000 T INFINITE
 0111 0112-0111 F04 TUB 18.00 0.750 K BRC 62.60 3.21 4.44 4.08 2.65 5.35 .0000000 T INFINITE
 0111 0081-0111 B19 TUB 24.00 1.000 K CHD 62.60 6.52 6.52 2.60 7.82 .0000000 T INFINITE

 0112 0112-0111 F04 TUB 18.00 0.750 K BRC 62.59 3.21 5.16 4.62 2.65 5.10 .0000000 T INFINITE
 0112 0081-0112 B18 TUB 24.00 1.000 K CHD 62.59 7.68 7.68 2.60 7.46 .0000000 T INFINITE
 0112 0113-0112 F04 TUB 18.00 0.750 K BRC 62.59 3.21 5.15 4.61 2.65 5.11 .0000000 T INFINITE
 0112 0094-0112 B18 TUB 24.00 1.000 K CHD 62.59 7.66 7.66 2.60 7.47 .0000000 T INFINITE

SACS V8i SELECTseries 3 (v5.6) ITS
 ID=a6hrm6momGt6eWi+d2ZtdnqXlmlncWV5aJZrepeFdmQ=

DATE 15-JUL-2020 TIME 16:51:31 FTG PAGE 294

* * * M E M B E R F A T I G U E R E P O R T * * *
 (DAMAGE ORDER)

| JOINT | MEMBER | GRUP | TYPE | ORIGINAL | | JNT | MEM | CHORD | GAP | * STRESS CONC. FACTORS * | | | | FATIGUE RESULTS | | | | REQUIRED | |
|-------|--------|------|------|----------|------|-----|-----|-------|------|--------------------------|------|-------|-------|-----------------|-------|--------|-----|----------|------|
| | | | | OD | WT | | | | | LEN. | (IN) | AX-CR | AX-SD | IN-PL | OU-PL | DAMAGE | LOC | SVC | LIFE |
| | ID | ID | ID | (IN) | (IN) | TYP | TYP | (FT) | (IN) | | | | | | | | | (IN) | (IN) |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|------|------|------|------|------|----------|---|----------|
| 0106 | 0106-0105 | F03 | TUB | 18.00 | 0.750 | K | BRC | 47.03 | 3.27 | 4.34 | 3.68 | 2.53 | 4.60 | .0000000 | T | INFINITE |
| 0106 | 0079-0106 | B14 | TUB | 22.00 | 1.000 | K | CHD | 47.03 | | 6.82 | 6.07 | 2.43 | 6.92 | .0000000 | T | INFINITE |
| 0106 | 0107-0106 | F03 | TUB | 18.00 | 0.750 | K | BRC | 47.03 | 3.27 | 4.32 | 3.67 | 2.53 | 4.61 | .0000000 | T | INFINITE |
| 0106 | 0092-0106 | B14 | TUB | 22.00 | 1.000 | K | CHD | 47.03 | | 6.79 | 6.06 | 2.43 | 6.93 | .0000000 | T | INFINITE |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|------|------|------|------|------|----------|---|----------|
| 0105 | 0107-0105 | F03 | TUB | 18.00 | 0.750 | K | BRC | 47.03 | 3.27 | 4.48 | 3.76 | 2.53 | 4.55 | .0000000 | T | INFINITE |
| 0105 | 0067-0105 | B15 | TUB | 22.00 | 1.000 | K | CHD | 47.03 | | 7.07 | 6.26 | 2.43 | 6.85 | .0000000 | T | INFINITE |
| 0105 | 0106-0105 | F03 | TUB | 18.00 | 0.750 | K | BRC | 47.03 | 3.27 | 4.51 | 3.78 | 2.53 | 4.54 | .0000000 | T | INFINITE |
| 0105 | 0079-0105 | B15 | TUB | 22.00 | 1.000 | K | CHD | 47.03 | | 7.13 | 6.30 | 2.43 | 6.84 | .0000000 | T | INFINITE |

| | | | | | | | | | | | | | | | | |
|------|-----------|-----|-----|-------|-------|---|-----|-------|------|------|------|------|------|----------|---|----------|
| 0107 | 0107-0105 | F03 | TUB | 18.00 | 0.750 | K | BRC | 47.03 | 3.27 | 4.46 | 3.75 | 2.53 | 4.56 | .0000000 | T | INFINITE |
| 0107 | 0067-0107 | B14 | TUB | 22.00 | 1.000 | K | CHD | 47.03 | | 7.04 | 6.23 | 2.43 | 6.86 | .0000000 | T | INFINITE |
| 0107 | 0107-0106 | F03 | TUB | 18.00 | 0.750 | K | BRC | 47.03 | 3.27 | 4.43 | 3.73 | 2.53 | 4.57 | .0000000 | T | INFINITE |
| 0107 | 0092-0107 | B14 | TUB | 22.00 | 1.000 | K | CHD | 47.03 | | 6.99 | 6.20 | 2.43 | 6.88 | .0000000 | T | INFINITE |

BIODATA PENULIS



Muhammad Nabil Giffary, lahir pada 15 Juli 1998. Penulis menempuh pendidikan mulai dari taman kanak-kanak hingga sekolah dasar di Sekolah Alam Insan Mulia Surabaya pada tahun 2001 – 2010. Penulis kemudian melanjutkan pendidikannya ke SMP Negeri 19 Surabaya pada tahun 2010 – 2013. Selanjutnya, penulis melanjutkan ke jenjang pendidikan sekolah menengah akhir di SMA Negeri 2 Surabaya pada tahun 2013 – 2016 dengan aktif sebagai anggota OSIS SMADA dan Smada Band. Penulis melanjutkan pendidikan ke jenjang perguruan tinggi dengan mengikuti ujian SBMPTN di tahun 2016 yang pada akhirnya diterima di Departemen Teknik Kelautan, Fakultas Teknologi Kelautan, Institut Teknologi Sepuluh Nopember. Pada tahun 2019 penulis menjalani kerja praktek di Kangean Energy Indonesia Ltd. sebagai *project engineer internship*. Selain itu, selama 4 tahun masa pendidikan perguruan tinggi penulis aktif dalam berbagai kegiatan kepanitiaan di antaranya IFC 2017 dan OCEANO 2017-2019. Penulis juga pernah mengikuti kegiatan sosial LITE *Project 1.0* pada tahun 2016. Tidak lupa sebagai pengabdian pada departemen, penulis aktif mengikuti Himpunan Mahasiswa Teknik Kelautan pada tahun 2017 – 2019 sebagai anggota Departemen Keprofesian. Sebagai tugas akhirnya, penulis mengerjakan judul “Perbandingan Umur Kelelahan Struktur *Jacket 3 Kaki* Modifikasi dan Konvensional” dan diselesaikan sebagai syarat kelulusan untuk mendapatkan gelar sarjana. Permasalahan yang dibahas oleh penulis merupakan salah satu bidang keahlian di Departemen Teknik Kelautan.

Email : mngiffary@gmail.com

Linked In : Muhammad Nabil Giffary